



BIOCOMEM
H2020 GRANT AGREEMENT NUMBER: 887075

Start date of project: 01/06/2020

Duration: 3 years

[WP7 – Dissemination and Exploitation]

D7.19
BIOCOMEM long term learning measures (courses and workshops) M24

Topic: BBI2019.SO3.R10: Develop bio-based high-performance materials for various and demanding applications
Funding scheme: Research and innovation actions
Call identifier: H2020-BBI-JTI-2019

| | | |
|--|--|---|
| Due date of deliverable: 30-11-2022 | Actual submission date: 12-12-2022 | Reference period: 31-07-2020-30-11-2022 |
| Document classification code (*): BIOCOMEM-WP7-D719-DLR-TUE-20221212-v0.1.docx | | Prepared by (**): TUE |

| Version | DATE | Changes | CHECKED | APPROVED |
|---------|------------|---------------|---------|----------|
| v0.1 | 12-12-2022 | First Release | TUE | FG |
| | | | | |
| | | | | |
| | | | | |
| | | | | |

| Project funded by European Union's Horizon 2020 research and innovation programme (2014-2020) | | |
|---|---|----------|
| Dissemination Level | | |
| PU | Public | X |
| PP | Restricted to other programme participants (including the Commission Services) | |
| RE | Restricted to a group specified by the consortium (including the Commission Services) | |
| CO | Confidential, only for BioCoMem s of the consortium (including the Commission Services) | |
| CON | Confidential, only for BioCoMem s of the Consortium | |

(*) for generating such code please refer to the Quality Management Plan, also to be included in the header of the following pages

(**) indicate the acronym of the partner that prepared the document

Content

| | |
|--|----------|
| 1. EXECUTIVE SUMMARY | 3 |
| 1.1. Description of the deliverable content and purpose..... | 3 |
| 2. Introduction | 4 |
| 2.1. Brief description of the project objectives | 4 |
| Appendices | 5 |

1. EXECUTIVE SUMMARY

1.1. Description of the deliverable content and purpose

As part of work package 7 of Biocomem, (Exploitation, Dissemination and Communication) TUE together with all partners would develop and execute workshops, courses and guided visits.

In particular the tasks foreseen are:

Two public Workshops: One on “Biomembranes for gas permeation” (general audience) at TUE (M24) and the final workshop focused on presenting the project results at the demo plant site (industry audience) (M36)

Webinars on the BIOCOMEM tools: Training sessions on software tools developed in WP2 will be organised remotely, via webinars, for each Demo Site. TUE and DMT will be in charge of the training courses.

Courses for university students: The project results will be integrated in BSc and MSc courses, in addition the consortium will develop a dedicated elective course to be held locally and distributed online.

Courses for professionals: The consortium will develop three short course modules on i) Advanced industrial catalysis; ii) Membrane separation and iii) Membrane design.

Guided visits to demo sites: Guided visits for stakeholders (engineers, end users, students, etc.) to the demonstration installation will be organised at a local, national and international levels. These visits will be hosted and supported by the demo plant owners.

2. Introduction

2.1. Brief description of the project objectives

BIOCOMEM's tasks in the WP7 are as follows

Two public Workshops: One on "Biomembranes for gas permeation" (general audience) at TUE (M24) and the final workshop focused on presenting the project results at the demo plant site (industry audience) (M36)

Webinars on the BIOCOMEM tools: Training sessions on software tools developed in WP2 will be organised remotely, via webinars, for each Demo Site. TUE and DMT will be in charge of the training courses.

Courses for university students: The project results will be integrated in BSc and MSc courses, in addition the consortium will develop a dedicated elective course to be held locally and distributed online.

Courses for professionals: The consortium will develop three short course modules on i) Advanced industrial catalysis; ii) Membrane separation and iii) Membrane design.

Guided visits to demo sites: Guided visits for stakeholders (engineers, end users, students, etc.) to the demonstration installation will be organised at a local, national and international levels. These visits will be hosted and supported by the demo plant owners.

Due to COVID and to allow larger audience the first workshop has been organized together with several other projects. The workshop, held online has been a great success with attendees participating from all over the world.

A report of the event is reported in Appendix 1.

A next workshop will be organized towards the end of the project, again by TUE and possibly with participation of other projects.

As for the training session and courses, the partners have prepared dedicated lectures that will be given at summer school (one organized at TUE on June 2023) as well as via webinars.

Two webinars will be organized in 2023 and given with free participation, the first one for undergraduate students and the second for professionals. Some of these lectures will be integrated in the course process design and in the course separation technologies for TUE students

An example of lecture materials are reported in the Appendix 2.

Finally, the site visits will be organized as soon as the prototypes will be ready.

Appendices

Appendix 1. report on first workshop

Appendix 2. lectures for long term learning

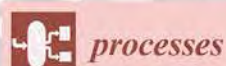
INTERNATIONAL WORKSHOP ON CO₂ CAPTURE AND UTILIZATION

TU/e - EINDHOVEN - 16-17 FEBRUARY 2021

ORGANIZED BY



SPONSORED BY





The projects sponsoring this workshop received support from the European Union's Horizon 2020 research and innovation under grants agreement reported below

| N° | Acronym | Project Title | Website | Grant agreement |
|----|-----------|---|---|-----------------|
| 1 | MEMBER | Advanced MEMBranes and membrane assisted procEesses for pre- and post-combustion CO2 captuRe | https://member-co2.com/ | 760944 |
| 2 | CARMOF | TAILOR-MADE 3D PRINTED STRUCTURES BASED ON CNTS AND MOFS MATERIALS FOR EFFICIENT CO2 CAPTURE | https://carmof.eu/ | 760884 |
| 3 | BIOCOMEM | Bio-based copolymers for membrane end products for gas separations | https://www.biocomem.eu/ | 887075 |
| 4 | C2FUEL | Carbon Captured Fuel and Energy Carriers for an Intensified Steel Off-Gases based Electricity Generation in a Smarter Industrial Ecosystem | https://c2fuel-project.eu/ | 838014 |
| 5 | COZMOS | Efficient CO2 conversion over multisite Zeolite-Metal nanocatalysts to fuels and OlefinS | https://www.spire2030.eu/cozmos | 837733 |
| 6 | eCOCO2 | Direct electrocatalytic conversion of CO2 into chemical energy carriers in a co-ionic membrane reactor | https://ecocoo.eu/ | 838077 |
| 7 | CO2Fokus | CO2 utilisation focused on market relevant dimethyl ether production, via 3D printed reactor- and solid oxide cell-based technologies | https://www.co2fokus.eu/ | 838061 |
| 8 | C4U | Advanced Carbon Capture for steel industries integrated in CCUS Clusters | https://c4u-project.eu/ | 884418 |
| 9 | REALISE | Demonstrating a Refinery-Adapted Cluster-Integrated Strategy to Enable Full-Chain CCUS Implementation | https://realiseccus.eu/ | 884266 |
| 10 | CONVERGE | CarbON Valorisation in Energy-efficient Green fuels | https://www.converge-h2020.eu/ | 818135 |
| 11 | KEROGREEN | Production of Sustainable aircraft grade Kerosene from water and air powered by Renewable Electricity, through the splitting of CO2, syngas formation and Fischer-Tropsch synthesis | http://www.kerogreen.eu/ | 763909 |

Carbon-intensive industries are mandatory to supply processed materials and products to cover EU citizen's needs. In a vision of a decarbonized Europe, these industries are always seen as negative components due to their massive CO₂ emissions but also since only 14% of the energy used to run these factories is coming from renewable sources.

What if we were able to generate additional value, capturing CO₂ flue gases & convert it into a fuel and energy carrier that could be used locally?

There is a large consensus at European level that CO₂ capture, either from energy intensive industries or even from air, is a necessity to be able to reduce the human effect on the observed climate changes.

At the same time, CO₂ is increasingly seen as a potential raw material for the C1 chemistry or to be used as energy carrier.

Several projects are running in parallel at national and international levels. This workshop gathered the last scientific results of the different running projects and made them available for scientists and students and industrial researchers in an informal atmosphere.

The scientific goal was to create a forum for open discussion on the latest developments on technologies for CO₂ capture and conversion. We think that the workshop should be open to all, without registration fees, and as such several projects decided to try to (partially) cover the costs of the workshop. In this way, also young students could participate freely and have the possibility to discuss the topic and the last developments in the field.

Chairman

Prof. Fausto Gallucci – Eindhoven University of Technology

Local organizing Committee

Fausto Gallucci

Fernanda Neira D'Angelo

Aitor Cruellas

Camilla Brencio

Brandon Leal

Sirui Li

Arash Rahimali

Berenger Wegman

Saskia Walravens



Introduction to the Projects

International Workshop on CO₂ Capture and Utilization,
16-17 February 2021, TU/E, Eindhoven, The Netherlands

Outline

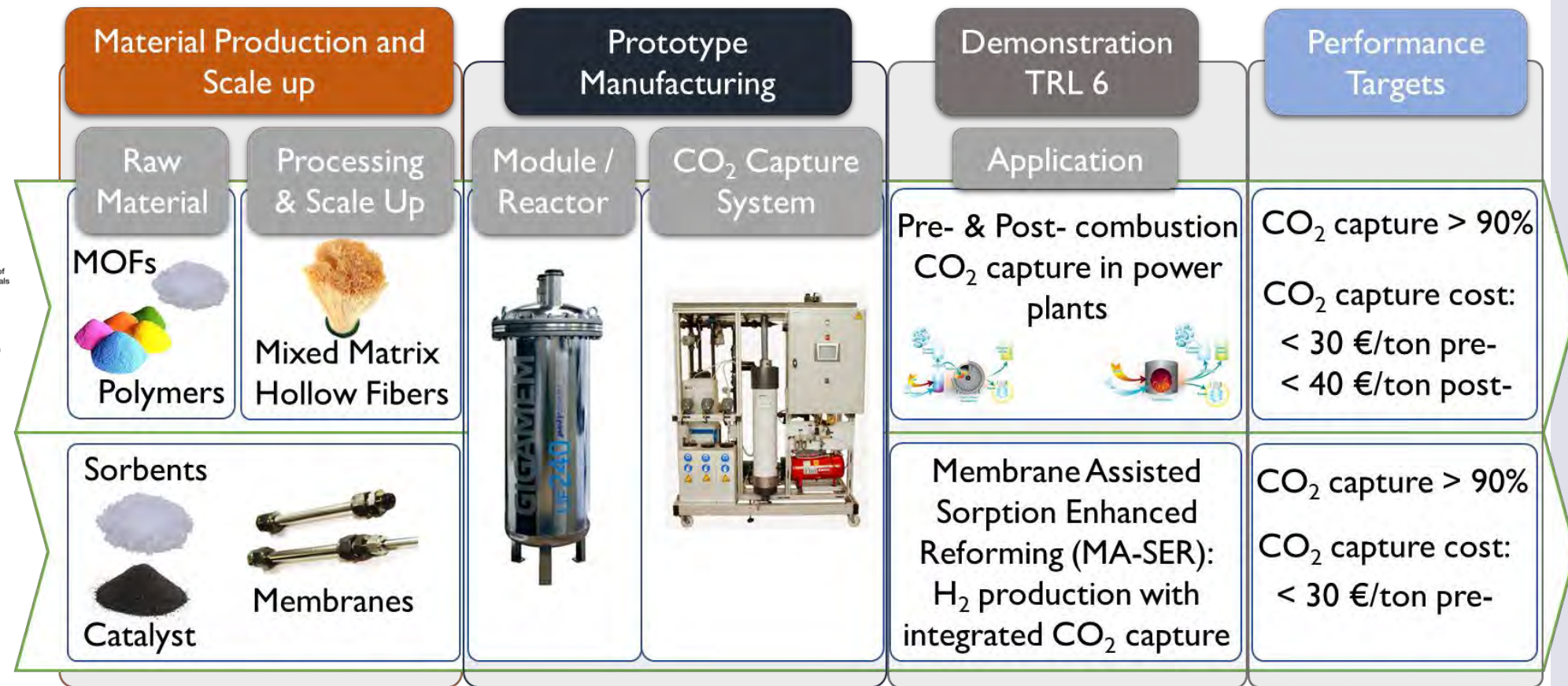
1. MEMBER
2. CARMOF
3. BIOCOMEM
4. C2FUEL
5. COZMOS
6. eCOCO2
7. CO2Fokus
8. C4U
9. REALISE
10. CONVERGE
11. KEROGREEN

| Nº | Topic | Acronym | Project Tytle | website | Coordinator or speaker |
|----|---|-----------|--|---|------------------------|
| 1 | NMBP-20-2017: High-performance materials for optimizing carbon dioxide capture | MEMBER | Advanced MEMBranes and membrane assisted procEsSES for pre- and post- combustion CO2 captuRe | https://member-co2.com/ | José Luis Viviente |
| 2 | NMBP-20-2017: High-performance materials for optimizing carbon dioxide capture | CARMOF | TAILOR-MADE 3D PRINTED STRUCTURES BASED ON CNTS AND MOFS MATERIALS FOR EFFICIENT CO2 CAPTURE | https://carmof.eu/ | Adolfo Benedito |
| 3 | BBI-2019-SO3-R10 - Develop bio-based high-performance materials for various and demanding applications | BIOCOMEM | Bio-based copolymers for membrane end products for gas separations | https://www.biocomem.eu/ | Oana David |
| 4 | CE-SC3-NZE-2-2018: Conversion of captured CO2 | C2FUEL | Carbon Captured Fuel and Energy Carriers for an Intensified Steel Off-Gases based Electricity Generation in a Smarter Industrial Ecosystem | https://c2fuel-project.eu/ | Camel Makhloufi |
| 5 | CE-SC3-NZE-2-2018: Conversion of captured CO2 | COZMOS | Efficient CO2 conversion over multisite Zeolite-Metal nanocatalysts to fuels and OlefinS | https://www.spire2030.eu/cozmos | Richard H. Heyn |
| 6 | CE-SC3-NZE-2-2018: Conversion of captured CO2 | eCOCO2 | Direct electrocatalytic conversion of CO2 into chemical energy carriers in a co-ionic membrane reactor | https://ecocoo.eu/ | José M. Serra |
| 7 | CE-SC3-NZE-2-2018: Conversion of captured CO2 | CO2Fokus | CO2 utilisation focused on market relevant dimethyl ether production, via 3D printed reactor- and solid oxide cell-based technologies | https://www.co2fokus.eu/ | Vesna Middelkoop |
| 8 | LC-SC3-NZE-5-2019-2020 - Low carbon industrial production using CCUS | C4U | Advanced Carbon Capture for steel industries integrated in CCUS Clusters | https://c4u-project.eu/ | Haroun Mahgerefteh |
| 9 | LC-SC3-NZE-5-2019-2020 - Low carbon industrial production using CCUS | REALISE | Demonstrating a Refinery-Adapted Cluster-Integrated Strategy to Enable Full-Chain CCUS Implementation | https://realiseccus.eu/ | Inna Kim |
| 10 | LC-SC3-RES-21-2018 - Development of next generation biofuels and alternative renewable fuel technologies for road transport | CONVERGE | CarbON Valorisation in Energy-efficient Green fuels | https://www.converge-h2020.eu/ | Giampaolo Manzolini |
| 11 | LCE-06-2017 - New knowledge and technologies | KEROGREEN | Production of Sustainable aircraft grade Kerosene from water and air powered by Renewable Electricity, through the splitting of CO2, syngas formation and Fischer-Tropsch synthesi | http://www.kerogreen.eu/ | Michael Tsampas |



Advanced MEMBranes and membrane assisted procEsses for pre- and post- combustion CO₂ captuRe

MEMBER project aims to reduce the cost of the Carbon Dioxide capture technologies by scaling-up and manufacturing advance materials (membranes, catalysts and sorbents) to develop membrane-based technologies that outperform current technology for pre- and post-combustion CO₂ capture in power plants as well as H₂ generation with integrated CO₂ capture.



<https://member-co2.com/>



This project has received funding from the European Union's Horizon 2020 research and innovation programme under grant agreement No 760944.

tecnalia Inspiring Business

TU/e Eindhoven University of Technology

TU Delft IFE

Institut für Energietechnik

Universidad Zaragoza

CENER

Technologies

C&CS

galp

polymem

HYGEAR COST-EFFECTIVE GAS SUPPLY

ECO Recycling

ZEG Power

Quantis

Kinetics Technology

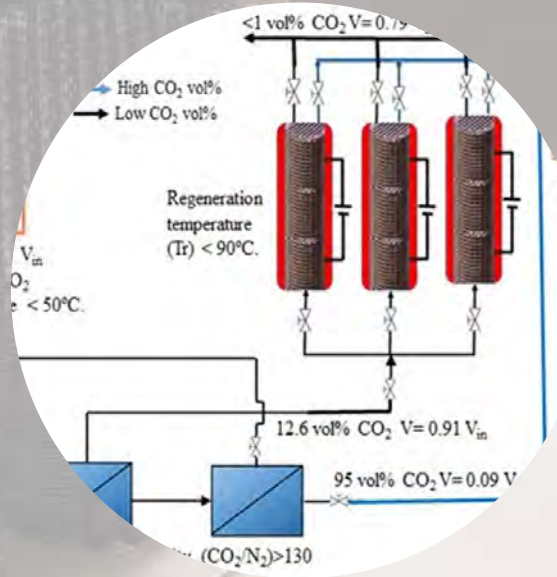
ARKEMA

JM Johnson Matthey

CARMOF Project

TAILOR-MADE 3D PRINTED STRUCTURES BASED ON
CNT AND MOF MATERIALS FOR EFFICIENT CO₂
CAPTURE

CARMOF is developing a hybrid CO₂ process combining **VTSA modules** based on 3D printed monoliths with thermoelectric regeneration and "in cascade" **membranes system**. The goal is to achieve high purity CO₂ streams from synergetic effects from both technologies



Bio-based copolymers for membrane end products for gas separations

Bio
Co
Mem



Bio-based Industries
Consortium


This project has received funding from the Bio Based Industries Joint Undertaking (JU) under the European Union's Horizon 2020 research and innovation programme, under grant agreement No 887075.

The JU receives support from the European Union's Horizon 2020 research and innovation program and the Bio Based Industries Consortium




C2FUEL Approach: Aligning local supply and demand

Dr Camel Makhloufi – ENGIE Lab CRIGEN - France



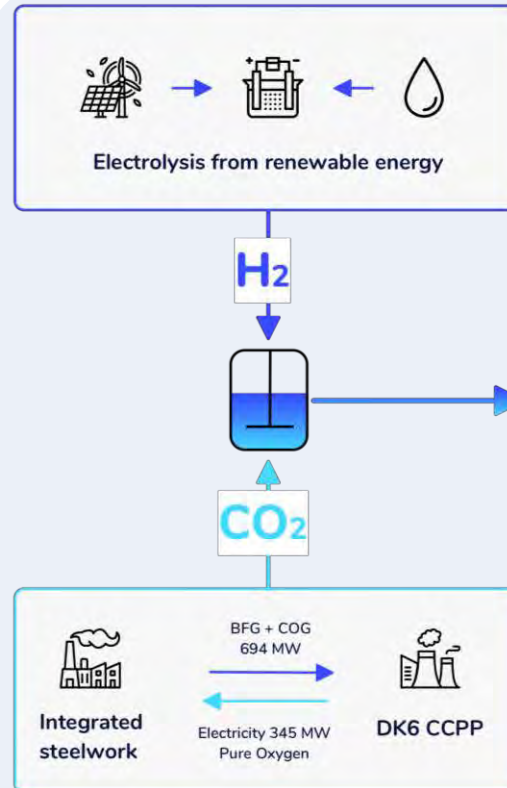
Dunkirk Integrated steel making factory



Large renewable penetration



Dunkirk Harbor

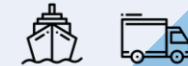


Formic acid as Hydrogen carrier

Decreasing the electricity footprint during boat charging on docks

C2FUEL Output

2,4 million ton of FA
100 000 ton of green hydrogen
1,8 TWh of green electricity
Seasonal storage using 3.6 TWh of renewable electricity



Dimethylether as Maritime and truck fuel

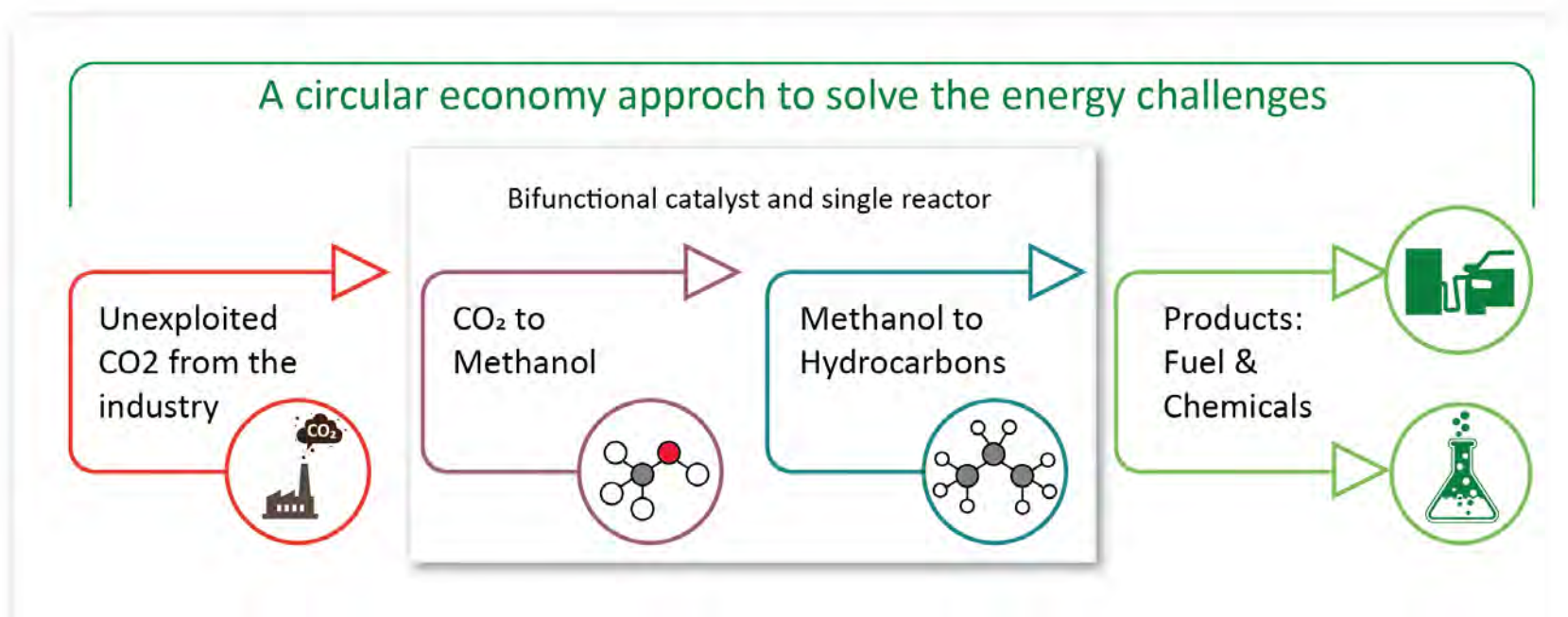
Displacing fossil fuel emission from power plant and decreasing harbor mobility footprint

C2FUEL Output

1,2 million ton of DME
320 000 ton of green H_2 produced using
11 TWh of renewable electricity

CO2MOS

Efficient CO₂ conversion over multisite Zeolite-Metal nanocatalysts to fuels and Olefins



Unni Olsbye,
University of Oslo,
Coordinator

Other
partners



جامعة الملك عبد الله
للعلوم والتقنية
King Abdullah University of
Science and Technology



TATA STEEL



COZMOS: Efficient CO₂ conversion over multisite Zeolite-Metal nanocatalysts to fuels and Olefins.

This project has received funding from the European Union's Horizon 2020 research and innovation programme under Grant Agreement No. 837733.



Direct electrocatalytic conversion of CO₂ into chemical energy carriers in a co-ionic membrane reactor

AIM: Set-up a technology for direct synthesis of carbon-neutral jet fuels from CO₂ using renewable energy and electrochemical catalytic membrane reactors. Bench-testing targets a 500 W multi-tubular system.

- Single-step electrolysis and one-pot catalytic conversion.
- Operating conditions:
T = 350-450 °C and > 25 bar.



Product:
Jet fuel



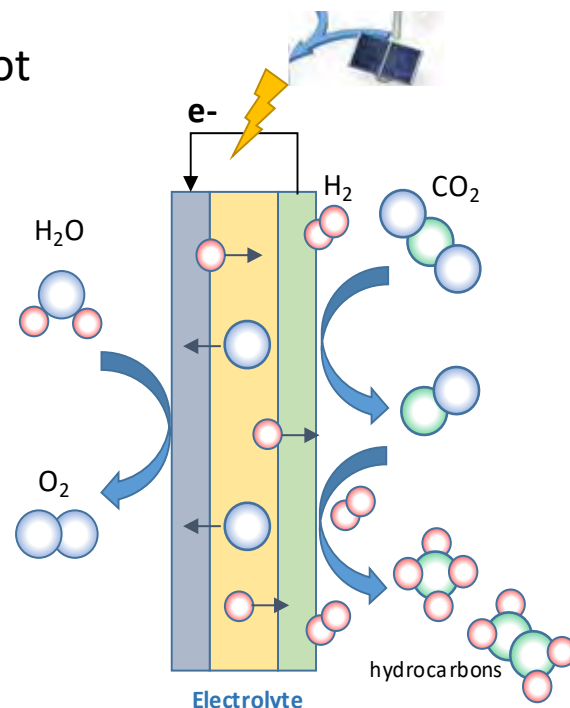
Efficiency:
> 85%



Full integration:
compact sized reactor



Final TRL:
5



Co-Electrolysis Reactor

PARTNERS



H2020-LC-SC3-2018-NZE-CC | Duration: May 2019 – May 2023 | EC funding: 3.9 M€

This project has received European Union's Horizon 2020 research and innovation funding under grant agreement N° 838077.

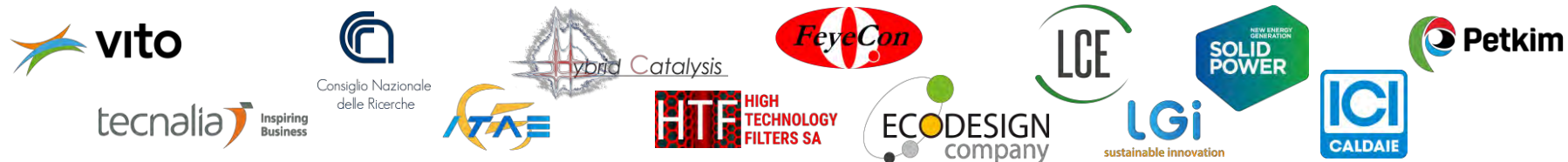


Follow us!



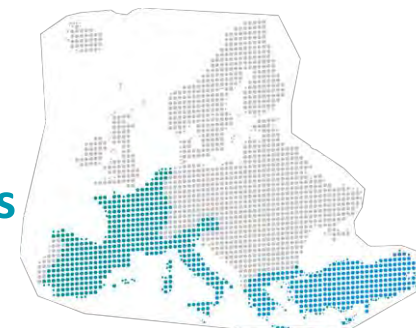
LinkedIn

<https://ecocoo.eu>



CO₂ utilisation focused on market relevant dimethyl ether production, via 3D printed reactor and solid oxide cell based technologies

Vesna Middelkoop, VITO



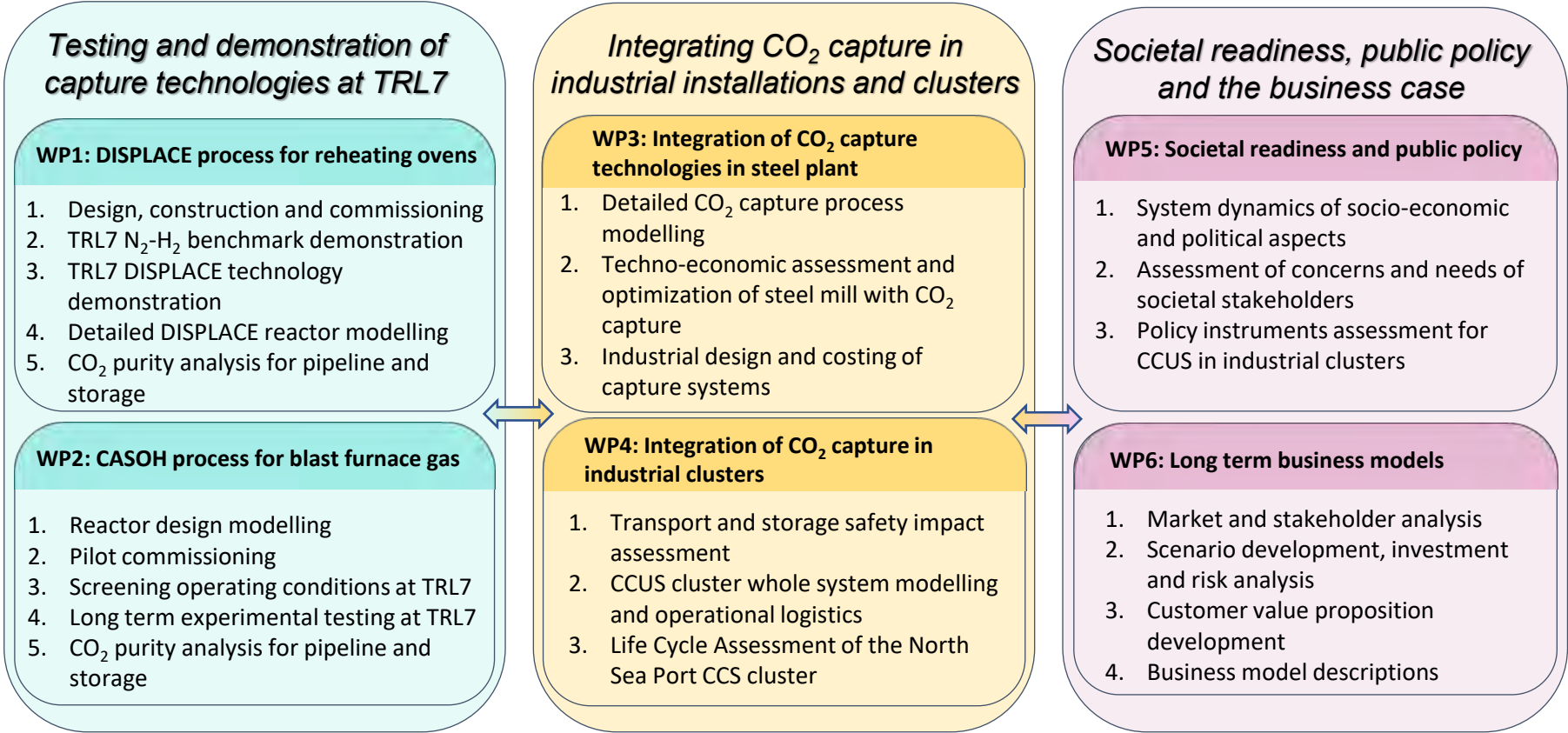
1500 N L/h CO₂/H₂ feed, > 30 % CO₂ conversion, 3.5 kW SOE 50 % conversion demo in industrial environment in 2022



Advanced Carbon Capture for Steel Industries Integrated in CCUS Clusters

• C⁴U addresses the essential elements for the optimal integration of CO₂ capture in the iron and steel industry as part of the CCUS chain. This spans demonstration of two highly efficient solid based CO₂ capture technologies for optimal integration into an iron and steel plant and detailed consideration of the safety, environmental, societal, policy and business aspects for successful incorporation into the North Sea Port CCUS industrial cluster.

<https://c4u-project.eu/>



This project has received funding from the European Union's Horizon 2020 research and innovation programme under grant agreement No. 884418.

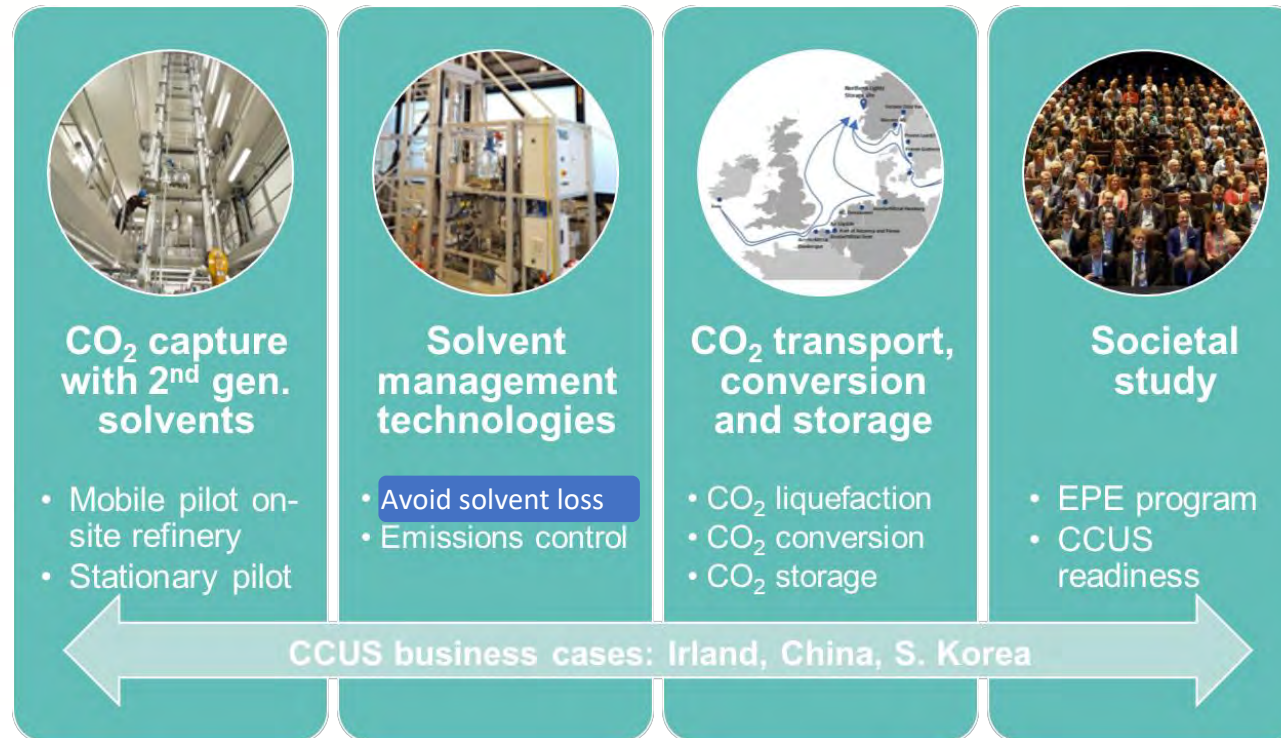
Project Coordinator

Haroun Mahgerefteh
University College London
h.mahgerefteh@ucl.ac.uk

Project Period
April 2020 - March 2024

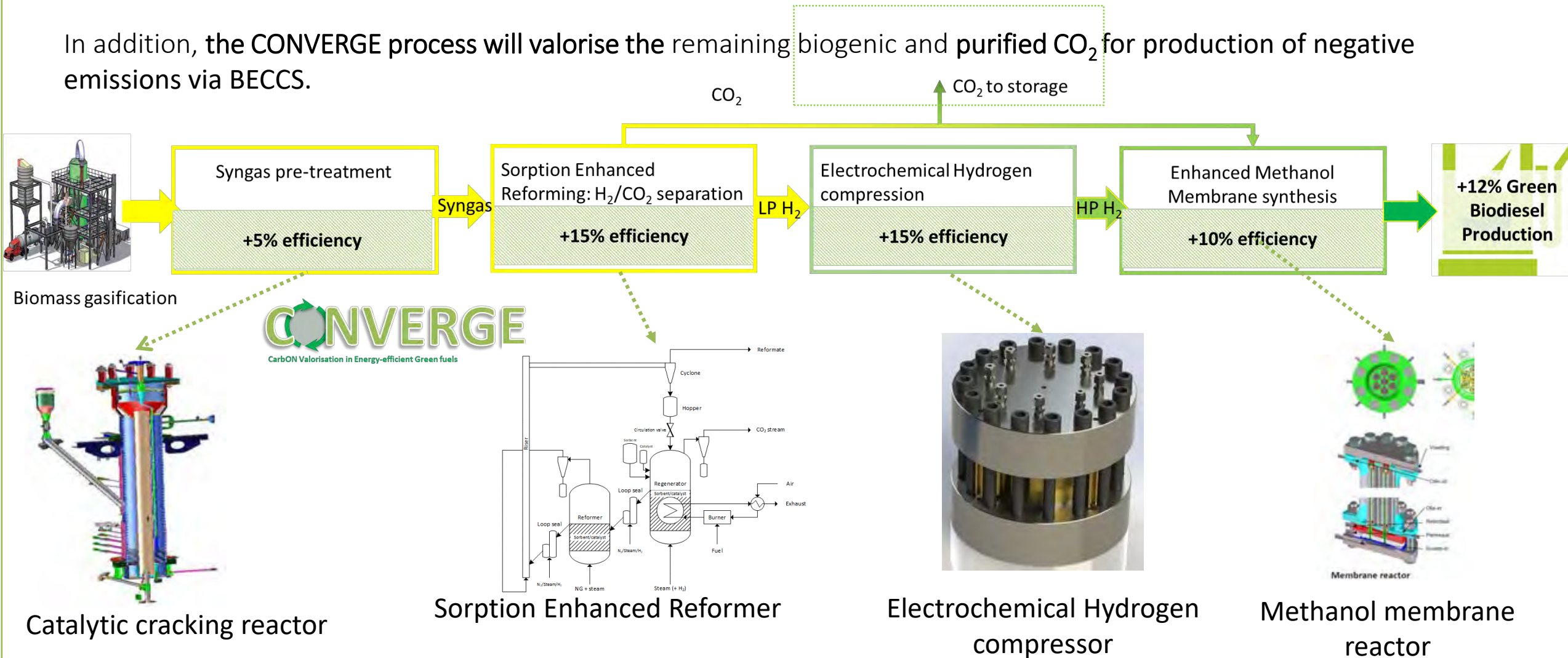
Overall budget
€ 13,845,496

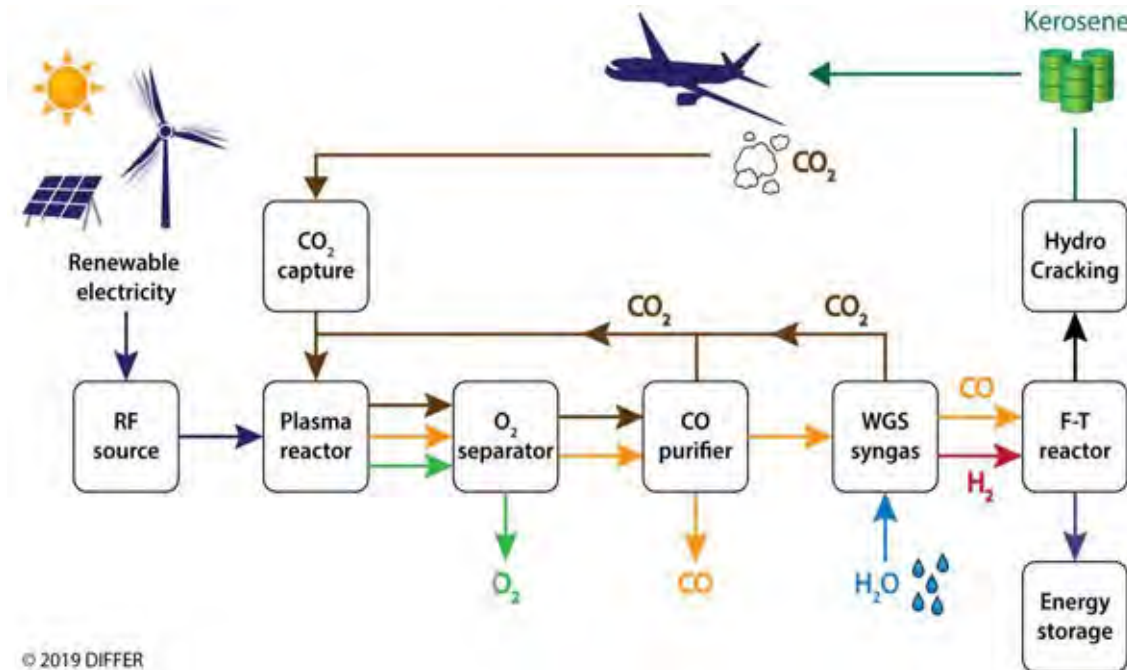
Demonstrating a refinery-adapted cluster-integrated strategy to enable full-chain CCUS implementation – REALISE (May 2020 – April 2023)



The **CONVERGE** project will validate an innovative process which will increase the biodiesel production by 12% per secondary biomass unit used and reduce the CAPEX by 10%. The **CONVERGE technologies will be validated** for more than **2000 cumulated hours** taking these from the discovery stage (TRL3) to development stage (TRL5).

In addition, the CONVERGE process will valorise the remaining biogenic and purified CO₂ for production of negative emissions via BECCS.





The KEROGREEN CO₂ plasma route to CO and alternative fuels

M.N. Tsampas, DIFFER, THE NETHERLANDS



Kerogreen aim: Demonstration of the full chain process from renewable, electricity, CO₂ (captured) and H₂O to kerosene.

- Research and optimization of individual process steps TRL (1-3) → 4
- Integration phase at Karlsruhe Institute of Technology → 3 L per day
- Duration 2018-2022

Program

Day 1

| Opening & Plenary sessions (chairperson Fausto Gallucci) | | |
|--|--|---|
| 9:00-9:30 | All coordinators - Introduction to projects | |
| 9:30-10:00 | Dr. E. De Coninck (CTO ArcelorMittal) - The zero Emission Plant | |
| 10:00-10:30 | Dr. Walter Eevers (CO2 Value Europe) | |
| 10:30-11:15 | Coffee break and posters | |
| | Session 1A (chairperson Jose Luis Viviente) | Session 1B (chairperson Camel Makhoulfi) |
| 11:15-11:35 | Dr. O. David - A review of the membrane development steps from material to final product | Dr. M. Noponen and Dr. X. Sun - High temperature electrolysis and co-electrolysis |
| 11:35-11:55 | Dr. V. Spallina - System simulation for integration of CO ₂ capture technologies into steelworks and CCUS clusters | Prof. J Serra - Direct electrocatalytic conversion of CO ₂ into chemical energy carriers in a co-ionic membrane reactor |
| 11:55-12:15 | Dr. M. Saric - Methanol membrane reactor: modelling and experimental results | Dr. V. Middelkoop - CO2Fokus at a glance: CO ₂ utilisation focused on DME production, via 3D printed reactor and solid oxide cell based technologies |
| 12:15-12:35 | Dr. Adam Deacon - Realising the potential of MOFs through efficient scale-up | Dr. M. Tsampas - The KEROGREEN CO ₂ plasma route to CO and alternative fuels |
| 12:35-12:55 | Dr. M. Etxeberria-Benavides - PBI based mixed matrix hollow fiber membranes for pre-combustion CO ₂ capture | Dr. G. Bonura - 3D-printing in catalysis: Development of efficient hybrid systems for the direct hydrogenation of CO ₂ to DME |
| 12:55-14:00 | Lunch break | |
| | Plenary session (chairperson Fausto Gallucci) | |
| 14:00-15:00 | Dr. Angels Orduna (Spire 2030) | |
| | Session 2A (chairperson Giampaolo Manzolini) | Session 2B (chairperson Vesna Middelkoop) |
| 15:00-15:20 | Dr. G. Garcia - LCA and TEA of the COZMOS technology | Dr. M. Sleczkowski and Dr. Pablo Ortiz - Turning gas separation membranes green with biobased block copolymers |
| 15:20-15:40 | Dr. A. Mattos or Dr. A. Mitchell - How can public policy and business model innovation be developed to address challenges of CCUS and realise the opportunity? | Dr. A. Benedito - CARMOF Project: a CO ₂ capture demonstrator based on membrane and solid sorbents hybrid process |
| 15:40-16:00 | Dr. L. Engelmann - Perception of CO ₂ -based fuels and their production in international comparison | Dr. R.H. Heyn - Introduction to the COZMOS project |
| 16:00-16:20 | Dr. N. Dunphy - Social studies in REALISE project | Dr. L. Petrescu - Converge technology for efficiency methanol production with negative CO ₂ emissions: energy and environmental analysis |
| 16:20-17:05 | Coffee break and posters | |

Day 2

| <i>Opening & Plenary Sessions (chairperson Fernanda Neira D'Angelo)</i> | | |
|---|---|--|
| 9:30-10:00 | All coordinators - Introduction to projects | |
| 10:00-11:00 | Dr. K. Bakke - Northern Lights – concept, plans and future | |
| 11:00-11:45 | Coffee break and posters | |
| | <i>Session 3A (chairperson José Serra)</i> | <i>Session 3B (chairperson Oana David)</i> |
| 11:45-12:05 | Dr. A. De Paula Oliveira - SER and SEWGS for CO ₂ capture: experimental results | Msc. A. Sliousaregko - Industrial membrane requirements for CO ₂ removal from different gas mixtures - Current practices and developments |
| 12:05-12:25 | MSc. S. Poto - Membrane reactors for DME production | Dr. I. Kim - Technologies demonstration in REALISE |
| 12:25-12:45 | Dr. U. Olsbye - Catalyst development within the COZMOS project | Dr. N. Kanellopoulos - Hybrid VTSA pilot plant and design of industrial demo plant for CO ₂ capture |
| 12:45-13:05 | Dr. S. Krishnamurthy - CO ₂ capture using 3D printed PEI adsorbents supported by carbon nanostructures | Mr. Paul Cobden and Prof. C. Abanades - Pilot preparation for demonstration in the C4U project |
| 13:05-13:25 | Dr. S. Perez - Process intensification in the conversion of CO ₂ with a milli-structured reactor | Mr. T. Swinkels - Decentralized FA based power generators |
| 13:25-13:45 | Dr. F. de Sales Vidal Vazquez - The KEROGREEN syngas route to alternative fuels and chemicals | Dr. L. Roses - Design and development of a membranebased post-combustion CO ₂ capture system |
| 13:45-14:30 | Lunch break | |
| 14:30-15:30 | <i>Round table and questions - closure (chairpersons Fausto Gallucci and Fernanda Neira)</i> | |

INTERNATIONAL WORKSHOP ON CO₂ CAPTURE AND UTILIZATION

TU/e - EINDHOVEN - 16-17 FEBRUARY 2021

Opening & Plenary sessions (chairperson Fausto Gallucci)

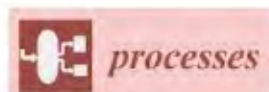
All coordinators - Introduction to projects

Dr. E. De Coninck (CTO ArcelorMittal) - The zero Emission Plant

ORGANIZED BY



SPONSORED BY





ArcelorMittal

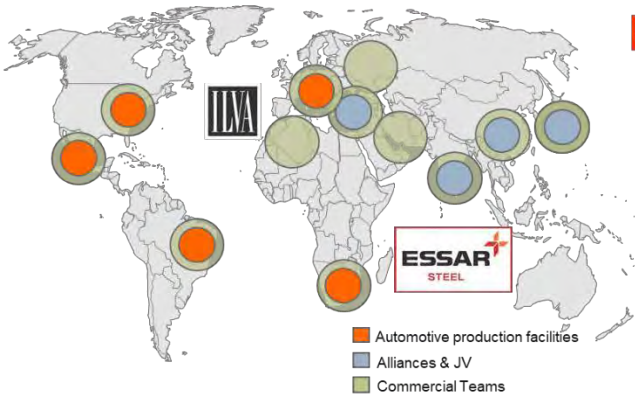


ArcelorMittal : possible pathways towards
THE LOW EMISSION PLAN(T)

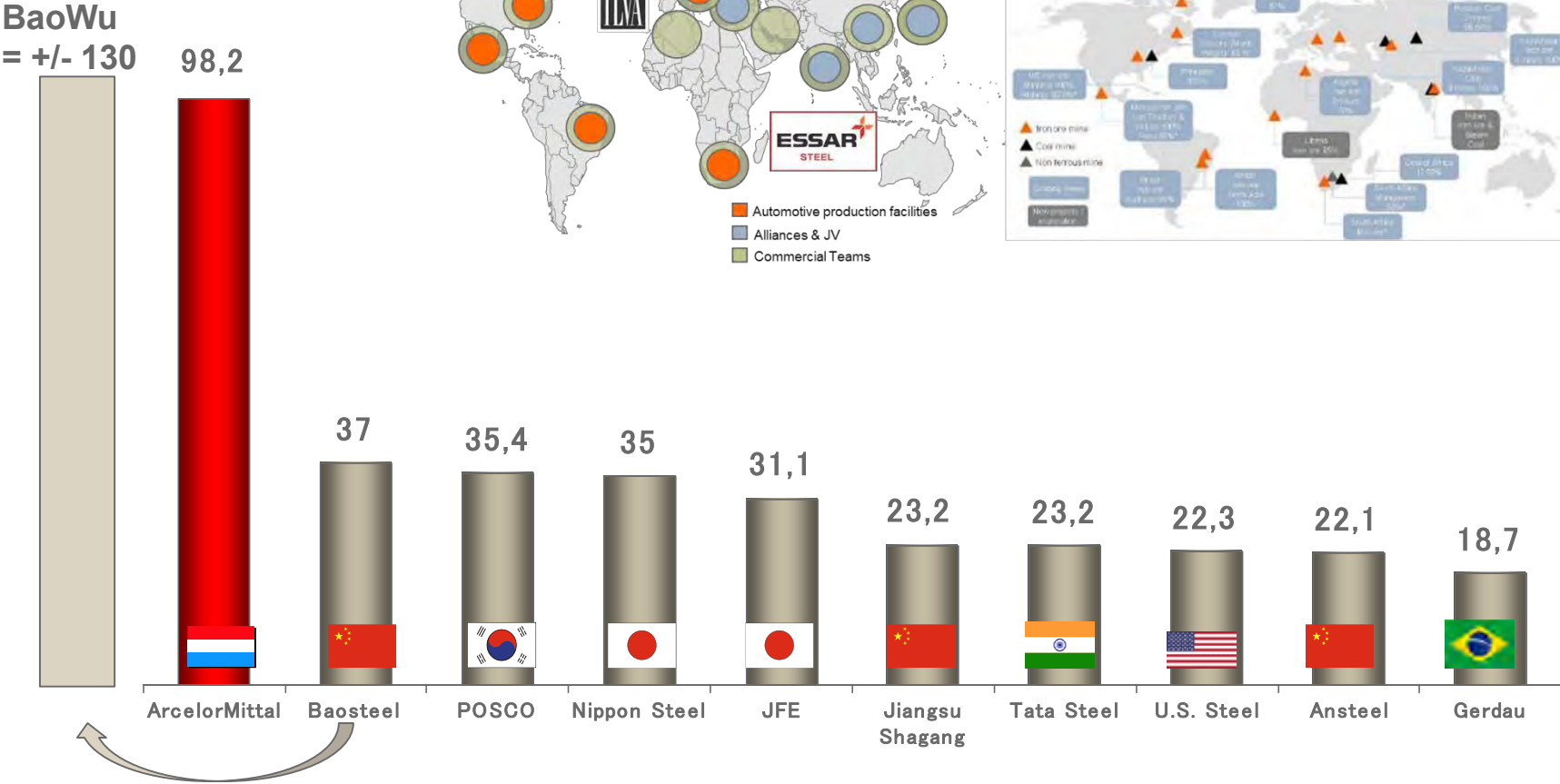
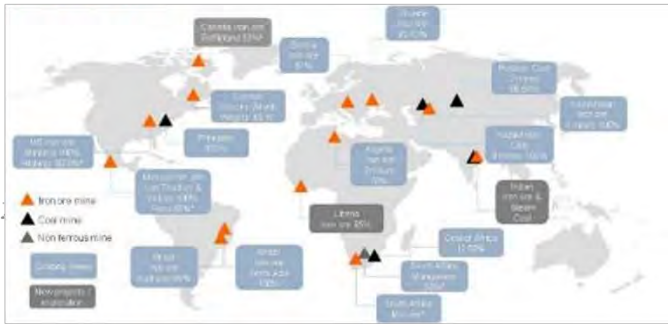
July 2020

Largest steel producers (in mt crude steel)

ArcelorMittal's industrial and commercial network



Mining business portfolio



* Source: Worldsteel

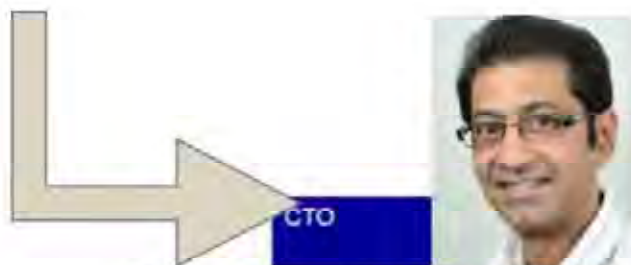
Group Management



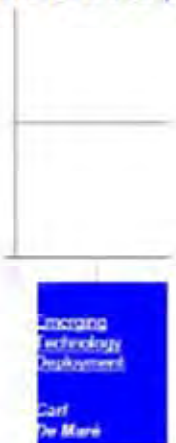
Aditya MITTAL
Chief Executive Officer
(CEO)



ArcelorMittal
Lakshmi N. MITTAL
President of the Board



Pinakin CHAUBAL |



LIS team = low impact steel making



LIS* Eric De Coninck
Wim Van Der Stricht
Jean Borlée



Give carbon
a second life
~~eternal~~

Agenda :

1. European history of steelmaking
2. Others are still at the very beginning of this history
3. What can Europe afford ?
4. Low emission principles
 - a) Gas separation
 - b) CO re-use by chemical industry
 - c) CO₂-H₂-chemistry : new technologies
 - d) CO₂ sale
 - e) CO₂ storage
5. Some political issues

The challenge of the steel industry = C-footprint reduction



Conventional steel making = blast furnaces (BF) Electrical steel making = electric arc furnaces (EAF)

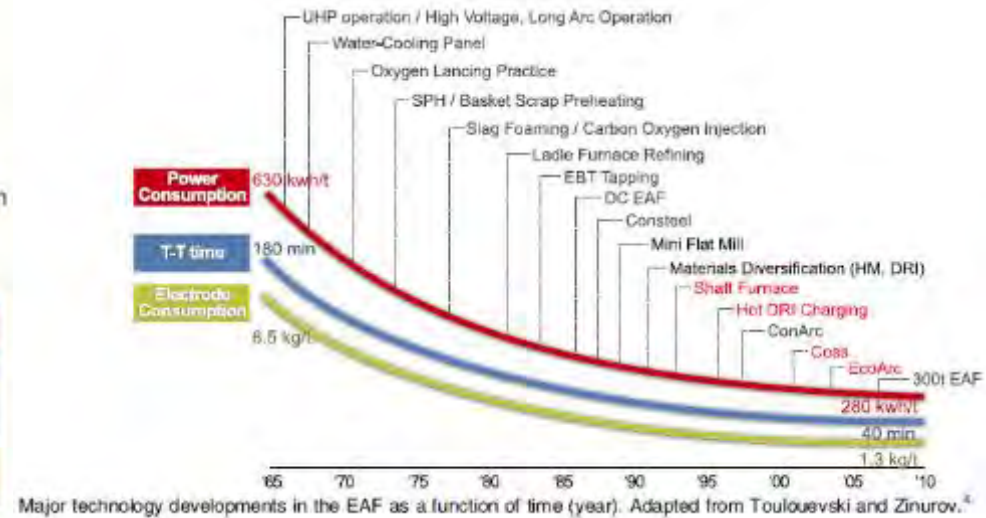
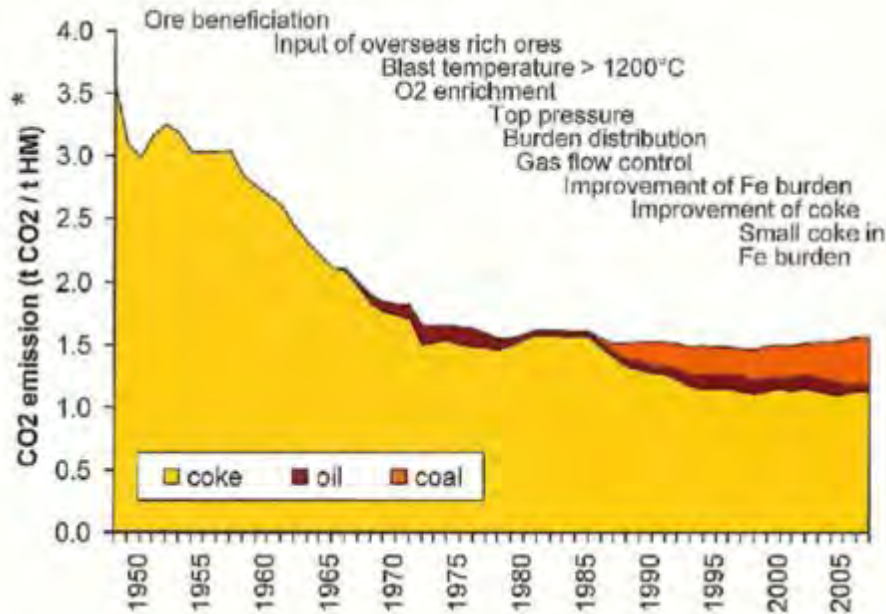
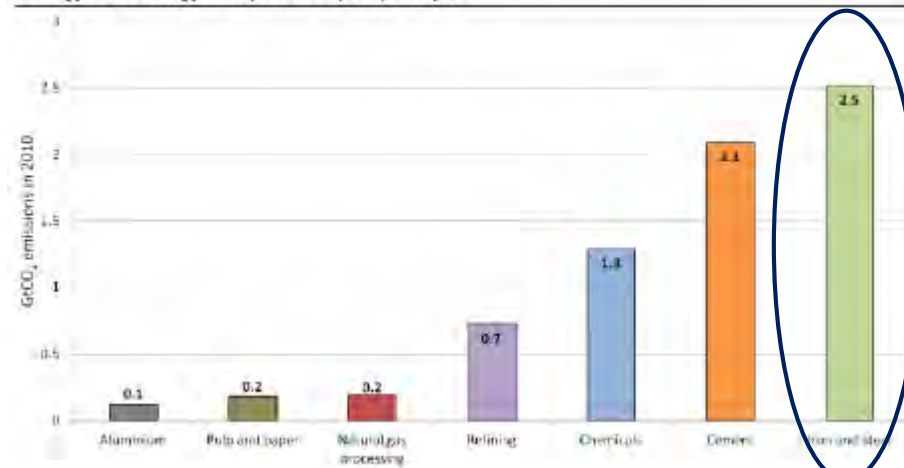


Figure 1. Global emissions from the seven most CO₂-intense industrial sectors in the IEA Energy Technology Perspectives (ETP) analysis

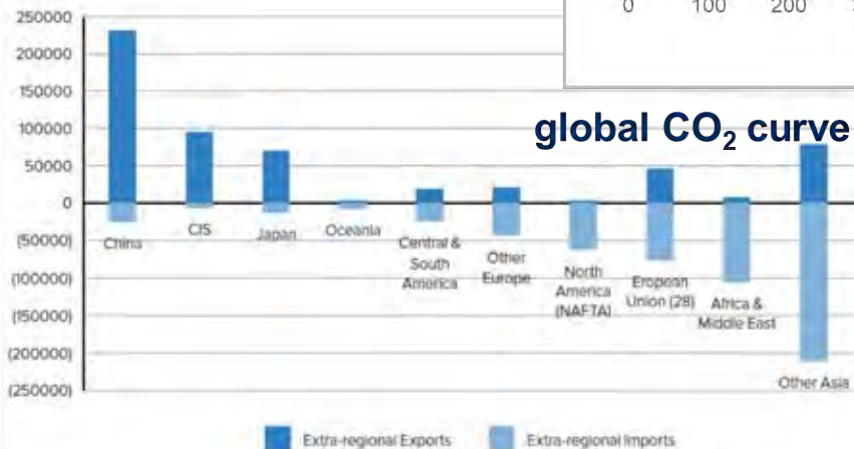
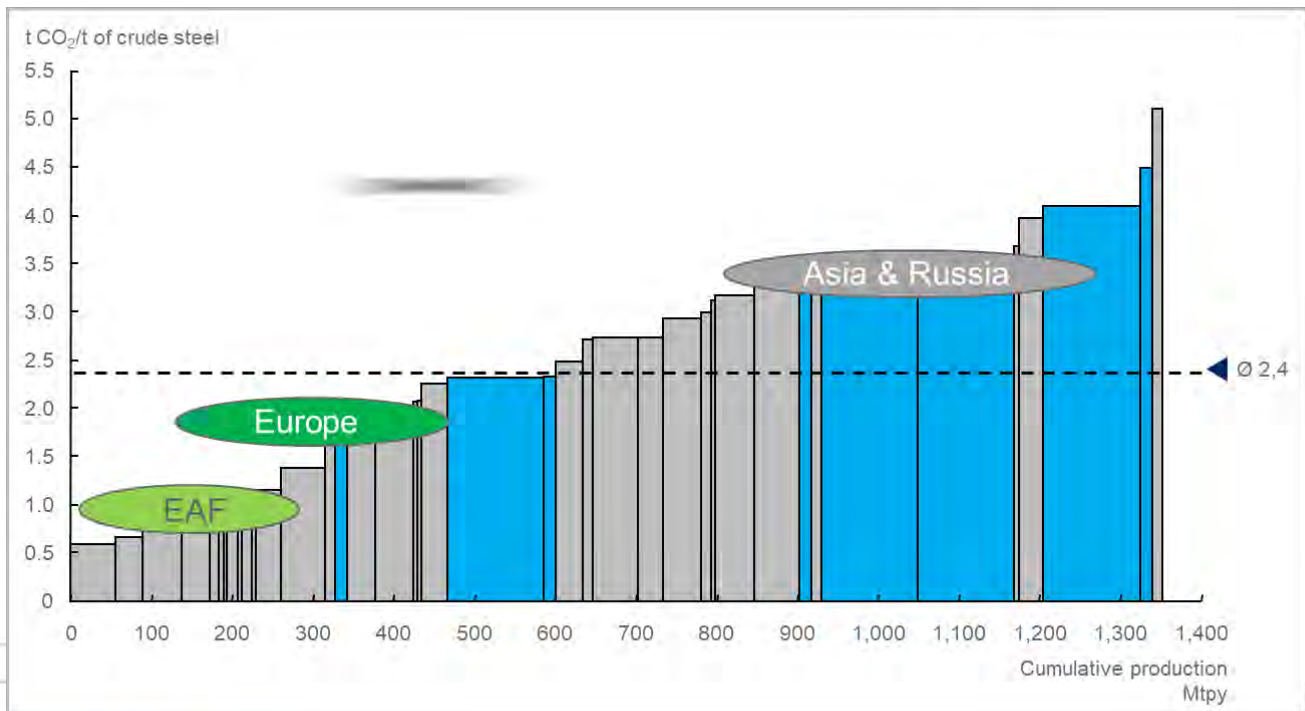


1,8 billion tons of steel in 2018

30% of industrial CO₂-emissions.
6,7% of anthropogenic CO₂-emissions

They are amongst the highest of industries....

China/India
Other



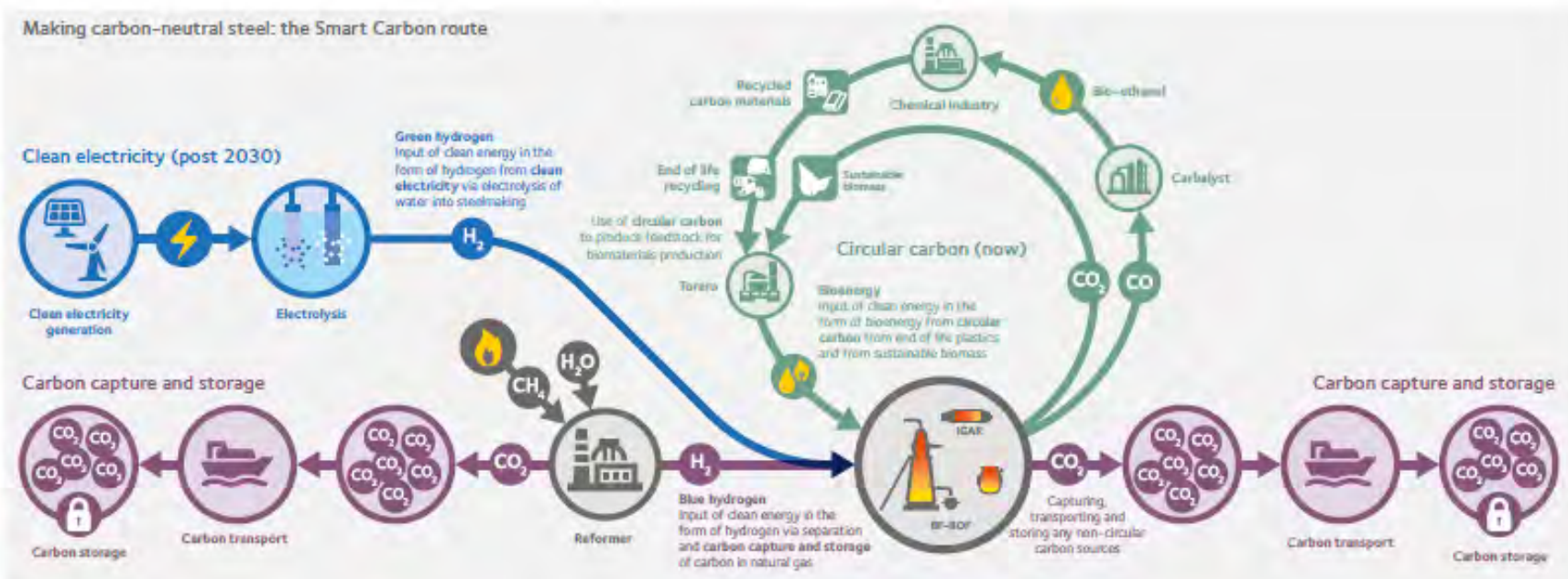
C-footprint reduction : the main emitters are not located in Europe !!!

Figure 3.1.2. World trade of carbon embodied in commodity steel by region (kton CO₂) in 2016

AM decarbonation plan : -30% by 2030, carbon neutrality by 2050

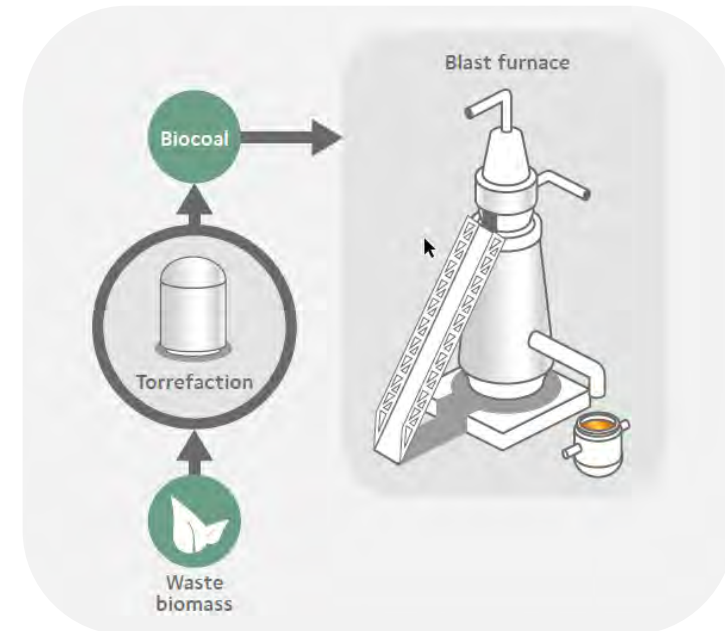
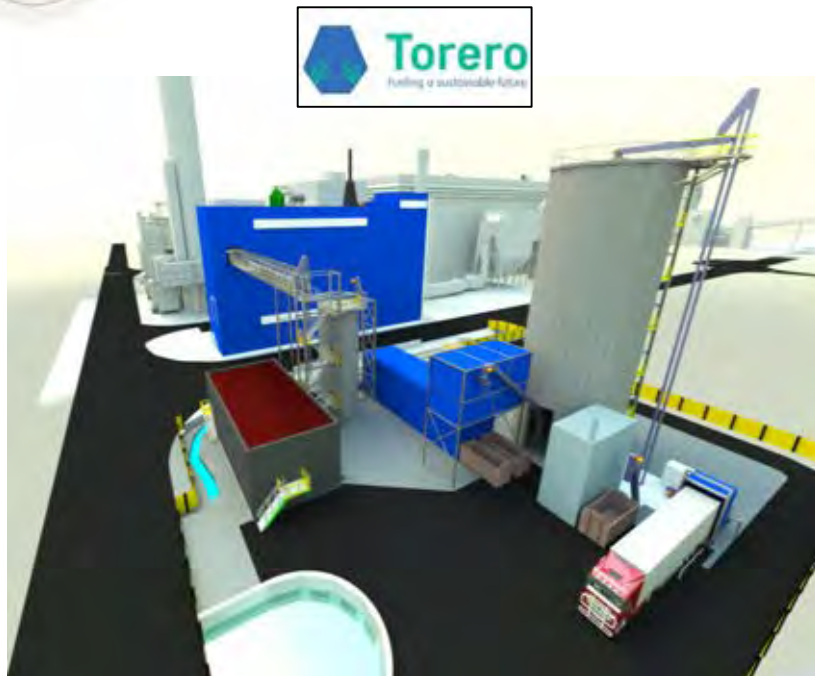
Several measures to be developed :

- Energy efficiency and recovery
- Maximum use of affordable renewables (scrap melting) and C-free hydrogen (DRI)
- Use of biomass
- Use of circular carbon products (e.g. waste plastics)
- Re-use of carbon emissions (CCU)
- Storage of carbon emissions (CCS)




AM decarbonation plan : biogenic carbon : free of CO2 allowances, is available in small volumes, e.g. waste wood....

Circular Carbon – Upgrading waste wood into “Bio-Coal” and plastics into circular carbon



Torero – 30m€ demo project to convert 120.000 ton waste materials into “bio-coal” in ArcelorMittal Gent

Carbon can be re-used :



Scientific Advice Mechanism (SAM)

Novel carbon capture and utilisation technologies

Group of Chief Scientific Advisors
Scientific Opinion 4/2018

Scientific Opinion
Novel Carbon Capture and Utilisation Technologies

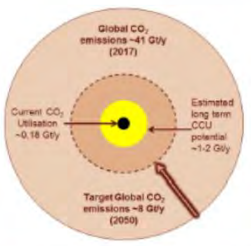


Figure 8 – Global CO₂ emissions and the role of CCU. The figure shows also the target global emissions for 2050 as well as a simplified estimation for the CCU potential including all the possible uses (simplified and adapted^{21, 22}).

CORESVM

CarbOn-monoxide RE-use through industrial SYMBiosis between steel and chemical industries

CORESVM

CarbOn-monoxide RE-use through industrial SYMBiosis between steel and chemical industries

CO-rich waste gases can be converted into products with a reduction of CO₂ emissions and other negative impacts.

Using waste gases as a feedstock, instead of for energy, can result in emission reductions from the production of energy and products of up to 21-34% compared to the baseline. In addition, the process of cleaning up waste gases for use as a feedstock also results in a concentrated stream of CO₂, which lends itself to Carbon Capture and Storage (CCS). While roughly a third of the direct emissions from waste gases can be mitigated through use as a feedstock, an additional third is made capture ready in the process. If CCS is implemented alongside waste gas recycling at a European scale, this could result in a reduction of up to 3% of European CO₂ emissions. In addition to reducing CO₂ emissions, when substituting waste gases for biobased feedstocks, water demands, wastewater production, and land use reduced, with positive implications for biodiversity.



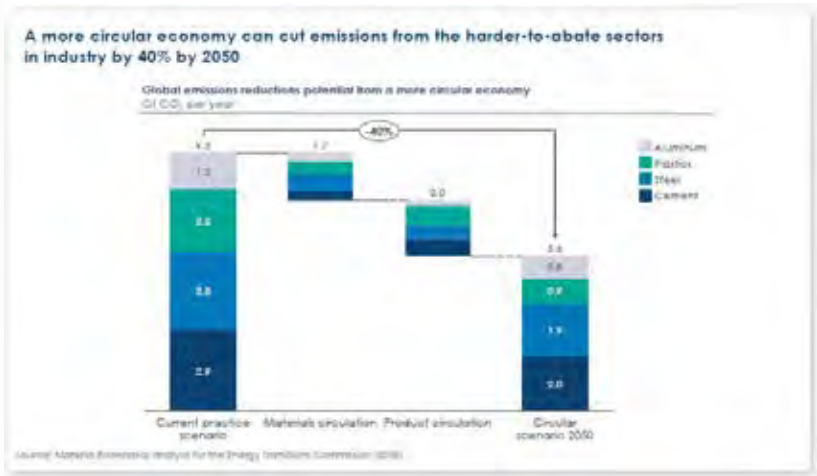
recent Risk Management position paper (DNV, 2011) states that using a variety of carbon utilisation technologies can potentially reduce annual CO₂ emissions by 3.7 Gt. This equates to approximately 10% of current annual CO₂ emissions. A 10% replacement of building materials by CO₂ captured in stable minerals would reduce CO₂ emissions by 1.6 Gt. CCS is the only option to decarbonise many industrial sectors. CCS is currently the only large-scale mitigation option available to cut the emissions intensity of production by over 50% in these sectors.

Take home message

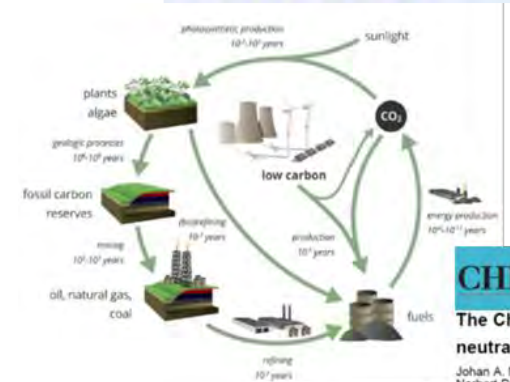
Trading renewable energy by using CO₂ has a potential impact on mitigation of climate changes of over 7 Gtons CO₂ equivalent.



| CO ₂ uses | Existing (future) CO ₂ demand (Mt per h) |
|--------------------------------------|---|
| Enhanced oil recovery | 30-300 (<100) |
| Urea | 3-30 (<10) |
| Food and beverage | ~ 17 (35) |
| Water treatment | 1-5 (<5) |
| Other | 1-2 (<6) |
| Enhanced coal bed methane recovery | (10-100) |
| CO ₂ concrete curing (MC) | (10-300) |
| Algae cultivation | (>300) |
| Mineralisation (MC) | (>300) |
| Red mud stabilisation (MC) | (5-30) |
| Baking soda (MC) | <1 |
| Liquid fuels (methanol, formic acid) | (>600) |



Hitchhiker's Guide to Carbon Capture and Utilisation



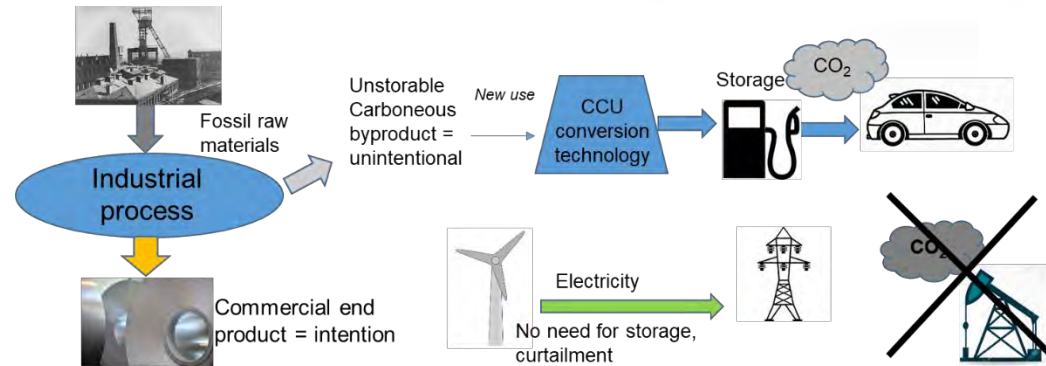
CHEMUSCHEM
The Chemical Route to a CO₂-neutral world

Johan A. Martens,^{1,10} Annemie Bogaerts,^{1,10} Norbert De Kimpel,^{1,10} Pierre A. Jacobs,^{1,10} Guy B. Marin,^{1,10} Korneel Rabaey,^{1,10} Mark Saeyns^{1,10} and

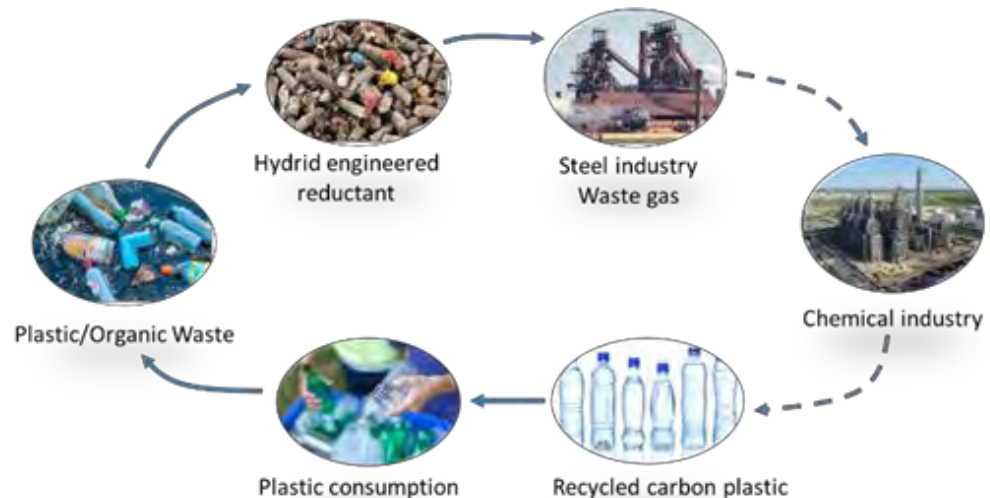
The Low Emission Plant principles

Technical principles :

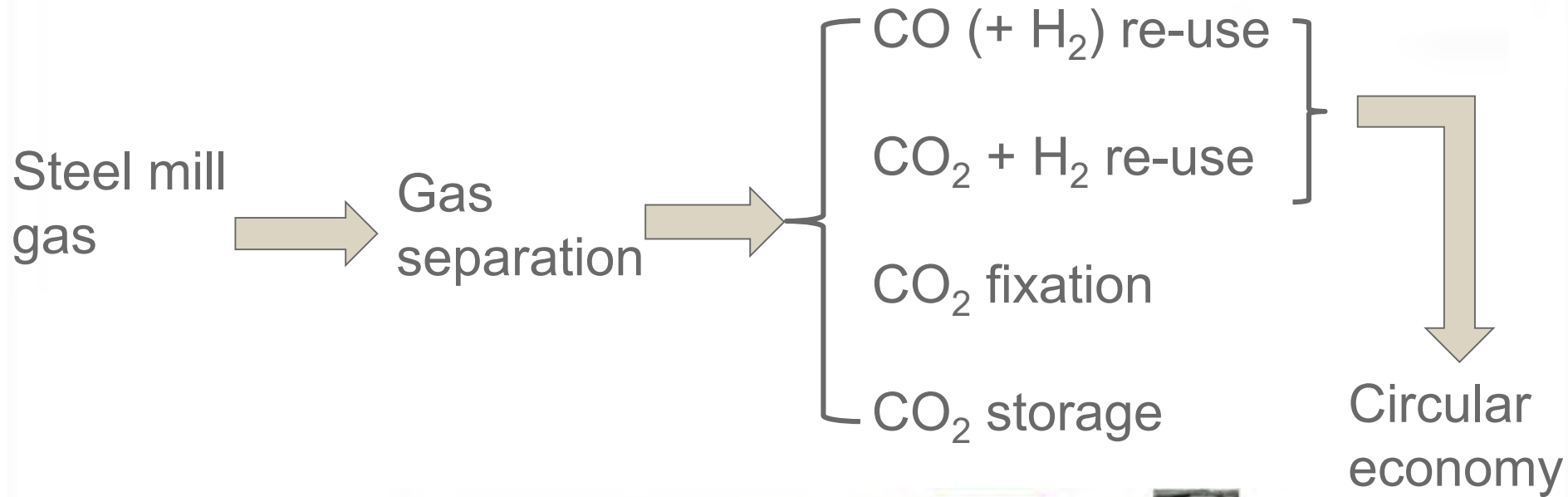
- Half of the steel mill gases is CO, which is burnt for power production. By not burning the CO a lot of CO₂ is avoided.
- This CO can be used for fuel and chemical production.
- The lack of electricity on the grid, can be compensated by the production of RENEWABLE electricity. This is the major lever to reduce the CO₂ emissions
- By separating the CO from the CO₂, pure CO₂ is available for re-use or storage.



Only the re-use of C
can ignite a
CIRCULAR economy



The different steps of the Zero Emission Plan(t) concept of ArcelorMittal



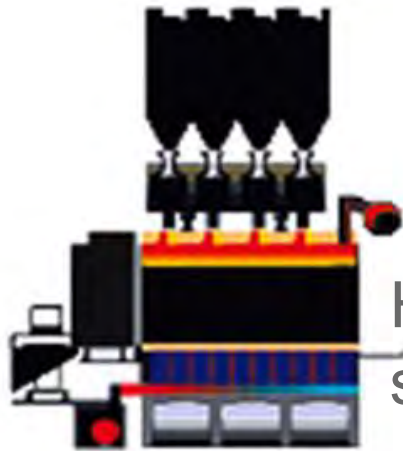
The steel mill of the future will still produce gasses



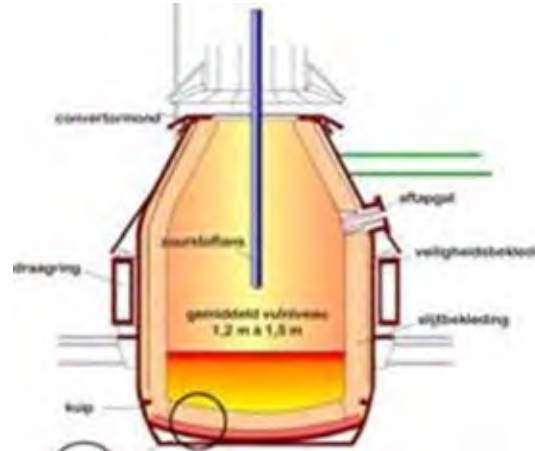
ArcelorMittal

Coke Oven gas

Basic Oxygen Furnace gas



H₂ and CH₄
source



CO source

Peak name

Benzene
Toluene
Ethylbenzene
p-Xylene
m-Xylene
o-Xylene
DCPCD
Styrene
Ethylacetylene
Vinylacetylene
Hydrogensulfide
Corbonylsulfide
Methylmercaptan
Carbondisulfide
Thiophene
Ethane
Ethylene
Propane
Propylene
iso-Butane
n-Butane
Acetylene
trans Butene-2
1-Butene
iso-Butene
cis Butene-2 + Neopentane*
n-Pentane
Butadiene 1-3
Methyl Acetylene

Blast Furnace gas

CO₂ , CO and
N₂ source

BF Gas : 62 %
BOF Gas : 10%
CO Gas : 28%

52% of the gas energy
replaces natural gas in
the plant

Power plant : 48%

15/09/2020

Con

The steel mill of the future will provide the single gas components



Steel mill
gases
 $\text{CO}/\text{CO}_2/\text{H}_2/\text{N}_2$

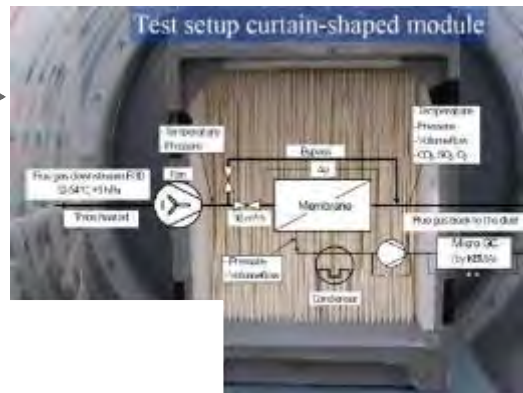


DMEA
Solvents

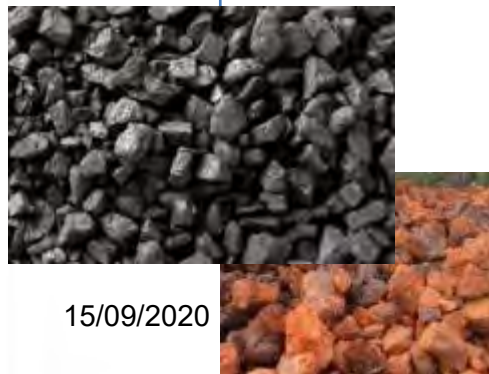
(V)PSA



AM Saldanha Works VPSA



MEMBRANE



15/09/2020

The steel mill of the future will provide the single gas components



3D : pilot project 2019 – 2023 (Dunkirk)

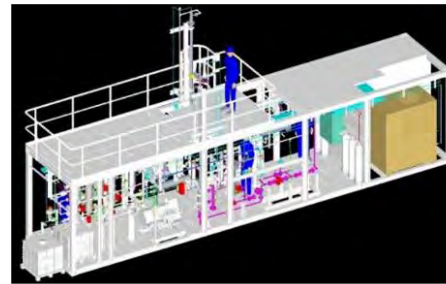
pré-FEED done by IFPEN



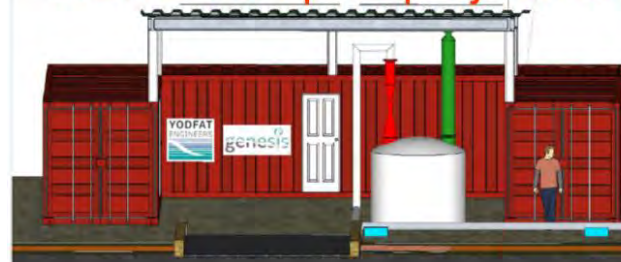
IFPEN mini-pilot in Solaize

Carbon2Value : pilot project 2018 – 2020

INTERREG sponsored project



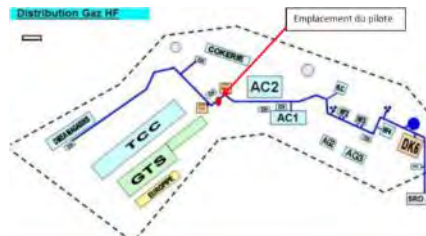
GENESIS : pilot project 2019 – 2021



Membrane separation :



Capture of 0,5 t/h CO₂
from 1.100 Nm³/h BF-
gas to study feasibility

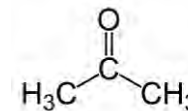
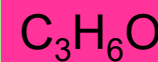
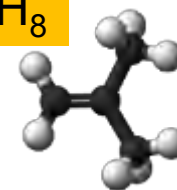
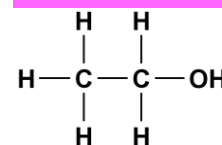
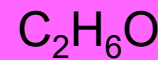


The steel mill of the future will sell CO



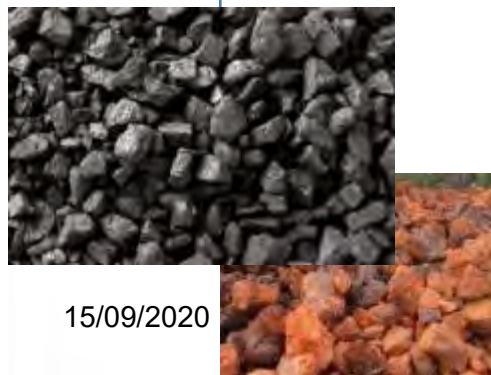
Valorisation of steel mill CO

Sale to chemical industry
Conversion into valuable hydrocarbons



H₂- sources =

- Coke Oven gas
- H₂ surplus from chemical partner
- Electrolysis



15/09/2020

The steel mill of the future will sell CO

struction

Civil works
Zone J

Starting installation RO and Ethanol
piping

Steelconstruction
distillation



Civil works PSA

Closing walls
main building

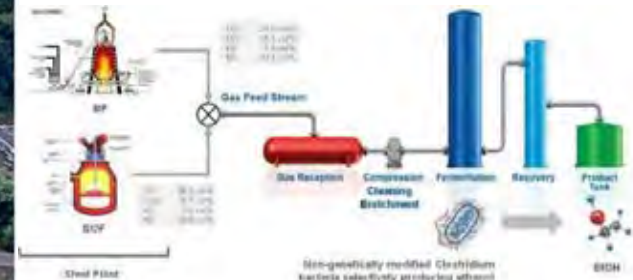
Finishing high wall
zone transformer

Installation GC pit

Installation
compressor MAN

Install piperack +
crossing Knippegroen

The Gent Ethanol plant



CCU
CCS

EtOH production = X T/y
CO₂ avoided = 2,1 X T/y
CO₂ captured = 6,6 X T/y
Total CO₂ = 8,7 X ton/y

Potential of 300 kton EtOH/year = 380
Mt/year = over 700 kT/y of CO₂ savings



Shougang Commercial Plant

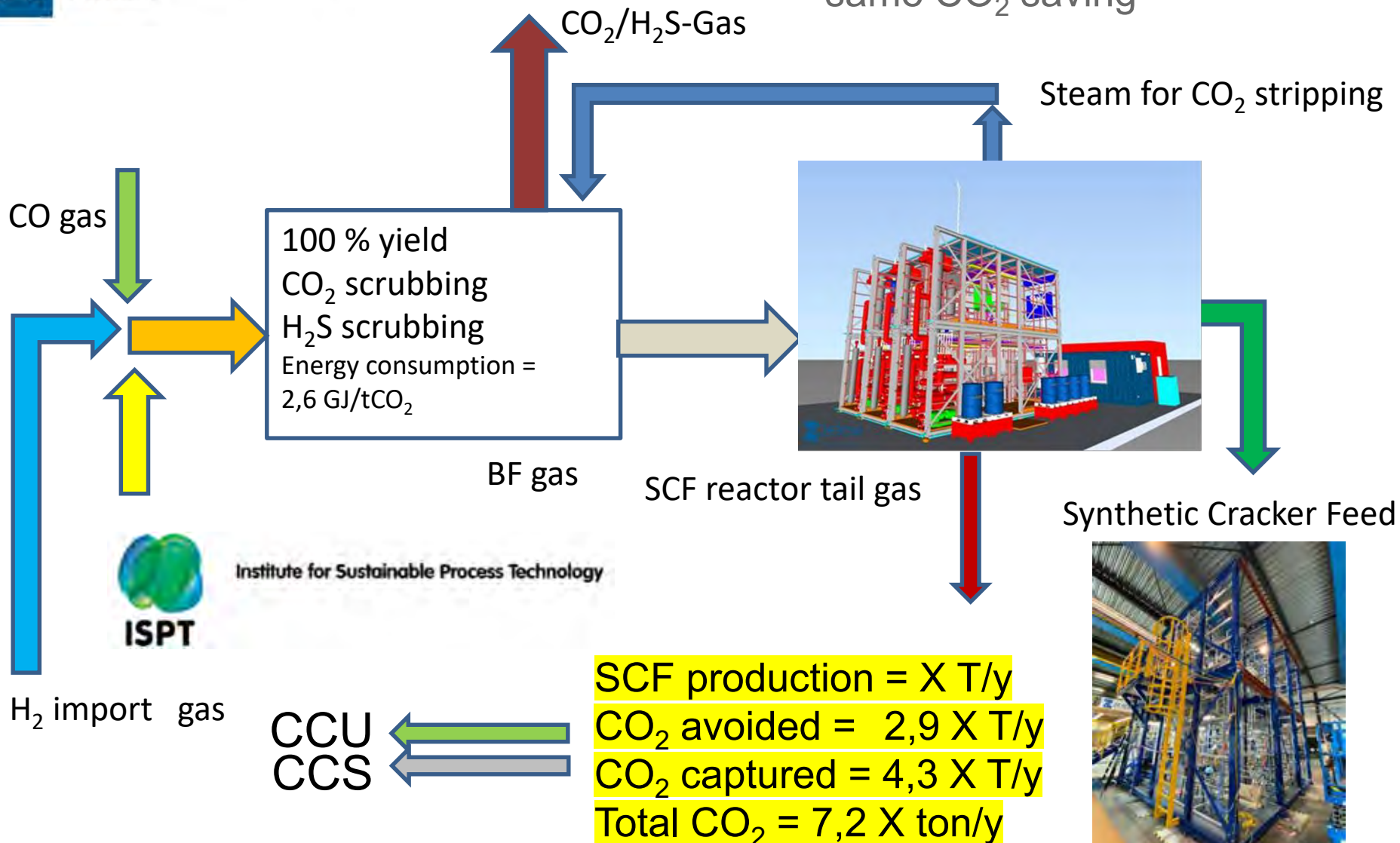


The steel mill of the future will sell CO



Rijksdienst voor Ondernemend
Nederland

CAPEX = 10% of investment
cost of wind energie, for the
same CO₂ saving



The steel mill of the future will sell CO₂ - derivatives



Valorisation of steel mill CO₂

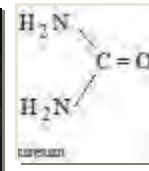
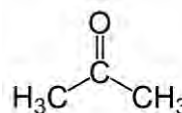
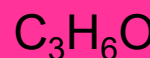
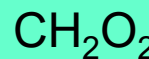
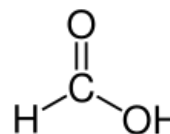
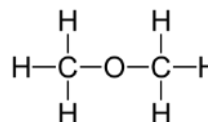
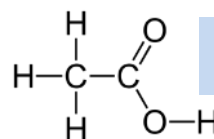
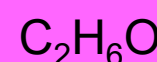
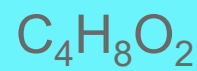
Fuels - chemicals



Raw CO₂

H₂- sources =

- Coke Oven gas
- H₂ surplus from chemical partner
- Electrolysis

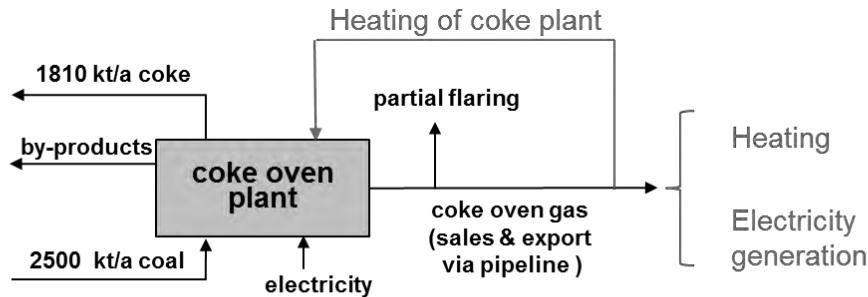


Cellule électrochimique



15/09/2020

The steel mill of the future will sell CO₂ - derivatives



Today

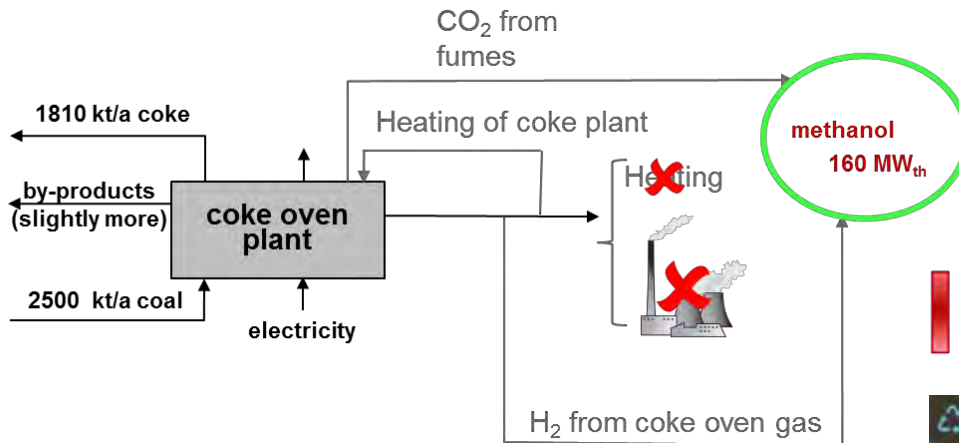


In a standby coal fired power plant



Heating
Electricity generation

<https://www.carbonrecycling.is/news/co2-to-methanol-plant-china>



recycled carbon transport fuel

Shuncheng Steel China

In Future



Carbon Recycling International (CRI) and Shougang Steel have signed an agreement with Chinese technology developer Carbon Recycling International (CRI) to design a pilot-scale CO₂-to-methanol plant that will produce low-carbon transport fuel in China. The agreement was signed at CRI's headquarters in Reykjavik, Iceland. The plant will be located in Shougang Steel's facility in Beijing. The plant will produce 100,000 tonnes of methanol per year, which will be used to produce 100,000 tonnes of low-carbon steel. The plant will also produce 100,000 tonnes of CO₂ per year, which will be used to produce 100,000 tonnes of low-carbon steel. The plant will also produce 100,000 tonnes of CO₂ per year, which will be used to produce 100,000 tonnes of low-carbon steel.

MeOH production = X T/y
CO₂ avoided = 1,3 X T/y
CO₂ captured = (1,3 X T/y)
Total CO₂ = 1,3-2,6 X ton/y
+ additional PP closure
Total CO₂ = 7 X ton/y

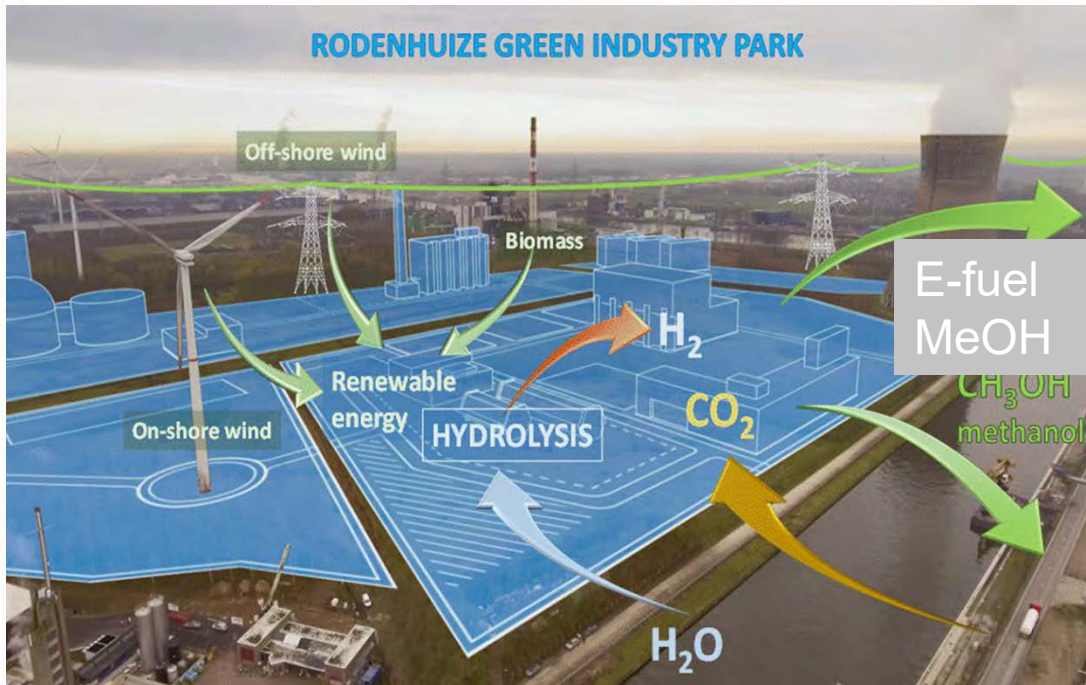
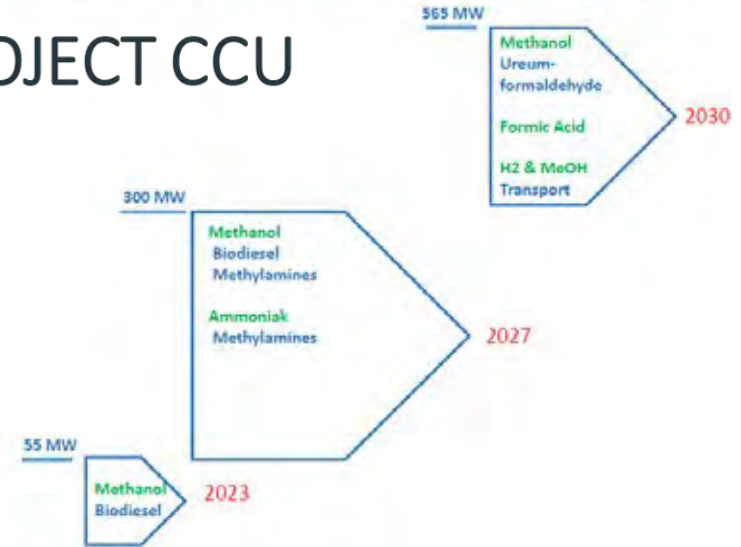
CCU
CCS

confidential

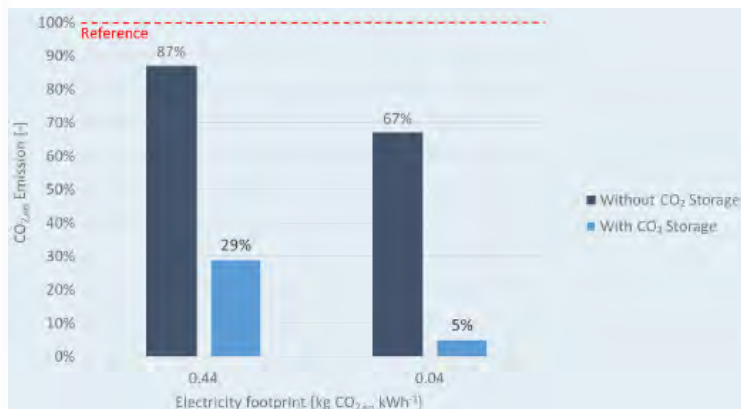
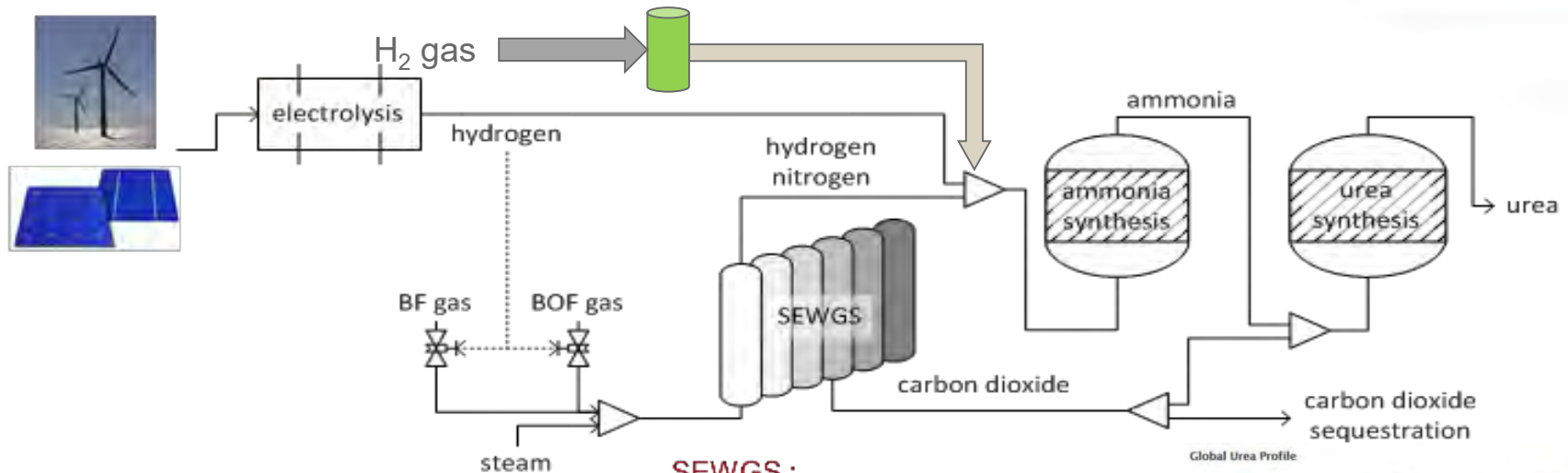
The steel mill of the future will sell CO₂ - derivatives



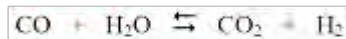
RODENHUIZE - DEMONSTRATIEPROJECT CCU



In integrated steel mills .. a combination of gases can be used



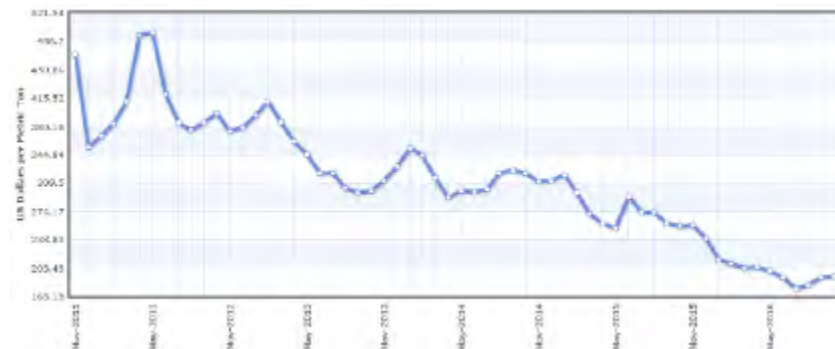
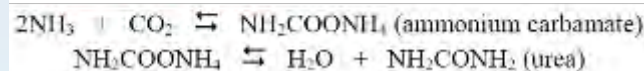
SEWGS :



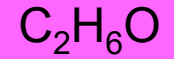
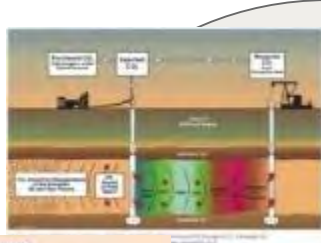
Ammonia production :



Urea production :



The steel mill of the future will sell CO₂



Sale of the CO₂ (industrial gas supplier, green houses, EOR ...)

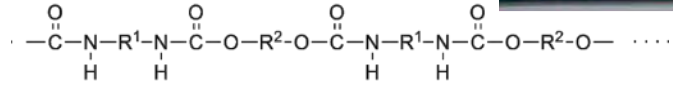


Carbonation minerals – slags - ..



Photo 1: overview of the rotating batch autoclave

Polyurethane



CO₂ to fuels and chemicals

CO₂ high temperature electrolysis with renewable electricity

CO₂ reforming in plasma torches with renewable electricity

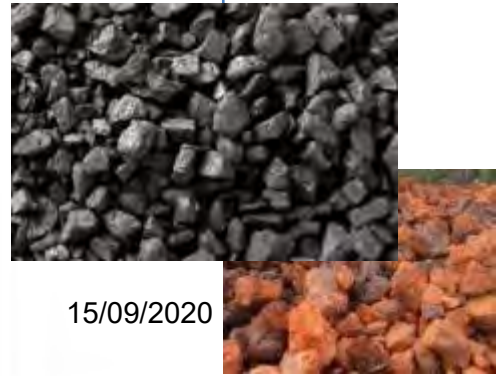


Raw CO₂

Valorisation of steel mill CO₂



Figure 1 : plasma flame of a 2 MW torch



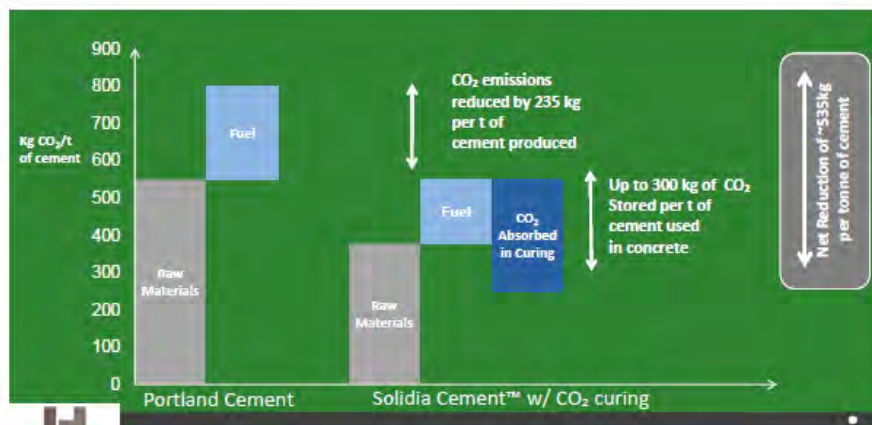
15/09/2020

The steel mill of the future will sell CO₂

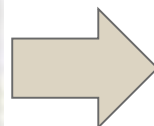


PCC
production

Up to 70% reduction in CO₂ footprint/t of cement used in concrete



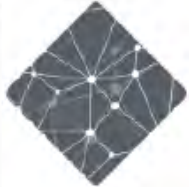
Metal Dust



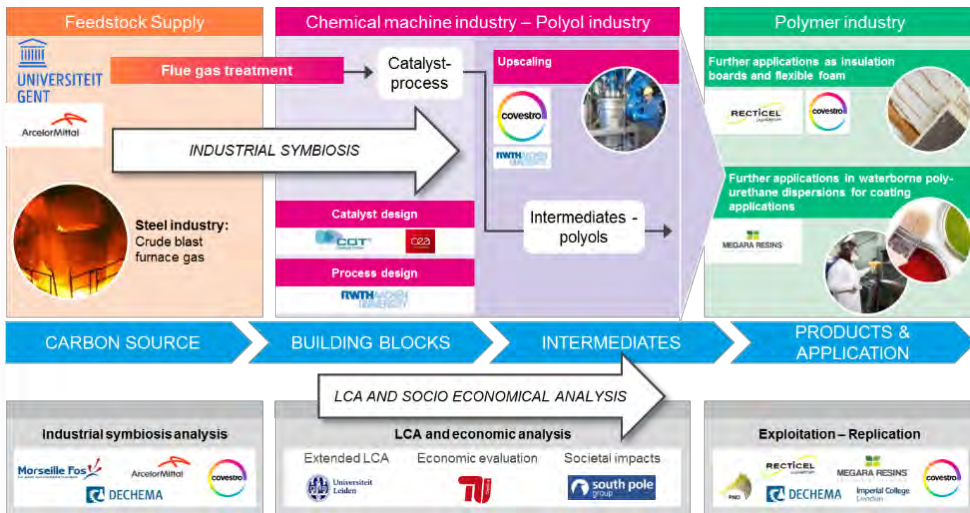
INDUSTRIAL PRODUCTION IN THE NETHERLANDS



Confidential

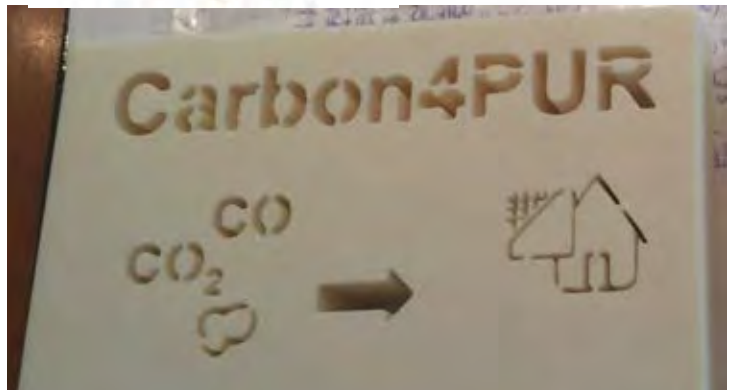


Carbon4PUR

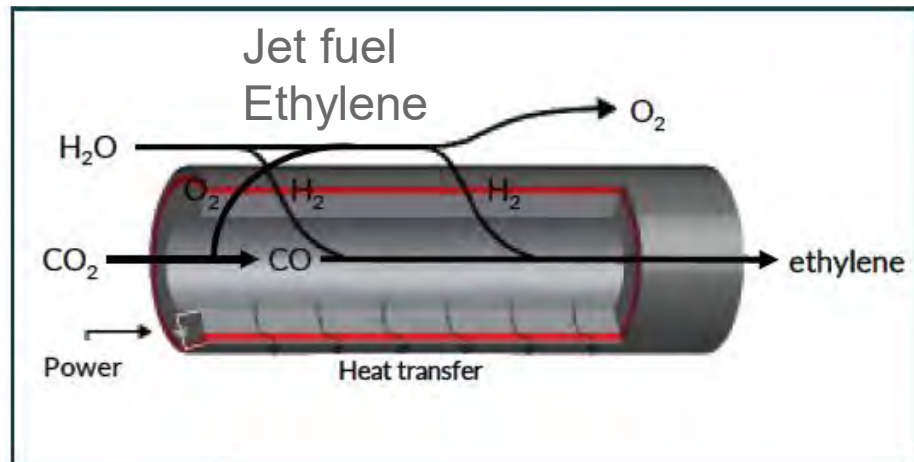


15/09/2020

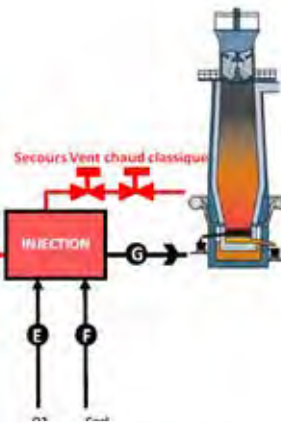
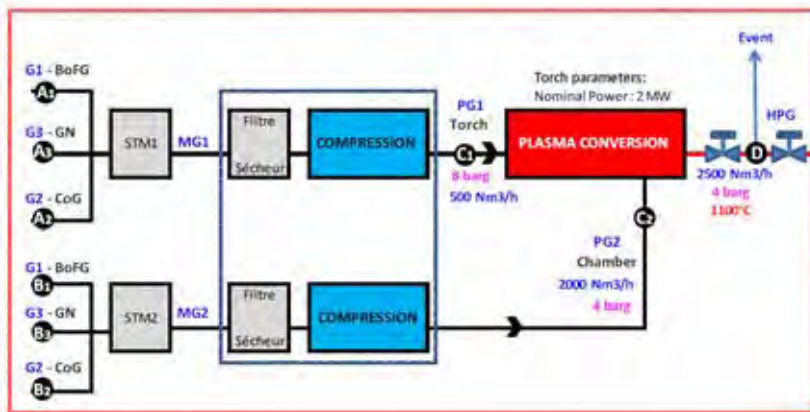
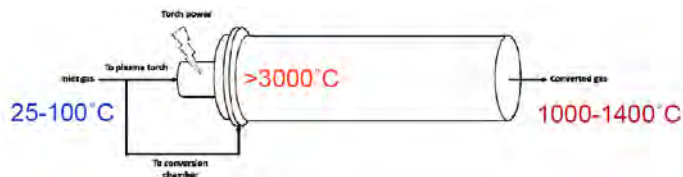
CONFIDENTIAL



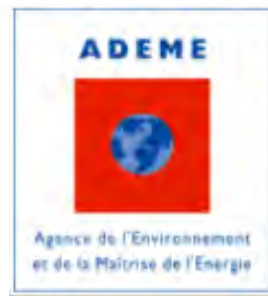
PUR production = X T/y
CO₂ avoided = 0,2 X T/y



IGAR project at AMAL Dunkirk



EUROPLASMA
Plasma torches applied to energy and environment



? connections (pipes to be installed)



Algae project at AM Fos sur Mer

15/09/2020



Photo 3 : Bassin 10 m² de culture de micro algues marines avec fumées industrielles – site ArcelorMittal.



H₂ based steelmaking project at AM Hamburg

ArcelorMittal Hamburg erprobt Wasserstoff in der Stahlproduktion

2019 Top 5 DRI Producing Nations

| COUNTRY | PRODUCTION (Million Tons) |
|--------------|---------------------------|
| India | 33.74 |
| Iran | 28.52 |
| Russia | 8.03 |
| Mexico | 5.97 |
| Saudi Arabia | 5.79 |

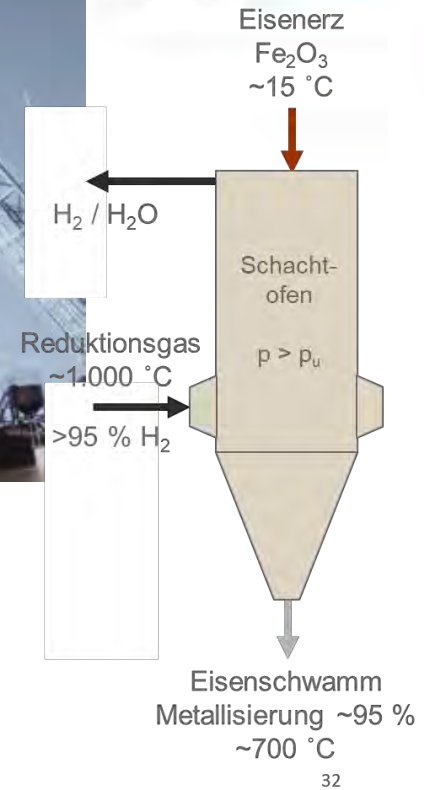
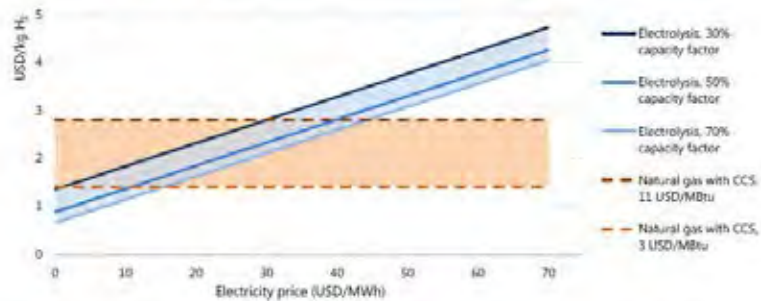


Figure 17. Comparison of hydrogen production costs from electricity and natural gas with CCS in the near term

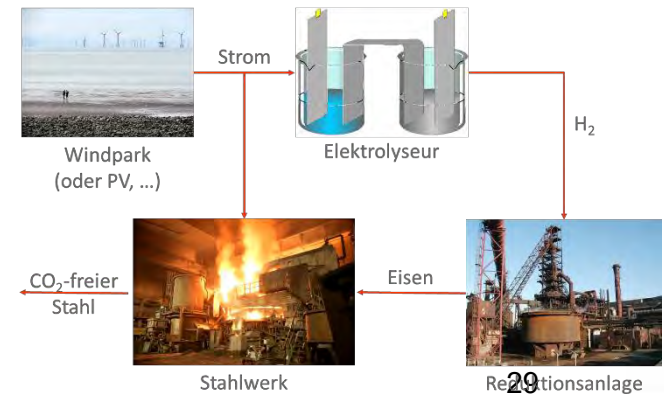


Notes: CAPEX: electrolyser USD 300/kW_e, SMR w CCS USD 1.50/kW_e, full load hours of hydrogen from natural gas 8 300 h; efficiencies (LHV): electrolyser 70%, gas with CCS 69%, capture rate for gas with CCS of 90%, discount rate: 8%.

Source: IEA (2019), The Future of Hydrogen: Seizing Today's Opportunities

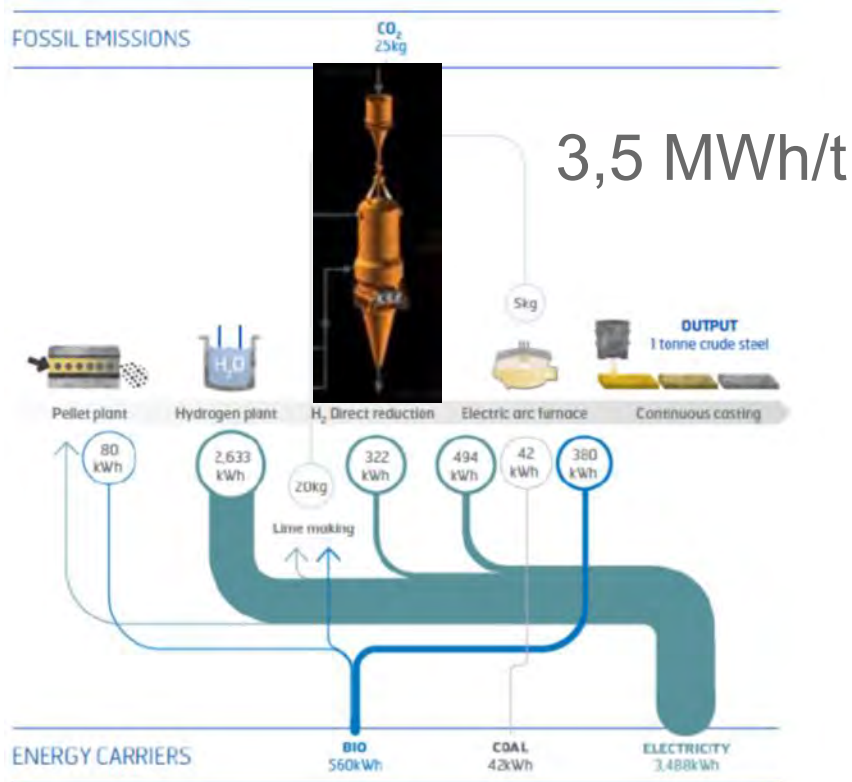
Depending on local gas prices, electricity at USD 10/MWh to USD 40/MWh and at full load hours of around 4 000 h is needed for water electrolysis to become cost competitive with natural gas with CCUS.

Vision für CO₂-freie Stahlerzeugung



AM is looking to the use of renewable electricity in different ways :

Use of green hydrogen in DRI making :



Direct electrolysis of Fe :



3,11 MWh/t



The steel mill of the future may have a legal problem ... and no market for its products



RED 2 : 2020 - 2030 Recycled Carbon Fuels

Many of these products will cost more than the fossil products

1. The LCA-methodology has to be defined and accepted in a delegated act. The minimum threshold of GHG reduction is not yet fixed (renewable electricity is privileged for transport = EV)
2. Member states can decide themselves if they allow Recycled Carbon Fuels in the energy mix for transport
3. The CO₂ taxes for re-used carbon may not be eliminated (ETS)

The promotion of recycled carbon fuels can also contribute towards the policy objectives of energy diversification and transport decarbonisation when they fulfil the appropriate minimum greenhouse gas savings threshold. It is therefore appropriate to include those fuels in the obligation on fuel suppliers, whilst giving Member States the option not to consider these fuels in the obligation if they do not wish to do so. Since those fuels are of non-renewable nature, they should not be counted towards the overall EU-target for energy from renewable sources.

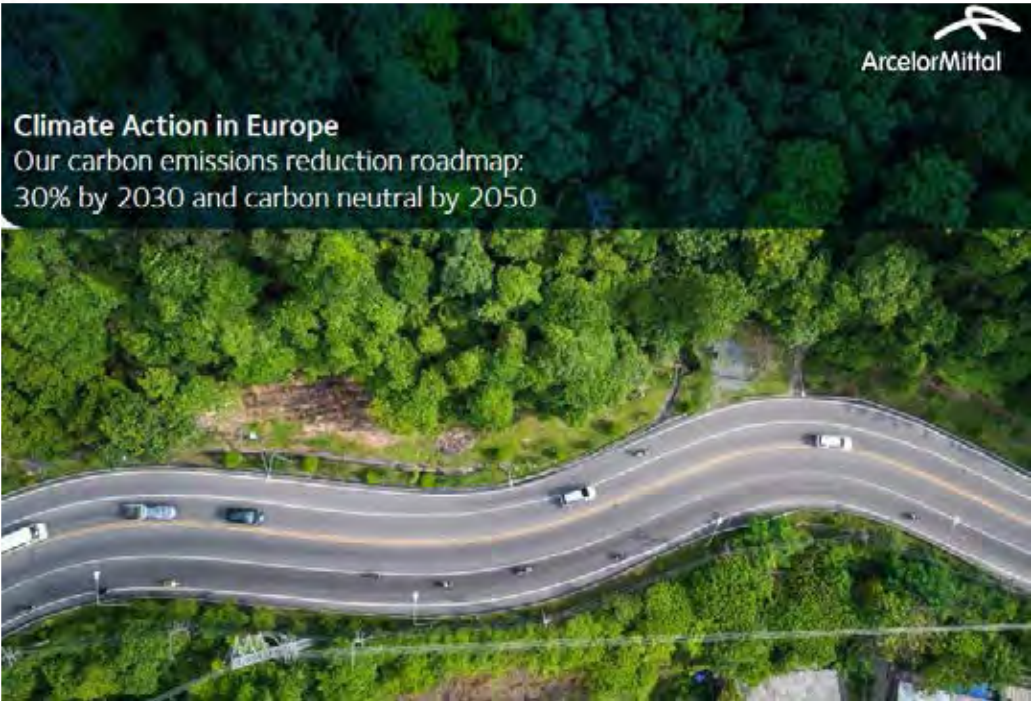
EUROPEAN COMMISSION



greenhouse gas emission savings from renewable liquid and gaseous transport fuels of non-biological origin and recycled carbon fuels, which shall ensure that no credit for avoided emissions be given for carbon dioxide whose capture already received an emission credit under other legal provisions.

15/09/2020

Confiden



Climate Action in Europe
Our carbon emissions reduction roadmap:
30% by 2030 and carbon neutral by 2050



Climate Action
Report 1
May 2019

"Our ambition
is to significantly
reduce our
carbon footprint."

The Zero Emission plant....



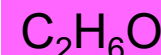
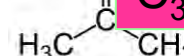
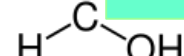
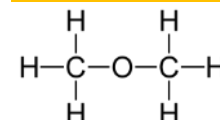
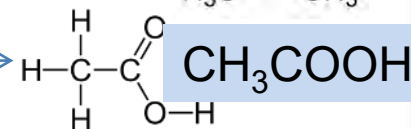
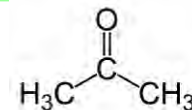
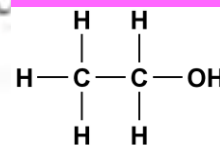
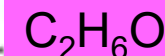
Steel mill
gases
 $\text{CO}/\text{CO}_2/\text{H}_2$

Clean H_2
From COG,
electrolysis or excess
from chemical industry



Clean CO/H_2

Sale to chemical industry



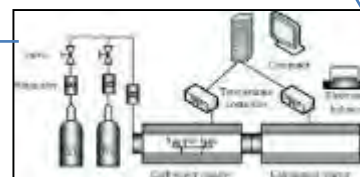
Clean
 CO



Clean CO_2/H_2

Ra

CO_2
conversion with
renewable
electricity



Sale to gas
industry

EOR

CSS

Public pipe

15/09/2020

Thank you for your attention

INTERNATIONAL WORKSHOP ON CO₂ CAPTURE AND UTILIZATION

TU/e - EINDHOVEN - 16-17 FEBRUARY 2021

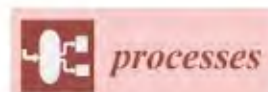
Session 1A (chairperson Josè Luis Viviente)

- 11:15-11:35 Dr. O. David - A review of the membrane development steps from material to final product
- 11:35-11:55 Dr. V. Spallina - System simulation for integration of CO₂ capture technologies into steelworks and CCUS clusters
- 11:55-12:15 Dr. M. Saric - Methanol membrane reactor: modelling and experimental results
- 12:15-12:35 Dr. Adam Deacon - Realising the potential of MOFs through efficient scale-up
- 12:35-12:55 Dr. M. Etxeberria-Benavides - PBI based mixed matrix hollow fiber membranes for pre-combustion CO₂ capture

ORGANIZED BY



SPONSORED BY



WE
CAN DO
SO MUCH
TOGETHER

INTERNATIONAL WORKSHOP ON CO₂ CAPTURE AND UTILIZATION
TU/E - EINDHOVEN - 16-17 FEBRUARY 2021

Membrane development steps: from material to final product

Dr Oana David

FUNDACION TECNALIA RESEARCH & INNOVATION

is a private non profit research centre.



Main figures
in 2017

PEOPLE IN TECNALIA

1,445 STAFF

 **57 %**
MEN

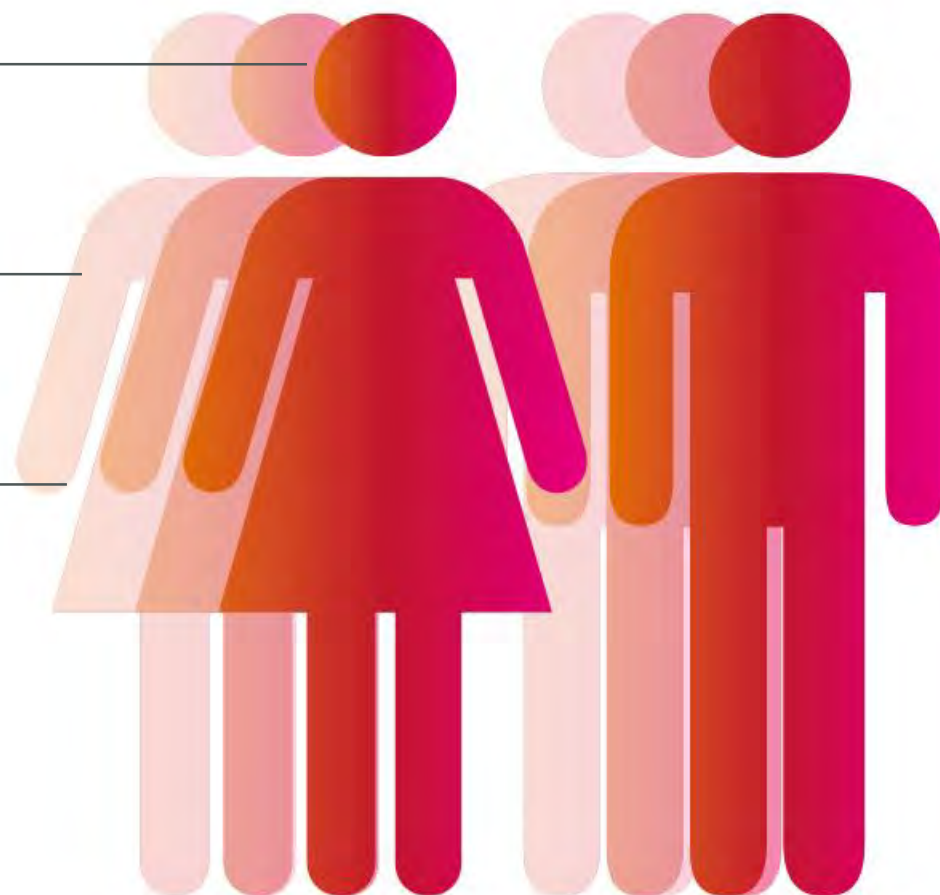
 **43 %**
WOMEN

 **27** DIFFERENT
NATIONALITIES

43 AVERAGE
AGE

249 NUMBER OF
PhDs

Figures on 31 December 2017.



BALANCE OF ACTIVITIES AND FUNDING

FIGURES ON
31 DECEMBER 2017

INCOME

104 MILLION
EUROS

19,7%

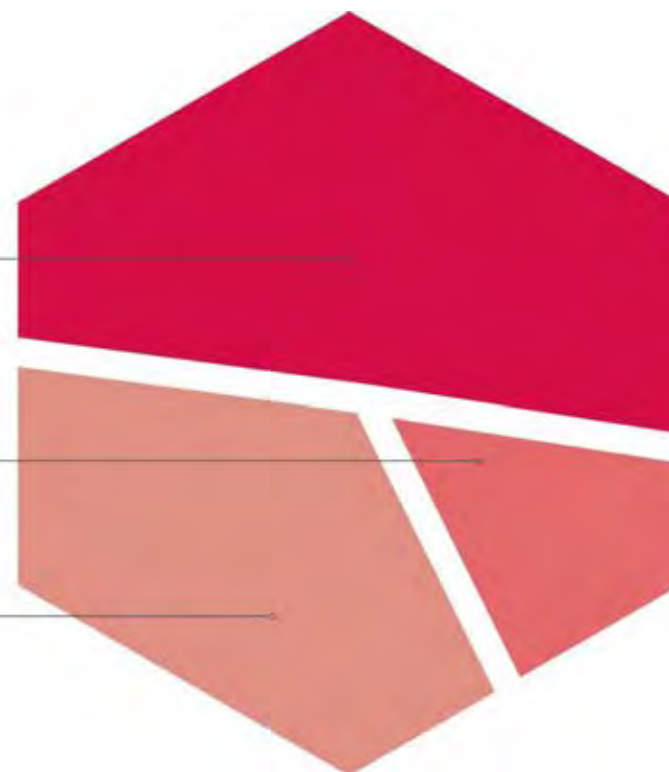
NON-
COMPETITIVE
PUBLIC
FUNDING

47,1%

PRIVATE
FINANCING
AND OTHERS

33,2%

COMPETITIVE
PUBLIC
FUNDING



FUNDACION TECNALIA RESEARCH & INNOVATION

is a private non profit research centre.

6 INTERCONNECTED BUSINESS DIVISIONS

+ EMERGING BUSINESSES

BUILDING TECHNOLOGIES



ENERGY AND ENVIRONMENT



ICT



INDUSTRY AND TRANSPORT



HEALTH



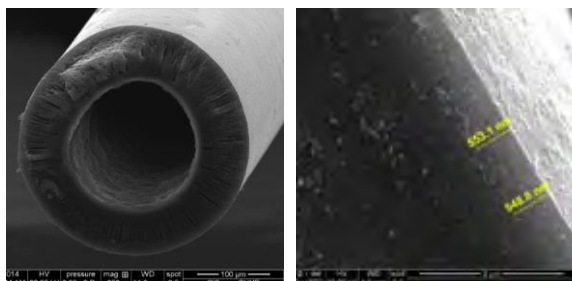
LAB SERVICES



Membrane Technology and Process Intensification research group at TECNALIA

Polymeric and Mixed matrix membranes

Combination of polymer matrix with inorganic fillers: MOFs, zeolites,...



Applications

- CO₂ Pre-combustion (H₂/CO₂)
- CO₂ Post-combustion (N₂/CO₂)
- Biogas upgrading (CO₂/CH₄)
- Natural gas upgrading (CO₂/CH₄)

Carbon molecular sieve

Pyrolyzed polymers. Unique pore structure



Applications

- CO₂ Pre-combustion (H₂/CO₂)
- Biogas upgrading (CO₂/CH₄)

Palladium membranes

Thin Pd supported membranes. High H₂ permeability & selectivity



Applications

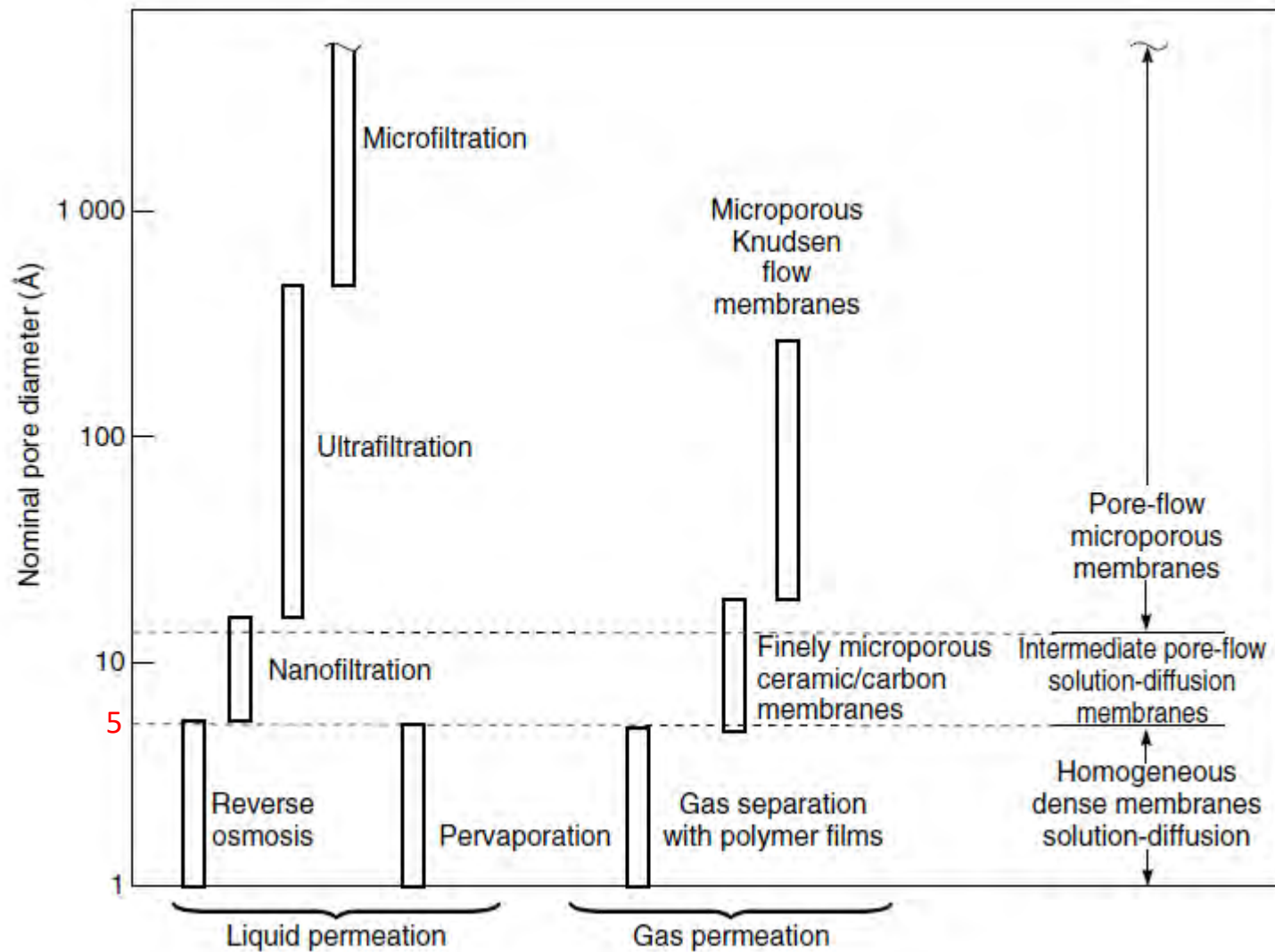
- CO₂ Pre-combustion (H₂/CO₂) & pure H₂ production

Membrane development steps: from material to final product

Outlook:



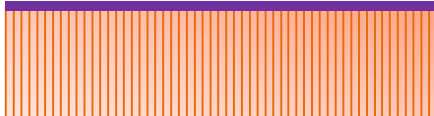



- ✓ Introduction to membrane processes
- ✓ Membrane structure and geometry for gas separation
- ✓ Membrane Development Strategy
- ✓ Applications and Tecnalia examples

Separation with membranes



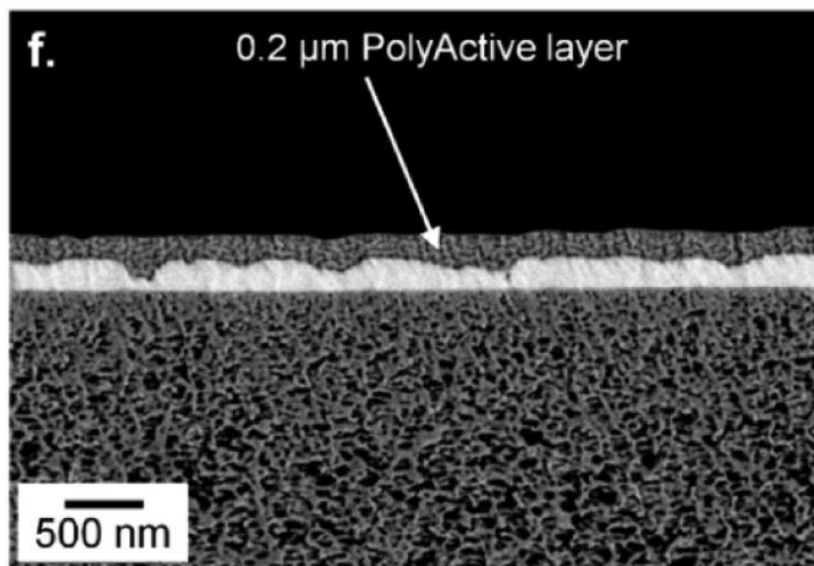
MEMBRANE STRUCTURE AND GEOMETRY

Commercial membranes

| Membrane structure | Homogeneous | Asymmetric | |
|---------------------|---|---|--|
| | | Monolithic | Composite |
| |  |  |  |
| Membrane processing | Solution film casting | Phase inversion $J_i = \frac{P_i \cdot \Delta p_i}{l}$ | Dip-coating Interfacial polymerisation |
| Geometry |  |  |  |

MEMBRANE STRUCTURE AND GEOMETRY

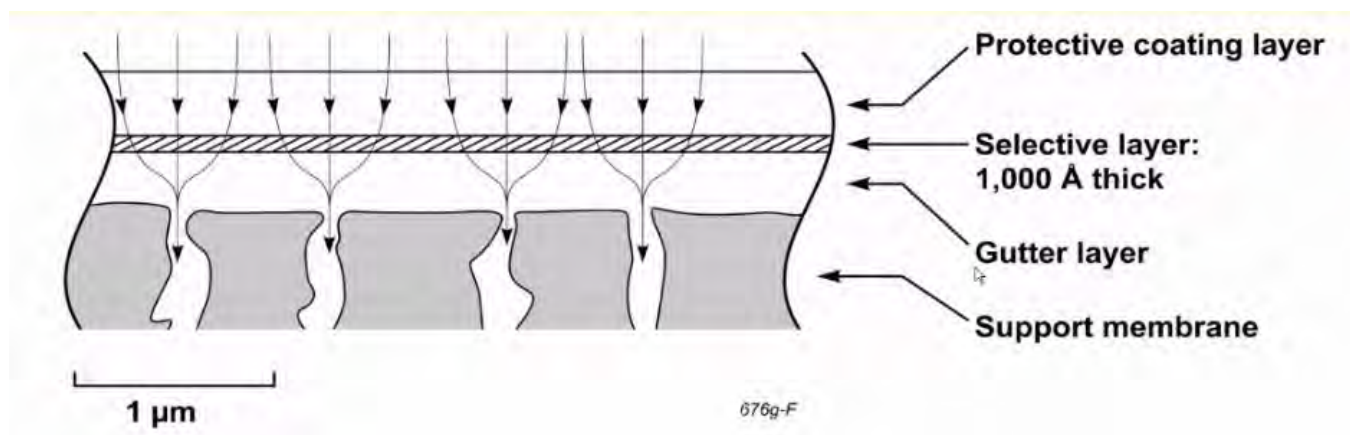
TFM: Thin film composite membrane



← PDMS

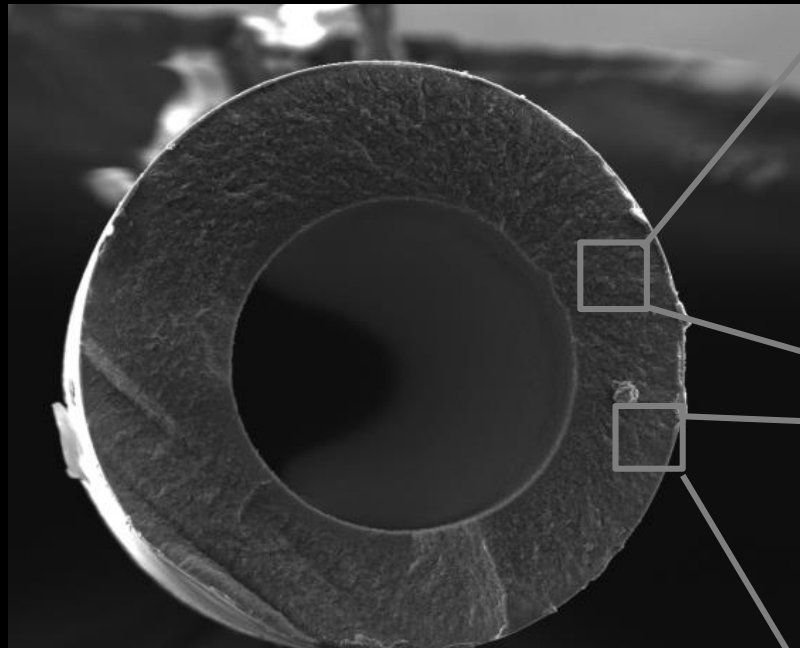
← PAN

ACS Appl. Mater. Interfaces 2018, 10, 26733–26744



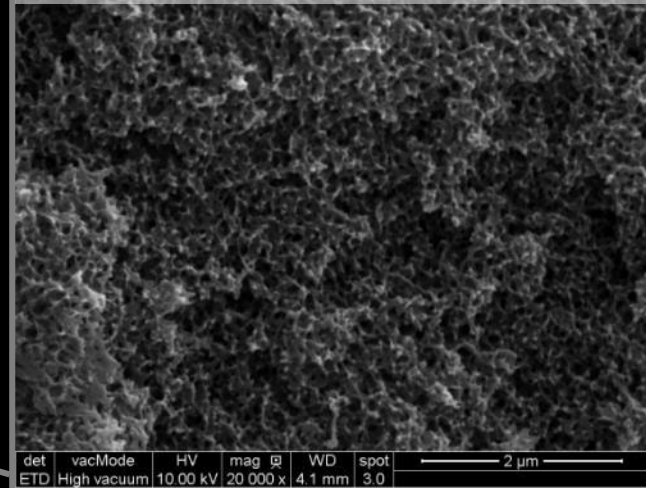
H. Lin et al. / Journal of Membrane Science 457 (2014) 149–161

Monolithic hollow fiber membrane

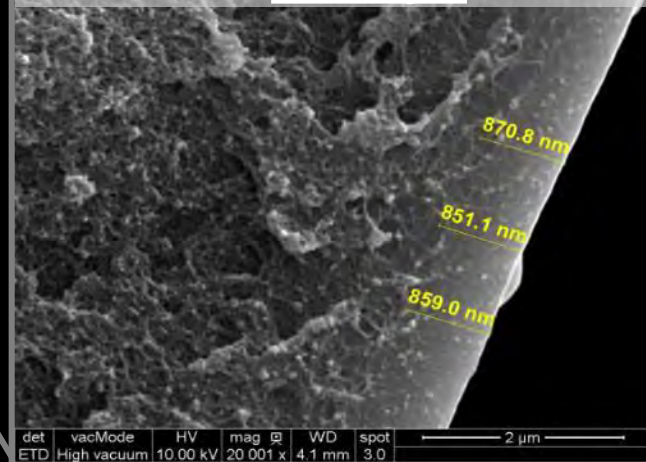


Asymmetric hollow fiber

Highly porous support



Very thin and dense separating skin layer

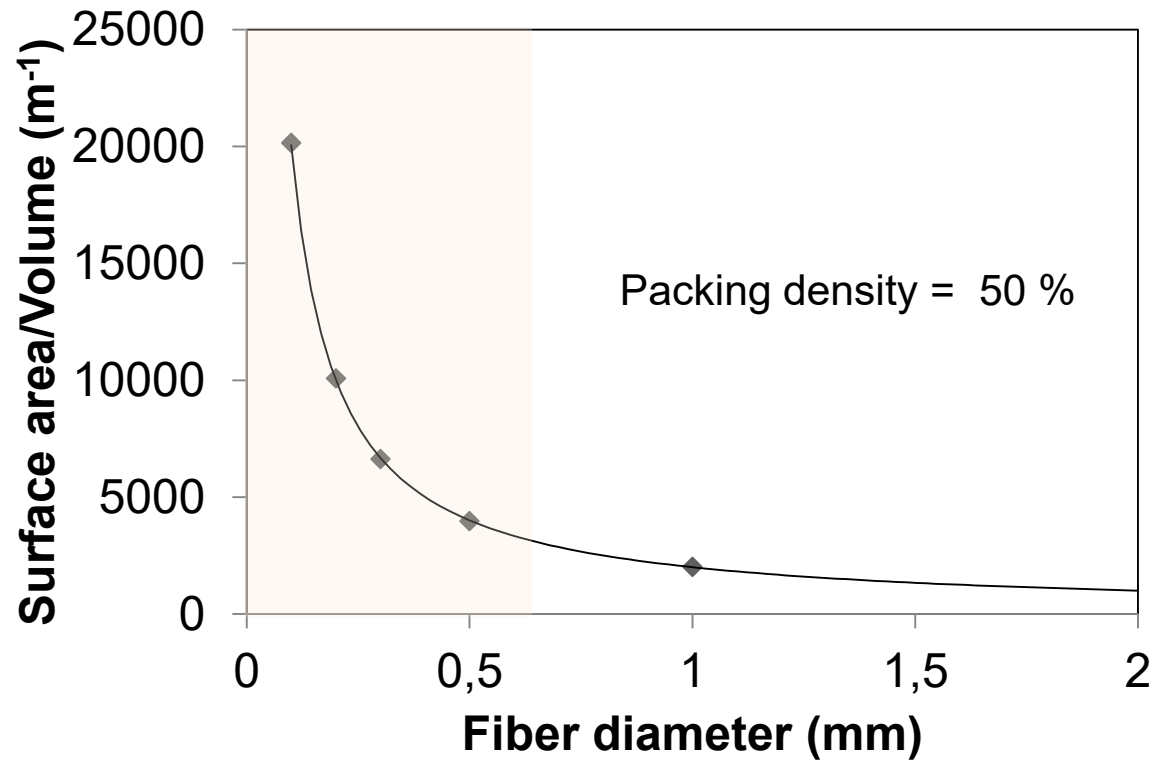


PRODUCTIVITY -

MEMBRANE GEOMETRY

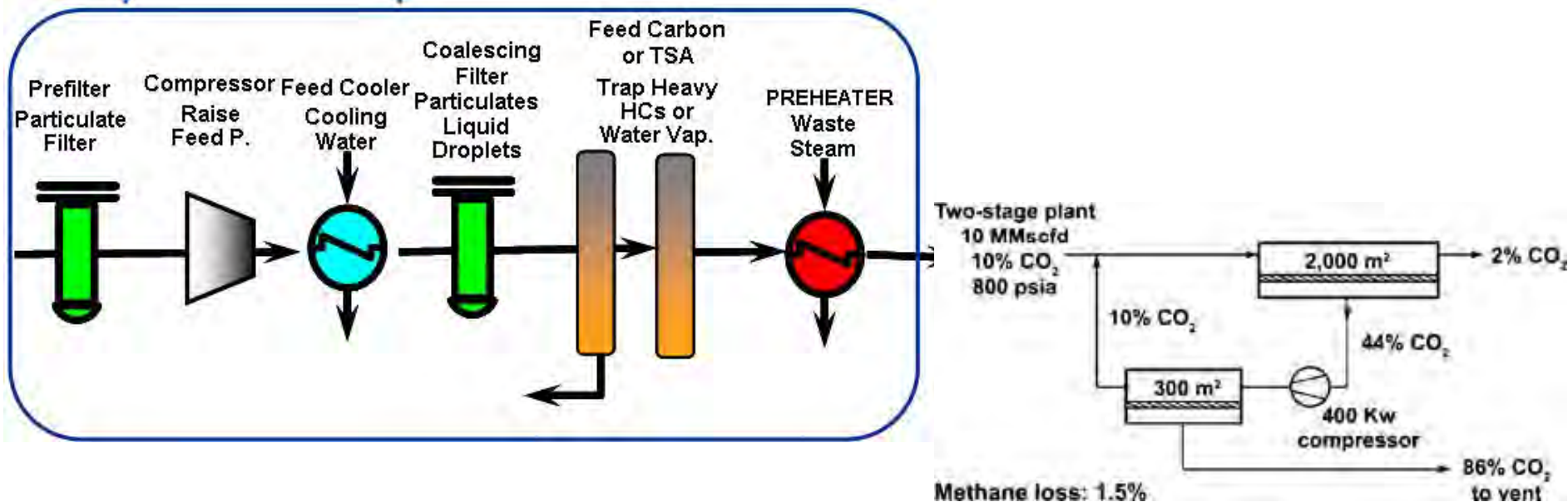


Perme



Process design and membrane system components

Natural gas treatment: CH₄/CO₂



Membrane Development Strategy

Process analysys and optimization



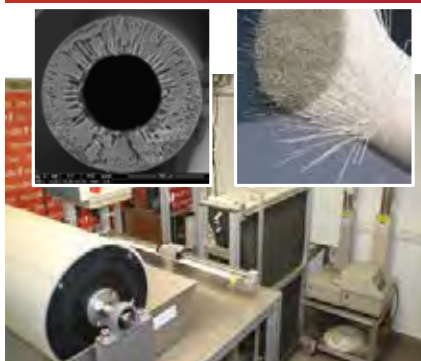
Analysis of the process (feed stream and desired performance) to propose the best performing possibilities.

Membrane development



Development/tuning up advanced membranes based on novel materials (Mixed Matrix, CMS or metallic membranes) to enhance the performance of the separation.

Membrane scale up and prototype construction



Production and integration into a prototype of different types of membranes.

Membrane characterization



Testing commercially available or internally developed membranes at different conditions that reproduce industrial requirements

Membrane Development Strategy

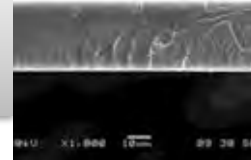
Defining target performance



Material development
and/or selection



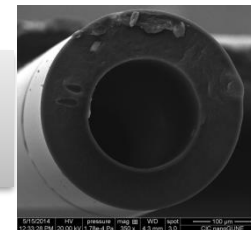
Dense film preparation and
characterization



*Intrinsic separation properties
Permeability and selectivity*



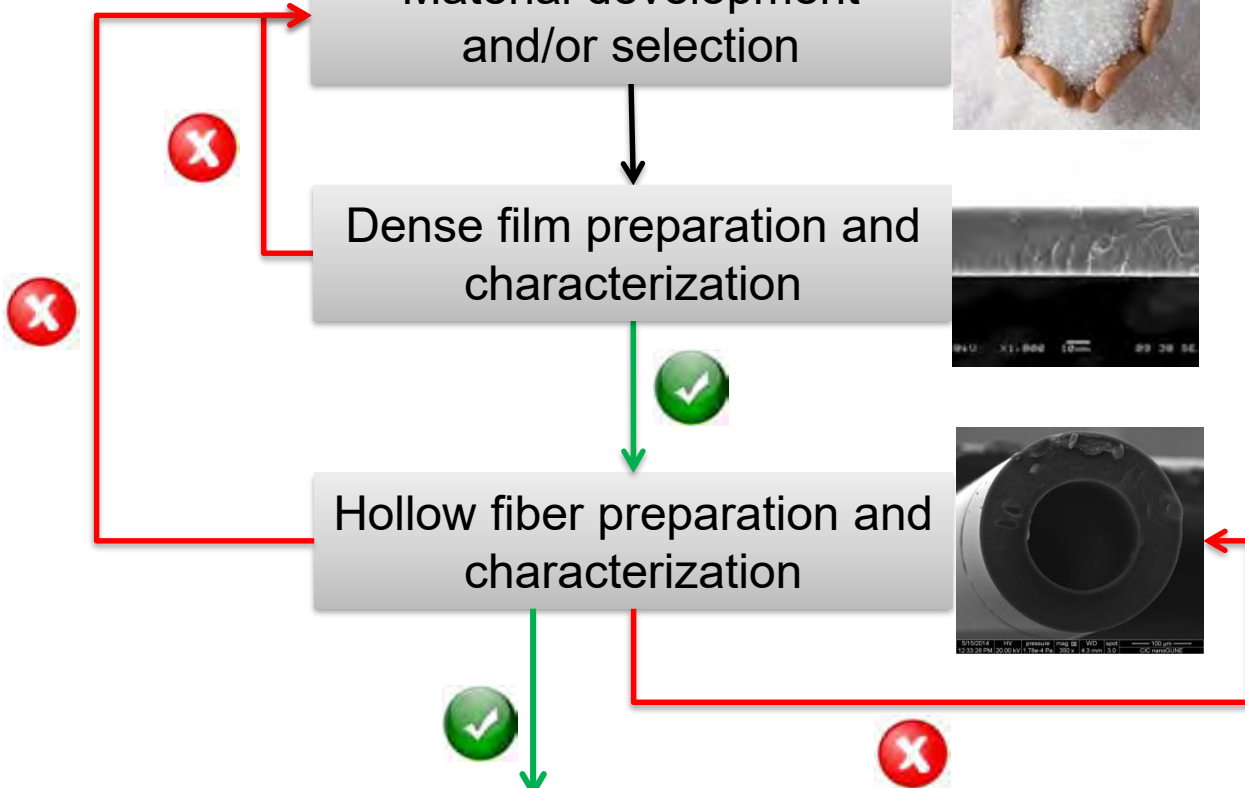
Hollow fiber preparation and
characterization



*Separation properties
Permeance and selectivity*



Possible to Scale-up, Prototype??



Post-combustion CO₂ capture

Industrial requirements

- 4-20% CO₂ ingas from power generator
 - Low/Atmospheric pressure
 - Vapour, O₂, SO_x, NO_x, NH₃, ...
 - High flows 40,000 Nm³/h
- To be competitive with amine or 90% CO₂ capture for installed prices not less than 50 €/m²

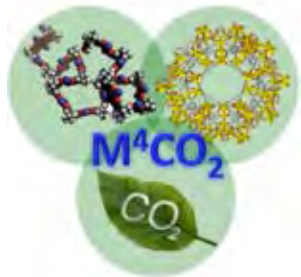
| Specifications | Value | Unit |
|---|--------|------------------|
| P _{CO2} | >2,250 | GPU |
| CO ₂ /N ₂ selectivity | >30 | --- |
| Temperature | 100 | °C |
| Design pressure | 7 | bar |
| Costs | < 100* | €/m ² |

*Target set by the BioCoMem project

[Haibo Zhai \(2019\)](#)

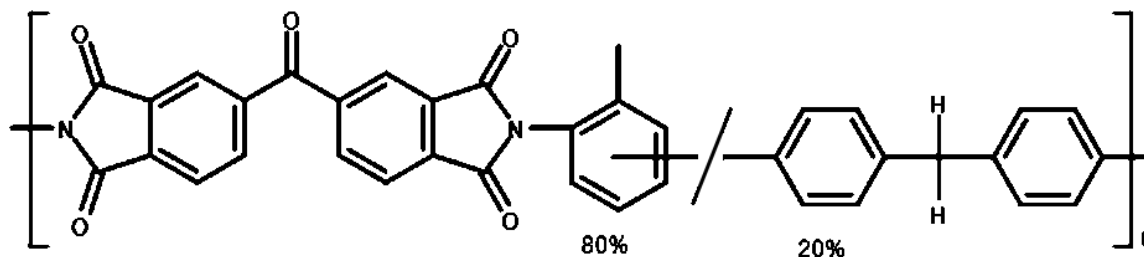
| Polymer | P _{CO₂} (Barrer) | Selectivity CO ₂ /N ₂ | Selectivity CO ₂ /CH ₄ | Test conditions | Ref. |
|------------------------------|---|--|---|----------------------------------|------|
| PEBAX 1657 (60PEO/PA6) | 79 | 52,7 | 16,8 | 30 °C | 1 |
| PEBAX 1074 (55PEO/PA12) | 110,67 | 51,4 | 11,09 | 25 °C | 2 |
| PEBAX 2533 (80PTMEO/PA12) | 149 | 15 | 7,28 | 25 °C | 3 |
| Polyactive | 202 | 44 | 15,2 | 35 °C | 4 |
| PE (Alathon 14) | 12,6 | 13 | - | - | 5 |
| 6FDA-DAM | 842,41 | 15,3 | 18 | T = 35°C/ p = 100PSI | 6 |
| PPO | 75,8 | 19,9 | 6,89 | T ^a : 30°C | 7 |
| Matrimid | 7 | 25 | 33,33 | T ^a : 35°C p: 3,5 bar | 8 |
| Cellulose Acetate | 6,3 | 30 | 30 | T ^a : 30°C p: nd | 7 |
| Polysulfone | 5,6 | 22,4 | 22,4 | T ^a : 30°C p: nd | 7 |
| Polietersulfone (Radel A) | 2,51 | 30,61 | 29,9 | T ^a : 35°C p: 10 atm | 9 |
| Polyeterimide (Ultem) | 1,32 | 28,09 | 37,71 | T ^a : 30°C p: nd | 7 |
| P84 | 0,99 | 40,20 | >40 | T ^a : 25°C | 10 |

1. JMS 467(2014)269–278
2. Chemical Engineering Research and Design 117 (2017) 177-189
3. Silicon 10, 1461–1467 (2018)
4. JMS 535 (2017) 350-356
5. Bixler, H. J.; Sweeting, O. J. In Science and Technology of Polymer Films; Sweeting, O. J., Ed.; Wiley-Interscience: New York, 1971; pp 1–130.
6. Polymer 54 (2013) 6226-6235
7. Abetz, V., et al Adv. Eng. Mater., 8 (2006) 328-358.
8. Polymer 49 (2008) 1594
9. JMS 277 (2006) 28-37
10. JMS 216 (2003) 195-205

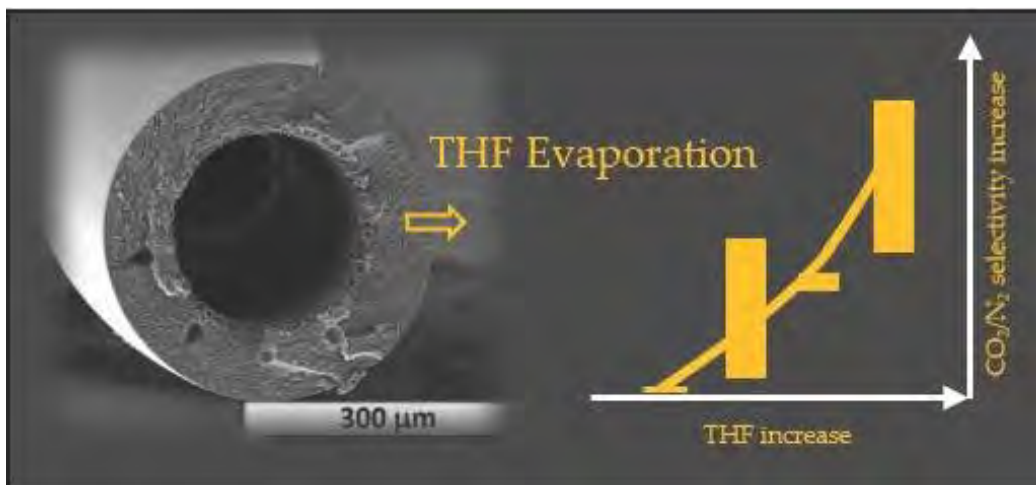


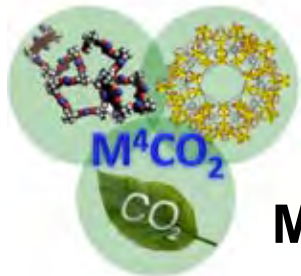
Post-combustion CO₂ capture

P84 Asymmetric hollow fiber membranes



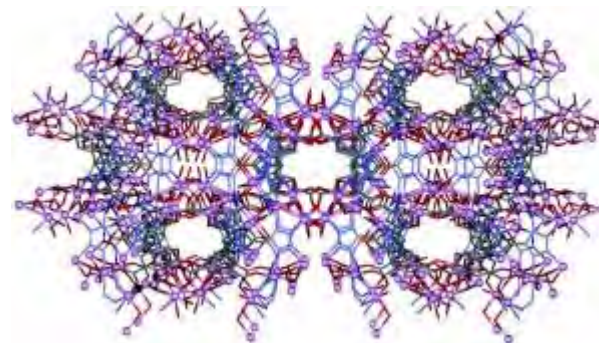
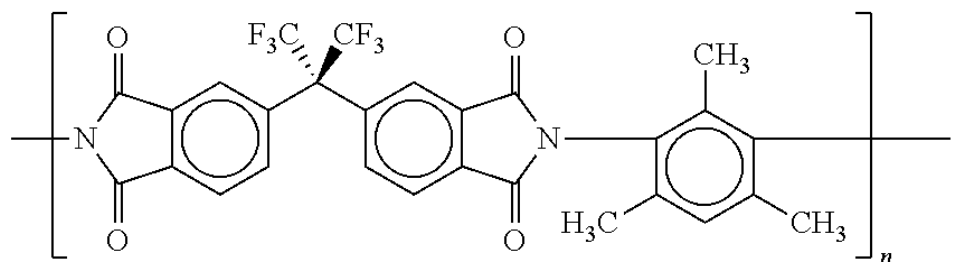
- highly thin (~56 nm) defect-free skin
- CO₂/N₂ selectivity of 40, and a CO₂ permeance of 23 GPU at 35 °C
- No post treatment necessary for post treatment
- Scaled up the process at 5000 m fiber with reproducible results





Post-combustion CO₂ capture

MMM flat sheet ZIF-94 Filler and 6FDA-DAM Polymer



Mixed Matrix Membranes

Filler (Molecular sieve)

+

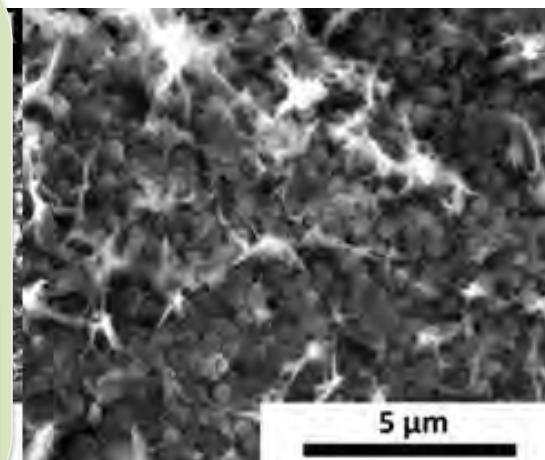
Matrix (Polymer)

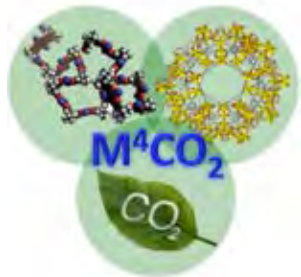


- Mechanical stability
- Easy processing



- Chemical stability
- Gas sieving properties

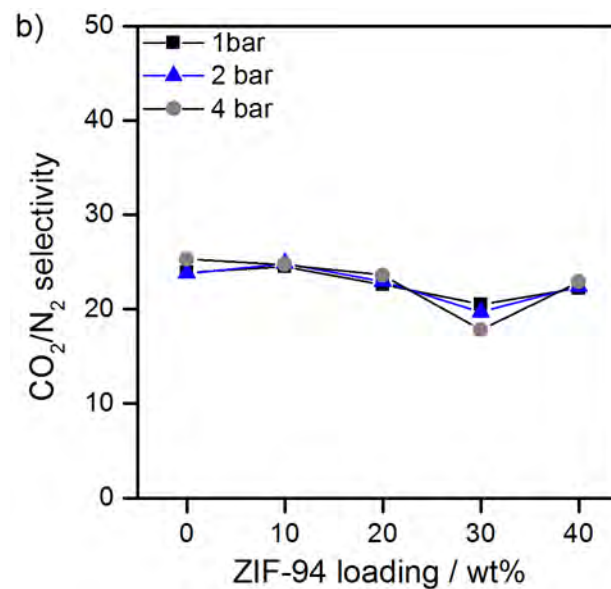
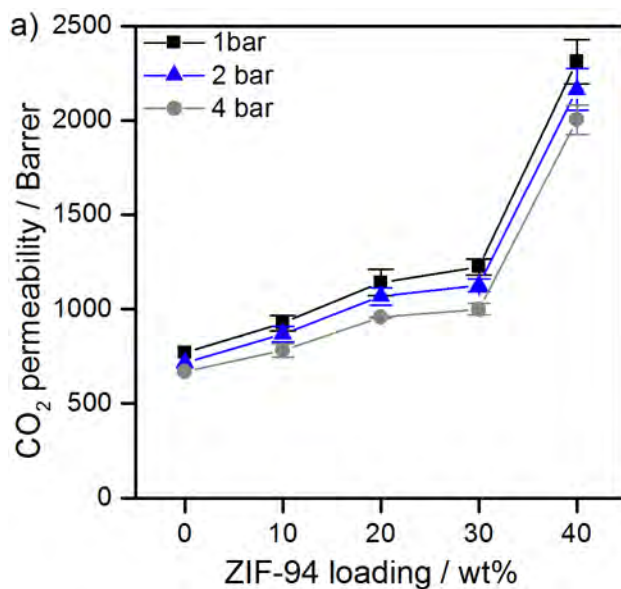




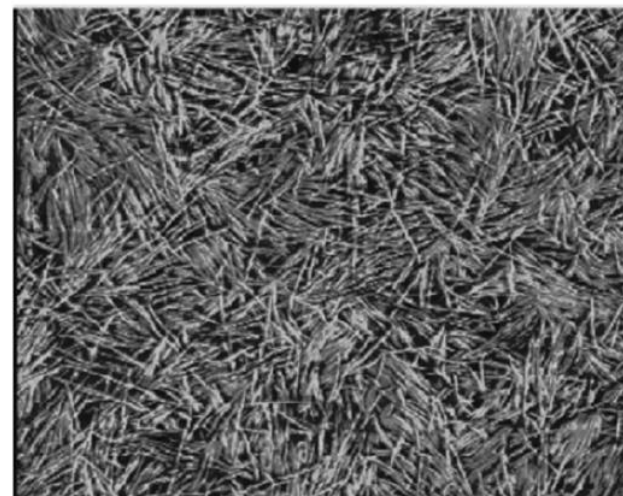
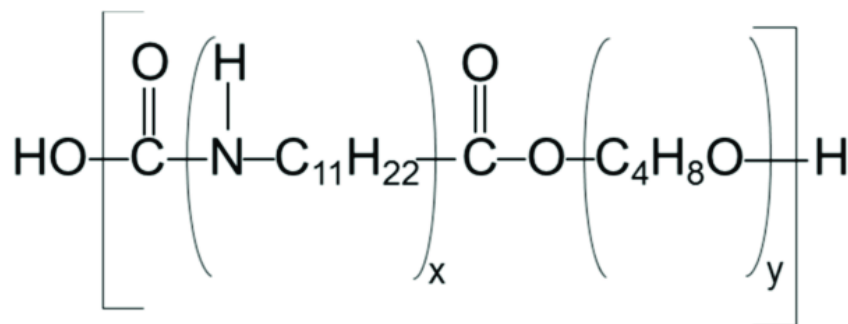
Post-combustion CO₂ capture

1MM flat sheet ZIF-94 Filler and 6FDA-DAM Polymer

Mixed Gas CO₂/N₂ = 15/85



Bio based PEBAX co-polymers



| Polymer | P _{CO₂} (Barrer) | Selectivity CO ₂ /N ₂ | Selectivity CO ₂ /CH ₄ | Test conditions | Ref. |
|------------------------------|---|--|---|-----------------|-----------------|
| PEBAX 1657 (60PEO/PA6) | 79 | 52,7 | 16,8 | 30 °C | 1 |
| PEBAX 1074 (55PEO/PA12) | 111 | 51,4 | 11,09 | 25 °C | 2 |
| PEBAX 2533 (80PTMEO/PA12) | 149 | 15 | 7,28 | 25 °C | 3 |
| Polyactive | 202 | 44 | 15,2 | 35 °C | 4 |
| Bio-PEBA | 320 | 46,6 | 14,2 | 35 °C | Biocomem |

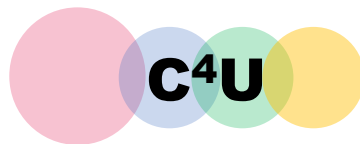
Thank you for your attention
Questions



Visit our blog:
<http://blogs.tecnaia.com/inspiring-blog/>



www.tecnaia.com



System simulation for integration of CO₂ capture technologies into steelworks and CCUS clusters

Vincenzo Spallina¹, Sergey Martynov², Richard Porter², Haroun Mahgerefteh²

¹Department of Chemical Engineering and Analytical Science, University of Manchester

²Department of Chemical Engineering, University College London

email: vincenzo.spallina@manchester.ac.uk

● ***International Workshop on CO₂ Capture and Utilization
16-17 February 2021***



Advanced Carbon Capture for Steel Industries Integrated in CCUS Clusters

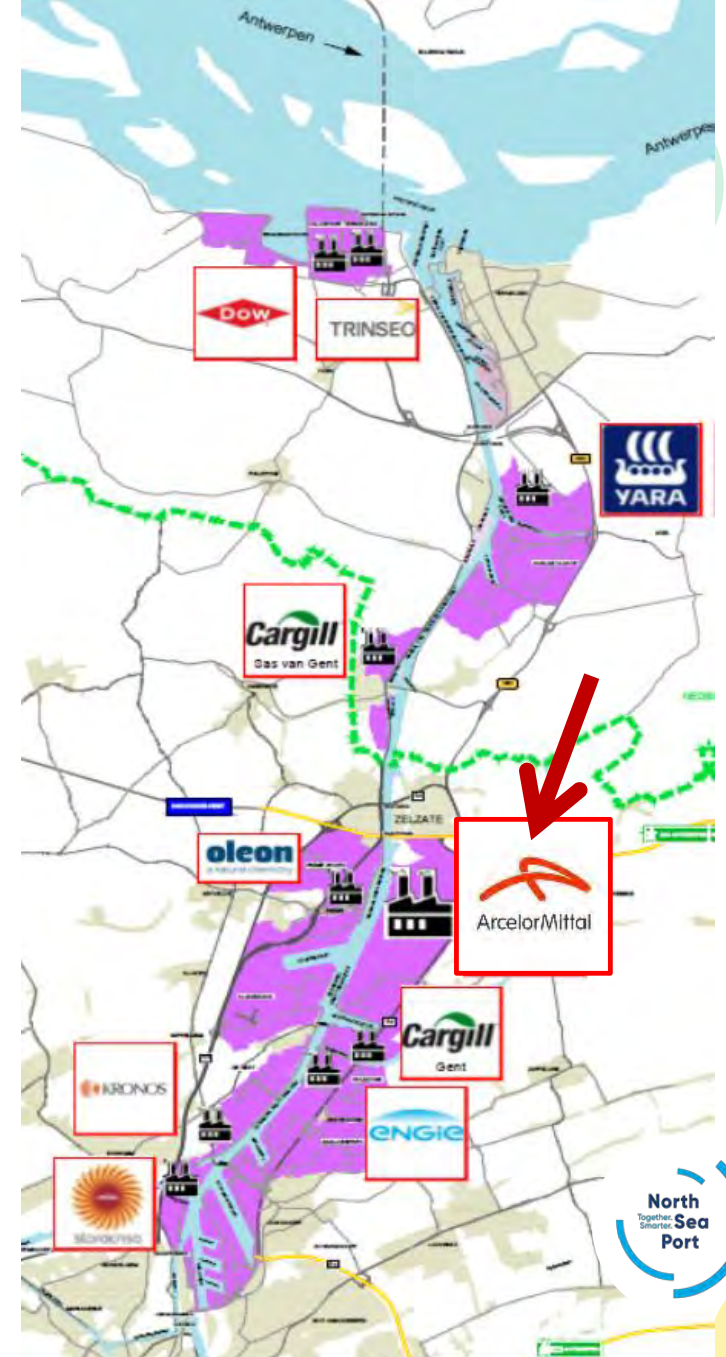
Start date: 1 April 2020
End date: 31 March 2024
Overall budget: € 13,845,496
Coordinator: Prof. Haroun Mahgerefteh, University College London



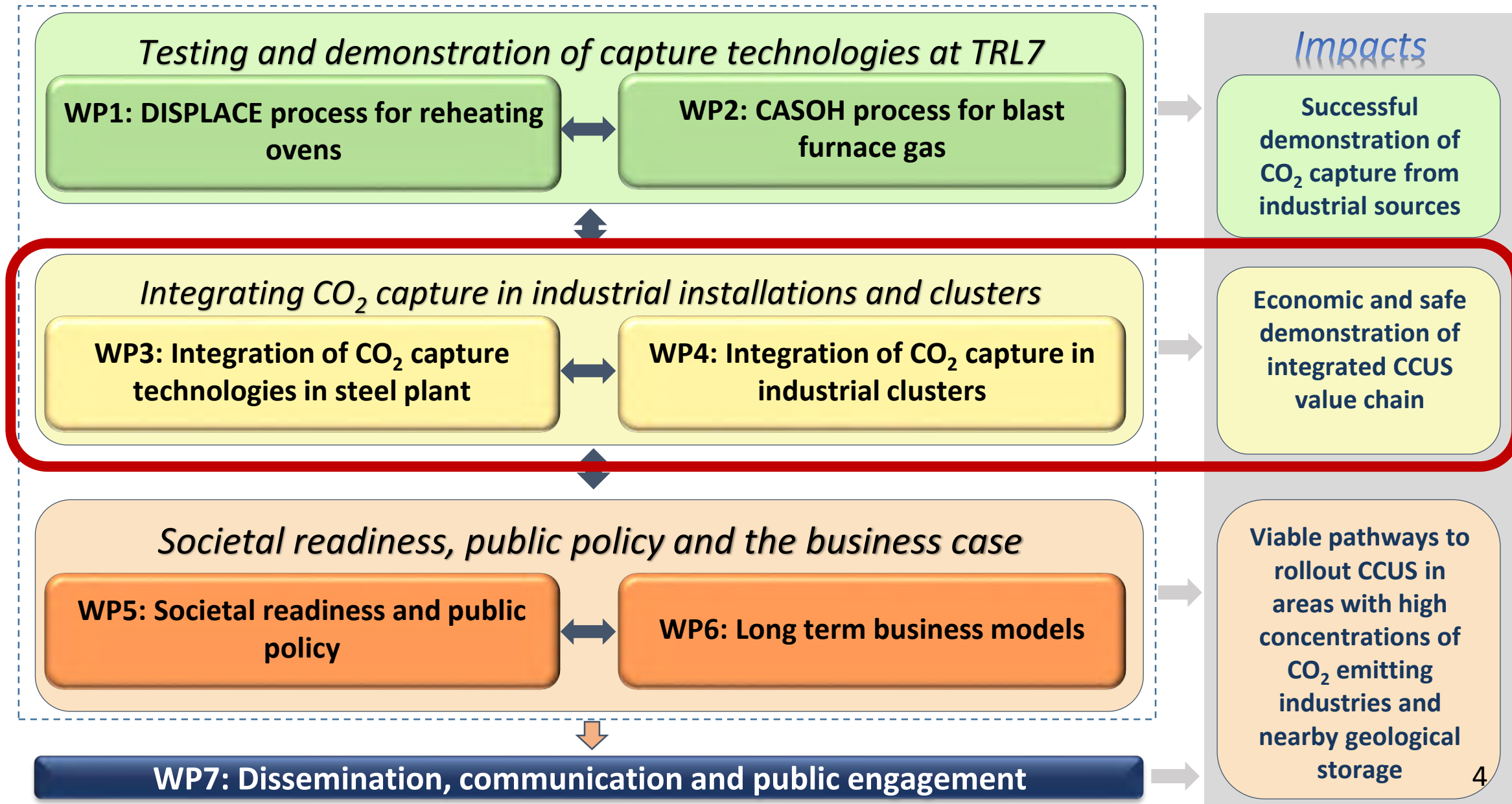
This project has received funding from the European Union's Horizon 2020 research and innovation programme under grant agreement No 884418

C⁴U: Headline Objectives

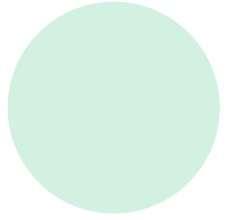
- Elevate two promising CO₂ solid based capture technologies from TRL5 to TRL7 & design for optimal integration in the steel industry
- Analyse the economic, environmental and business impacts of large scale process as part of the North Sea Port industrial cluster including CO₂ quality for the pipeline transportation & storage infrastructure
- Develop and test approaches with stakeholders and end-users to assess and advance societal readiness for CCUS in industrial clusters



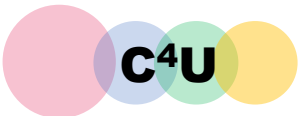
C⁴U PERT Diagram



Presentation overview



- C⁴U processes integrated in the steel mill
- The selection of the benchmark processes and their techno-economic performance
- The integration of the C⁴U in industrial clusters: challenge and opportunity
- Conclusions



WP 3 - Integration of CO₂ capture technologies in steel plant



POLITECNICO
MILANO 1863



ArcelorMittal



CSIC

CONSEJO SUPERIOR DE INVESTIGACIONES CIENTÍFICAS

MANCHESTER
1824

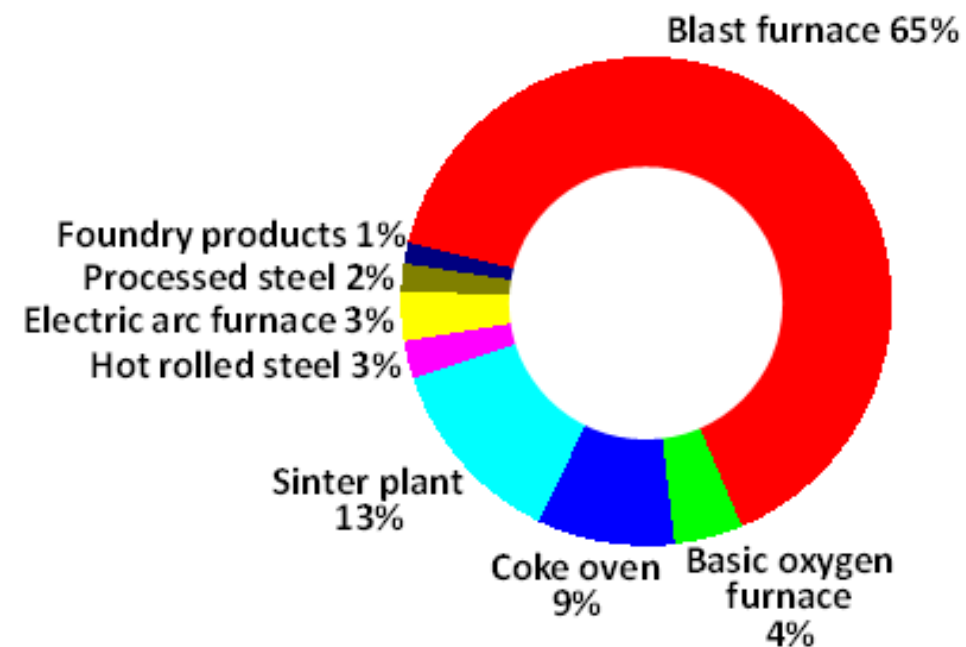
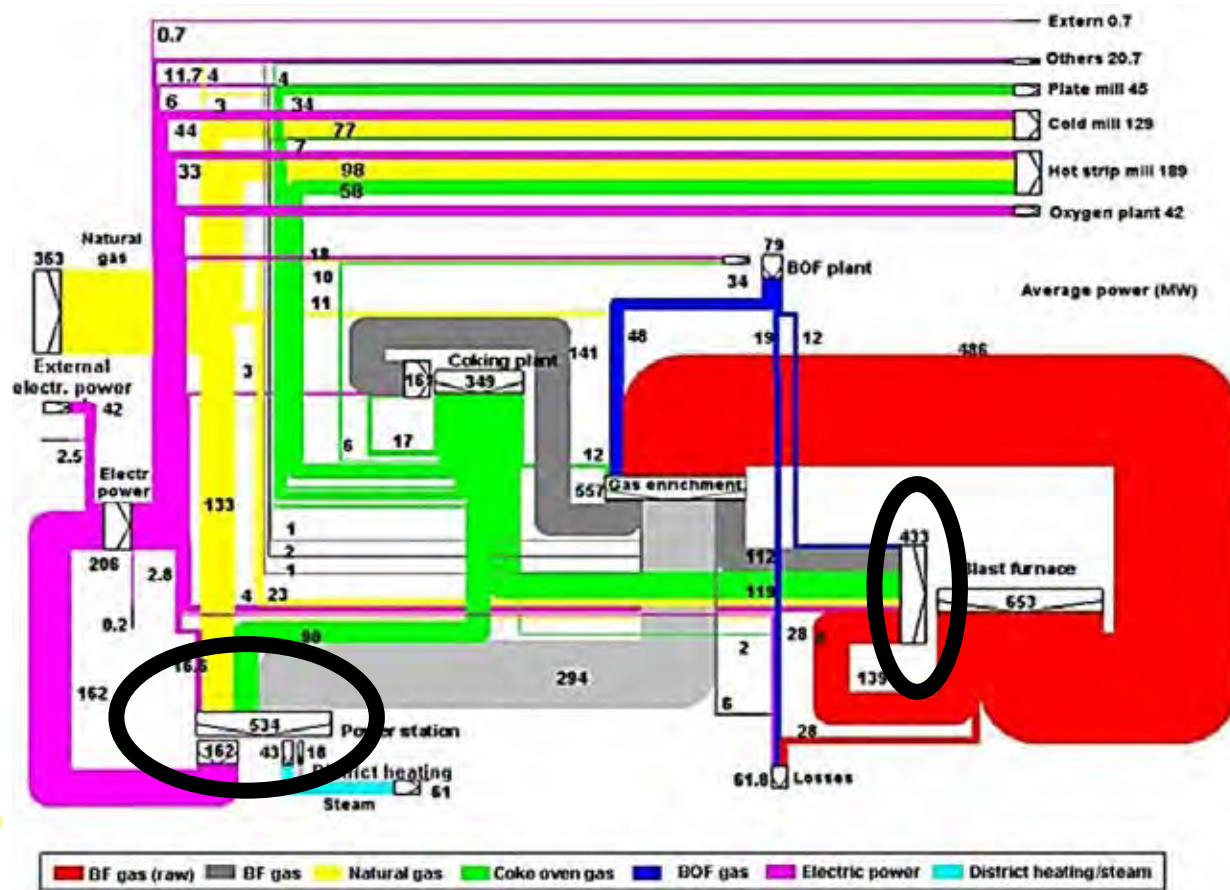
The University of Manchester

TNO innovation
for life

wood.

c4u

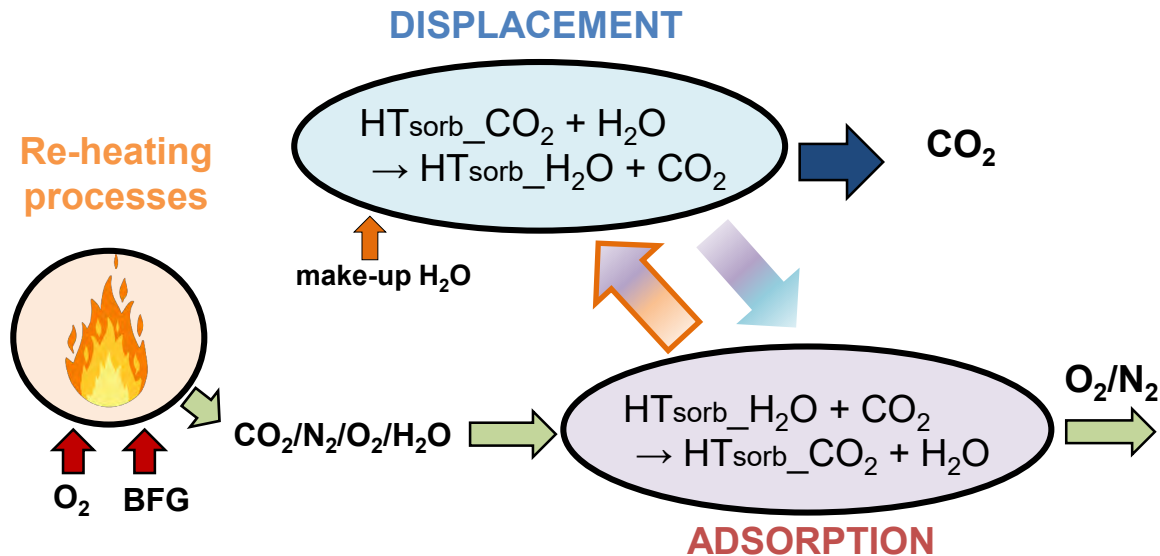
Integrated steelworks: a complex plant



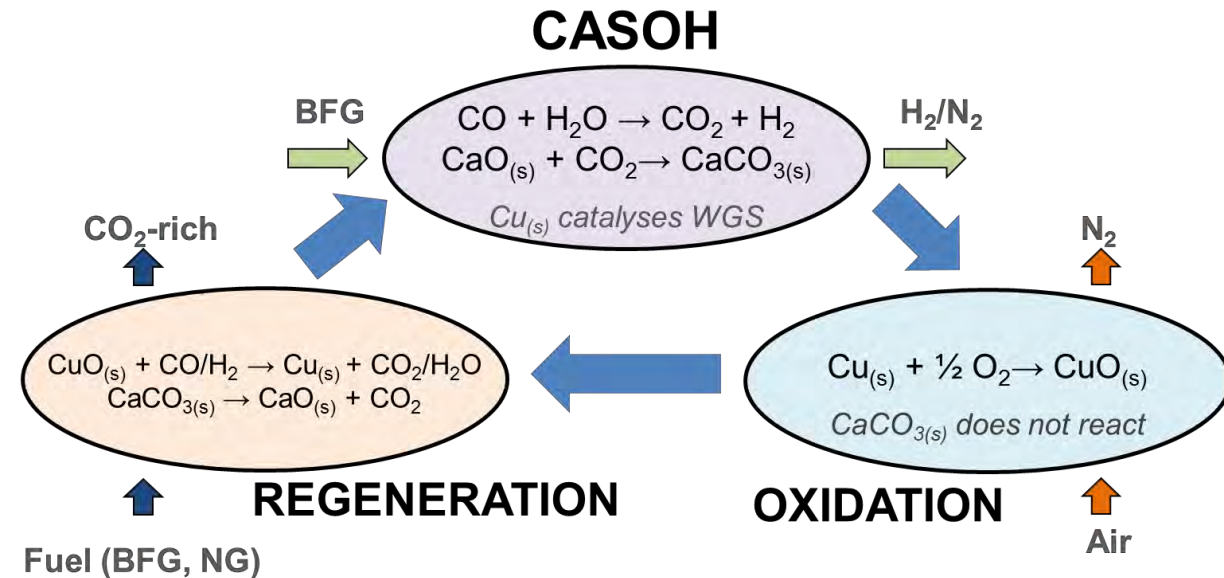
Breakdown of contribution to CO₂ emissions

C⁴U gas-solid technologies

DISPLACE



CASOH

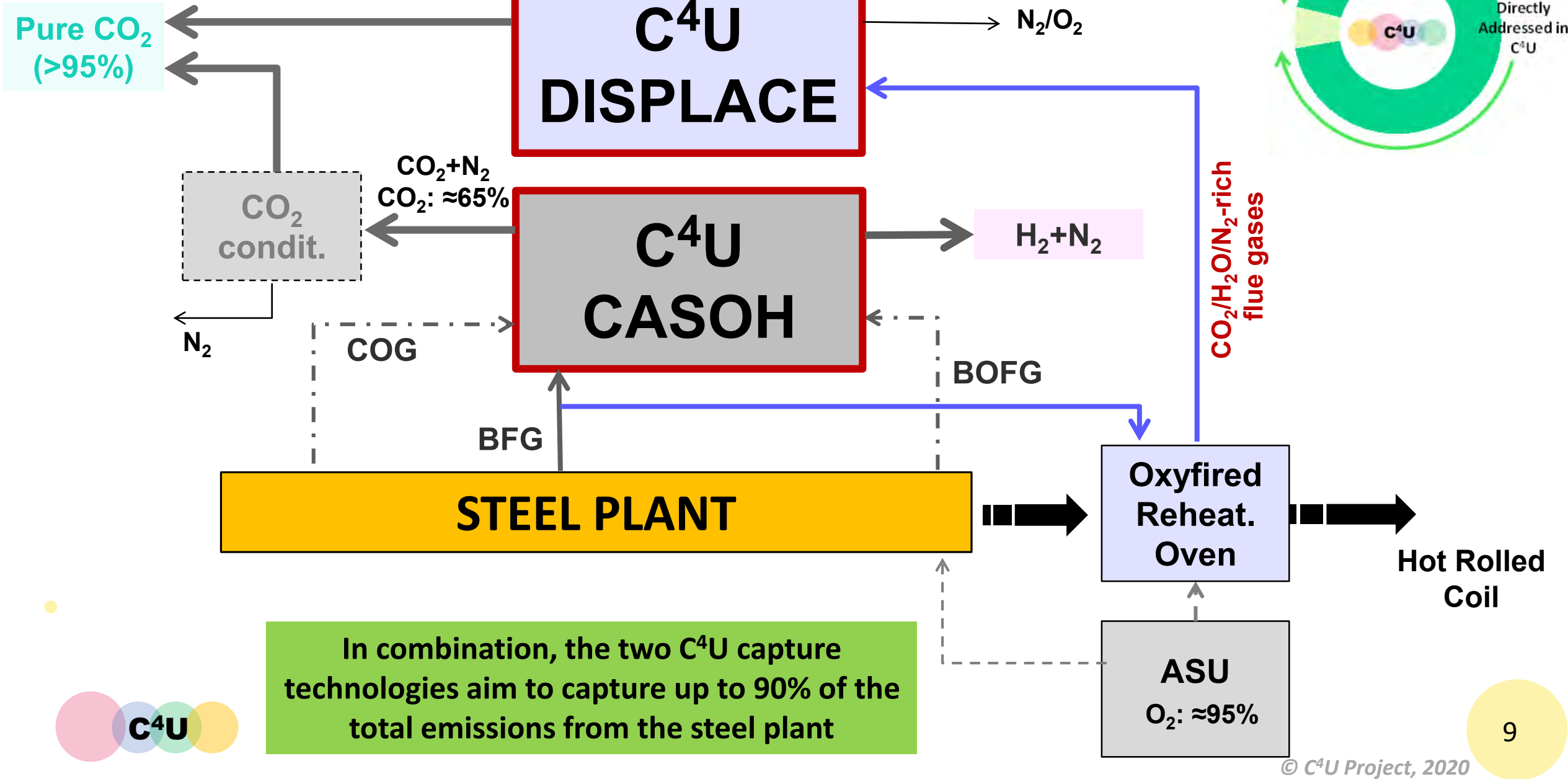


More details will be available tomorrow: **SESSION 3B** 12.45-13.05 (CET)

P. Cobden, C. Abanades - Pilot preparation for demonstration in the C⁴U project

© C⁴U Project, 2020

WP3: C⁴U CONCEPT AND INTEGRATION



WP3: METHODOLOGY

Task 3.1

- Methodology for the techno-economic assessment
- Reference case definition
- CO₂ capture process modelling (process design)

Task 3.2

- Parametric performance of the CO₂ capture technologies, both the reference and the C⁴U ones
- SPECCA and Cost of CO₂ avoided

Task 3.3

- Process design package for a full scale
- Cost estimation of the capture processes

Task 3.4

- The optimal integration of the C⁴U technologies in the integrated steel plant
- Determine the energy (SPECCA) and costs (Cost of CO₂ avoided) for the C⁴U technologies at defined CO₂ avoidance rates and CO₂ purities.

WP3: METHODOLOGY

Task 3.1

- Methodology for the techno-economic assessment
- Reference case definition
- CO₂ capture process modelling (process design)

Task 3.2

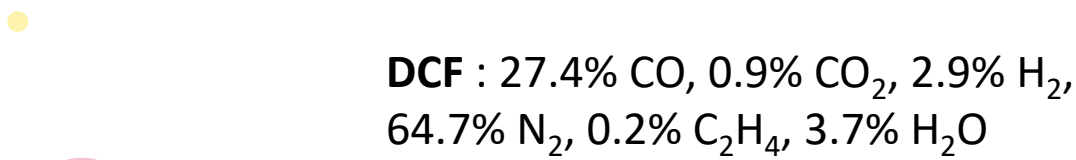
- Parametric performance of the CO₂ capture technologies, both the reference and the C⁴U ones
- SPECCA and Cost of CO₂ avoided

Task 3.3

- Process design package for a full scale
- Cost estimation of the capture processes

Task 3.4


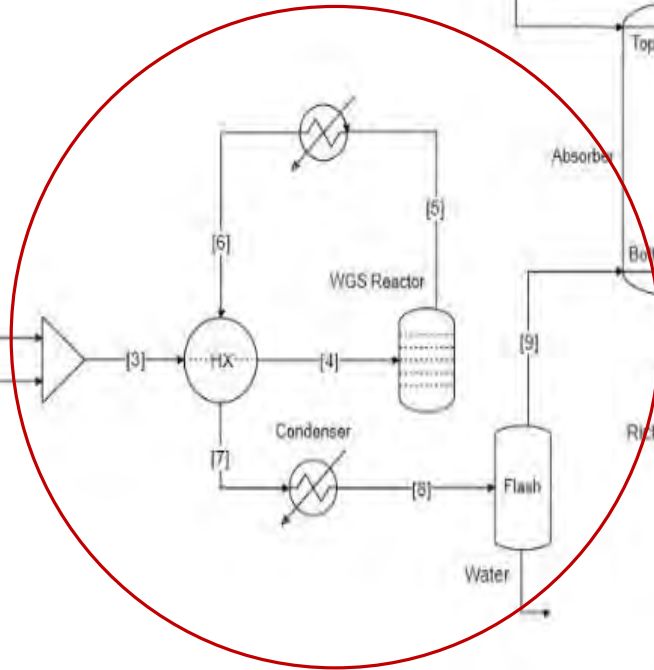
- The optimal integration of the C⁴U technologies in the integrated steel plant
- Determine the energy (SPECCA) and costs (Cost of CO₂ avoided) for the C⁴U technologies at defined CO₂ avoidance rates and CO₂ purities.



BFG flow rate: 125.1 kg/s

BFG composition: 22.7% CO, 21.2% CO₂, 2.4% H₂, 53.5% N₂, 0.2% C₂H₄

12



| Parameter | Value |
|--|----------------|
| MDEA CO ₂ absorption process | Same as before |
| HT WGS reactor | |
| Steam-to-CO ratio | 1.5 |
| Inlet Pressure (bar _a) | 2.9 |
| Inlet temperature (°C) | 300 |
| CO conversion (calculated at the equilibrium) | 76.3% |

METHODOLOGY: MAIN INDEXES

CO₂ capture rate of the technology

$$CCR[\%] = 1 - \frac{(\dot{N}_{CO_2} + \dot{N}_{CO} + \sum \zeta_c \cdot \dot{N}_c)_{out}}{(\dot{N}_{CO_2} + \dot{N}_{CO} + \sum \zeta_c \cdot \dot{N}_c)_{in}}$$

Specific Primary Energy Consumption for CO₂ Avoided

$$SPECCEA \left[\frac{MJ_{LHV}}{kg_{CO_2}} \right] = \frac{\left(\frac{1}{\eta_{capture}} - \frac{1}{\eta_{no,capt}} \right)}{E_{CO_2,no\ capt} - E_{CO_2,capture}}$$

Levelized Cost of Decarbonized Fuel

$$LCODF \left[\frac{\text{€}}{GJ} \right] = \frac{TAC \left[\frac{M\text{€}}{y} \right]}{\dot{m}_{DCF} \times LHV_{DCF} \times h/y} \times 1000$$

CO₂ avoidance cost

$$CCA \left[\frac{\text{€}}{t_{CO_2}} \right] = \frac{LCODF_{capture} - LCODF_{ref}}{E_{CO_2,ref} - E_{CO_2,capture}}$$

Additional cost of HRC for decarbonised steel mill

$$\Delta C_{HRC} \left[\frac{\text{€}}{t_{HRC}} \right] = \frac{TAC_{capture} + \Delta C_{el,capture} - TAC_{no\ capt}}{\dot{m}_{HRC}}$$

PERFORMANCE COMPARISON – TECHNO-ECONOMICS

| | Unit | no capture | Base case | Enhanced |
|---|---|------------|-----------|----------|
| Steel mill size | Mt _{HRC} /y | 3.16 | 3.16 | 3.16 |
| Carbon Capture Rate | [%] | | 46% | 83% |
| Cold gas efficiency | [%] | 100.0% | 100.0% | 90.5% |
| Overall energy efficiency | [%] | 100.0% | 81.8% | 56.7% |
| CO ₂ specific emissions | [kg _{CO2} /GJ _{LHV}] | 267.1 | 153.38 | 51.19 |
| CO ₂ capture avoidance | [%] | | 42.6% | 80.8% |
| ΔCO ₂ specific emissions ^{a)} | [kg _{CO2} /t _{HRC}] | 711.9 | 383.56 | 120.28 |
| SPECCA | [MJ _{LHV} /kg _{CO2}] | | 1.96 | 3.54 |

| | Unit | no capture | Base case | Enhanced |
|--------------------------------|-----------------------|------------|-----------|----------|
| LCODF | [€/GJ] | 5.20 | 9.73 | 14.78 |
| Δcost of HRC | [€/t _{HRC}] | | 11.99 | 21.65 |
| CO ₂ avoidance cost | [€/t _{CO2}] | | 39.84 | 49.38 |

WP4 - Integration of CO₂ Capture in Industrial Clusters



WP4: OBJECTIVES

Cluster 3 industrial port areas North Sea Port, Port of Antwerp and Port of Rotterdam responsible of 1/3 of CO₂ emissions from Benelux, approx. 60 Mt/a

Define common CO₂ transportation infrastructure for geological storage up to 10 Mt CO₂/a in the depleted gas fields (P18 fields)

Perform the whole economic, safe and environmental LCA of the integrated industrial cluster of the North Sea Port area.



WP4 - INTEGRATION OF CO₂ CAPTURE IN INDUSTRIAL CLUSTERS

Task 4.1 **Transport, utilisation and storage safety and operability**

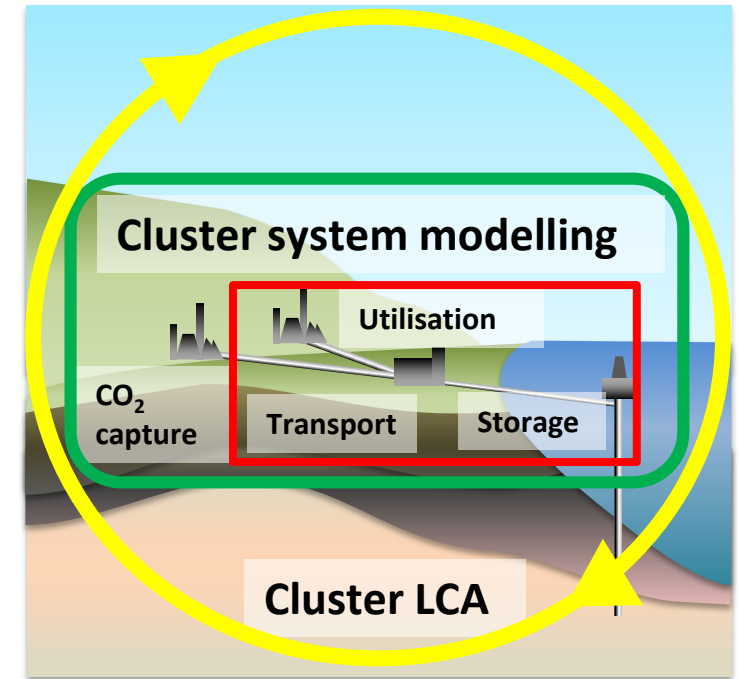
impacts Experimental and computational studies to evaluate the impacts of impurities in the CO₂ streams captured from steel plants, on the CO₂ utilisation, transport and storage

Task 4.2 **CCUS cluster whole-system modelling and operational logistics**

techno-economic evaluation to assess energy and cost penalties as a function of the CO₂ purity in the North Sea Port cluster for 2030 and 2050 decarbonisation scenarios.

Task 4.3 **Life Cycle Assessment (LCA) of the North Sea Port CCS cluster**

LCA assessment of the environmental impact of the North Sea Port CCS cluster.



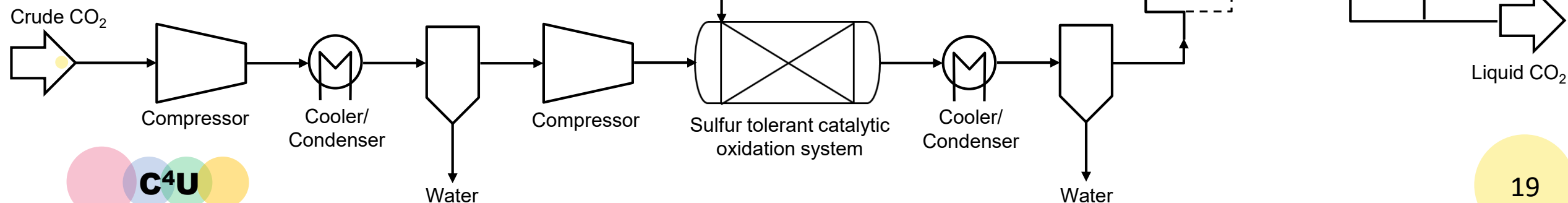
WP4: CO₂ purification challenge

European CO₂ quality specifications; e.g. Northern Lights¹

| Component | Concentration ppm (mole) | |
|---|--------------------------|--|
| Water, H ₂ O | ≤ 30 | Required to avoid formation of hydrates (blockage) and free water (corrosion) in the pressure vessels and process systems used for interim storage and transportation. |
| Oxygen, O ₂ | ≤ 10 | Required to avoid formation of corrosive species in the lower well completion where the CO ₂ mixes with reservoir brine containing chlorides. |
| Sulphur oxides, SO _x | ≤ 10 | Required to avoid accelerated corrosion in presence of water. Value set conservatively to allow wider range of materials. |
| Nitric oxide/ Nitrogen dioxide, NO _x | ≤ 10 | Required to avoid accelerated corrosion in presence of water. Value set conservatively to allow wider range of materials. |
| Hydrogen sulphide, H ₂ S | ≤ 9 | Toxic to personnel in case of accidental release. |
| Carbon monoxide, CO | ≤ 100 | Toxic to personnel in case of accidental release. |
| Amine | ≤ 10 | May react with and degrade several non-metallic materials |
| Ammonia, NH ₃ | ≤ 10 | Effects unknown |
| Hydrogen, H ₂ | ≤ 50 | May cause embrittlement of metals. |
| Formaldehyde | ≤ 20 | May react with oxygen to form formic acid. Other effects are unknown |
| Acetaldehyde | ≤ 20 | May react with oxygen to form acetic acid. Other effects are unknown |
| Mercury, Hg | ≤ 0.03 | Toxic to personnel entering vessels, replacing filters, etc. May cause embrittlement of metals. |
| Cadmium, Cd Thallium, Tl | ≤ 0.03 (sum) | Toxic to personnel entering vessels, replacing filters, etc. May cause metal embrittlement of metals. |

Challenging limits for iron & steel CCS

- Example potential solution: catalytic oxidation and separation of CO₂ impurities²
- Configurations and costs require assessment



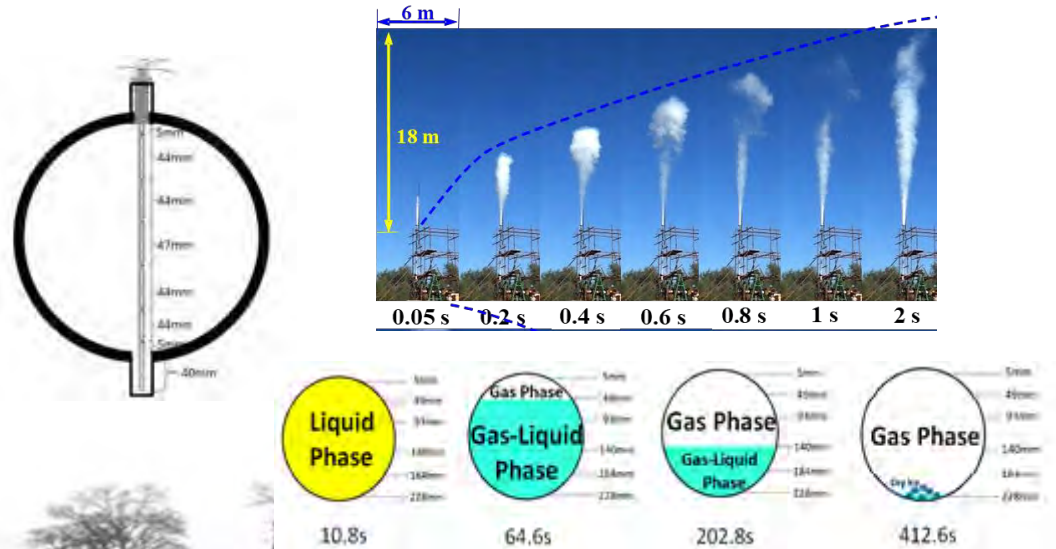
¹ Norwegian CCS Demonstration Project Norcem FEED, <https://ccsnorway.com/>

² Praxair. EP0952111A1. CO₂ purification system, 1999.

PIPELINE DECOMPRESSION EXPERIMENTS

OBJECTIVES

This task involves performing controlled pipeline decompression tests to assess the risk of solid CO₂ formation and transition to two-phase flow



Medium-scale test pipeline 40 m long, 2" i.d. (INERIS)

Large-scale test pipeline 256 m long, 233 mm i.d. (DUT)

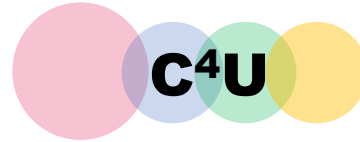
CONCLUSIONS

The C⁴U project will assess two advanced CO₂ capture technologies with respect to the solvent-based process which currently costs 50 €/tonCO₂ with a maximum capture efficiency of 83%

The sensitivity analysis at large scale on C⁴U technologies will include feedstock quality and CO₂ quality uses interlinking 2 WPs

The study will focus specifically on 3 industrial port areas North Sea Port, Antwerp and Rotterdam responsible of 1/3 of CO₂ emissions from Benelux, approx. 60 Mt/a

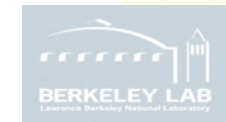
- Perform the whole economic, safe and environmental LCA of the integrated industrial cluster of the North Sea Port area



Advanced Carbon Capture for Steel Industries Integrated in CCUS Clusters

THANK YOU

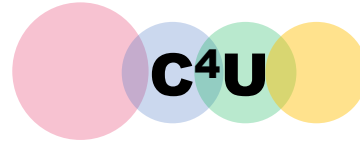
Questions ?



The contents of this presentation are the responsibility of University of Manchester & University College London and do not necessarily reflect the opinion of the European Union.



This project has received funding from the European Union's Horizon 2020 research and innovation programme under grant agreement No 884418



Advanced Carbon Capture for Steel Industries Integrated in CCUS Clusters

Supplementary slides

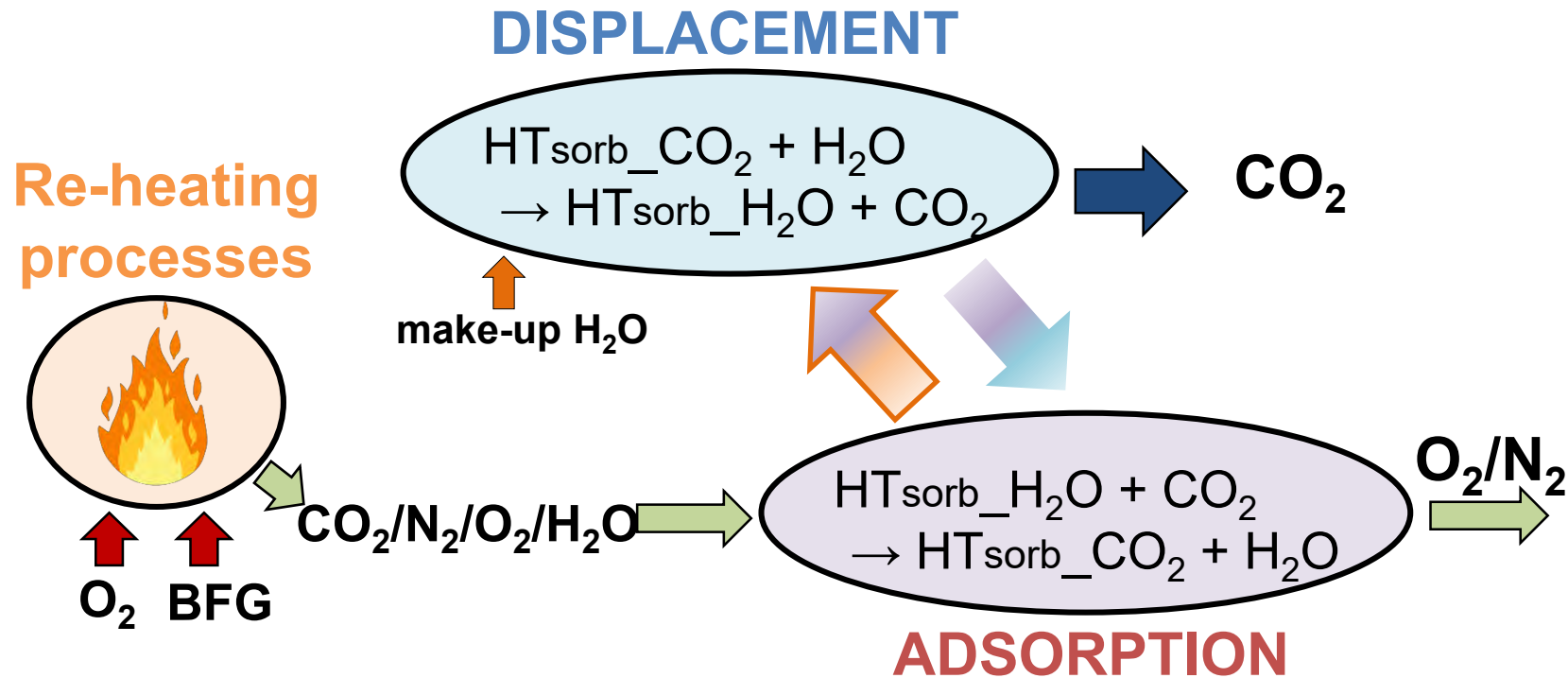


The contents of this presentation are the responsibility of University of Manchester & University College London and do not necessarily reflect the opinion of the European Union.



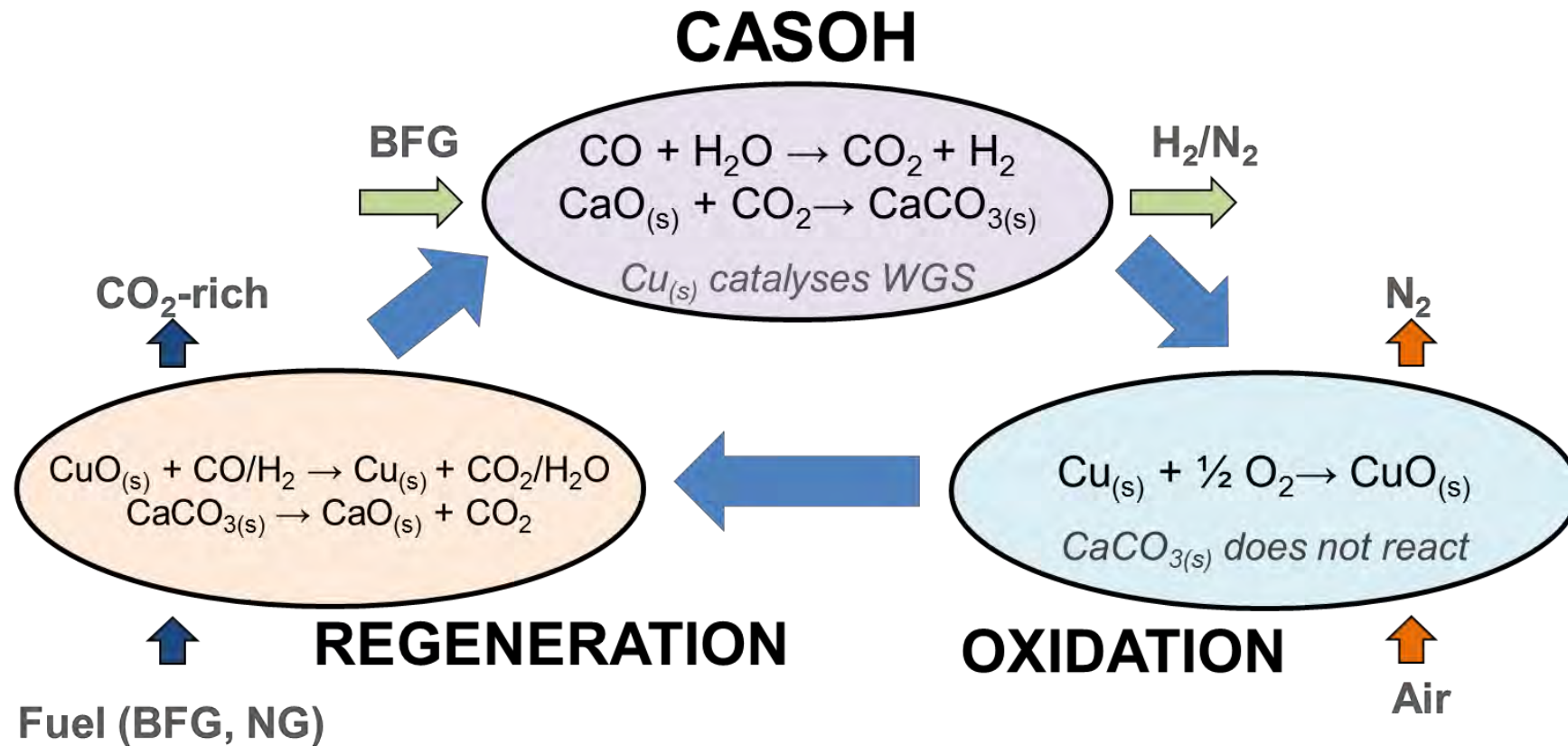
This project has received funding from the European Union's Horizon 2020 research and innovation programme under grant agreement No 884418

DISPLACE: High temperature sorption-displacement process using hydrotalcites for CO₂ sorption and recovery of steam



**shown above for CO₂ recovery from oxy-combustion use of Blast Furnace Gas*

CASOH: Calcium Assisted Steel mill Off-gas Hydrogen process for blast furnace gas



PERFORMANCE COMPARISON - TECHNICAL

| | Base case | Enhanced |
|--|-----------|----------|
| Total Fuel Input (MW) | 294.67 | 294.67 |
| Net power consumption (MW) | 14.9 | 33.7 |
| CO ₂ flow rate for storage (kg/s) | 36.5 | 65.8 |
| Specific electricity demand (kWh/kg _{CO2}) | 0.113 | 0.142 |
| Reboiler heat duty (MW) | 50.1 | 91.4 |
| Reboiler heat duty/CO ₂ flow rate for storage (MJ/kg _{CO2}) | 1.3 | 1.3 |
| Required heat for WGS (MW) | - | 66.5 |
| CO ₂ capture efficiency (%) | 46.5 | 83.80 |
| CO ₂ purity for storage (%) | 98.2 | 98.1 |
| Thermal energy output (DCF)(MW) | 294.61 | 266.80 |

PERFORMANCE COMPARISON – TECHNICAL

| | Unit | no capture | Base case | Enhanced |
|---|---|------------|-----------|----------|
| Steel mill size | Mt _{HRC} /y | 3.16 | 3.16 | 3.16 |
| Thermal input (BFG LHV) | [MW] | 294.67 | 294.67 | 294.67 |
| Thermal output (decarbonised fuel LHV) | [MW] | 294.67 | 294.61 | 266.80 |
| Heat requirements | [MW] | | 50.62 | 142.47 |
| Electricity requirements | [MW] | | 14.90 | 33.62 |
| Carbon Capture Rate | [%] | | 46% | 83% |
| Cold gas efficiency | [%] | 100.0% | 100.0% | 90.5% |
| Overall energy efficiency | [%] | 100.0% | 81.8% | 56.7% |
| CO ₂ specific emissions | [kg _{CO2} /GJ _{LHV}] | 267.1 | 153.38 | 51.19 |
| CO ₂ capture avoidance | [%] | | 42.6% | 80.8% |
| ΔCO ₂ specific emissions ^{a)} | [kg _{CO2} /t _{HRC}] | 711.9 | 383.56 | 120.28 |
| SPECCA | [MJ _{LHV} /kg _{CO2}] | | 1.96 | 3.54 |

PERFORMANCE COMPARISON - ECONOMICS

| | Unit | no capture | Base case | Enhanced |
|----------------------------------|-----------------------|------------|-----------|----------|
| Steel mill size | Mt _{HRC} /y | 3.16 | 3.16 | 3.16 |
| MDEA unit | [M€] | | 37.10 | 56.65 |
| WGS reactors+ heat exchangers | [M€] | | 0 | 12.36 |
| Gas expander | [M€] | | 3.73 | 2.80 |
| CO ₂ compressor units | [M€] | | 16.66 | 19.98 |
| Pumps | [M€] | | 0.02 | 0.02 |
| Total Equipment Cost | [M€] | | 57.50 | 91.81 |
| Total Direct Plant Cost | [M€] | | 117.31 | 187.29 |
| Total Plant Cost | [M€] | | 155.14 | 247.69 |
| Annualised Plant Cost | [M€/y] | | 17.69 | 28.24 |
| Fuel Cost | [M€/y] | 43.49 | 43.49 | 43.49 |
| variable, heat and electricity | [M€/y] | | 12.44 | 27.78 |
| fixed O&M | [M€/y] | | 7.76 | 12.38 |
| Total Annualised cost | [M€/y] | 43.49 | 81.37 | 111.9 |
| LCODF | [€/GJ] | 5.20 | 9.73 | 14.78 |
| Δcost of HRC | [€/t _{HRC}] | | 11.99 | 21.65 |
| CO ₂ avoidance cost | [€/t _{CO2}] | | 39.84 | 49.38 |



CONVERGE: CarbON Valorisation in Energy-efficient Green fuels

Green methanol synthesis for biodiesel production

16-17th February, Converge Workshop



Objectives: Membrane assisted methanol synthesis

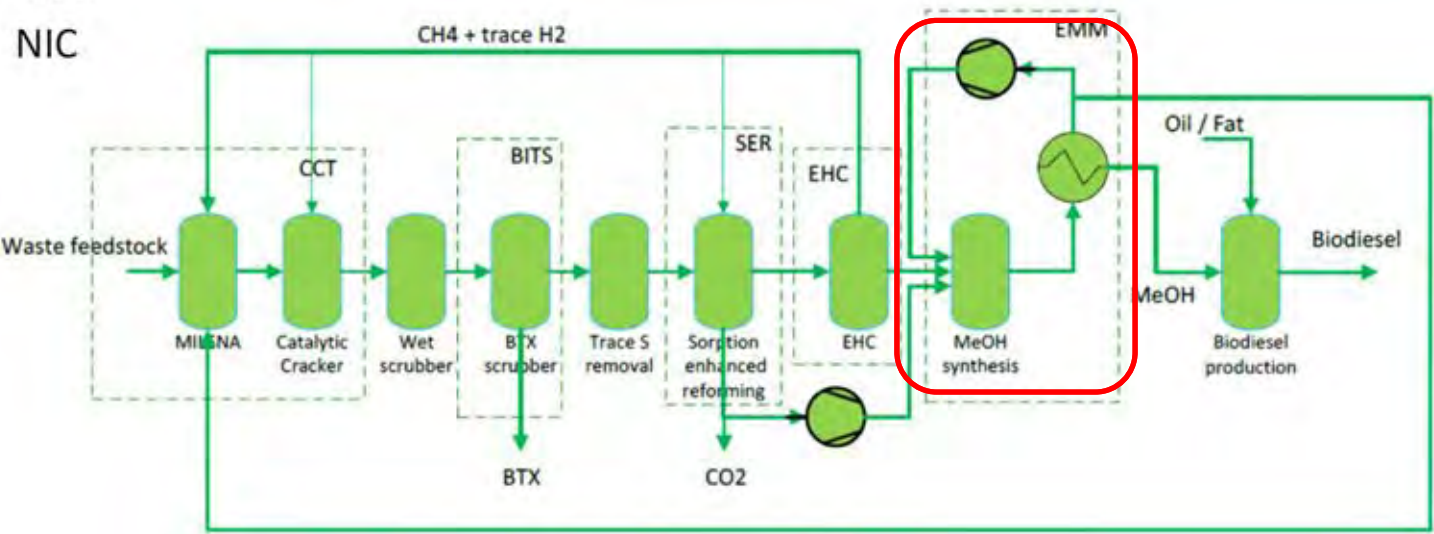
This project has received funding from the European Union's Horizon 2020 research and innovation programme under grant agreement No. 818135

Membrane assisted methanol synthesis.

- Develop stable membranes at reaction conditions
- Develop multi-tube membrane reactor, targeted conversion for feed CO_2/H_2 33% per pass
- Demonstration of integrated process at TRL 5

Partners involved:

- TNO
- NIC



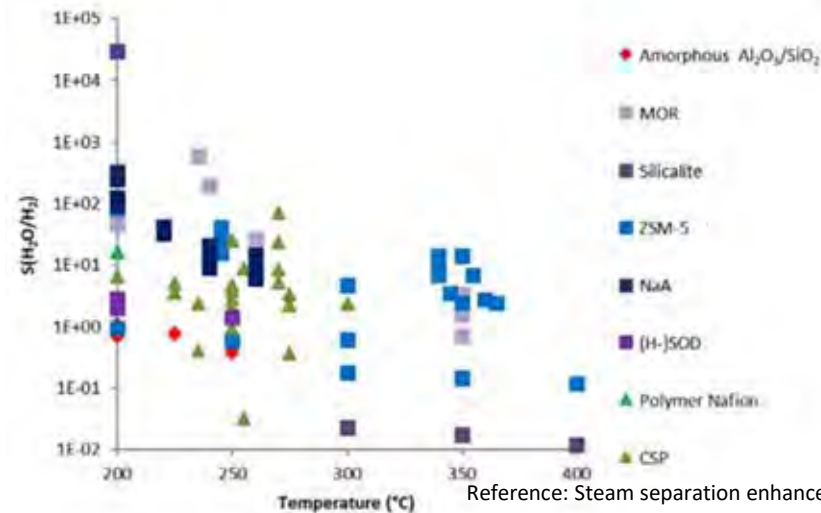
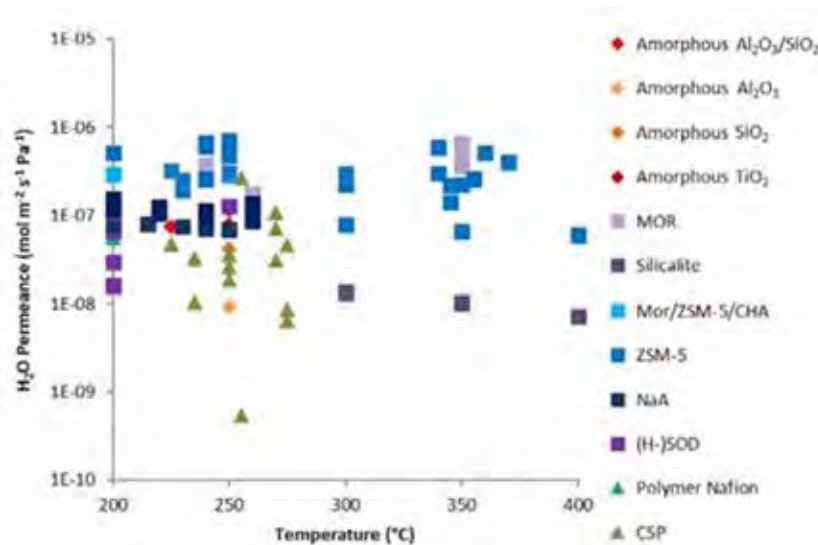
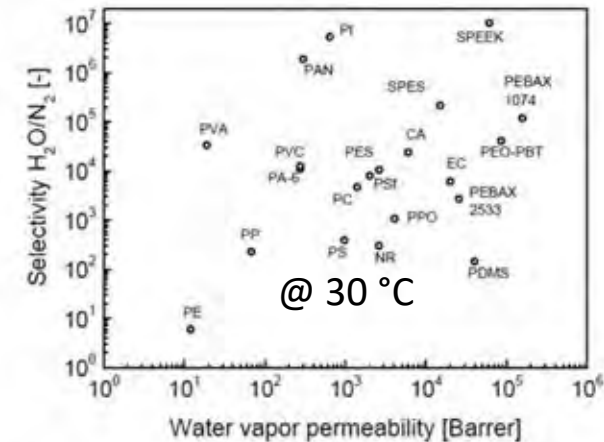
Membrane development - target

This project has received funding from the European Union's Horizon 2020 research and innovation programme under grant agreement No. 818135



Membrane development targets:

- 1) Stability at the methanol operating T and p (175-275°C), up to 100bar
- 2) High selectivity for steam and methanol
- 3) High steam/methanol permeability → high flux



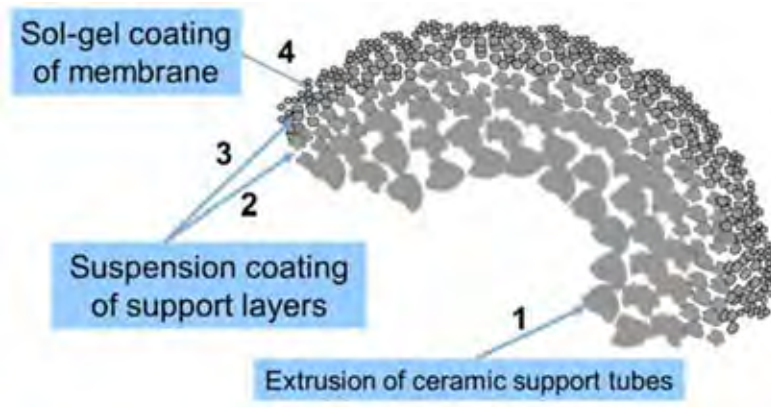
Reference: Steam separation enhanced reactions: Review and outlook, Jasper van Kampen, Jurriaan Boon, Frans van Berkel, Jaap Vente, Martin van Sint Annaland, Chemical Engineering Journal 374, 21019, 1286-1303



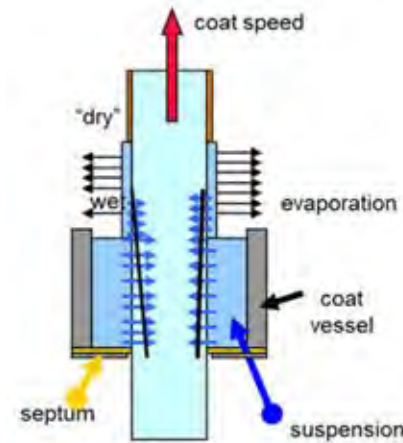
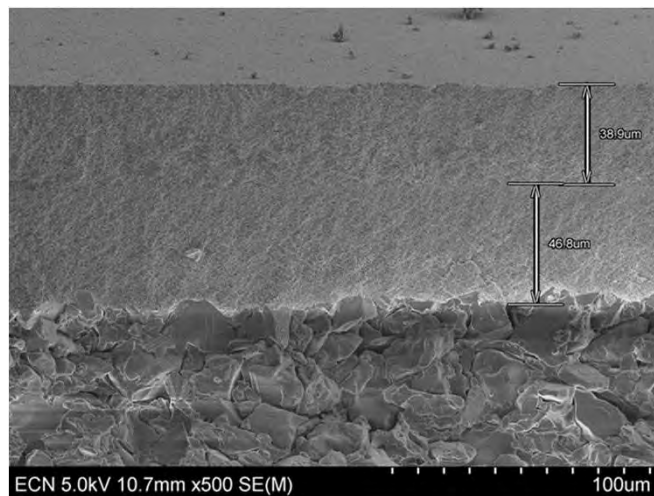
- Amorphous microporous APTES-PA (Aminopropyl triethoxysilane-Polyamide)
BETSE (1, 2-bis (triethoxysilyl) ethane)
- Polymeric SPEEK (sulfonated poly(ether ether ketone))
PI (Poly Imides)
PBI (Polybenzimidazol)
PDMS (Polydimethylsiloxane)
Li-Nafion

Membrane synthesis procedure -support

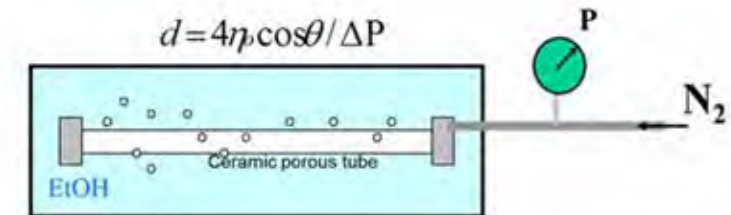
This project has received funding from the European Union's Horizon 2020 research and innovation programme under grant agreement No. 818135



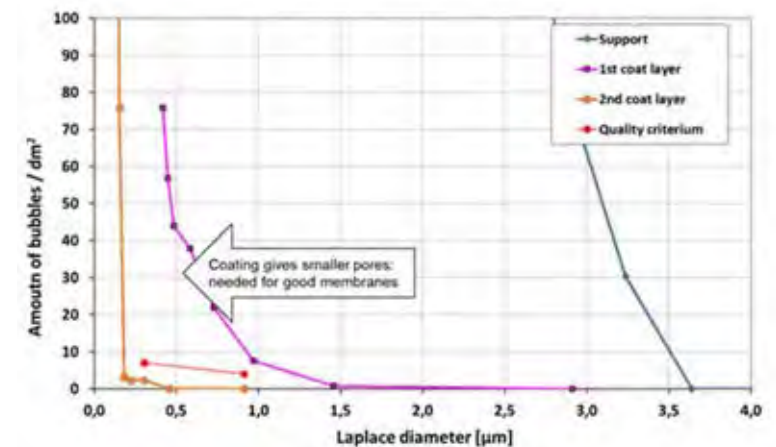
Membrane support layers



Coating process

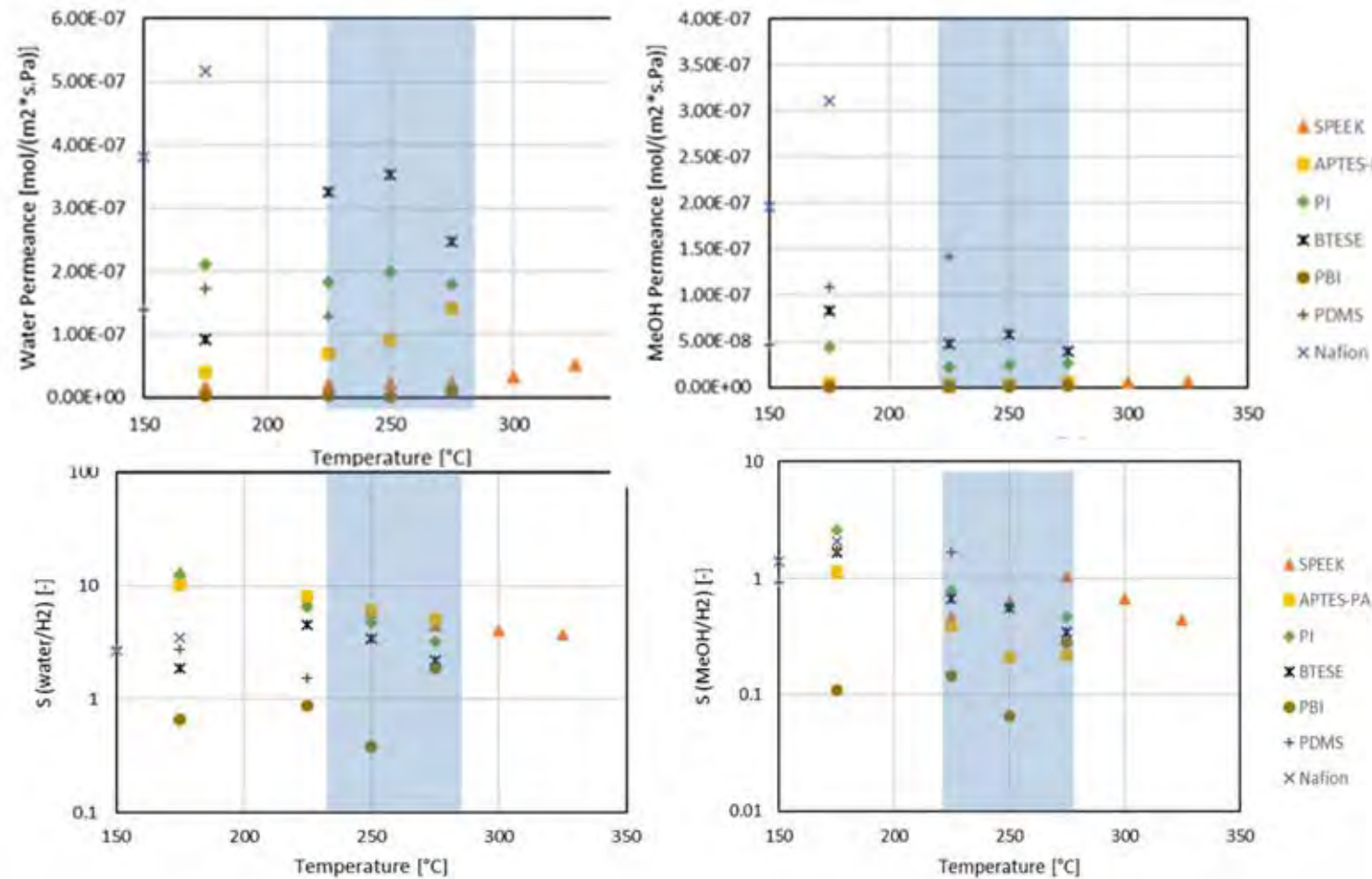


Bubble point test



Results membrane separation tests

This project has received funding from the European Union's Horizon 2020 research and innovation programme under grant agreement No. 818135



Test conditions:

- $p_{\text{feed}} = 35 \text{ bar}$, $p_{\text{perm}} = 1.5 \text{ bar}$, no sweep
- 60% H_2 , 10% (50/50)methanol/steam, 20% CO_2 , 1% CO , 9% N_2

Nafion, BETSE, PI highest steam and MeOH permeance

- BETSE performance decreases at 275°C , Nafion not selective at $T > 225^\circ$
- $\text{H}_2\text{O}/\text{H}_2$ selectivity highest for APTES-PA, SPEEK and PI
- MeOH/H_2 selectivity highest for PDMS 1.7, PI and BETSE $\sim 0.6\text{-}0.8$

Pre-selection:

- 1) PI
- 2) BETSE
- 3) APTES-PA

PDMS, Nafion \rightarrow no selectivity $> 225^\circ\text{C}$
 SPEEK \rightarrow low H_2O and MeOH permeance (10X lower than PI)

PBI \rightarrow low permeance, low selectivity

Conclusions

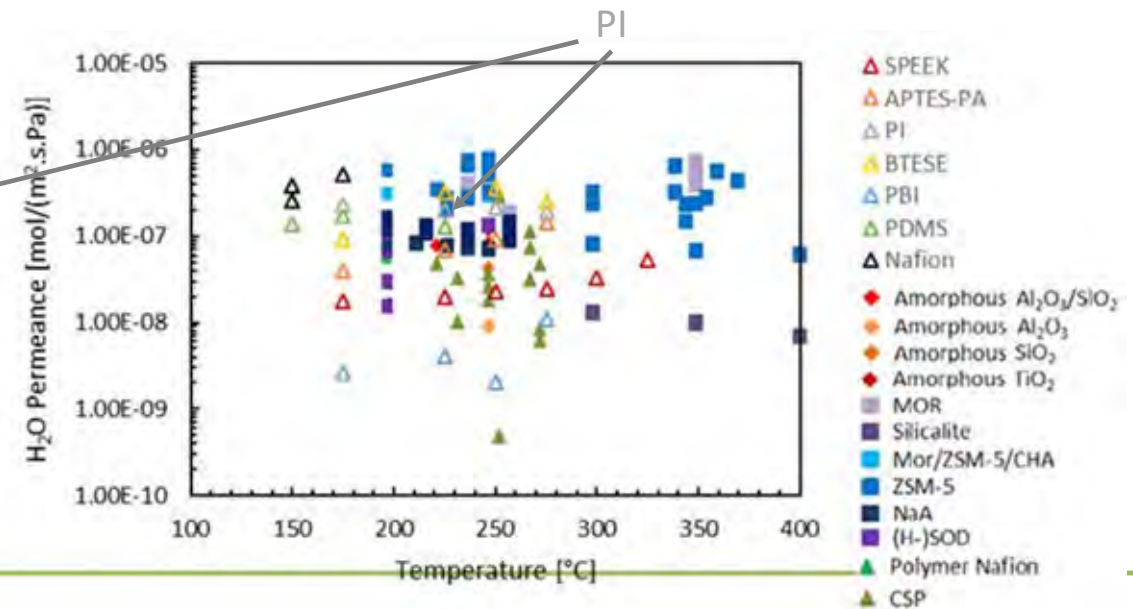
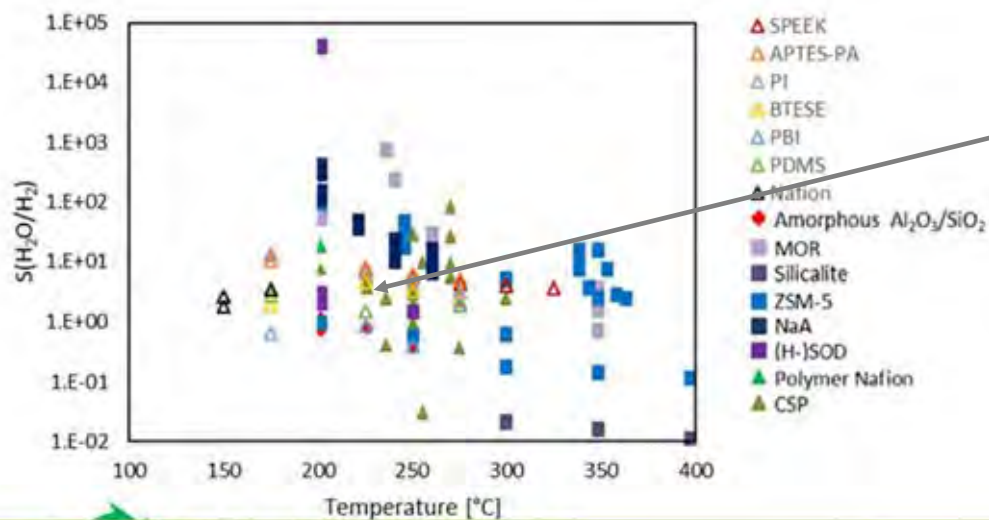
This project has received funding from the European Union's Horizon 2020 research and innovation programme under grant agreement No. 818135



- PI membrane preselected as the most promising to reach conversion targets. Membrane performance comparison steam/MEOH/mix ($T_{\text{range}} = 225\text{-}250\text{ }^{\circ}\text{C}$)

| | PI | BETSE | APTES |
|--|---------|-----------------------|-----------------|
| • $\text{H}_2\text{O}/\text{H}_2$ selectivity: | 4.7-6.5 | 3.5-4.3 | 6-8 |
| • MEOH/H_2 selectivity: | 0.6-0.8 | 0.6-0.7 | 0.2-0.4 |
| • H_2O permeance: | PI | $1.6 \cdot \text{PI}$ | $\text{PI}/2.3$ |
| • MeOH permeance: | PI | $2.2 \cdot \text{PI}$ | $\text{PI}/8.4$ |
| $\text{H}_2\text{O} > \text{H}_2 > \text{MEOH} > \text{CO}_2 > \text{CO} \approx \text{N}_2$ | | | |

- Steam/ H_2 behaviour compares well to literature



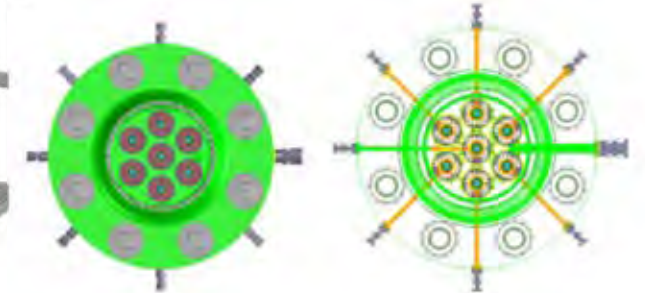
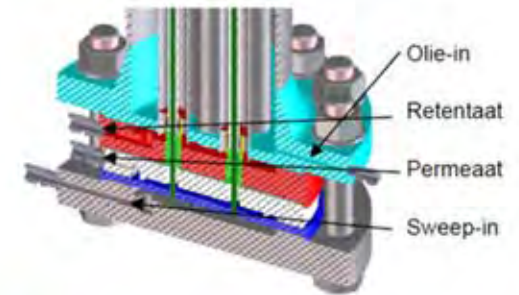
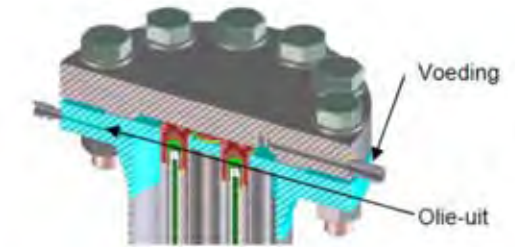
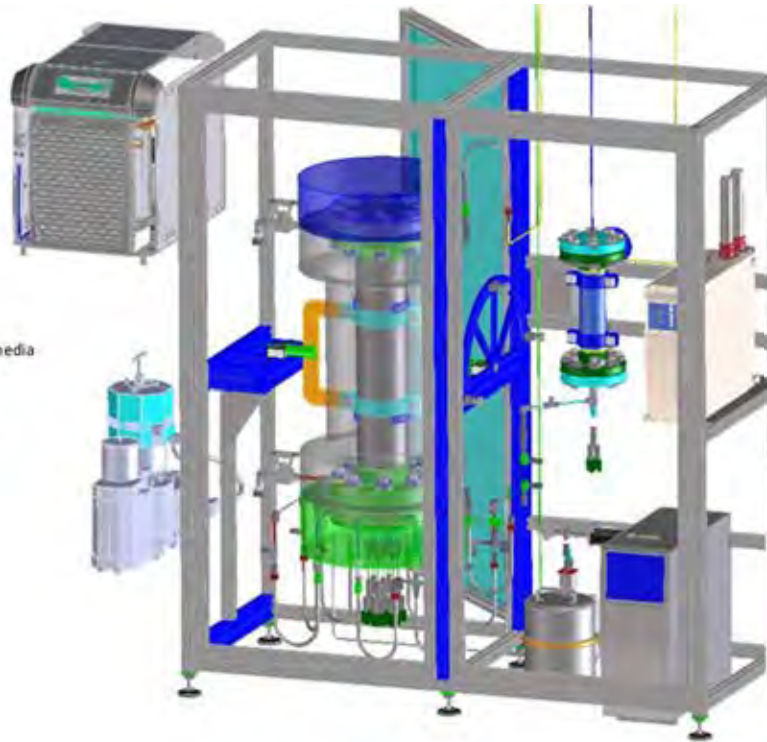
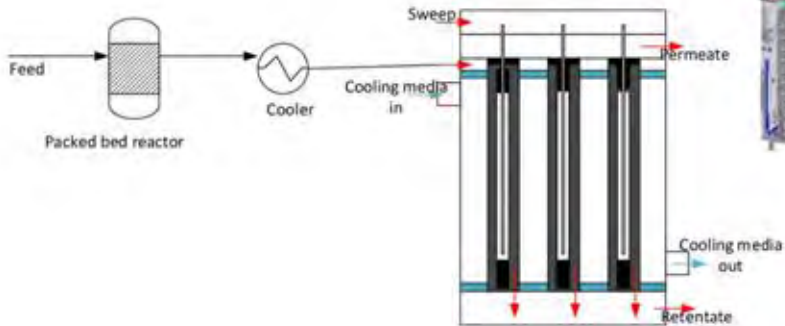
Next steps

This project has received funding from the European Union's Horizon 2020 research and innovation programme under grant agreement No. 818135



- Testing of preselected membranes in one tube membrane reactor
- Construction and testing of multi-tubular membrane reactor

Feed flow = 45 Nm³/min



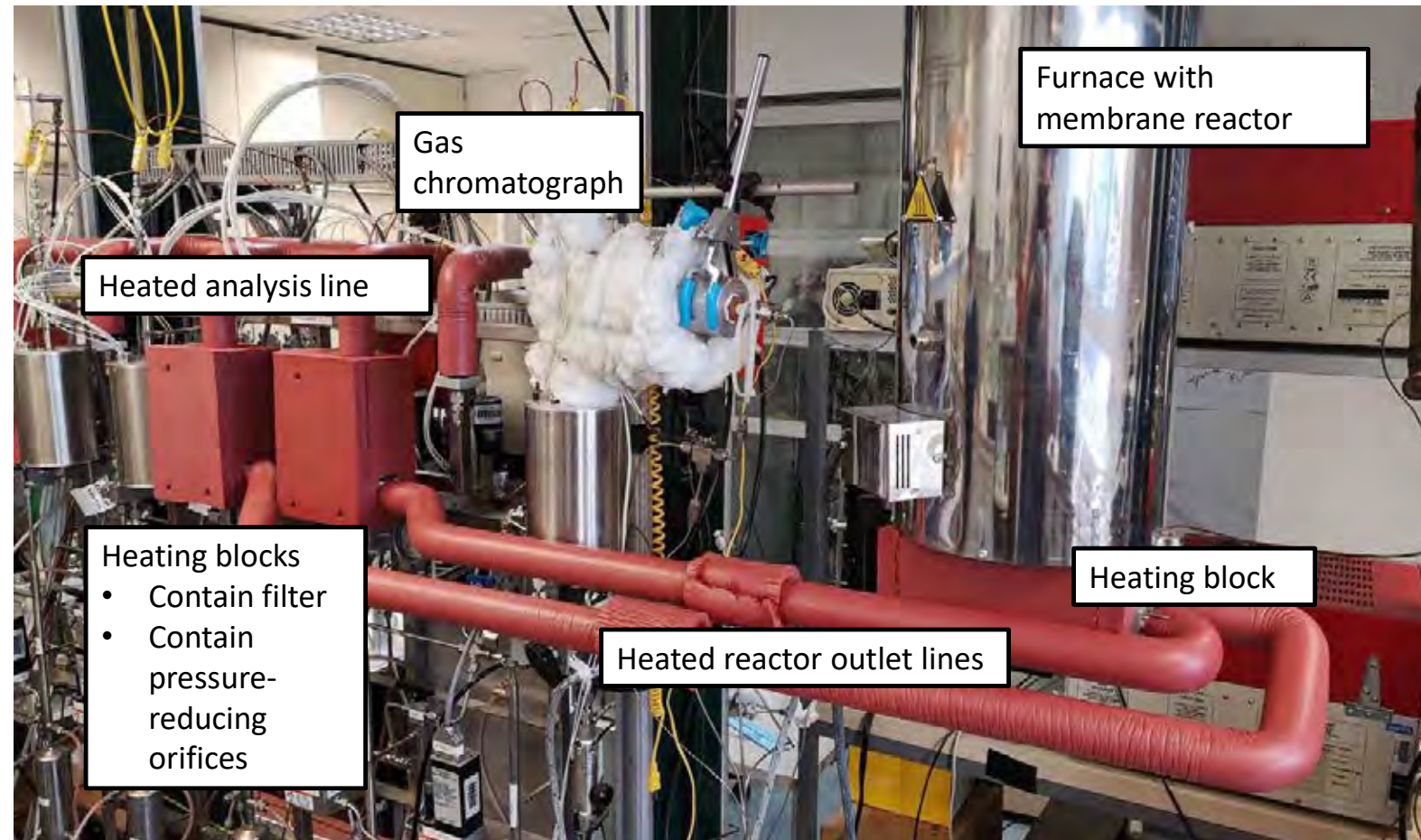
CONVERGE

CarbON Valorisation in Energy-efficient Green fuels



Testing rig upgrade at NIC

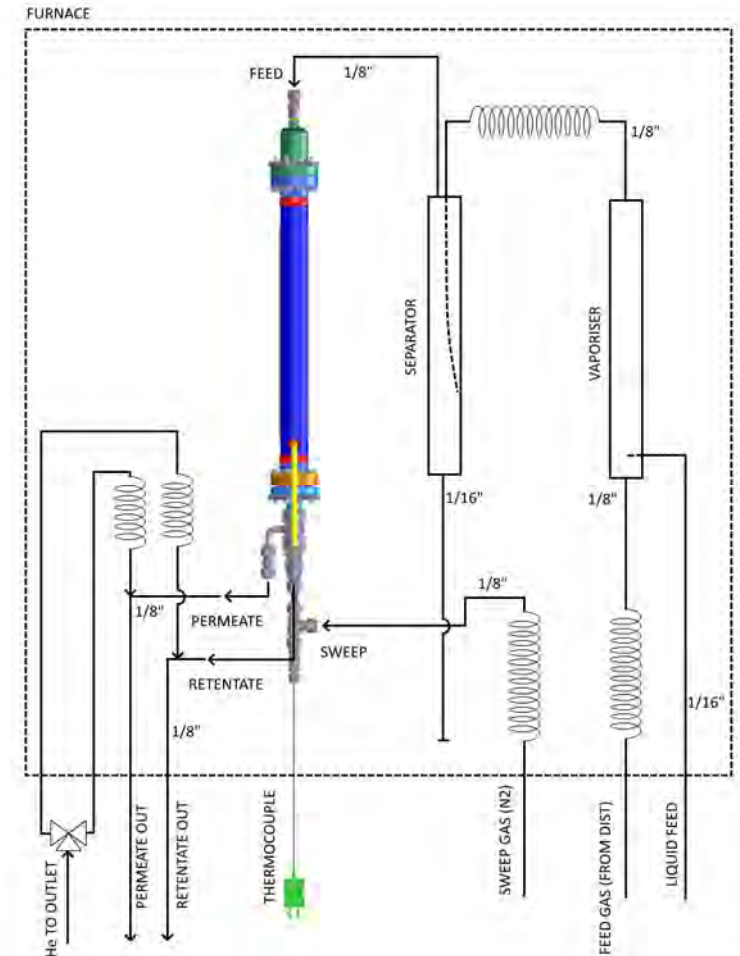
- Testing of the prominent membranes supplied by TNO.
- Advantages of NIC system:
 - high pressure op. (80 bar) and
 - high temperature op. (350°C).





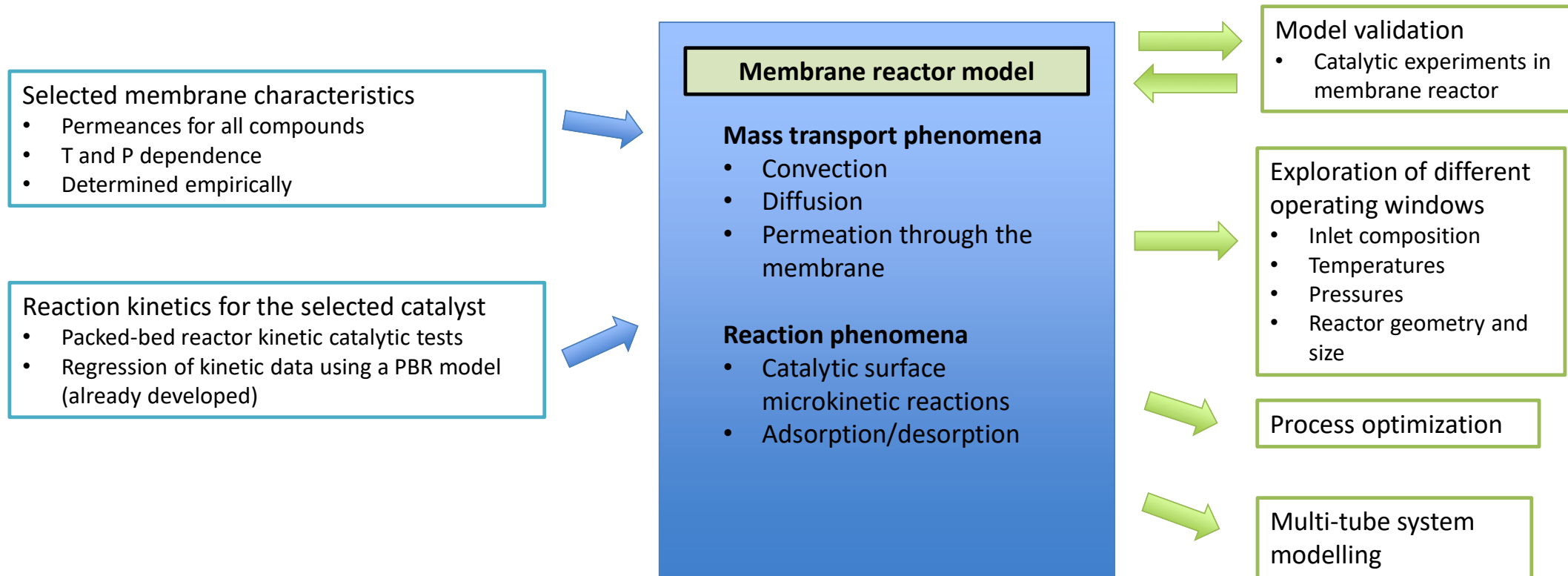
Inside the furnace with the membrane module

- Feed gas saturation with H₂O or MeOH to:
 - determine permeation and
 - simulate thermodynamical equilibrium gas mixture.
- He dilution to determine in-situ flow rates of permeate and retentate by gas chromatography.
- CO₂ is pumped into the feed gas using HPLC pump before membrane module.



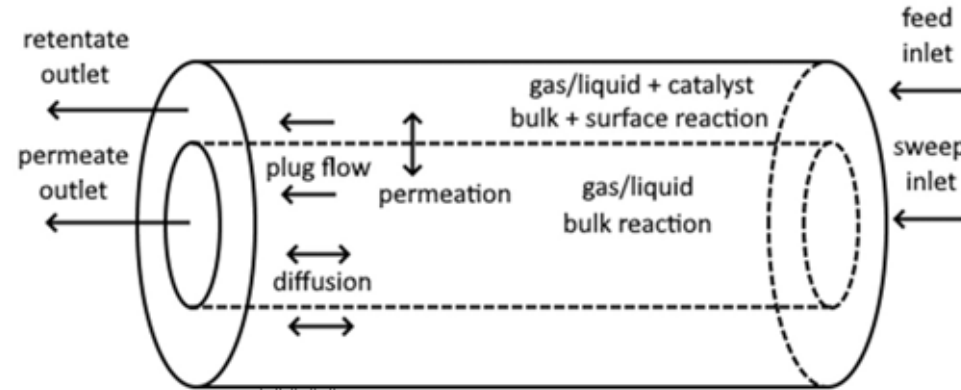


Modelling procedure





Model development



Retentate MB:
$$\frac{\partial C_i}{\partial t} = -v_{x,ret} \frac{\partial C_i}{\partial x} + \frac{D_i}{\tau} \frac{\partial^2 C_i}{\partial x^2} + C^* \frac{1-\varepsilon}{\varepsilon} R_{i,cat} + R_{i,bulk} - \frac{\dot{N}_{memb.}}{V_{ret} \varepsilon}$$

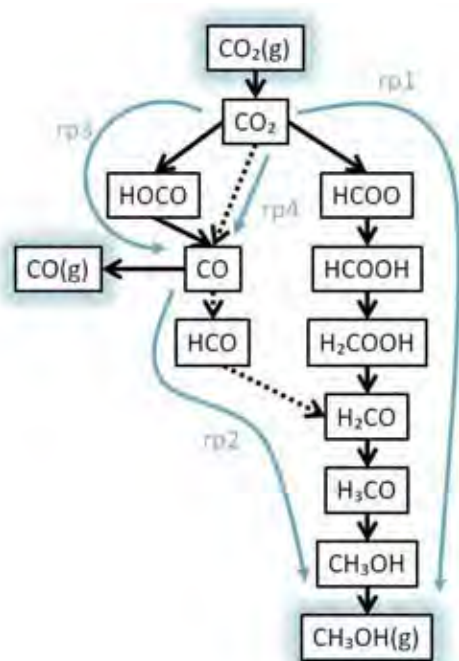
Permeate MB:
$$\frac{\partial C_i}{\partial t} = -v_{x,perm} \frac{\partial C_i}{\partial x} + D_i \frac{\partial^2 C_i}{\partial x^2} + R_{i,bulk} + \frac{\dot{N}_{memb.}}{V_{perm}}$$

Flow through the membrane:

$$\begin{aligned} \dot{N}_{memb.} &= A_{memb.} P_i (p_{i,ret} - p_{i,perm}) \\ &= A_{memb.} P_i RT (c_{i,ret} - c_{i,perm}) \end{aligned}$$



Model development: Kinetics of MeOH synthesis



Overall reaction scheme. Black arrows represent the elementary reaction steps and blue arrows the reaction pathways. Reaction species in black squares without "(g)" are adsorbed on the catalyst's surface.

- Surface reaction mechanism for methanol synthesis on CuZnAl
- Active sites: Cu (&), Zn (*)
- 5 gas phase species, 11 surface species
- 16 reversible surface reactions, 5 of which are adsorption/desorption reactions
- The constants obtained from literature were fitted to experimental data

| Reaction | optimized | | | | original Zn/Cu(211) | | | |
|---|------------|----------------|-------------|-----------------|---------------------|----------------|-------------|-----------------|
| | Afor [s-1] | Eafor [kJ/mol] | Aback [s-1] | Eaback [kJ/mol] | Afor [s-1] | Eafor [kJ/mol] | Aback [s-1] | Eaback [kJ/mol] |
| $H_2 + \& \rightleftharpoons H\& + H\&$ | 1.00E+03 | 51.00 | 1.77E+12 | 78.00 | 1.00E+03 | 51.00 | 1.77E+12 | 78.00 |
| $H\& + CO_2^* \rightleftharpoons HOCO^*\&$ | 4.62E+13 | 83.80 | 8.23E+13 | 104.28 | 3.91E+12 | 95.53 | 1.00E+11 | 123.51 |
| $H\& + H_2CO^*\& \rightleftharpoons H_3CO^*\& + \&$ | 3.12E+08 | 8.47 | 1.17E+11 | 88.29 | 4.66E+12 | 11.58 | 1.00E+11 | 114.82 |
| $H\& + H_3CO^*\& \rightleftharpoons CH_3OH^*\& + \&$ | 3.28E+12 | 112.01 | 6.98E+12 | 87.02 | 1.99E+14 | 143.77 | 1.44E+13 | 116.75 |
| $H\& + CO_2^* \rightleftharpoons HCOO^*\&$ | 1.69E+11 | 58.96 | 5.97E+14 | 142.86 | 3.57E+12 | 74.30 | 1.00E+11 | 188.16 |
| $H\& + HCOO^*\& \rightleftharpoons HCOOH^*\& + \&$ | 4.69E+09 | 60.20 | 2.71E+10 | 75.73 | 7.93E+12 | 114.82 | 1.77E+11 | 48.25 |
| $H\& + HCOOH^*\& \rightleftharpoons H_2COOH^*\& + \&$ | 1.13E+12 | 87.74 | 6.71E+13 | 75.98 | 1.26E+12 | 58.86 | 9.57E+13 | 58.86 |
| $H_2COOH^*\& + * \rightleftharpoons H_2CO^*\& + OH^*$ | 1.82E+13 | 59.21 | 4.26E+11 | 17.08 | 2.53E+13 | 50.17 | 1.86E+11 | 16.40 |
| $H\& + OH^* \rightleftharpoons H_2O^*\&$ | 6.43E+09 | 72.66 | 2.89E+10 | 72.73 | 1.22E+13 | 77.19 | 4.83E+11 | 70.44 |
| $CO_2^* + \& \rightleftharpoons CO\& + O^*$ | 3.98E+12 | 46.16 | 1.57E+12 | 52.88 | 1.04E+13 | 76.23 | 8.40E+12 | 65.61 |
| $H\& + O^* \rightleftharpoons OH^*\&$ | 5.90E+12 | 309.13 | 5.05E+10 | 226.11 | 1.88E+13 | 116.75 | 1.00E+11 | 198.77 |
| $HOCO^*\& \rightleftharpoons CO\& + OH^*$ | 3.16E+10 | 27.99 | 4.89E+11 | 65.23 | 6.60E+13 | 22.19 | 1.00E+11 | 58.86 |
| $CO_2 + * \rightleftharpoons CO_2^*$ | 7.53E+02 | -2.29 | 2.9E+09 | -29.13 | 7.41E+02 | -2.01 | 1.00E+13 | -30.88 |
| $CH_3OH + * + \& \rightleftharpoons CH_3OH^*\&$ | 2.59E+01 | -0.99 | 1.34E+13 | 43.01 | 8.68E+02 | -2.01 | 1.00E+13 | 39.56 |
| $H_2O + * \rightleftharpoons H_2O^*$ | 8.38E+02 | -1.69 | 1.31E+12 | 39.45 | 1.16E+03 | -2.01 | 1.00E+13 | 37.63 |
| $CO + \& \rightleftharpoons CO\&$ | 2.86E+02 | -0.98 | 3.25E+13 | 59.12 | 9.28E+02 | -2.01 | 1.00E+13 | 98.42 |

Reactions and reaction rate constants (original from literature and fitted to experimental data)

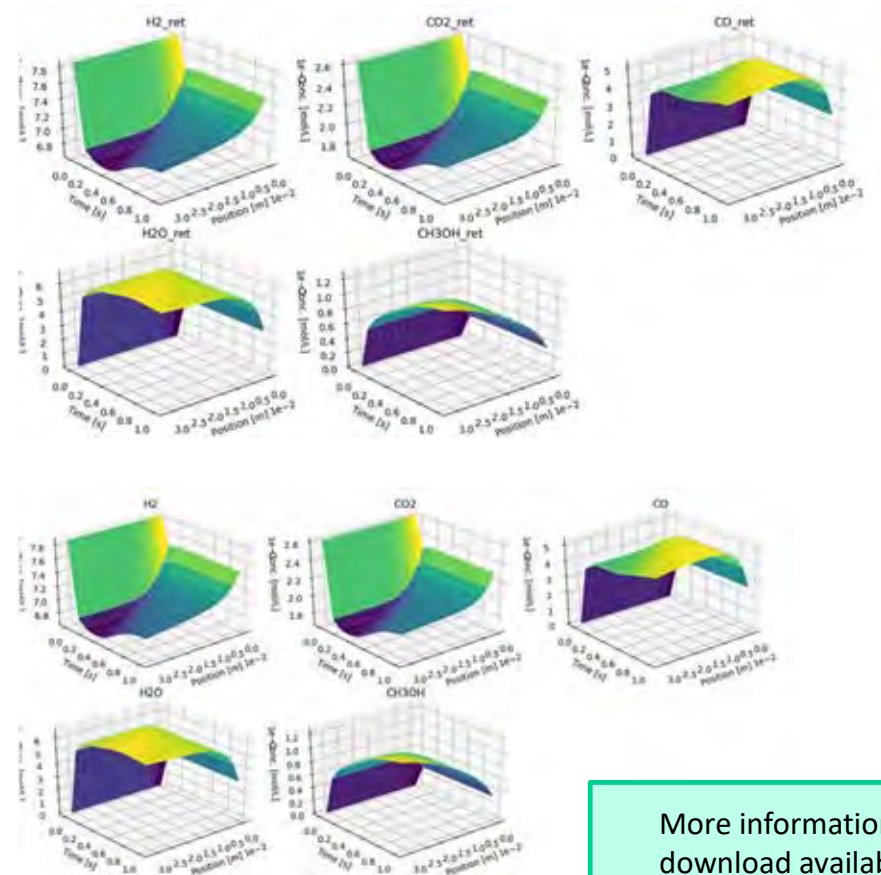


Model development

- Modeling in the programme CERRES developed at NIC



- ✓ Simulation of 14 different types of chemical reactors (including membrane reactor)
- ✓ Complex user-defined chemical kinetics
- ✓ Model-experiment compare
- ✓ Parameter optimization
- ✓ Sensitivity analysis
- ✓ Efficient computation
- ✓ Plot results and export data
- ✓ Easy to use (graphical user interface)
- ✓ Free for academic/teaching use



More information and download available at:

www.cerres.org



CarbON Valorisation in Energy-efficient Green fuels

CONVERGE Acknowledgements

CarbON Valorisation in Energy-efficient Green fuels

The CONVERGE project has received funding from the European Union's Horizon 2020 research and innovation programme under grant agreement N° 818135



CONVERGE: CarbON Valorisation in Energy-efficient Green fuels

WP4: Green methanol synthesis for biodiesel production



Johnson Matthey
Inspiring science, enhancing life

Realising the potential of MOFs through efficient scale-up

Adam Deacon

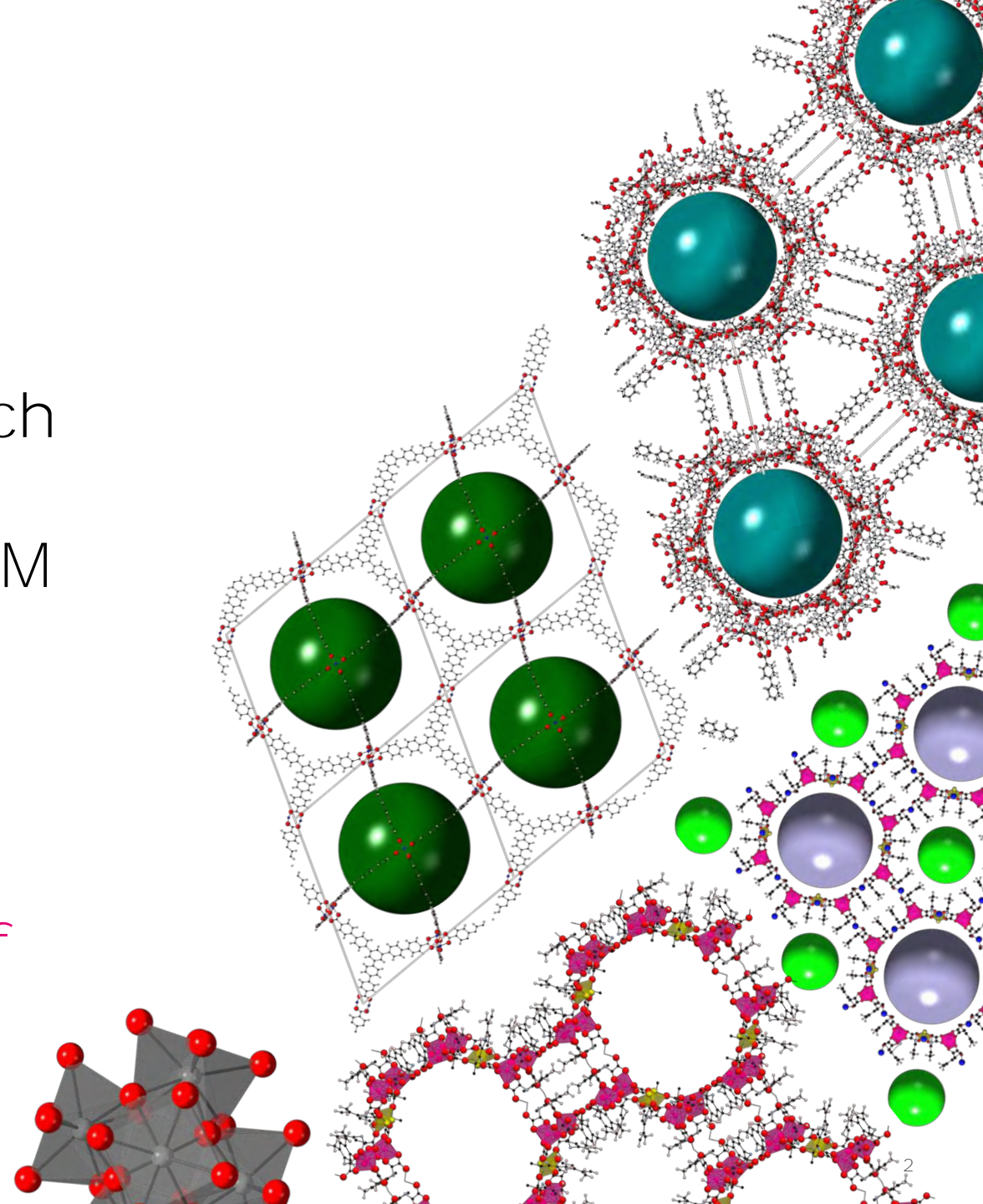
IWCCU 2021

16-02-2021

Agenda

- Who is JM?
- Our priorities for MOF research
- MOF scale-up case study at JM

Aim to give an overview of
MOF scale up work at JM.



A speciality
chemicals company
and a world leader in
sustainable
technologies

Over 200 years of
history dating
back to 1817

R&D Focused, with
~12% of employees
working in R&D.
100+ PhDs funded by JM
throughout world



We serve global markets



Automotive



Pharmaceutical and medical



Chemicals



Oil and gas



Agrochemicals and fertilisers



Food and beverage



Energy generation and storage

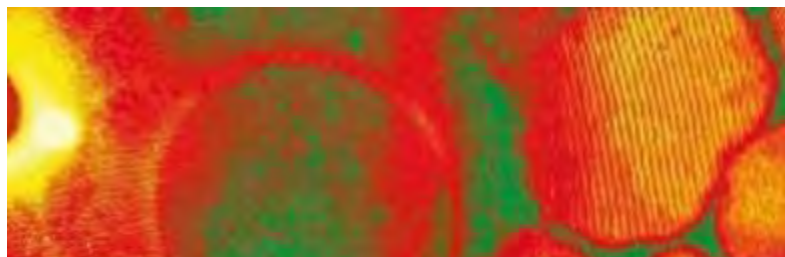


Glass



Other industrial

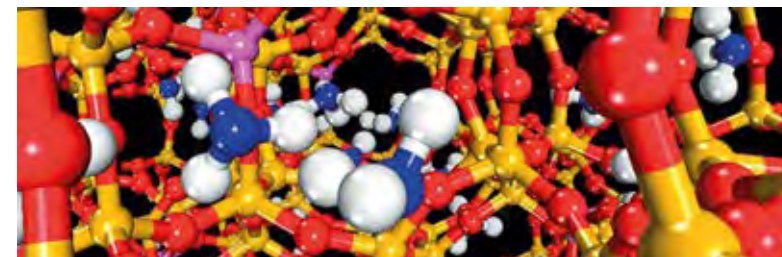
World class science and technology expertise



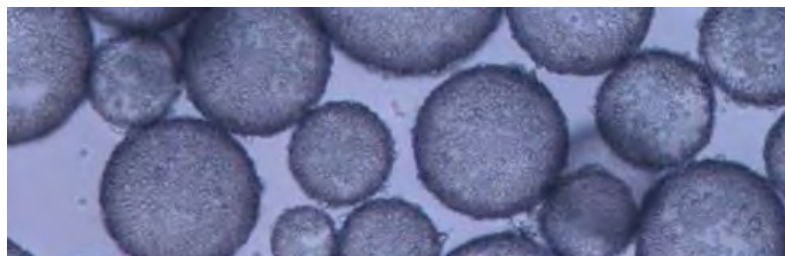
Characterisation and modelling



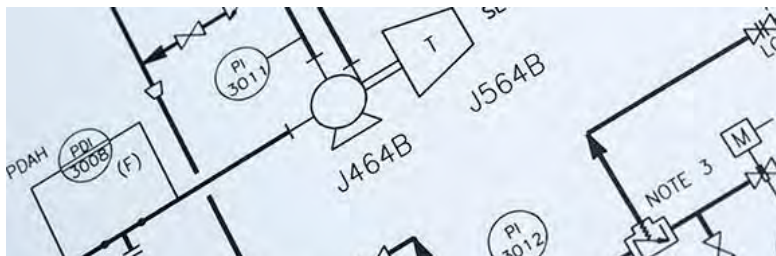
Chemical synthesis



Material design and engineering



Product formulation



Process optimisation



Surface chemistry and coatings



Pgm chemistry and metallurgy



Catalysis and advanced materials



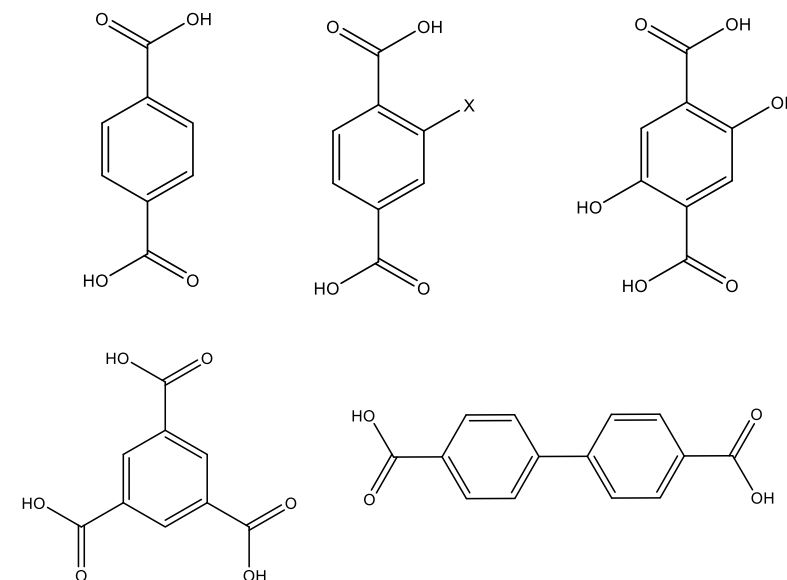
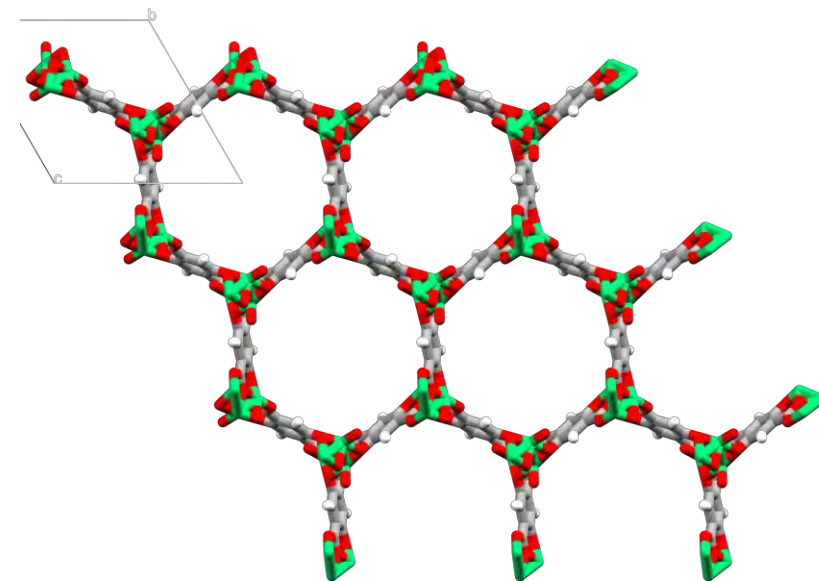
Electrochemistry

What are Metal-Organic Frameworks (MOFs)?

Functional hybrid materials consisting of metal nodes connected by organic linkers.

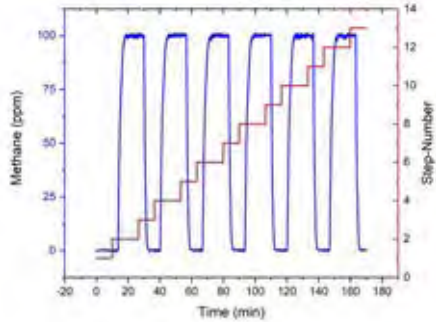
- High surface areas
 - 1 g of material possessing the same surface area as a football pitch
- Huge number of possible structures with ~70 k reported [1].
- Functionality arises from:
 - Porosity, pore structure, metal nodes & linker functional groups
- Certain MOFs are stable under harsh conditions
- Lots of academic interest over the last ~30 years
- Several products using MOFs now exist
 - TruPick™ & ION-X

Need to develop large scale, cost effective scale-up routes to make these application a reality

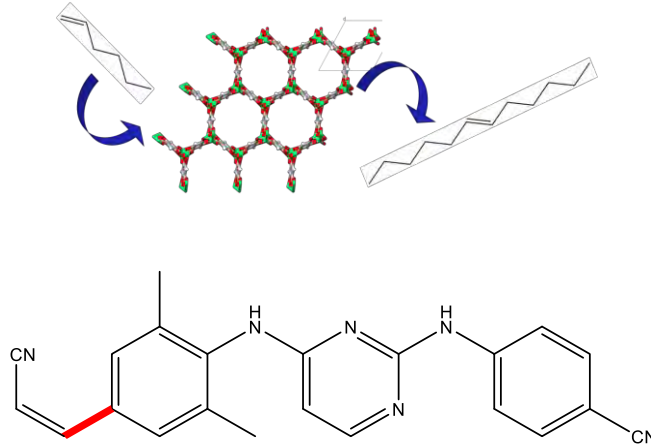


Current key priorities in JM MOF work

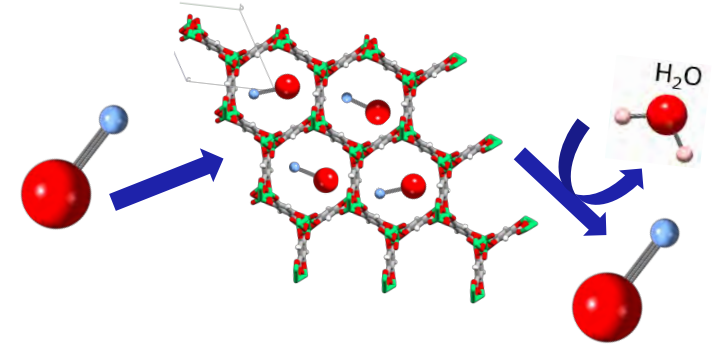
Separations and purification



Fine Chemical Catalysis



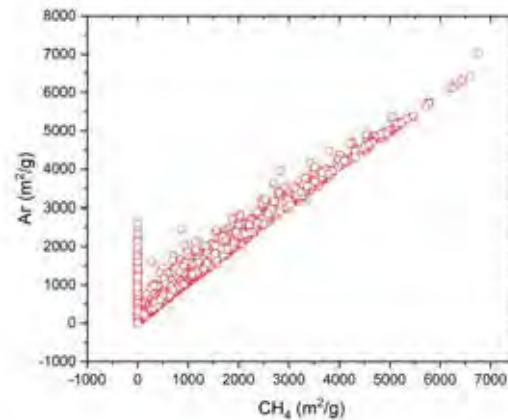
Controlled release



Forming and scale-up



Modelling

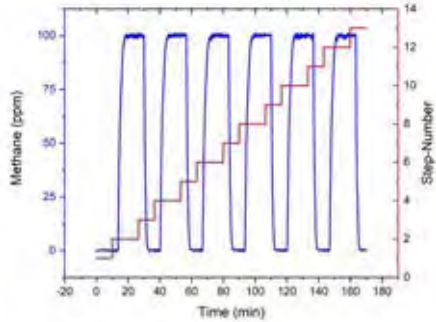


In-situ monitoring

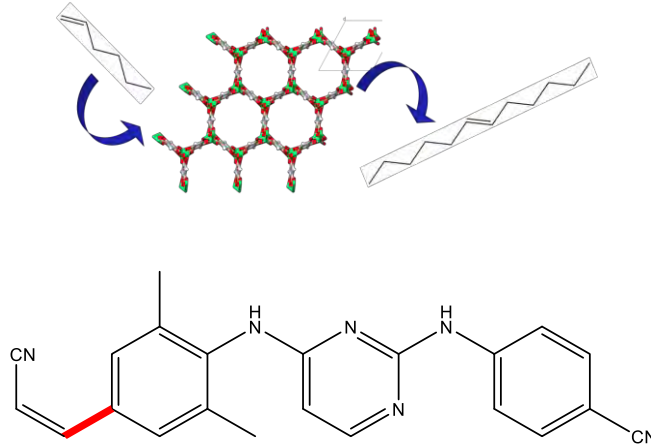


Current key priorities in JM MOF work

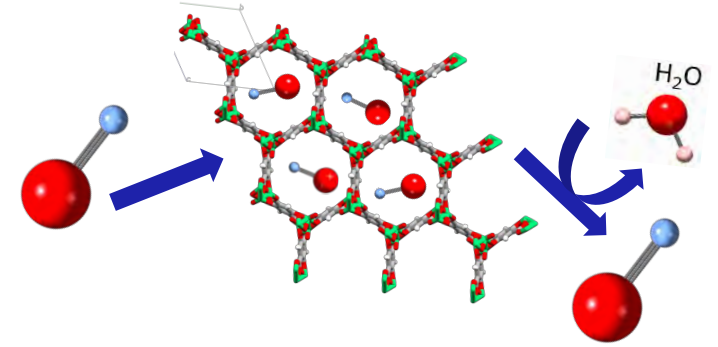
Separations and purification



Fine Chemical Catalysis



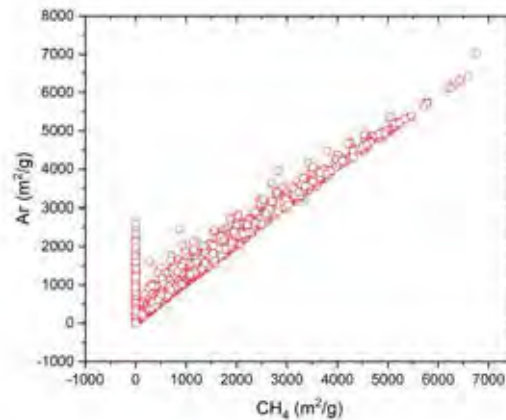
Controlled release



Forming and scale-up



Modelling



In-situ monitoring



Scale-up considerations

Chemical

- Concentration
- Temperature
- Solvent

Physical

- Mixing
- Separation
- Washing
- Waste
- Product performance

| Solvent | Safety Score | Health Score | Env. Score | Ranking |
|------------------|--------------|--------------|------------|-------------|
| H ₂ O | 1 | 1 | 1 | Recommended |
| EtOH | 4 | 3 | 3 | Recommended |
| MeOH | 4 | 7 | 5 | Problematic |
| THF | 6 | 7 | 5 | Problematic |
| DMF | 3 | 9 | 5 | Hazardous |
| Sulfolane | 1 | 9 | 7 | Hazardous |

D. Prat, et al., *Green Chem.*, 2016, 18, 288-296

Reduction of raw materials is key for MOF scale-up

Nano ZIF-8 scale-up case study

Properties

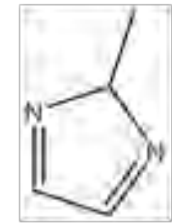
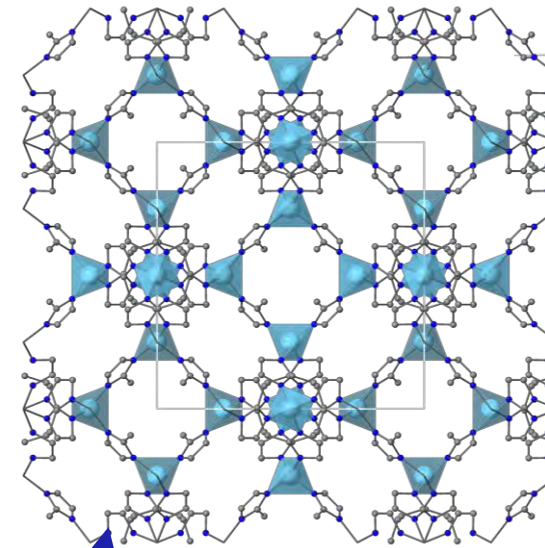
- Very high surface area $\sim 1600 \text{ m}^2\text{g}^{-1}$
- High thermal stability – stable 400°C
- Pore aperture – 3.4 \AA

Application

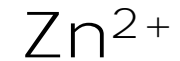
- Used in pre-combustion application - separation of H_2/CO_2
- Nano sized needed for membrane applications



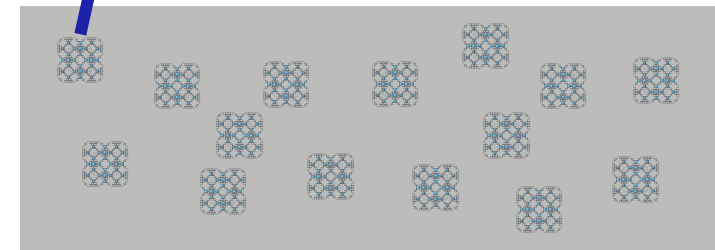
ZIF-8



2-Methylimidazole

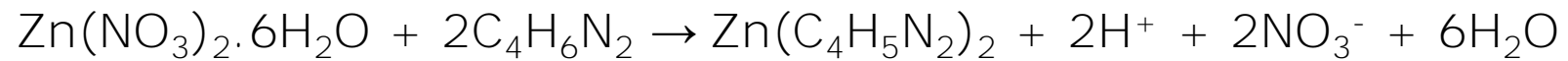
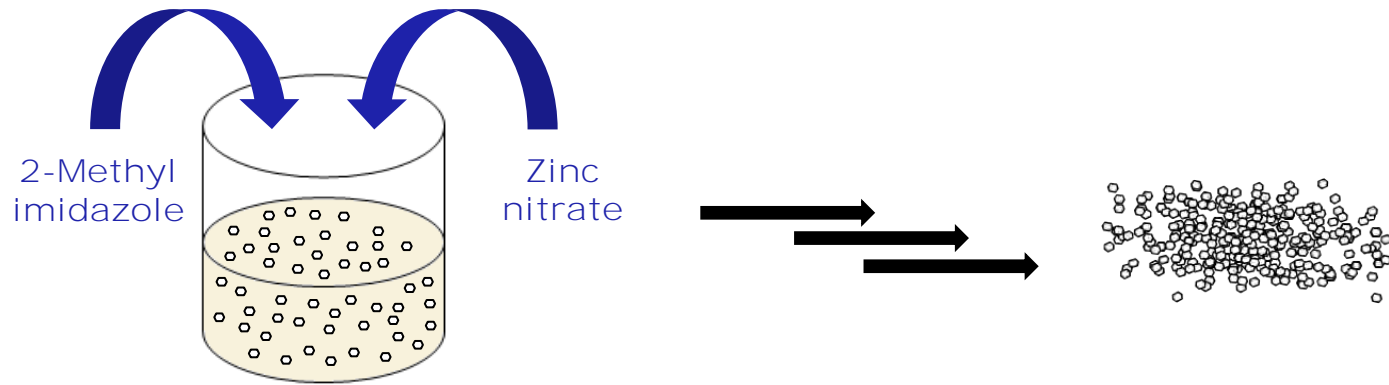


Zinc nitrate



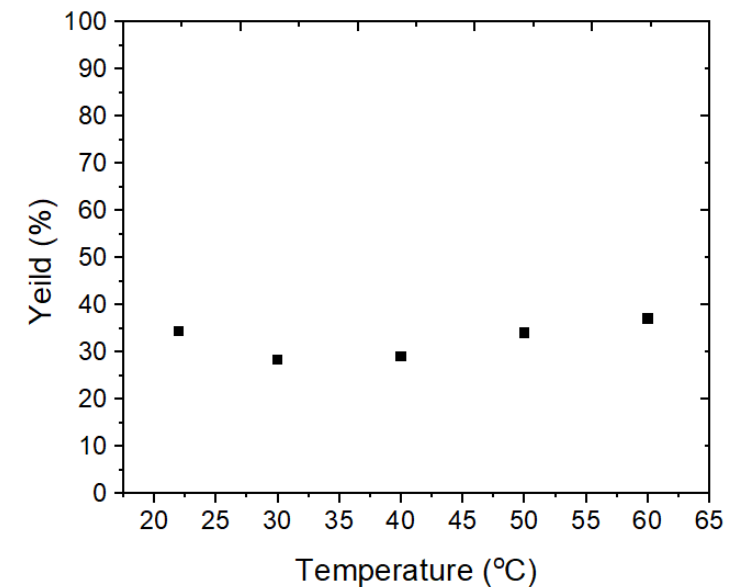
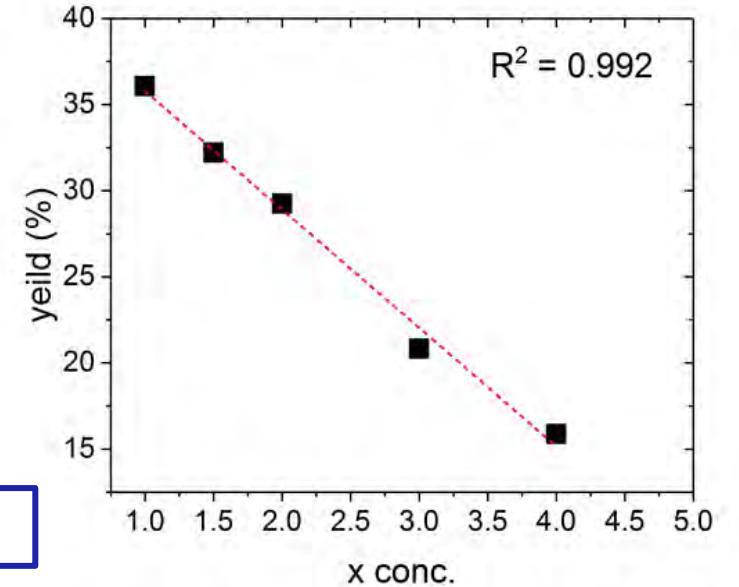
Mixed matrix membrane

Original nano ZIF-8 route



- Dilute conditions needed
 - Large quantities of Methanol used ~ 5 L MeOH needed for 5 g of nano ZIF-8

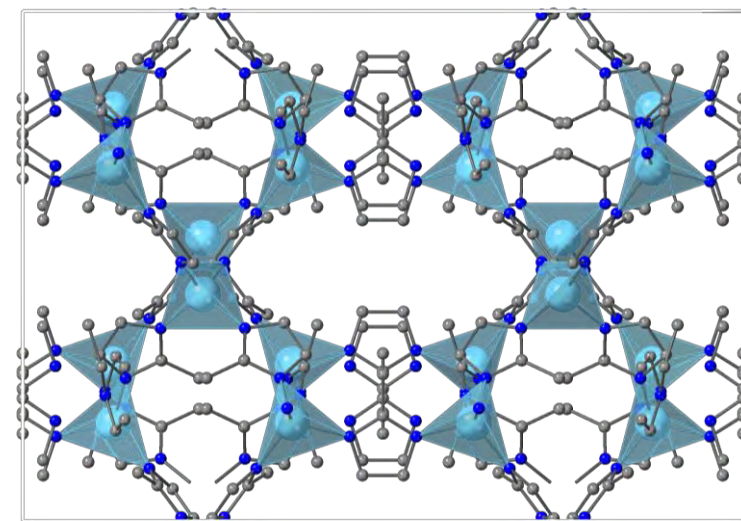
Parameter study showed its difficult to improve the original synthesis.



ZIF-L as an alternative route to nano ZIF-8

Properties

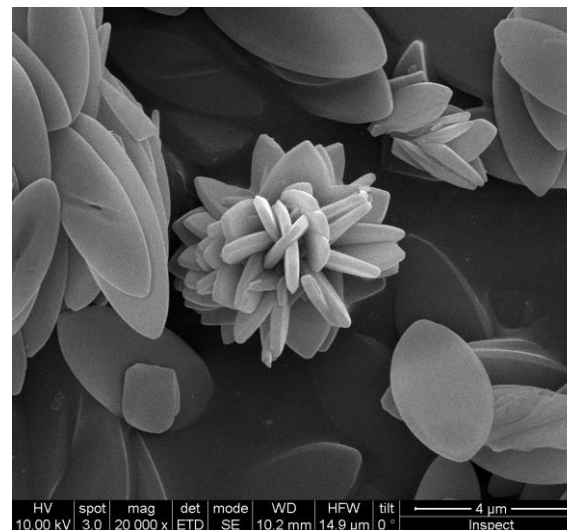
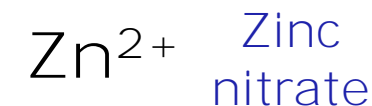
- ZIF-L is a dense phase polymorph of ZIF-8
- Consists of same raw materials as ZIF-8
- 2D material connected by linker molecules – leaf shape
- Low porosity – $92 \text{ m}^2\text{g}^{-1}$



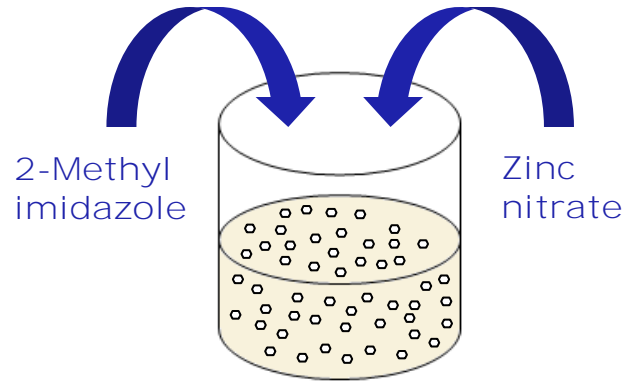
ZIF-L



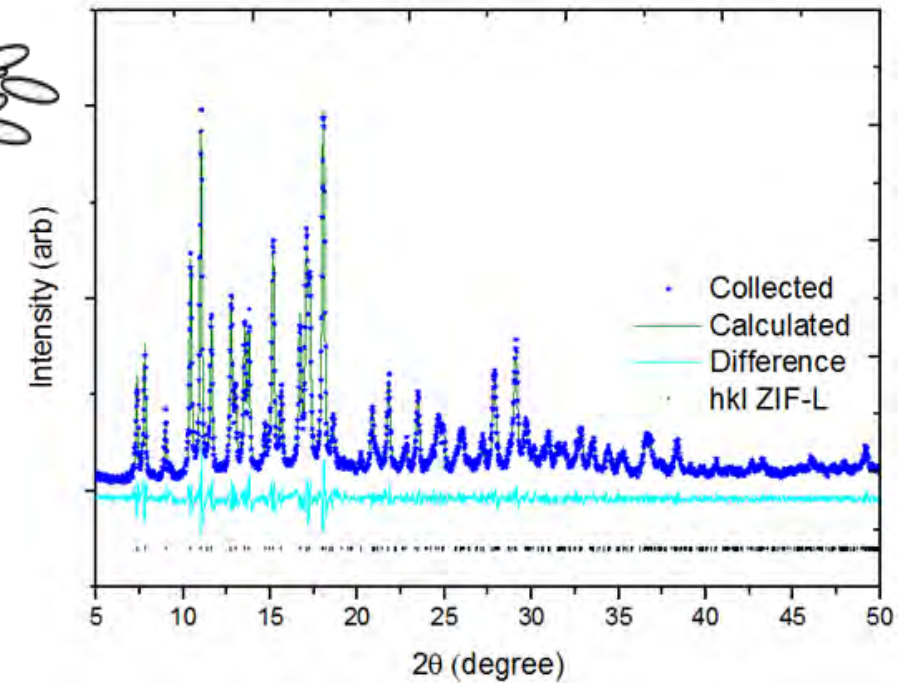
2-Methylimidazole



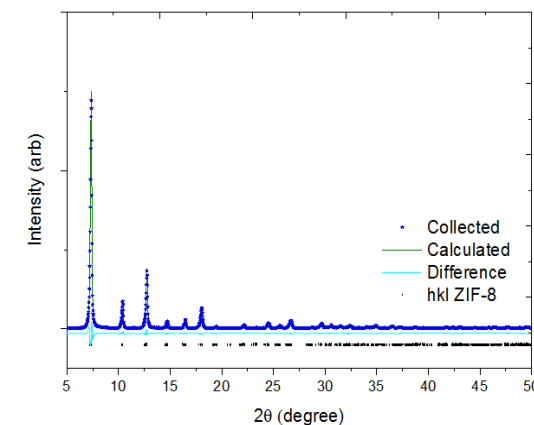
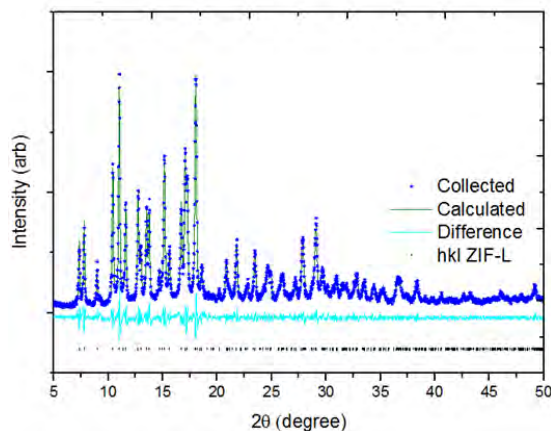
ZIF-L as an alternative route to nano ZIF-8



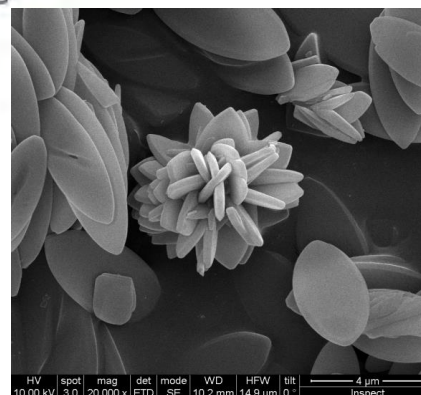
- Simple synthesis in water
- Concentrated reaction
- High yield ~ 90 %



JM



ZIF-8 BET surface
area $\sim 1600 \text{ m}^2\text{g}^{-1}$

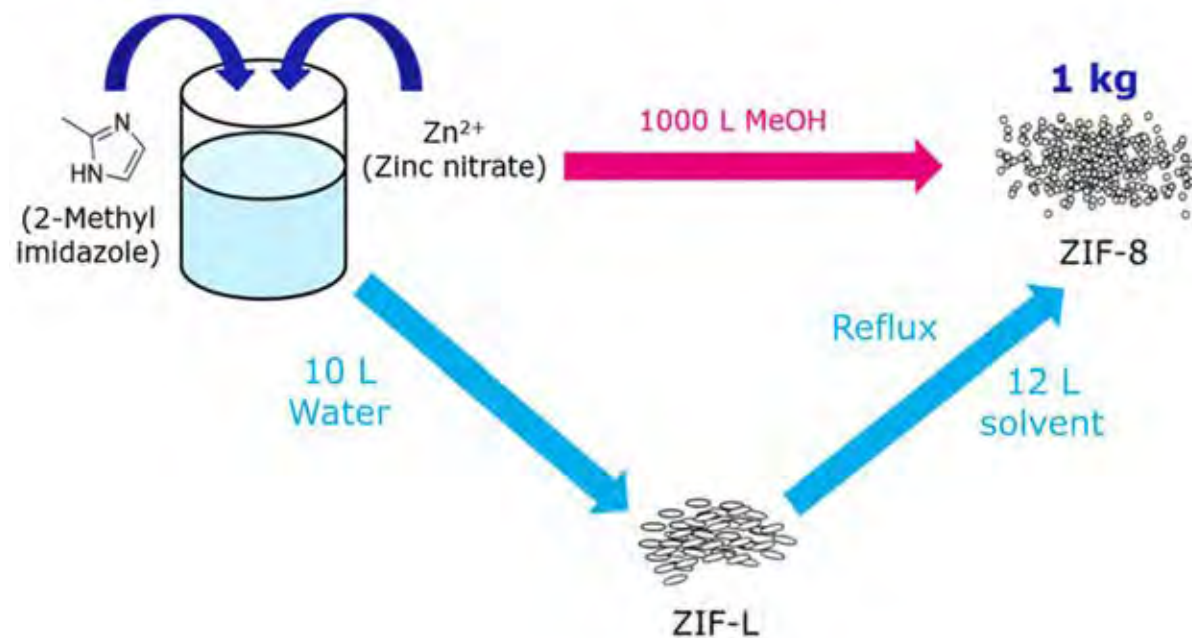


ZIF-L BET
surface area
92 m²g⁻¹

Nano-ZIF-8 case study summary

Developed scalable route

- Two order of magnitude solvent reduction
- Doubled overall all yield of nano-ZIF-8 synthesis
- Replaced methanol with non-toxic solvent
- Industrial scale concept for nano ZIF-8 designed.



7x reduction in cost to produce

Other scale-up examples

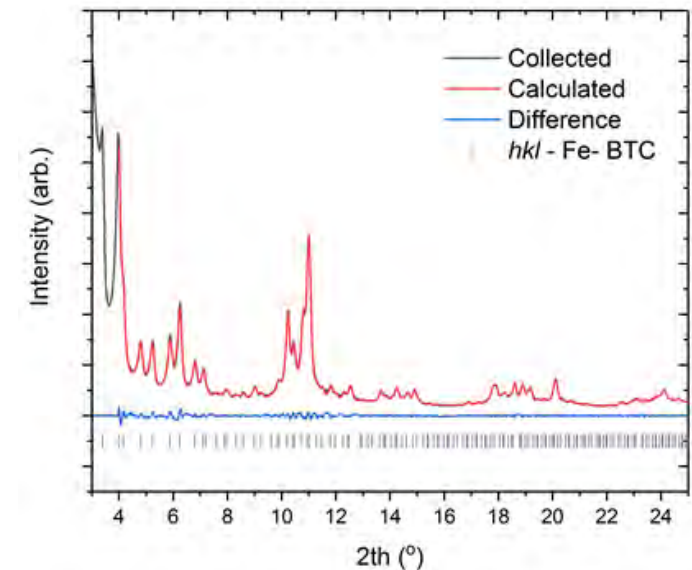
Scale-up: Fe-BTC

- 60 L batch reaction vessel
- Washed in purpose built setup
- 15 kg MOF produced
- BET surface area $\sim 1500 \text{ m}^2/\text{g}$



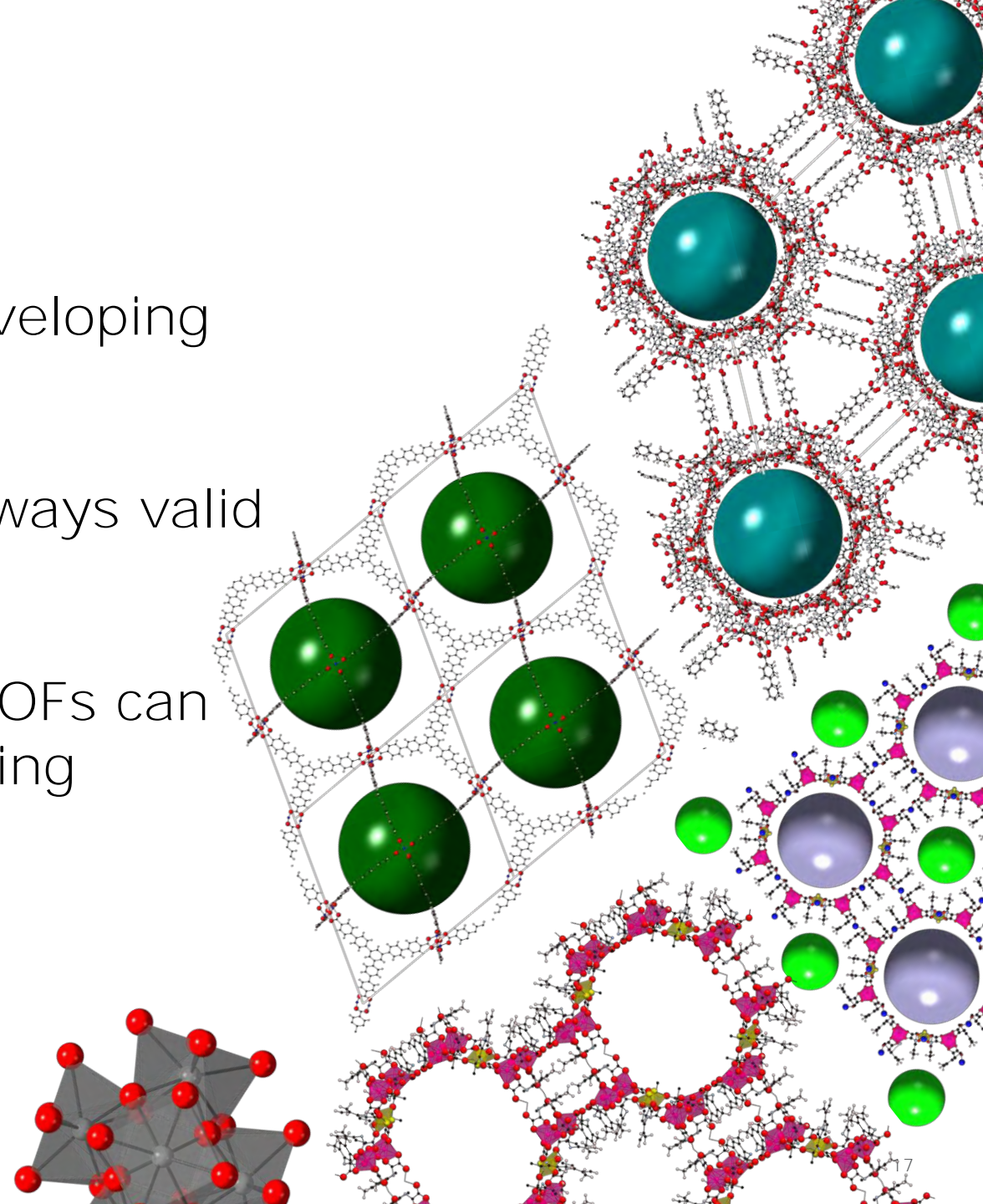
Scale-up: CPO-27-Ni

- 10 kg CPO-27-Ni
- Used in heat pump and desalination demonstrator unit in Egypt



Summary

- Reducing raw materials cost key to developing large scale synthesis
- Conventional scale-up methods not always valid
 - Chemistry of MOFs is important
- Commercial large scale synthesis of MOFs can be achieved with the right understanding



Acknowledgments

JM

Felicity Massingberd-Mundy

Timothy Johnson

Stephen Poulston

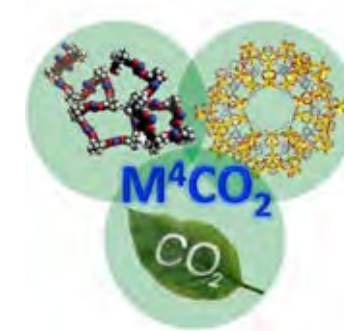
New Applications Group – Sonning

Catalyst Research Group – Chilton

UNIZAR

Joaquin Coronas

Magdalena Malankowska



adam.deacon@matthey.com

JM

The research leading to these results has received funding from the European Union Seventh Framework Programme (FP7/2007-2013) under grant agreement n° 608490 (project M⁴CO₂), grant agreement n° 685727 (project ProDIA) and under grant agreement No 760944 (MEMBER project)

WE
CAN DO
SO MUCH
TOGETHER

INTERNATIONAL WORKSHOP ON CO₂ CAPTURE AND UTILIZATION
TU/E - EINDHOVEN - 16-17 FEBRUARY 2021

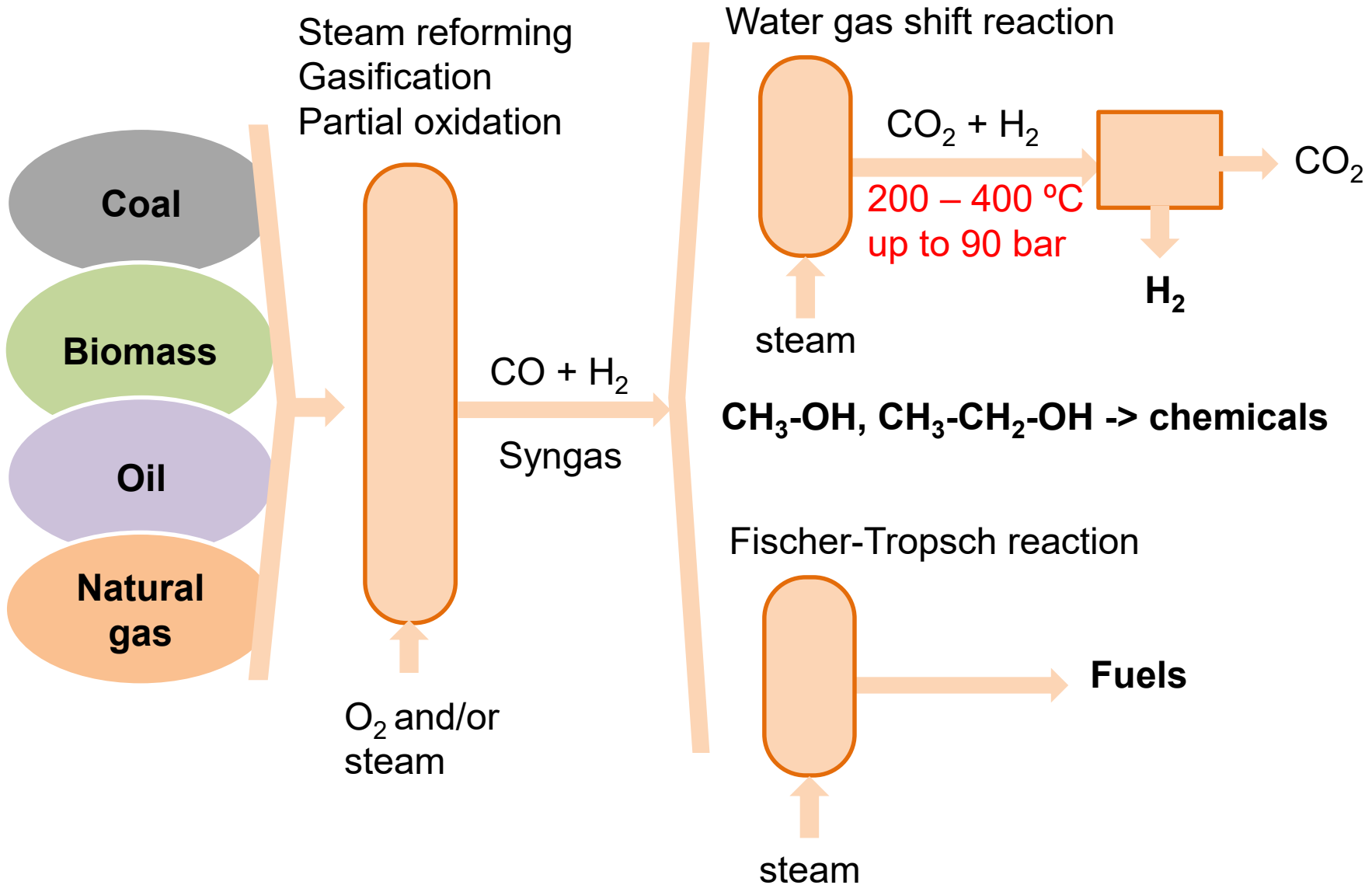
PBI based mixed matrix hollow fiber membranes for pre-combustion CO₂ capture

Dr Miren Etxeberria Benavides
TECNALIA

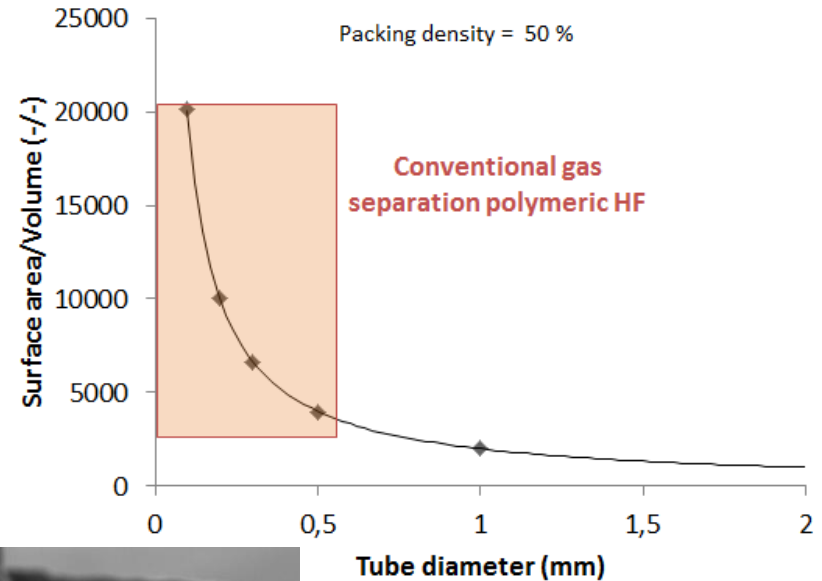


Pre-combustion CO₂ capture

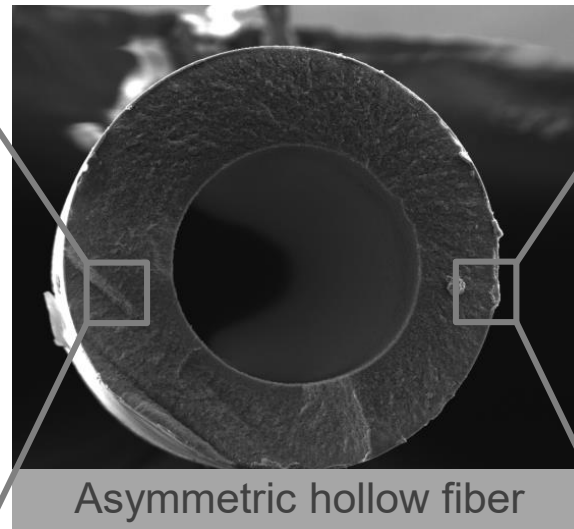
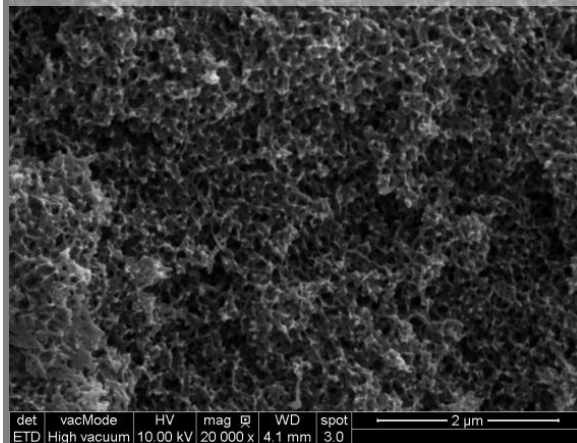
Chemical transformations before combustion = pre-combustion carbon capture



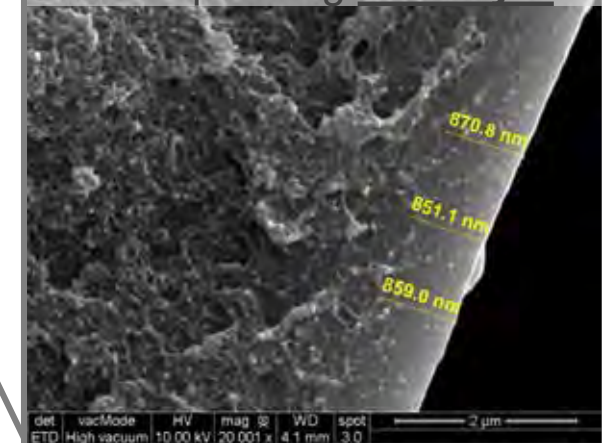
HOLLOW FIBER MEMBRANES



Highly porous support



Very thin and dense separating skin layer



Membrane Development Strategy

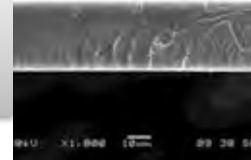
Defining target performance



Material development
and/or selection



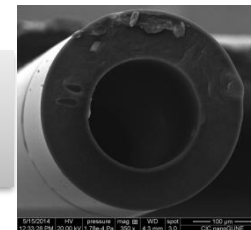
Dense film preparation and
characterization



*Intrinsic separation properties
Permeability and selectivity*



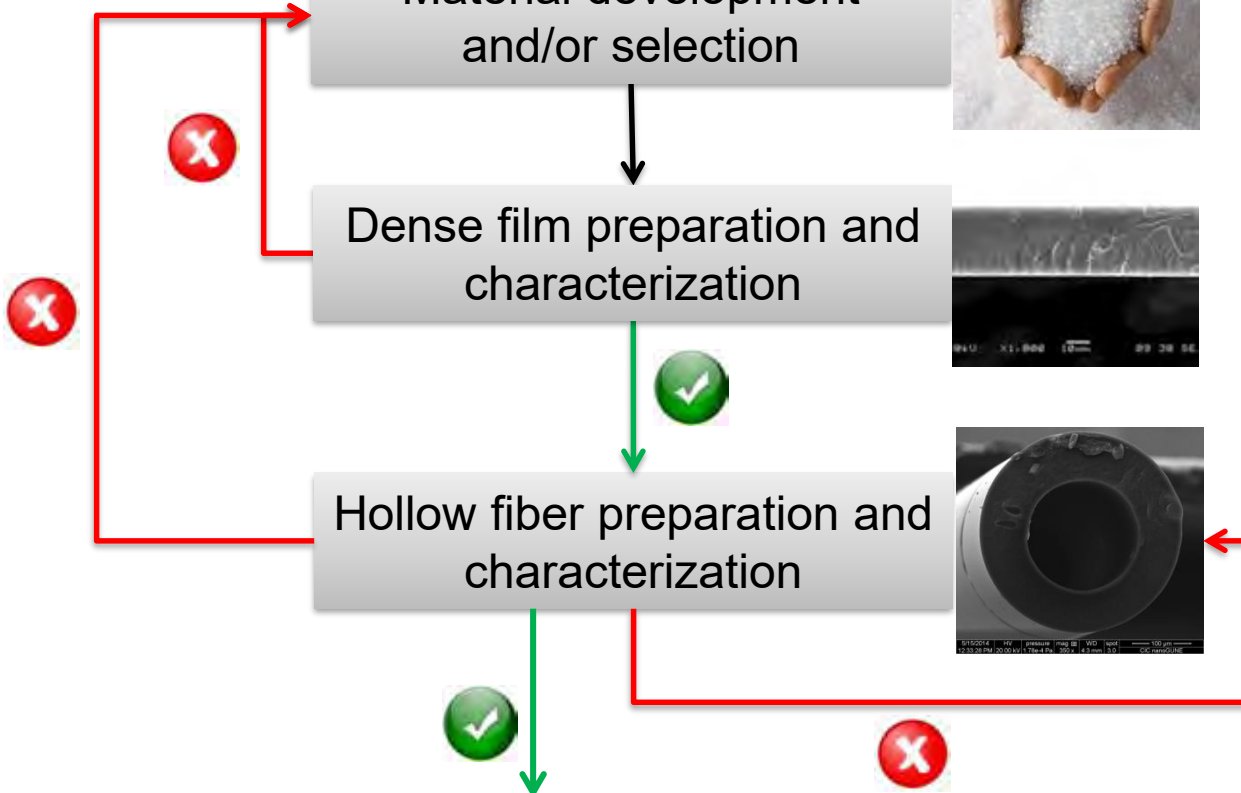
Hollow fiber preparation and
characterization



*Separation properties
Permeance and selectivity*

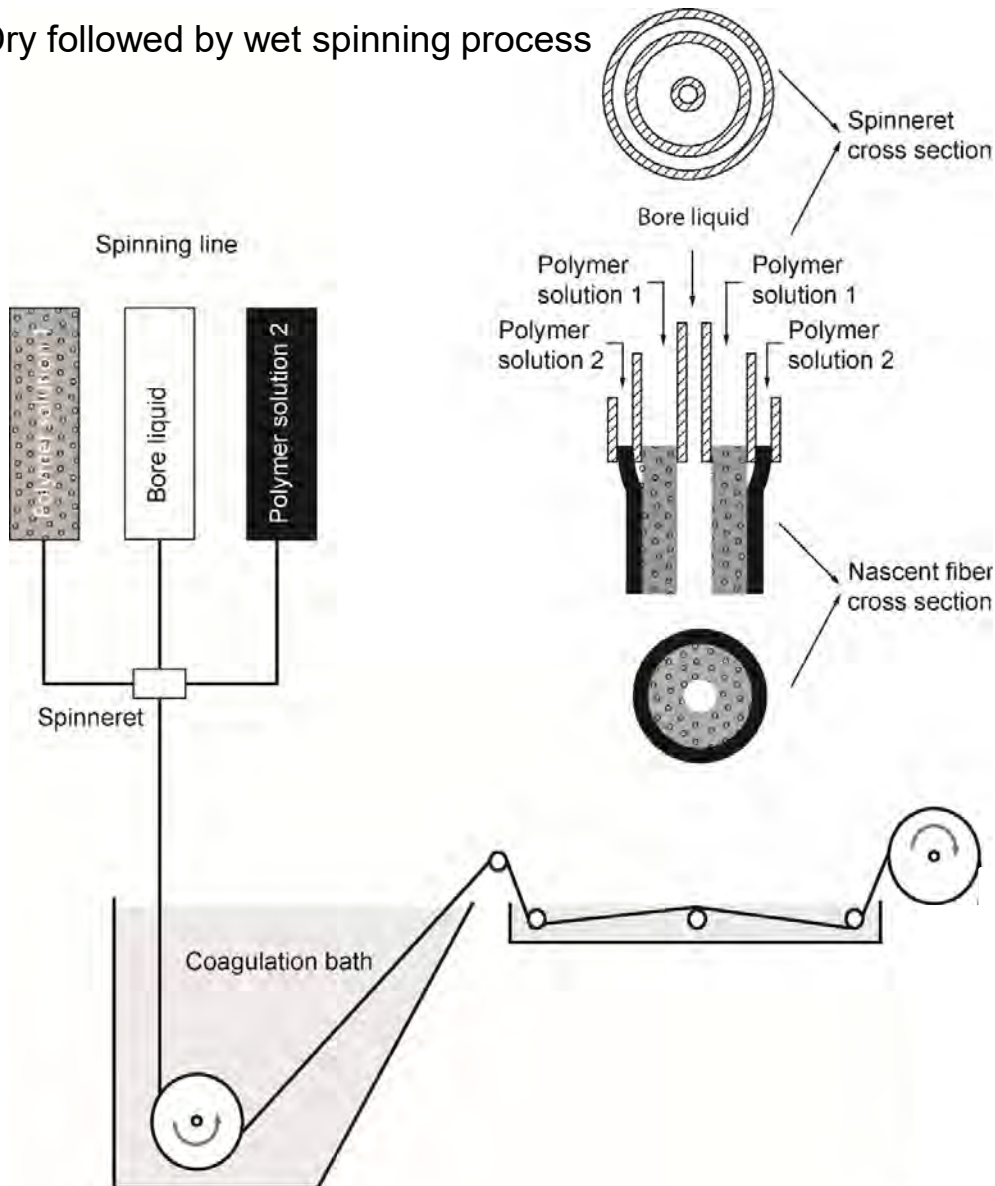


Possible to Scale-up, Prototype??



HOLLOW FIBER SPINNING

Dry followed by wet spinning process



Process parameters

Dope Composition
Dope Flow rate
Bore Composition
Bore Flow Rate
Spinning Temp
Coagulation Bath Temp
Air Gap height
Take-up rate
Room T
Humidity



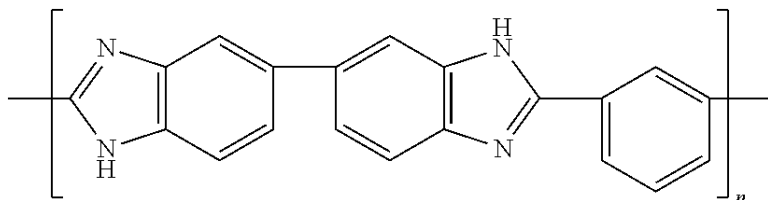
M⁴CO₂ project

The M⁴CO₂ project aims at developing and prototyping Mixed Matrix Membranes based on highly engineered Metal organic frameworks and polymers (M4) for energy efficient CO₂ capture in power plants and other energy-intensive industries both for pre-combustion and post combustion applications

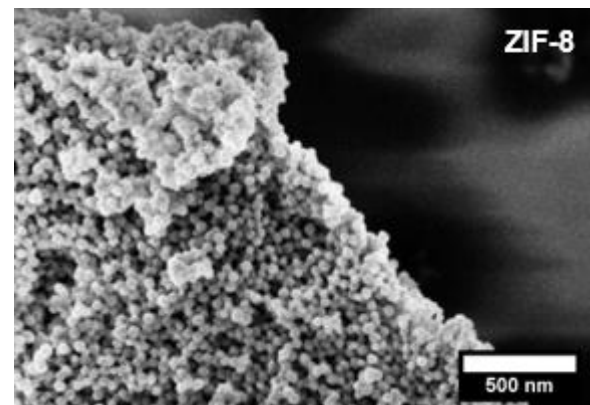
PBI Asymmetric hollow fiber



T_g 420°C



Filler: ZIF-8 powder

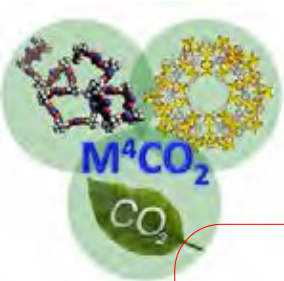


Particle size ~ <60 nm

Kinetic diameter (Å)

H₂ 2.89

CO₂ 3.3



H₂/CO₂ separation performance at 150°C

Single gas test (SG)

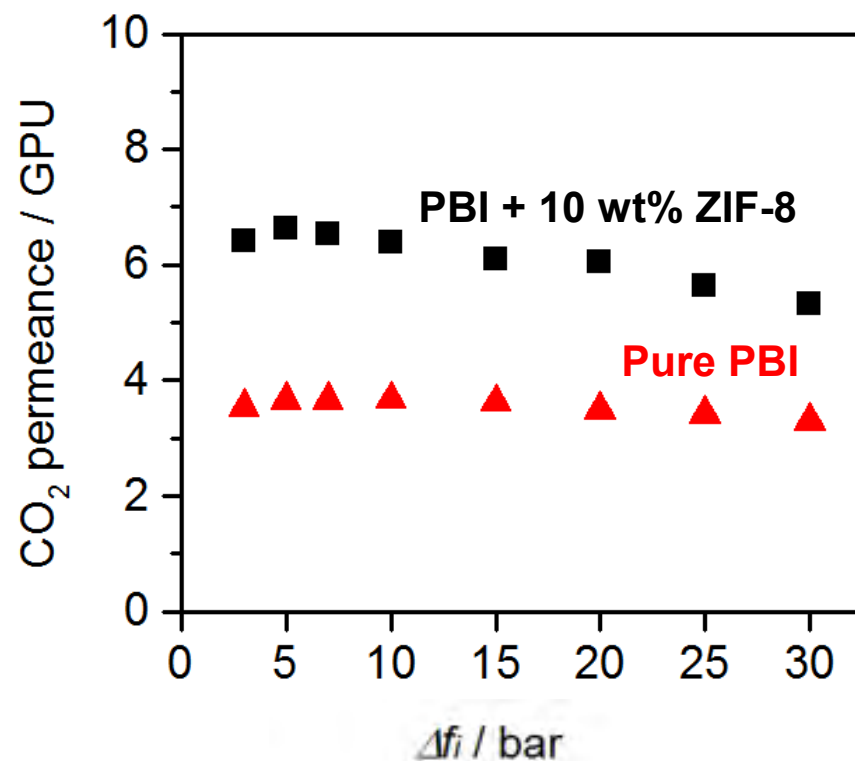
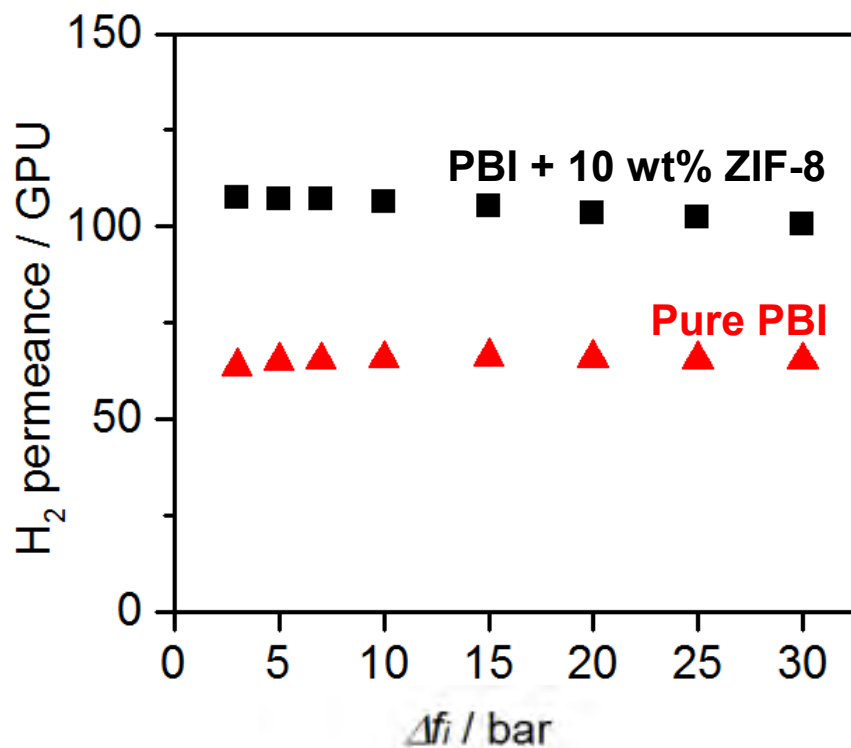
Pure PBI

63 GPU H₂; 17.8 H₂/CO₂

vs

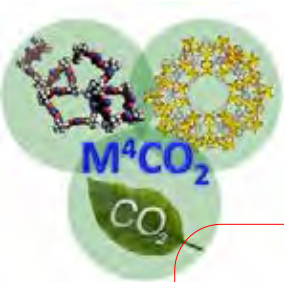
PBI + 10 wt% ZIF-8

107 GPU H₂; 16.6 H₂/CO₂



Dense PBI film
20 Barrer H₂; 20 H₂/CO₂

Journal of Membrane Science 461 (2014) 59–68



H_2/CO_2 separation performance at 150°C

Single gas test (SG)

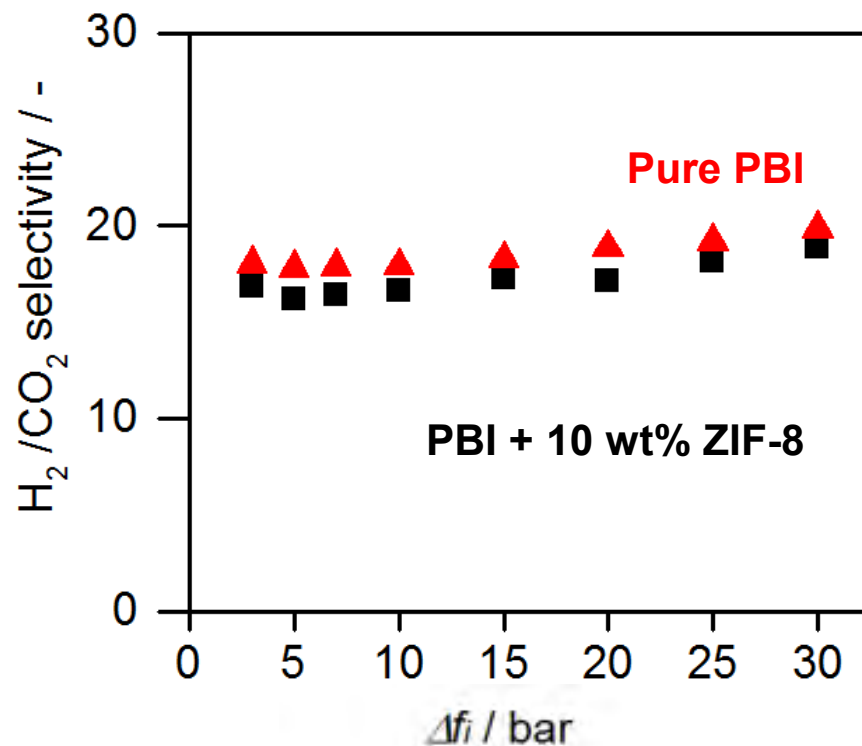
Pure PBI

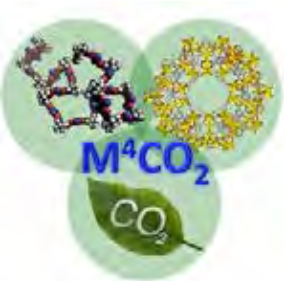
63 GPU H_2 ; 17.8 H_2/CO_2

vs

PBI + 10 wt% ZIF-8

107 GPU H_2 ; 16.6 H_2/CO_2



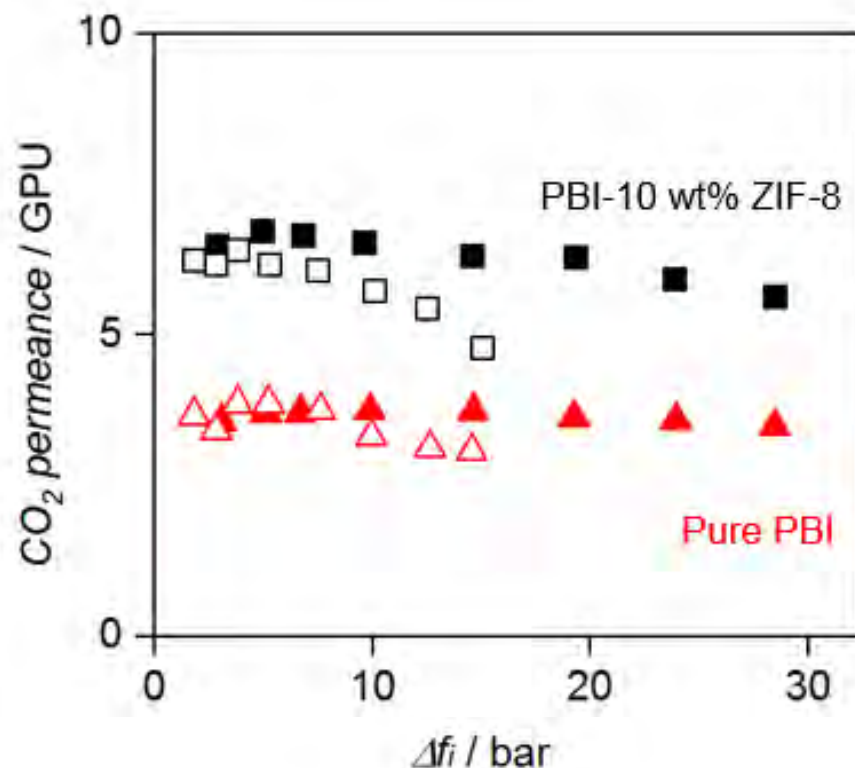
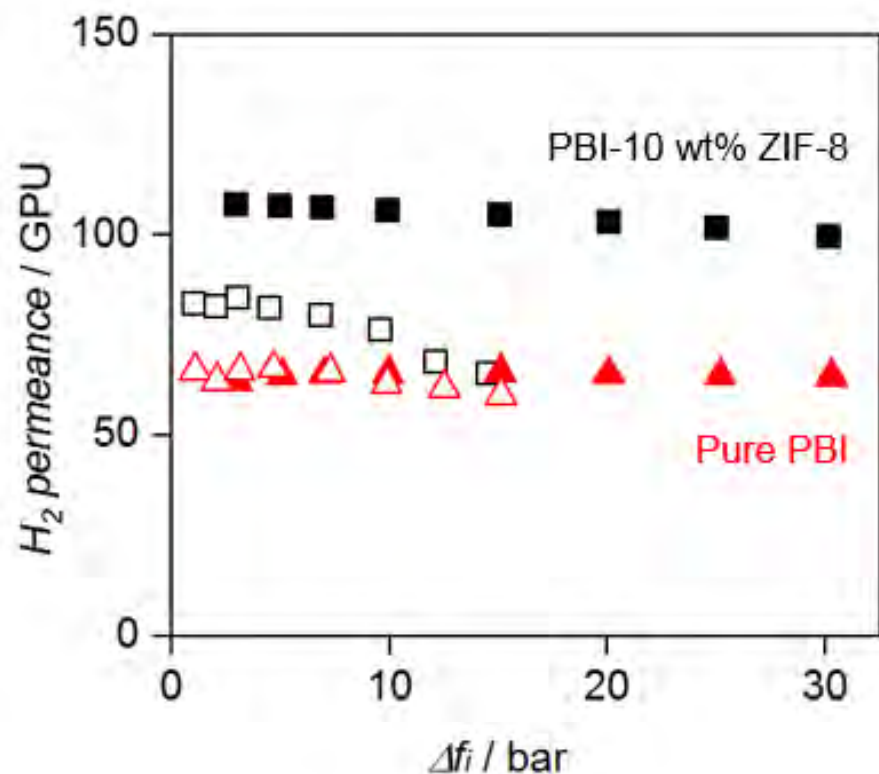


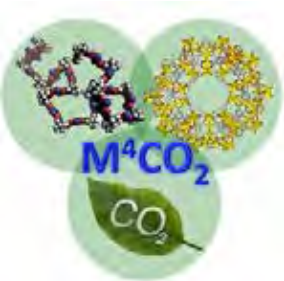
H₂/CO₂ separation performance at 150°C

Single gas test
(closed symbols)

vs

Mixed gas test (50/50 H₂/CO₂)
(open symbols)



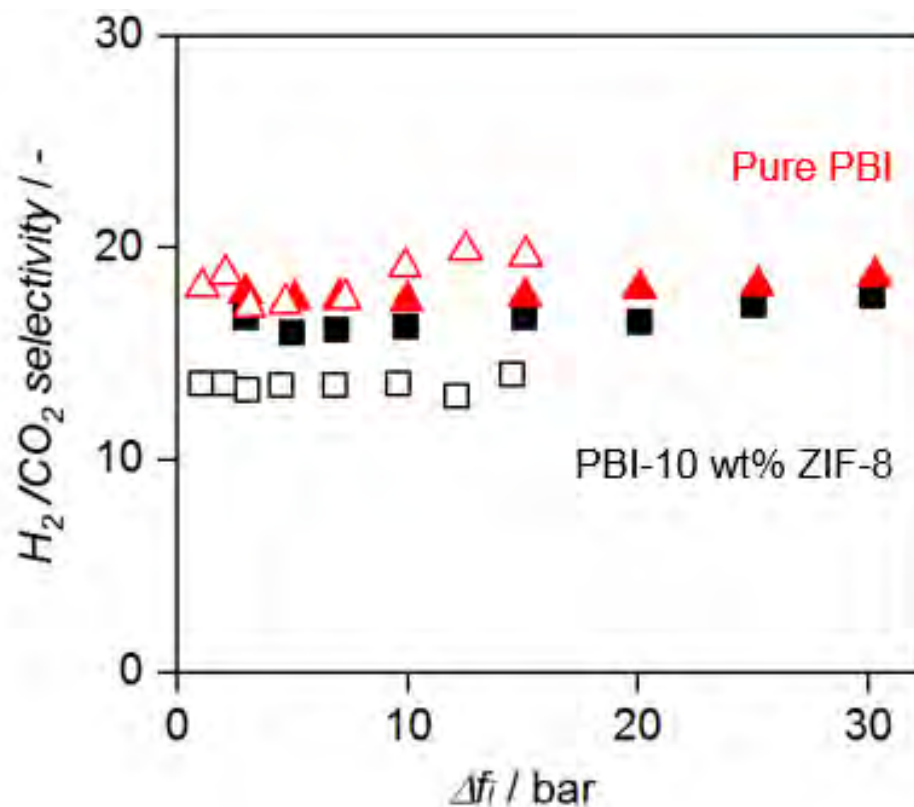


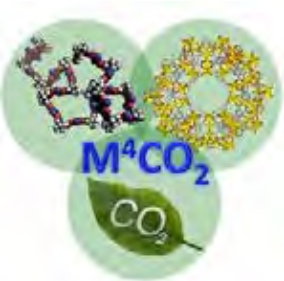
H₂/CO₂ separation performance at 150°C

Single gas test
(closed symbols)

vs

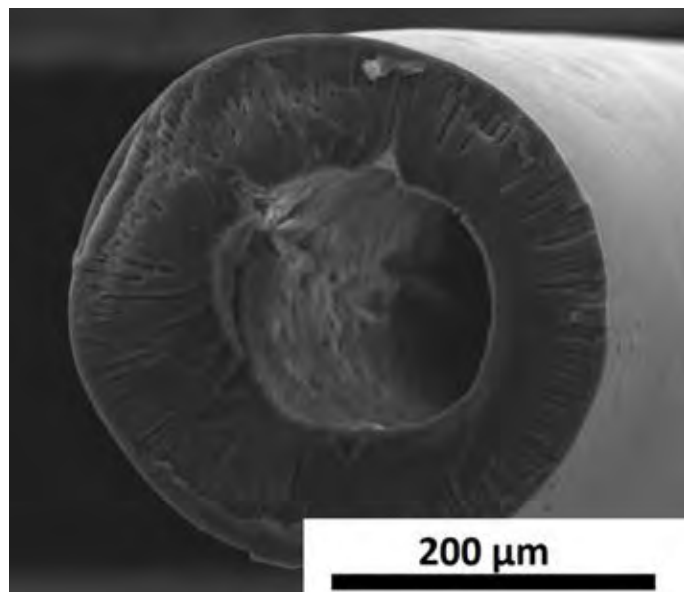
Mixed gas test (50/50 H₂/CO₂)
(open symbols)





M⁴CO₂ project

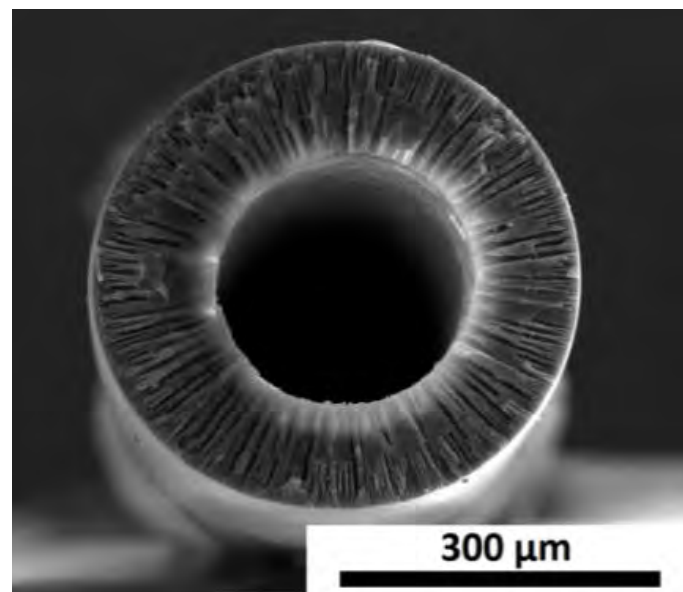
Pure PBI



Maximum take up rate: 20 m/min

OD/ID: 370 μm / 160 μm

PBI + 10 wt% ZIF-8



Maximum take up rate: 14 m/min

OD/ID: 470 μm / 250 μm

*Mechanical stability
(Mandrel test)*





MEMBER project

The key objective of the MEMBER Project is the **scale-up and manufacturing of advanced materials** (membrane and sorbents) and their demonstration at industrially relevant conditions in novel membrane based technologies that outperform current technologies for pre- and post-combustion CO₂ capture in power plants as well as H₂ generation with integrated CO₂ capture

Prototype A

Pre-combustion CO₂
capture

MMM hollow fiber
membranes

Prototype B

Post-combustion CO₂
capture

MMM hollow fiber
membranes

Prototype C

Pure H₂ production
with integrated CO₂
capture

Pd-based
membranes



MEMBER project

Objectives for PBI based membrane scaling up:

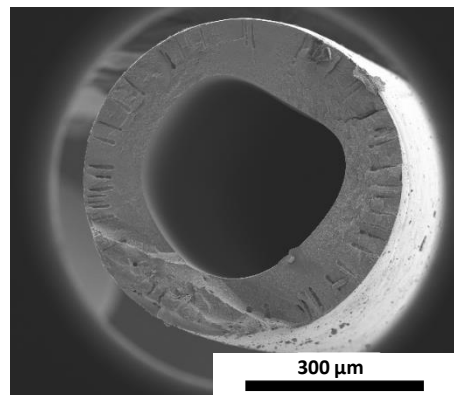
- Increase production rate (take-up rate)
- Decrease fiber dimensions
- Improve mechanical properties



MEMBER project

PBI

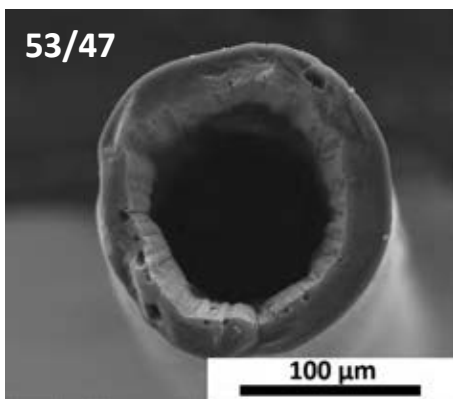
Take up rate: 6 m/min



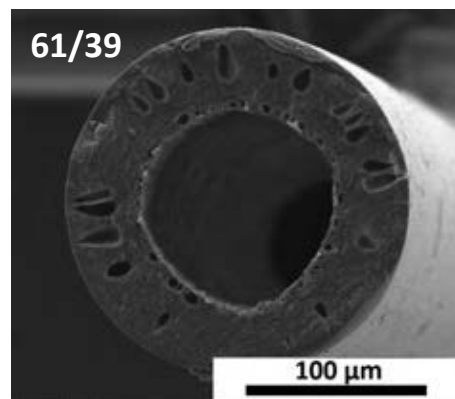
540 μm / 340 μm

PBI/PVP

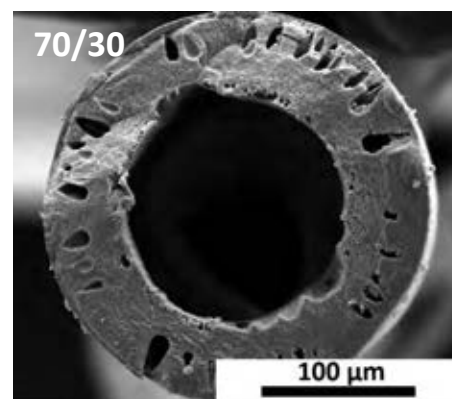
Take up rate: 25-50 m/min



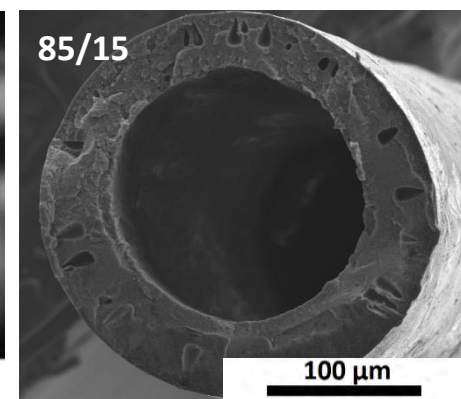
175 μm / 115 μm



195 μm / 110 μm



275 μm / 165 μm

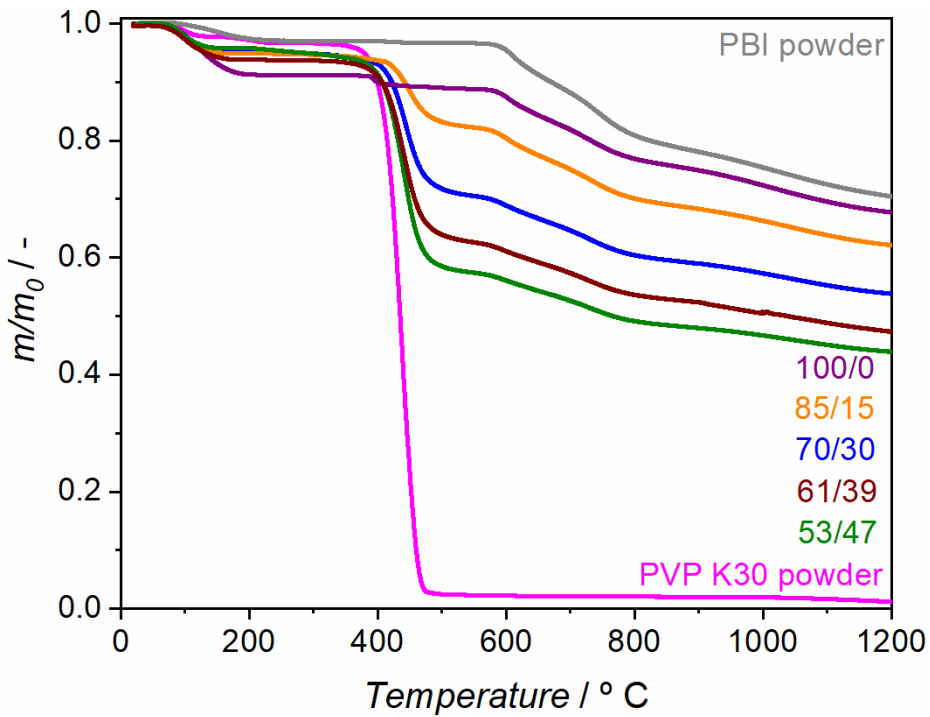


270 μm / 175 μm



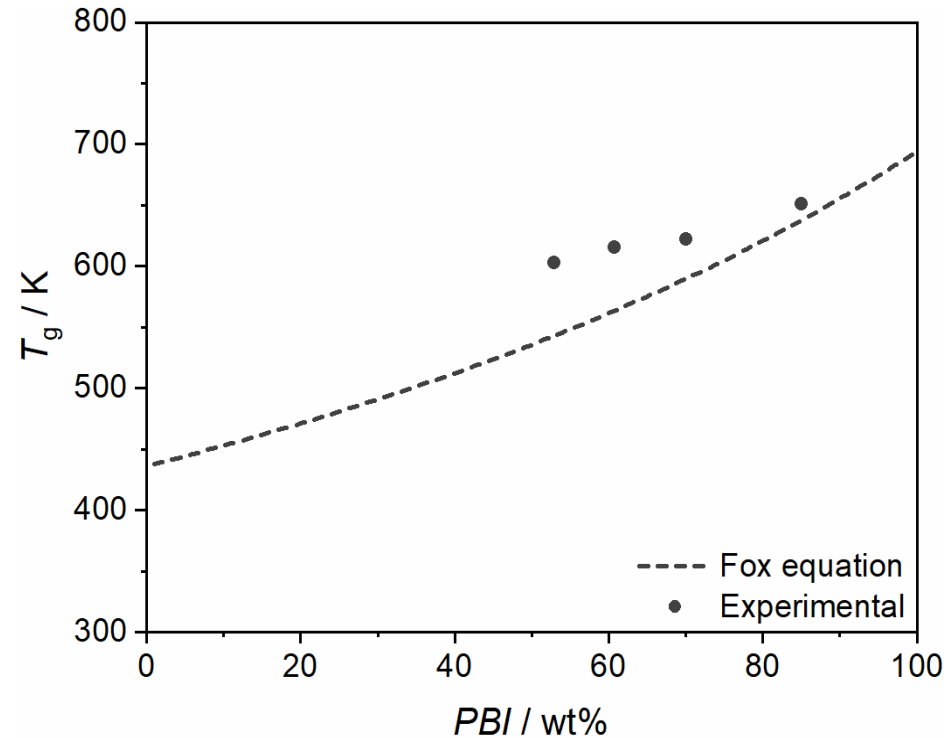
PBI/PVP blend fibers

TGA



Thermally stable up to $\sim 340^{\circ}\text{C}$

DSC



Hydrogen bonds between the N-H group of PBI and the C=O group of PVP



H₂/CO₂ separation performance at 150°C



Mixed gas test (50/50 H₂/CO₂)

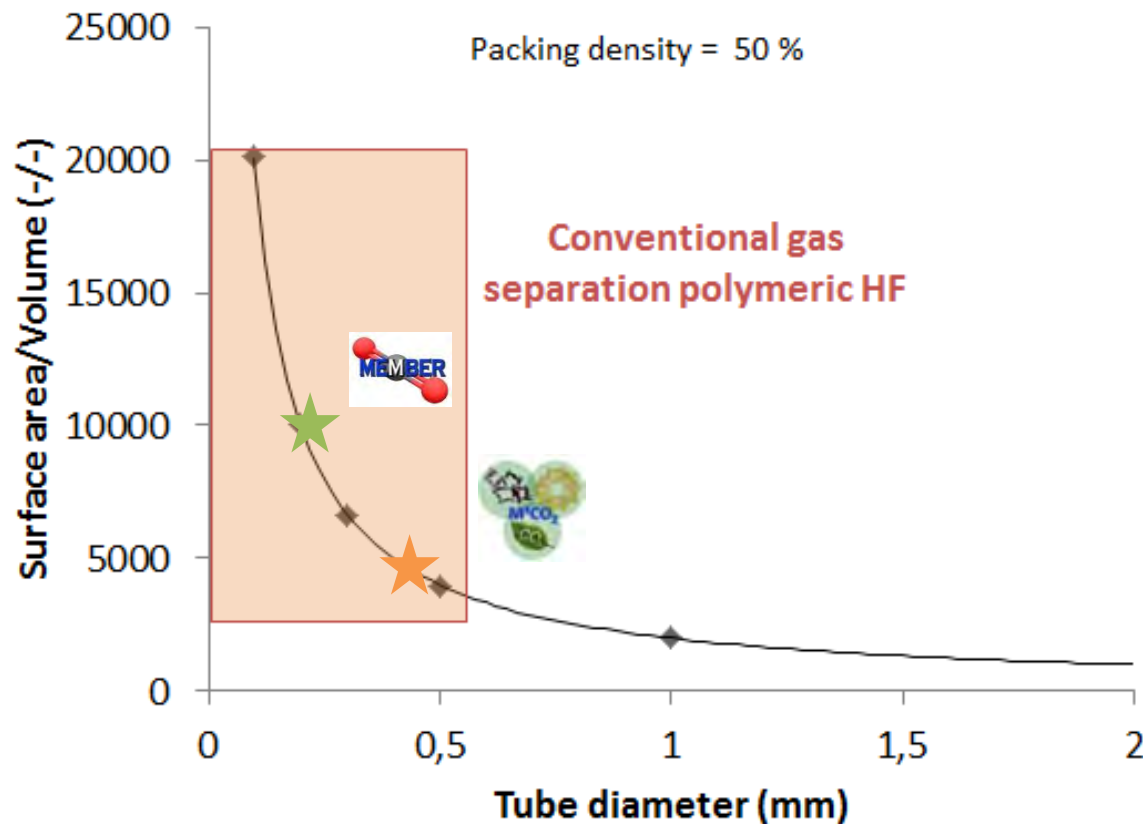
| | H ₂ Permeance (GPU) | H ₂ /CO ₂ Selectivity (-) | OD/ID (μm) | Take up rate (m/min) | Defect healing treatment (PDMS) |
|--------------|--------------------------------------|--|---------------|----------------------------|---------------------------------------|
| PBI/PVP | 56 | 16.6 | 275/165 | 25 | No |
| 10 wt% ZIF-8 | 121 | 10.2 | 290/175 | 25 | Yes |
| 5 wt% ZIF-8 | 31 | 17 | 270/175 | 25 | No |

*Mechanical stability
(Mandrel test)*



M⁴CO₂ project vs MEMBER project

| | Take up rate | Fiber diameter | Surface area/volume | PDMS coating | Mechanical stability (mandrel test) | PBI quantity required for m ² of fiber |
|--|--------------|----------------|---------------------|--------------|-------------------------------------|---|
|  | 14 m/min | 470 μm | ~ 5000 | Yes | X | ~30 g PBI / m ² |
|  | 25 m/min | 270 μm | ~ 10000 | No | ✓ ee | ~15 g PBI / m ² |



Conclusions

- PBI/ZIF-8 mixed matrix hollow fiber membranes:
 - ZIF-8 incorporation into the PBI polymer matrix strongly influences gas transport, specifically in mixed gas permeation
 - Improvement of fiber performance for H₂/CO₂ separation with filler addition at 150 °C is compromised at high operating feed pressures (30 bar)
- PBI/PVP blend asymmetric hollow fiber membranes
 - PVP addition: as spun fiber elasticity increases, industrially relevant take up rate values (25-50 m/min)
 - Mechanically robust and small diameter (< 300 µm) fibers have been successfully prepared
 - Blend fibers are thermally stable up to ~340 °C

Acknowledgement

This research has received funding from the European Union's Seventh Framework Programme (FP/2007-2013) under grant agreement number 608490 and Horizon 2020 research and innovation programme (H2020) under grant agreement n° 760944.



Thank you very much for your attention!

Questions



Visit our blog:
<http://blogs.tecnalia.com/inspiring-blog/>



www.tecnalia.com

INTERNATIONAL WORKSHOP ON CO₂ CAPTURE AND UTILIZATION

TU/e - EINDHOVEN - 16-17 FEBRUARY 2021

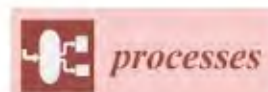
Session 1B (chairperson Camel Makhloufi)

- 11:15-11:35 Dr. M. Noponen and Dr. X. Sun - High temperature electrolysis and co-electrolysis
- 11:35-11:55 Prof. J Serra - Direct electrocatalytic conversion of CO₂ into chemical energy carriers in a co-ionic membrane reactor
- 11:55-12:15 Dr. V. Middelkoop - CO₂Fokus at a glance: CO₂ utilisation focused on DME production, via 3D printed reactor and solid oxide cell based technologies
- 12:15-12:35 Dr. M. Tsampas - The KEROGREEN CO₂ plasma route to CO and alternative fuels
- 12:35-12:55 Dr. G. Bonura - 3D-printing in catalysis: Development of efficient hybrid systems for the direct hydrogenation of CO₂ to DME

ORGANIZED BY



SPONSORED BY



HIGH TEMPERATURE ELECTROLYSIS AND CO-ELECTROLYSIS

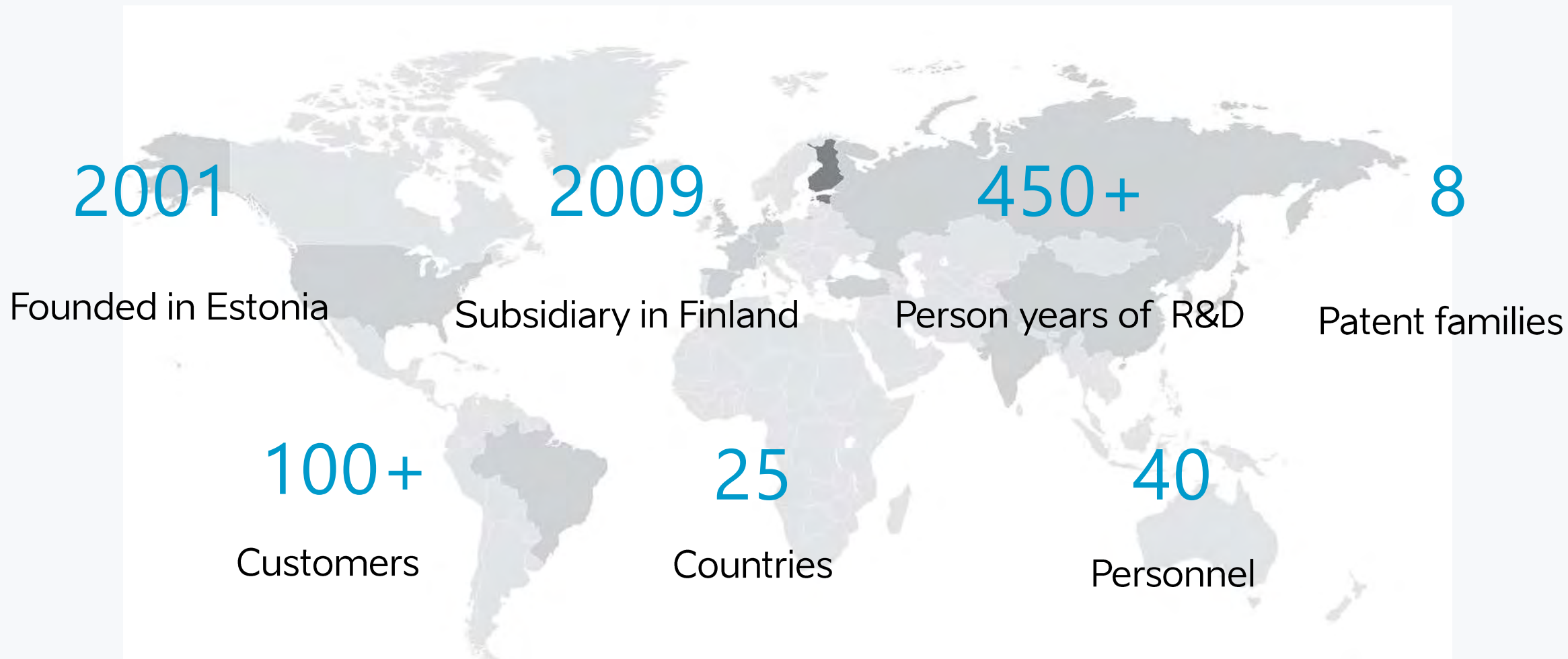
Matti Noponen, Timo Lehtinen (Elcogen)
Xiufu Sun (DTU)



PRESENTATION AGENDA

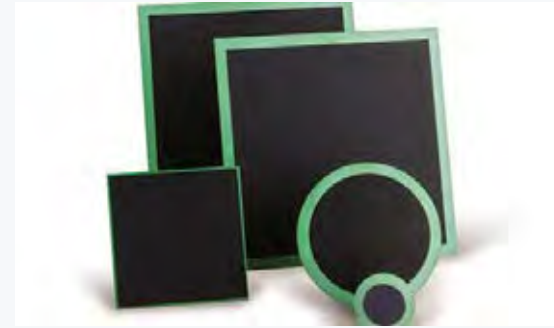
- Who We Are
- The Elcogen advantages
- C2FUEL project
- Acknowledgements

ELCOGEN AT A GLANCE



ELCOGEN PRODUCT FAMILIES

- World-leading planar, ceramic, anode-supported cells (ASC). Patent-protected
- Low operating temperature of 650°C enables longer lifetimes
- Cells and stacks made with low cost raw materials and designed for mass manufacturing
- Low cost and uniquely designed SOC's drive major cost reductions at the system level

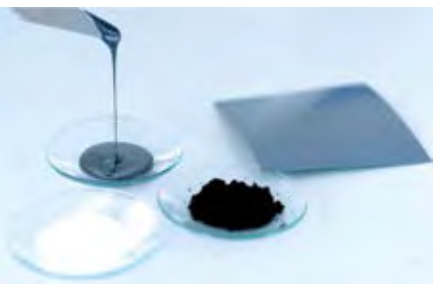


elcoCell



elcoStack

- Sustainable technologies for energy conversion and storage
- 230 researchers, technicians and PhD students
- Research spanning from fundamental investigations to component and prototype manufacture
- Focus on industrial collaboration and industrially relevant processes



Solid oxide cells



Polymer exchange membrane cells



Batteries

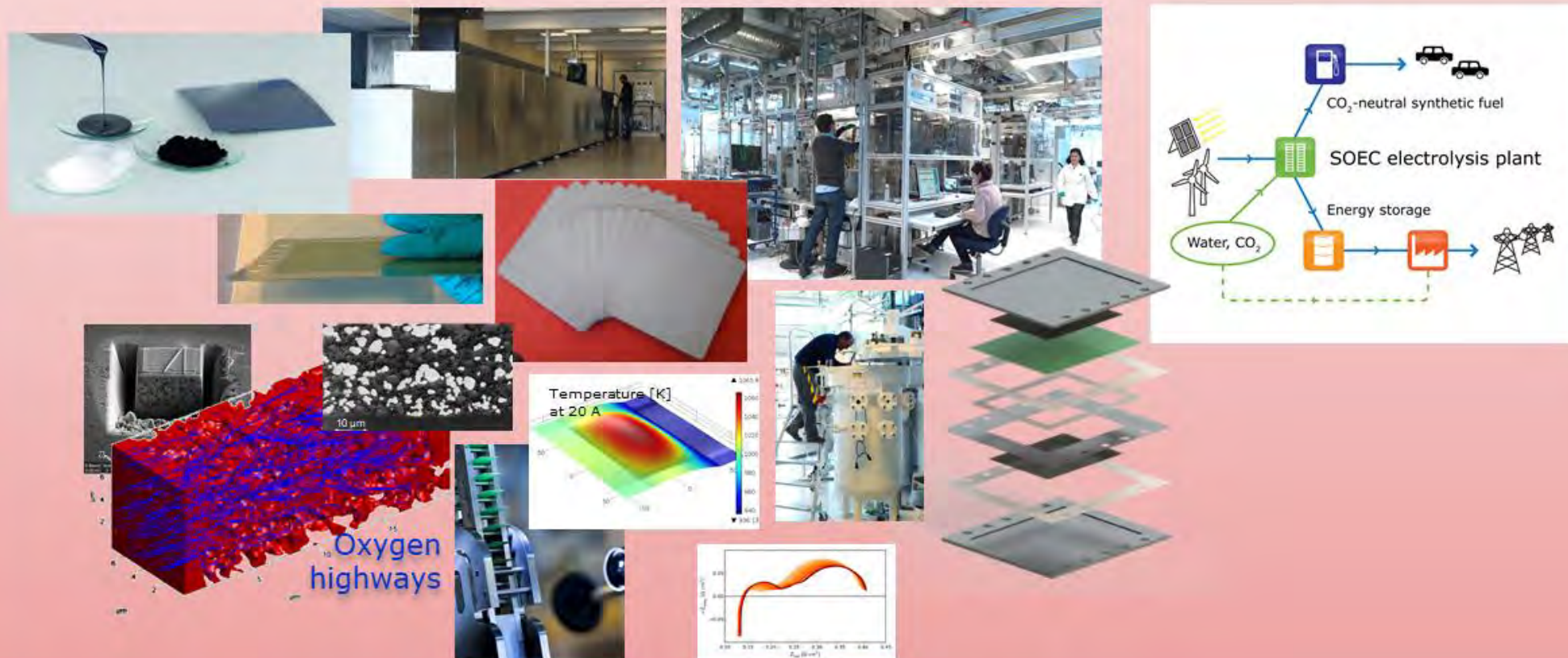


Gas separation

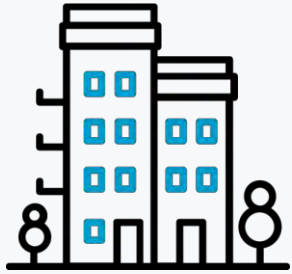


Solar cells

• Solid oxide cell at DTU Energy:



SINGLE TECHNOLOGY – MULTIPLE APPLICATIONS



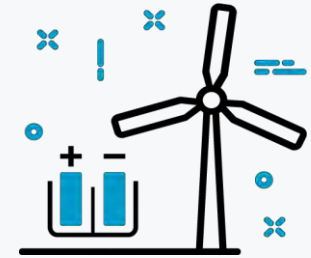
Residential: Single & Multi-Family



Commercial & Industrial CHP



Long-range Transportation



Electrolysers for Energy Storage and Power to Fuel

THE ELCOGEN ADVANTAGE



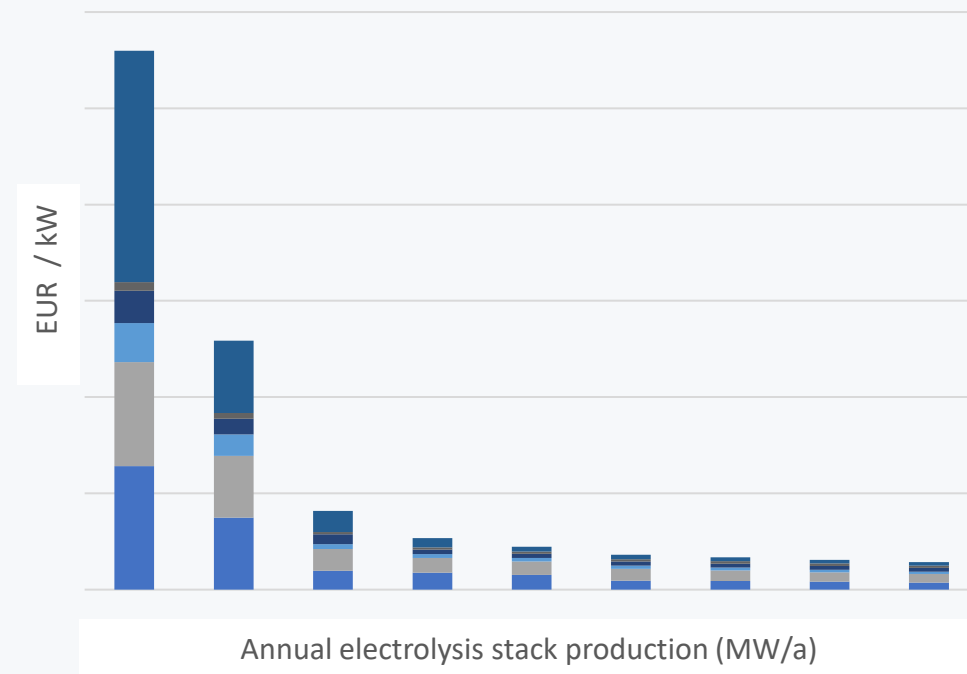
Elcogen is the SOC technology best positioned to address the 3 critical market barriers of Efficiency, Lifetime and Cost

Note: The targets in this chart apply to Elcogen stacks.

Note: ¹Elcogen's leading stack electrical efficiency of 74% (in fuel cell mode) has been measured with a 119-cell, commercial-grade 3kW stack using natural gas. ²Durability of stack design has been proven through long-term tests reaching 20,000 hours, indicating a total lifetime of 40,000 hours for the stack. ³Assumes a 1GW/year production capacity.

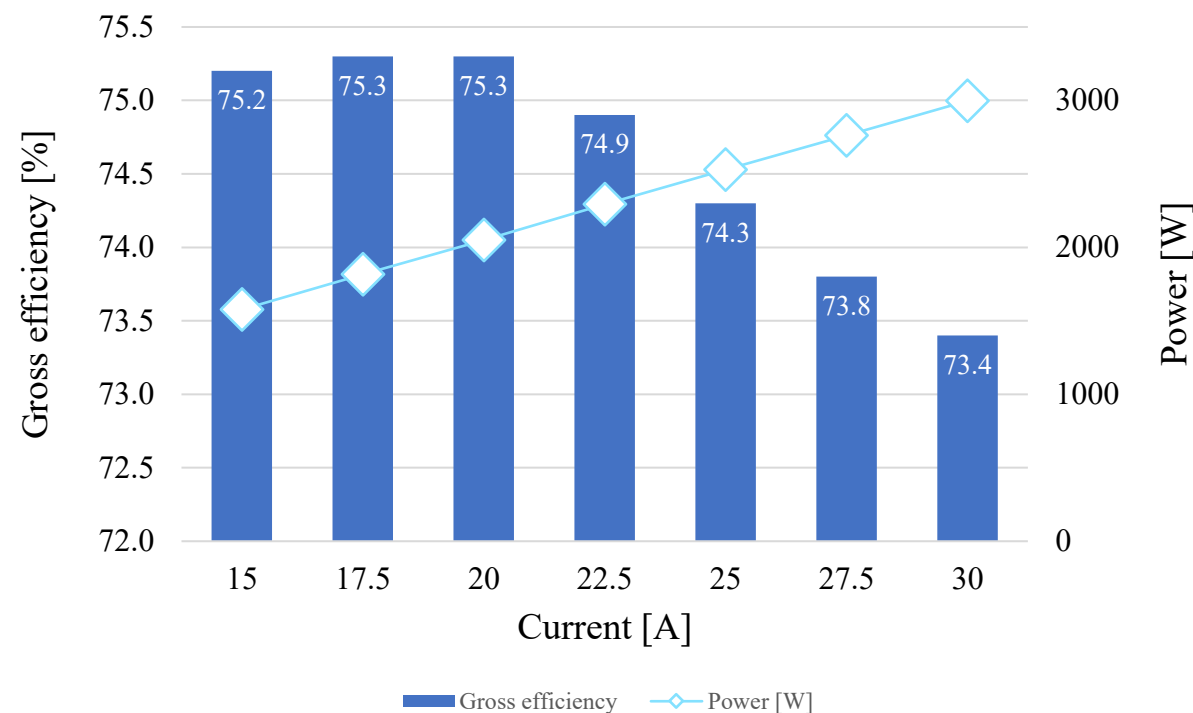
ELCOGEN ADVANTAGE – COST

- Elcogen's stack cost analysed closely with the manufacturing partners
- Production volume is the main driver in cost reduction
- Elcogen has started a factory project with the aim to introduce 50 MW/a production capacity



THE ELCOGEN ADVANTAGE – EFFICIENCY (FUEL CELL)

- Ultra high energy conversion efficiencies are achieved with commercial E3000 stacks
- Elcogen stacks exceed 75 % efficiencies already at 600 °C (LHV, NG)
- The efficiency is enabled by unique, patent protected unit cell and stack designs

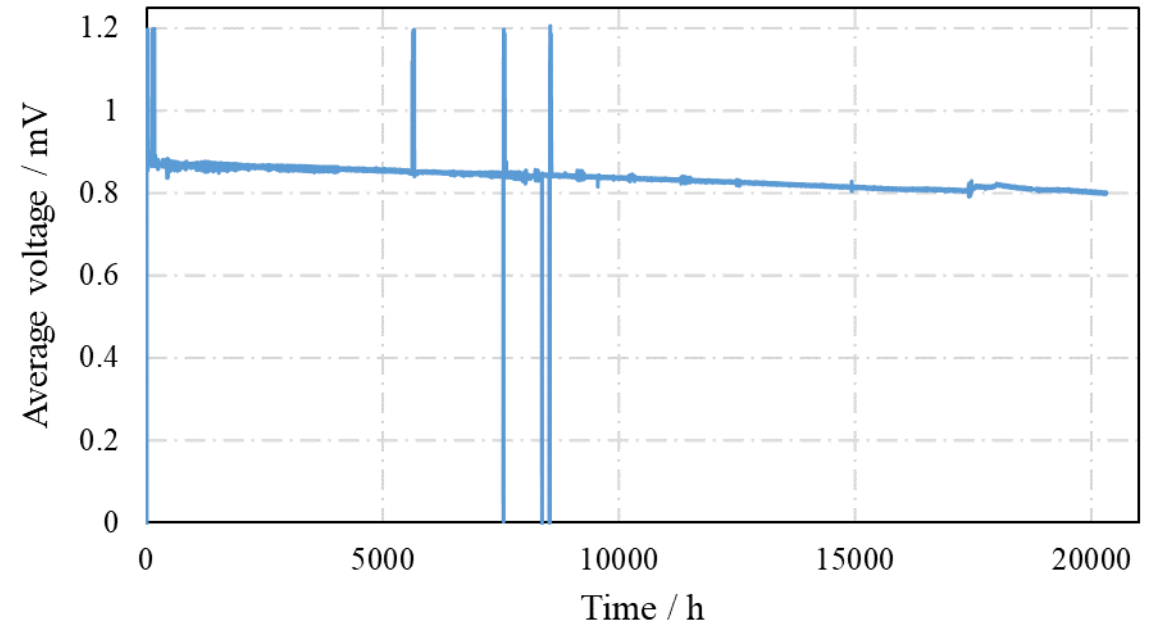


TEST CONDITIONS

| | |
|------------------------------|-------------|
| Stack inlet temperature | 590 °C |
| Fuel | Natural gas |
| Anode off gas recycle (sim.) | 70 % |
| Air flow | 330 NI/min |

THE ELCOGEN ADVANTAGE – LIFETIME (FUEL CELL)

- Stack lifetime testing conducted in a real fuel cell systems
- Ongoing tests exceeding 20 000 hours
- Degradation rate linear with constant slope of $15 \text{ m}\Omega\cdot\text{cm}^2 / 1000 \text{ h}$ (i.e. $0.4 \% / 1000 \text{ h}$)
- By assuming linear degradation, Elcogen stack technology has 40 000 hours lifetime expectation



TEST CONDITIONS

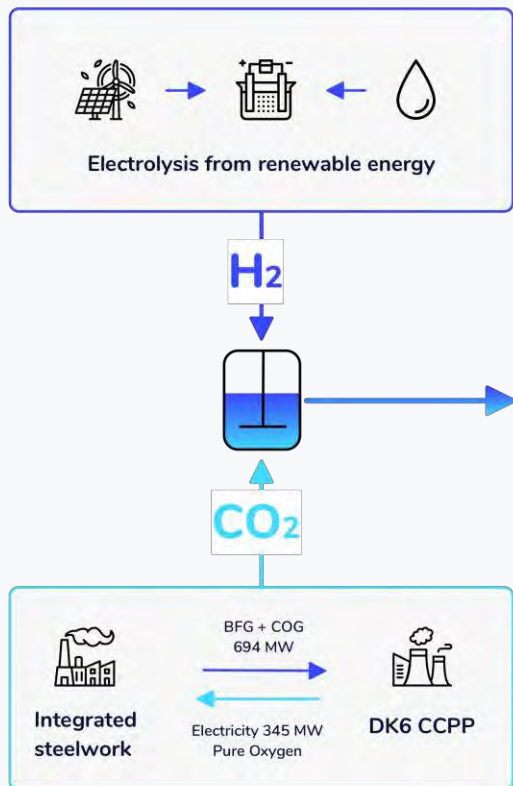
| | |
|-------------------------|-------------|
| Stack inlet temperature | 590 °C |
| Fuel | Natural gas |
| Fuel utilization | 60 % |
| Steam-to-carbon ratio | 2.2 |
| Oxygen utilization | 20 % |

A EUROPEAN RESEARCH & INNOVATION PROJECT

- This project has received funding from the European Union's Horizon 2020 research and innovation programme under grant agreement No 838014
- The project started on July 1st 2019, and will last 4 years (until 2023)
- Elcogen role is to provide high temperature steam electrolysis technology for the project (cell, stack and system)
- DTU role is to conduct cell and stack characterization and stack modelling in the project



C2FUEL OVERALL TARGET: 2.4 MILLION TCO₂ AVOIDED PER YEAR



Formic acid as Hydrogen carrier

Decreasing the electricity footprint during boat charging on docks

C2FUEL Output

- 2,4 million ton of FA
- 100 000 ton of green hydrogen
- 1,8 TWh of green electricity
- Seasonal storage using 3.6 TWh of renewable electricity



Dimethylether as Maritime and truck fuel

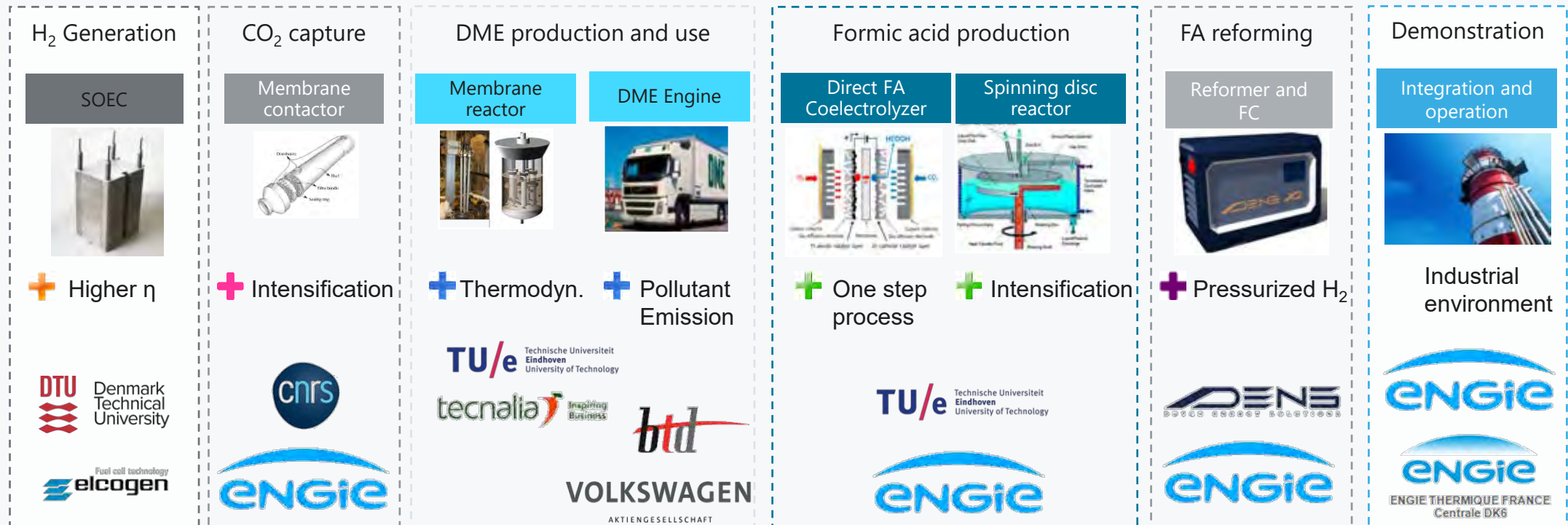
Displacing fossil fuel emission from power plant and decreasing harbor mobility footprint

C2FUEL Output

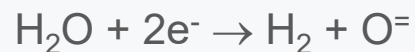
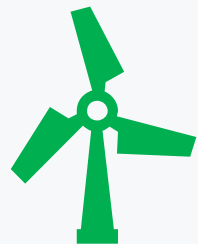
- 1,2 million ton of DME
- 320 000 ton of green H₂ produced using
- 11 TWh of renewable electricity

FROM TRL 3 TO TRL 6 ON INNOVATIVE TECHNOLOGIES

- C2FUEL partnership covers the whole value chain of conversion of CO₂ for carbon-captured fuel production.



STEAM ELECTROLYSIS VS CO-ELECTROLYSIS



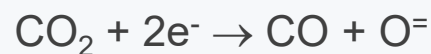
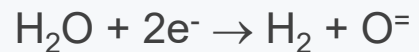
CO₂ capture

Reforming or other means

Synthesis gas

Liquid fuel synthesis

EFFICIENCY IMPROVEMENTS
THROUGH HT ELECTROLYSIS

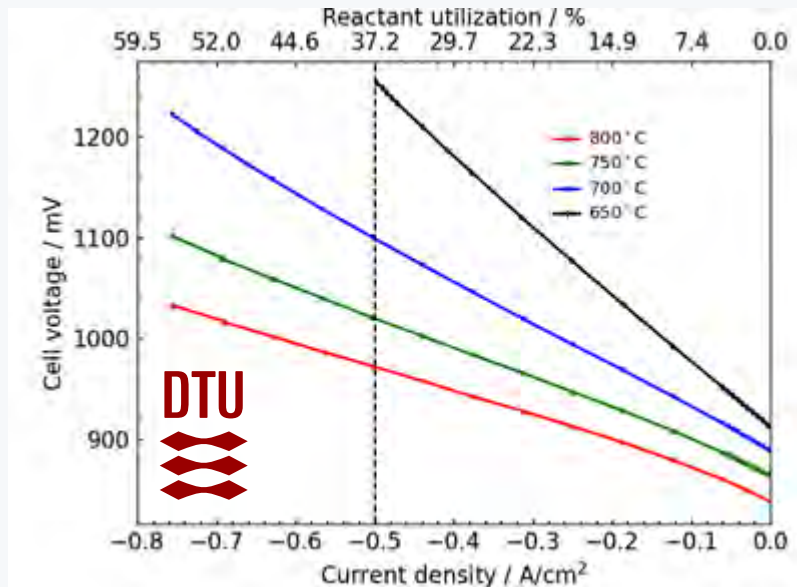


Synthesis gas

Liquid fuel synthesis

SIMPLIFIED PROCESS THROUGH
CO-ELECTROLYSIS

DETAILED CHARACTERIZATION OF UNIT CELLS

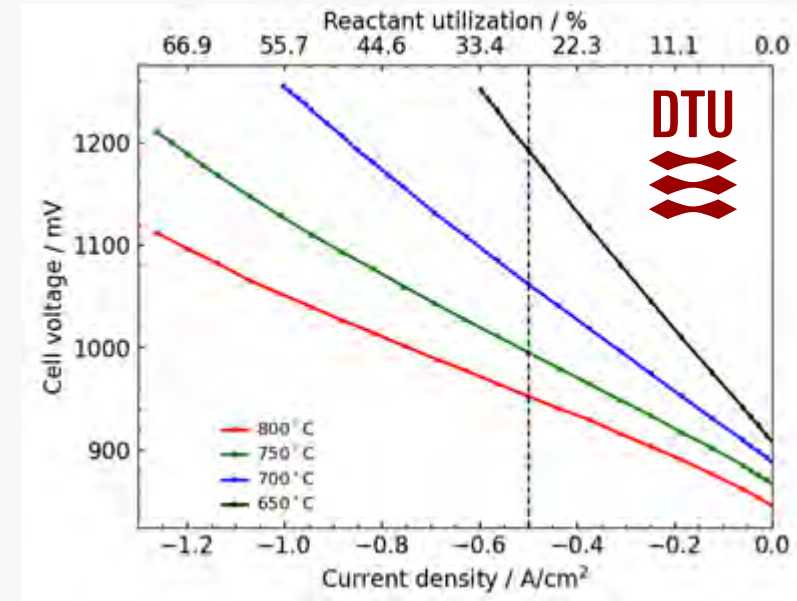


Steam electrolysis mode

| | |
|---|-----------------|
| Cathode flow rate | 13.4 l/h |
| Inlet composition [H ₂ O, CO ₂ , H ₂] | 90 %, 0 %, 10 % |

Specific energy consumption below 3.06 kWh/Nm³ (1.28 V) at relevant current densities

Outlet composition in equilibrium determined by pressure, inlet gas composition, and temperature, current

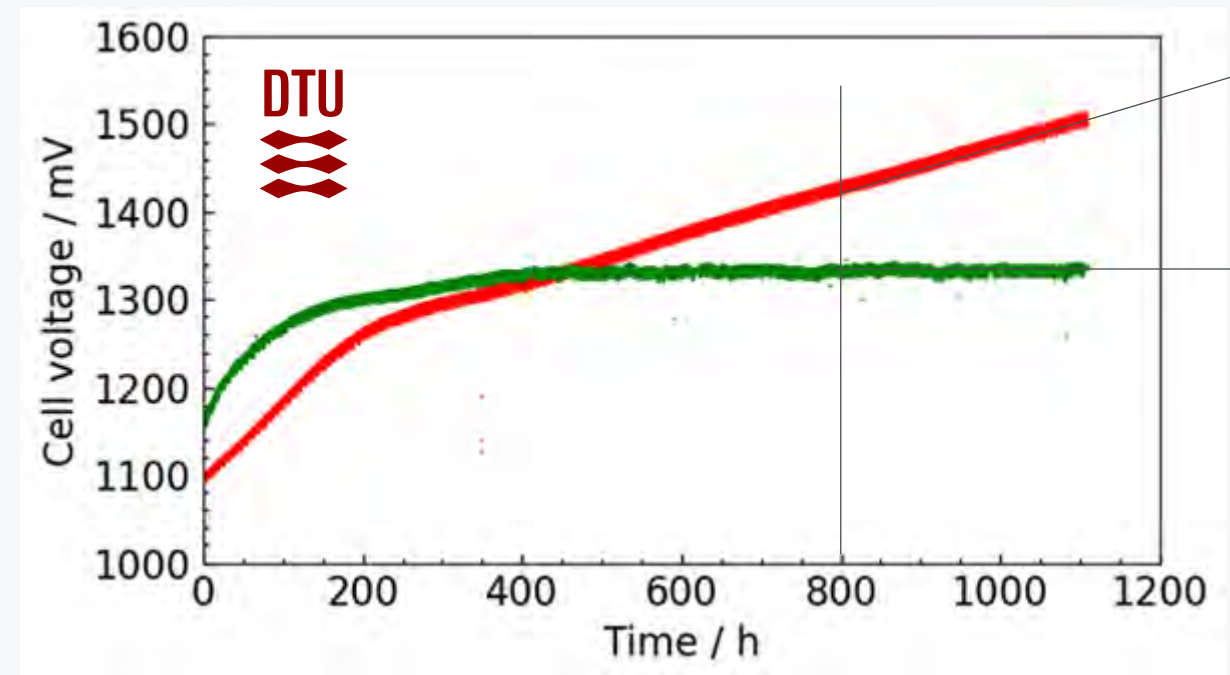


Co-electrolysis mode

| | |
|---|------------------|
| Cathode flow rate | 10 l/h |
| Inlet composition [H ₂ O, CO ₂ , H ₂] | 45 %, 45 %, 10 % |

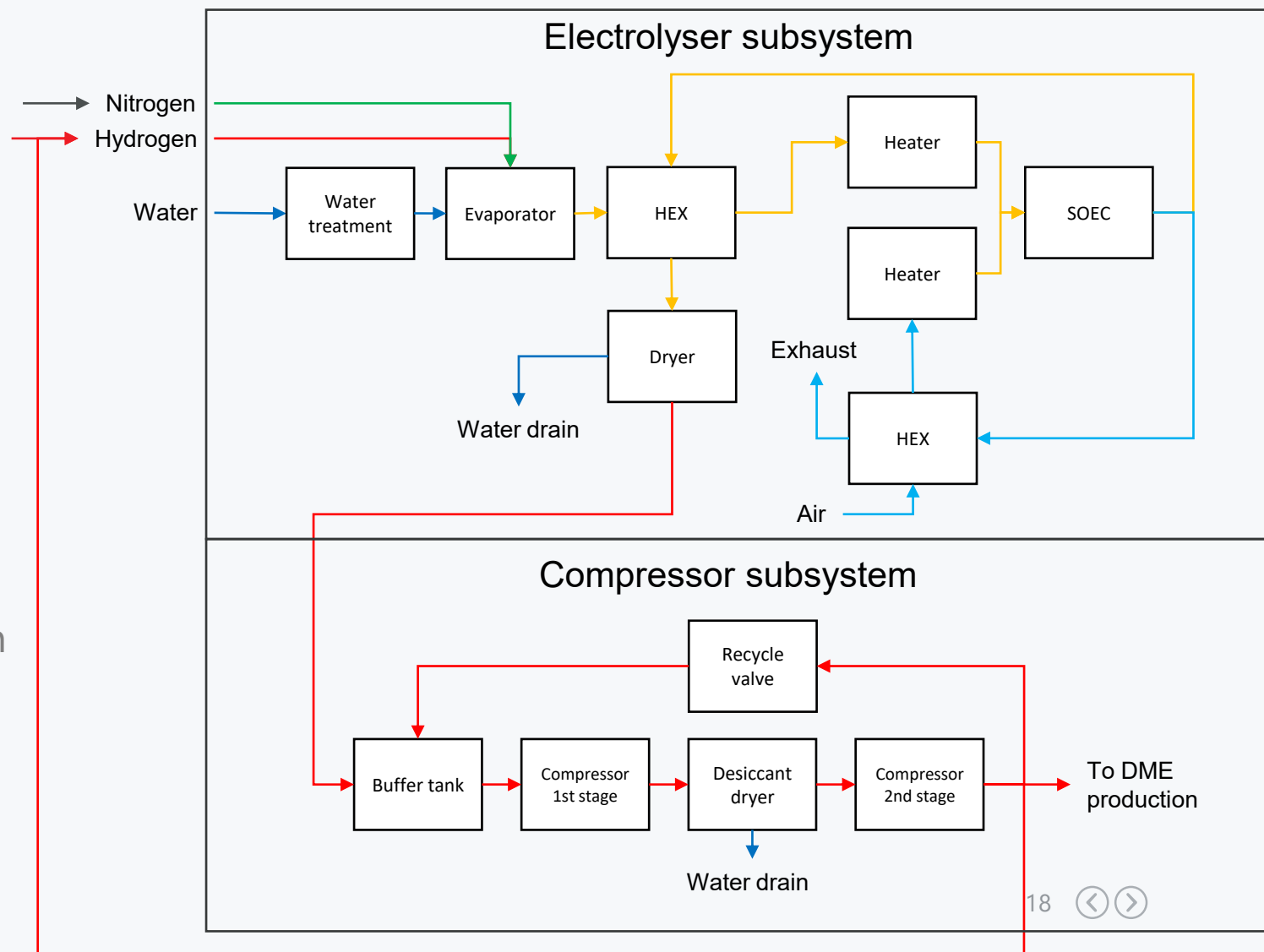
DEGRADATION TESTING AND LIFETIME LIMITING FACTORS

- Major focus on understanding lifetime limiting factors through long term experiments
- Example shows the importance for conducting the lifetime testing at different operation conditions
 - Test with different reactant utilizations
 - Degradation rate is changed from virtually zero ($1 \text{ mOhm.cm}^2/\text{kh}$) to rapid escalation ($510 \text{ mOhm.cm}^2/\text{kh}$)



SIMPLIFIED PI-DIAGRAM OF ELECTROLYSER DEMONSTRATOR

- SOE stack operation environment aimed to be designed as mild as possible
- Pressure level in stack as close to atmospheric as possible, pressurizing through diaphragm compressor
- Flow rates with large variation window
- Heat management via multiple mechanisms
- Hydrogen circulated back to stack inlet
- Water purification process highlighted in the process



ELECTROLYSER DEMONSTRATOR

- The electrolyser unit and compression system are installed into containers
- Containers are designed modular and can be operated independently
- Electrolysis system designed to produce 1Nm³/h of atmospheric pressure hydrogen from Type I water
- Compressor container system compresses produced hydrogen to 40 bar and dries it to -60°C dew point (ref. atm. pressure) equals to ~19 ppmVOL
- Containers will be installed outdoors at the DK6 site with other bricks of the C2FUEL project demonstration system



Layouts of compressor (left) and electrolyser (right) containers

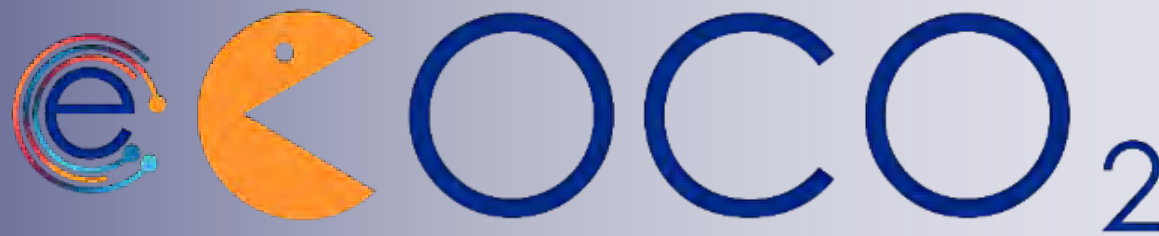
ACKNOWLEDGEMENTS



This project has received funding from the European Union's Horizon 2020 research and innovation programme under grant agreement No 838014.



THANK YOU FOR YOUR ATTENTION!



Direct electrocatalytic conversion of CO₂ into chemical energy carriers in a co-ionic membrane reactor

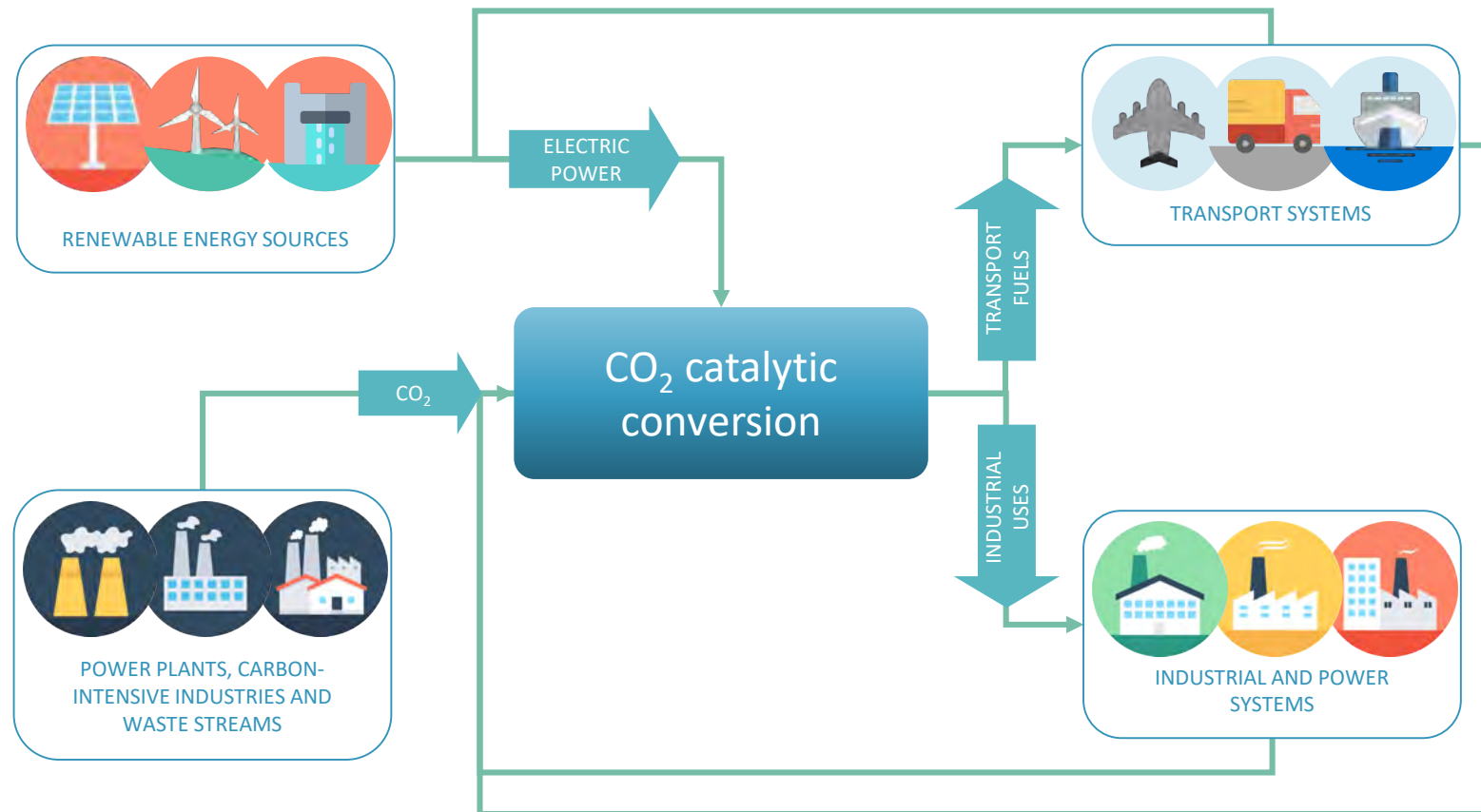
José M. Serra



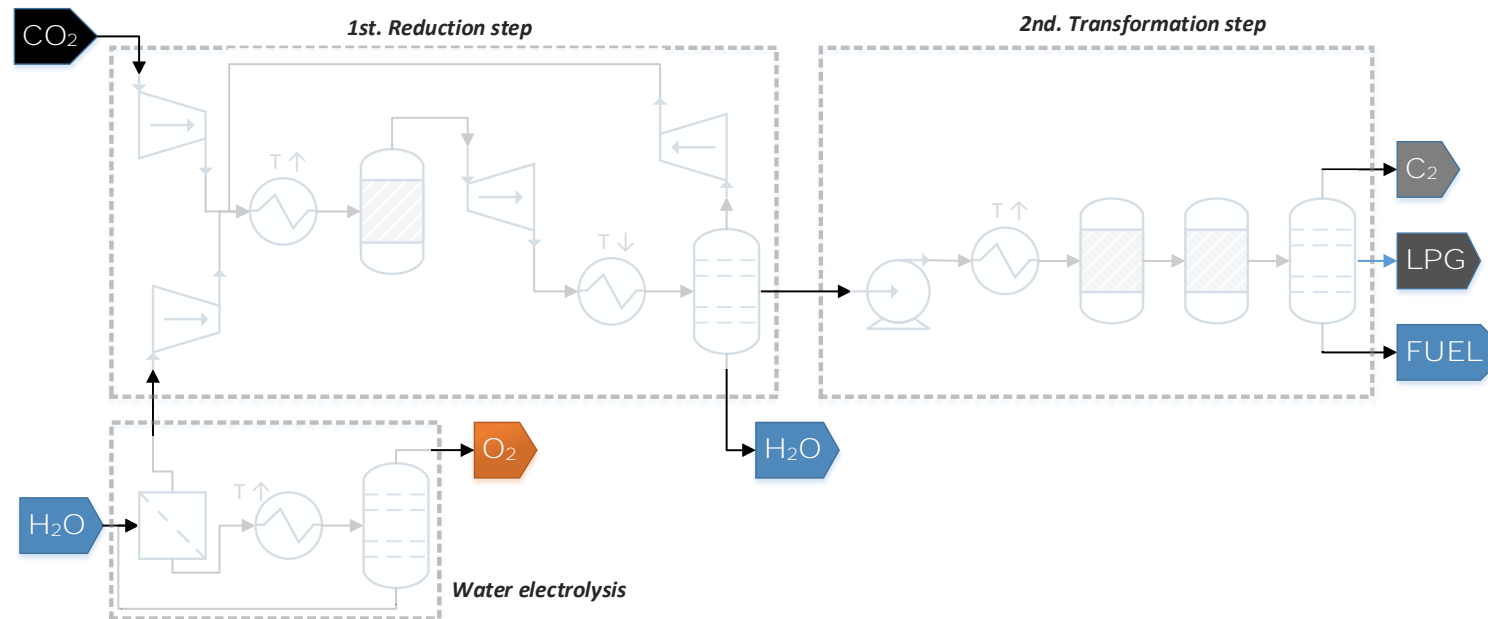
This project has received
European Union's Horizon 2020
research and innovation funding
under grant agreement
Nº 838077.

CO₂ catalytic conversion

combined solution for energy storage and carbon footprint reduction



Current CO₂-to-fuel technologies



Multi-step approach
involves a sequence of
separated processes



High costs
up to 300 €/ MWh CAPEX
and 750 €/MWh OPEX

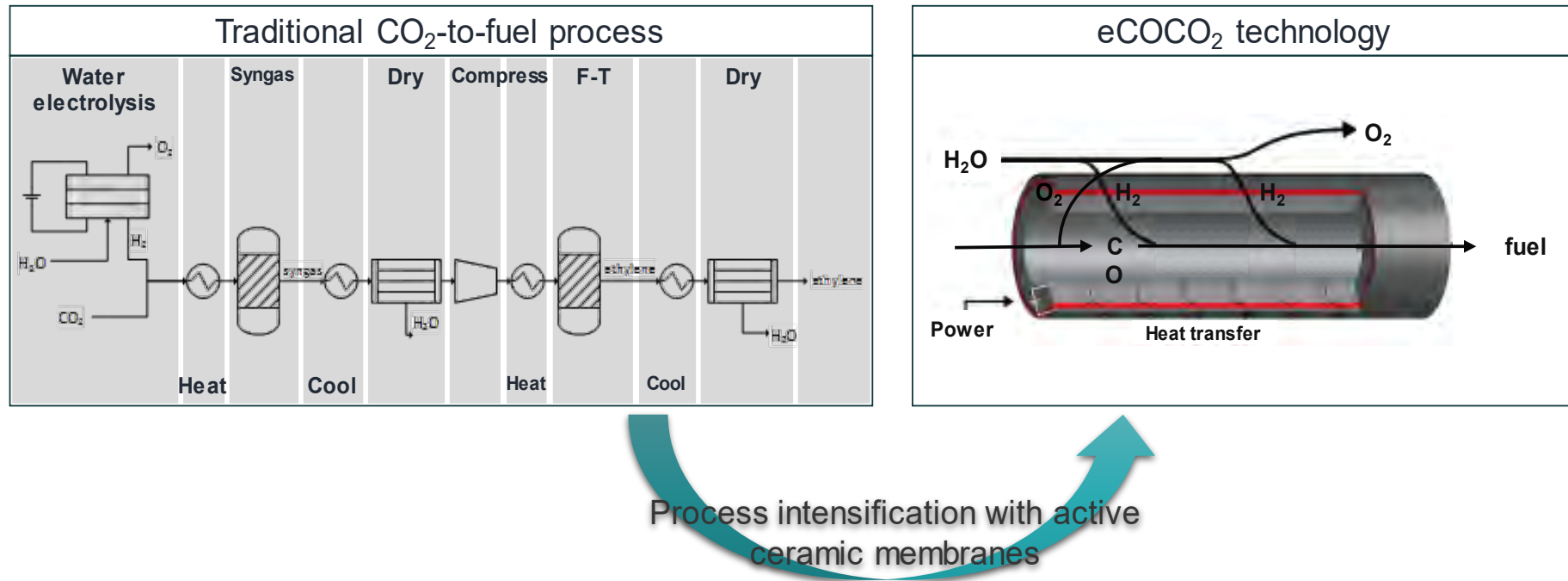


Highly energy intensive
with overall energy efficiency
values around 60%

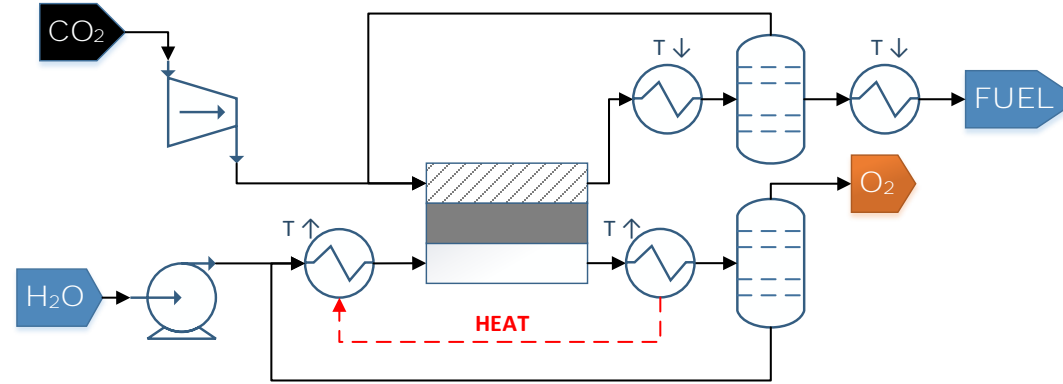


Single-step electrolysis and one-pot catalytic conversion

Membrane Reactor for the direct electrocatalytic conversion of CO₂ and steam into hydrocarbons



(Intensified) Single-step electrolysis and one-pot catalytic conversion



Product:
Jet fuel



Efficiency:
> 85%



Full integration:
compact sized reactor

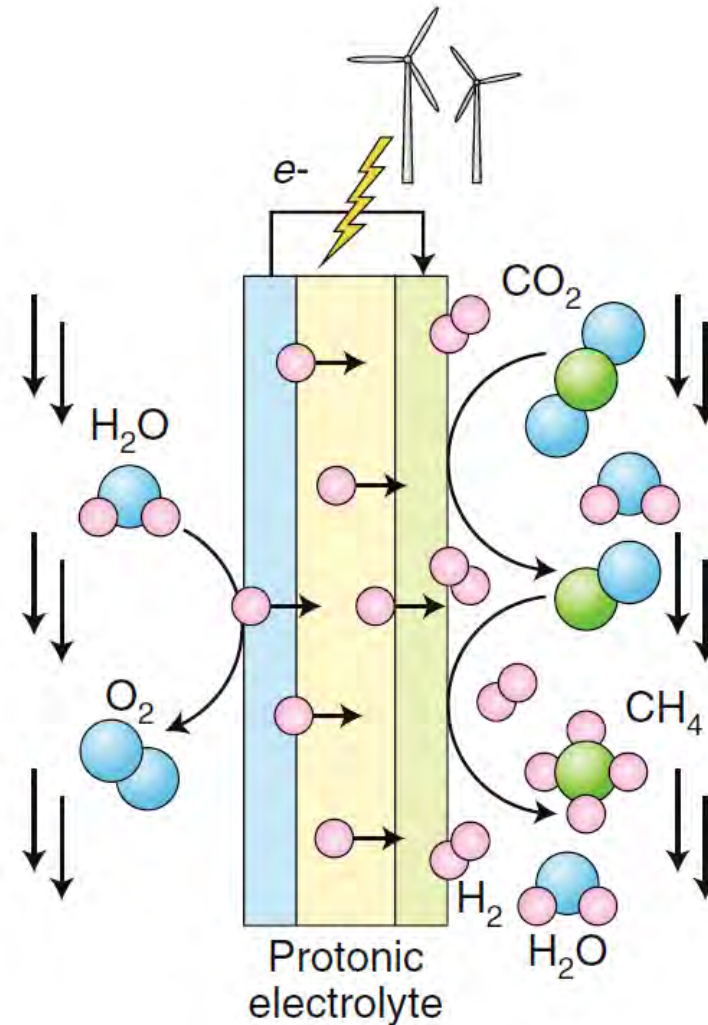


Final TRL:
5

Set-up a technology for conversion of CO₂, using renewable electricity and water steam, to carbon-neutral jet fuel, at high energy efficiency, very high CO₂ conversion rate and moderate-to-low cost.



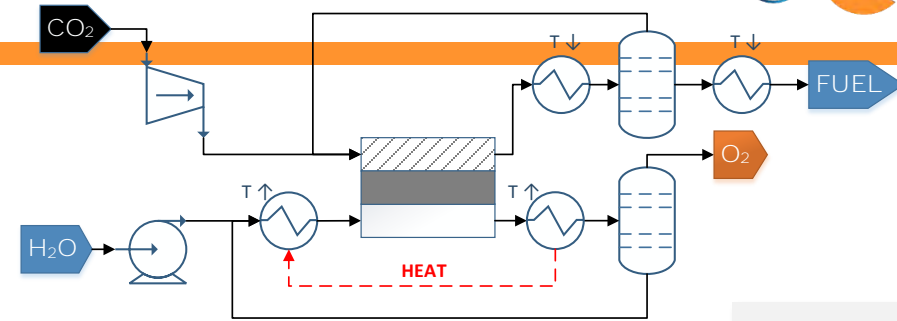
Single-step electrolysis and one-pot catalytic conversion



eCOCO₂ Approach



Concepts behind the intensification



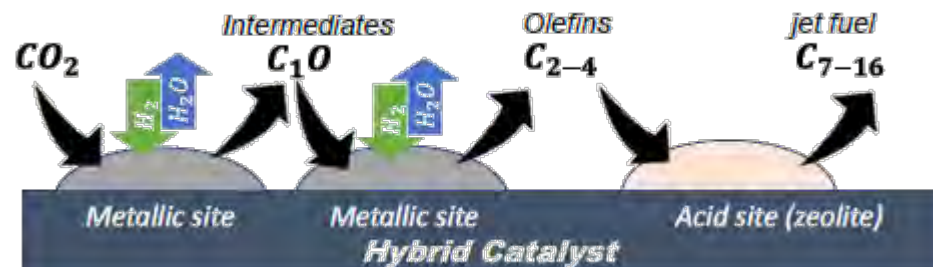
Enabling Components

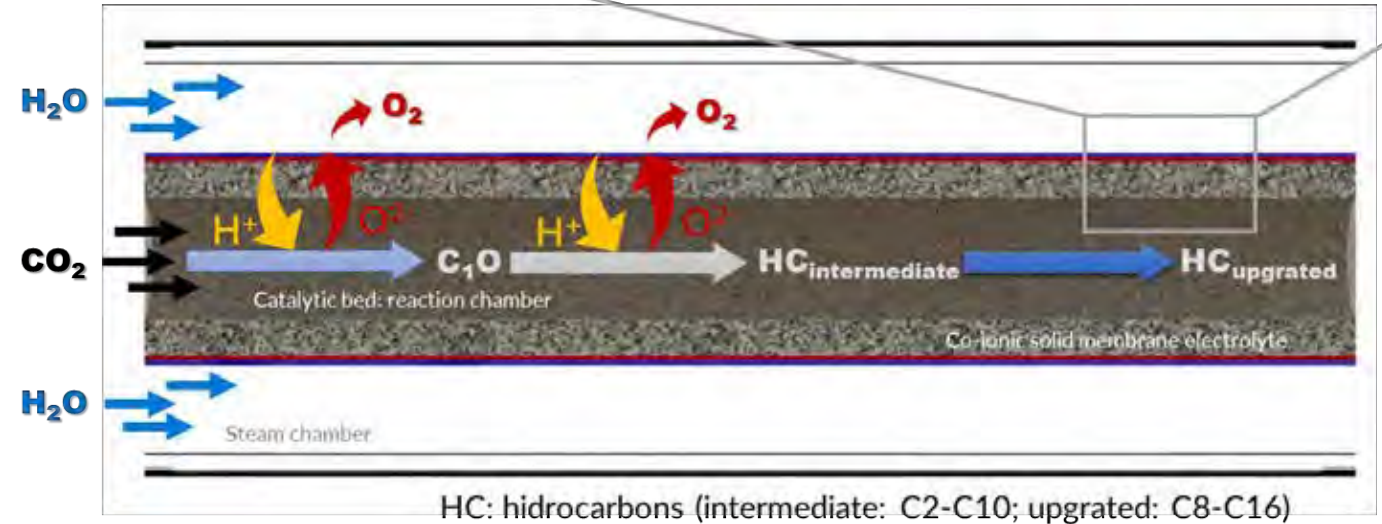
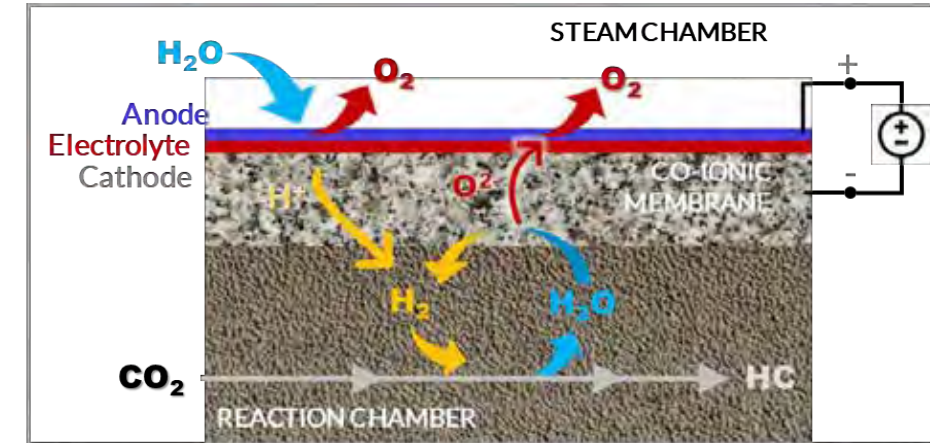
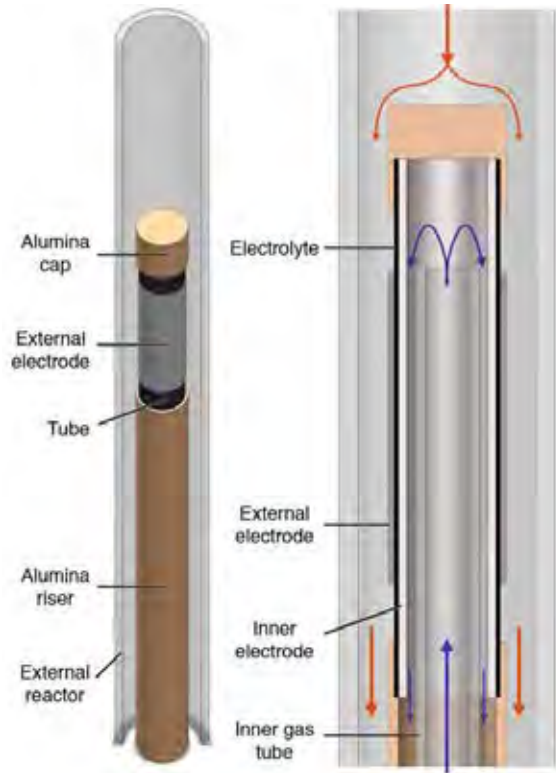
- In-situ **heat** integration: Integrating chemical **reactor** and water **electrolyzer** balance **exothermic** HC synthesis and **endothermic** water splitting
- Shifting the **equilibrium** by removing the H₂O formed in the CO₂ hydrogenation
- Avoid the effect of **high p_{H₂O}** in kinetics and catalyst degradation (e.g. zeolite) at high X_{CO₂}
- Control of p_{H₂} along the reactor favors conversion to target products
- Sequential catalytic reactions: RWGS + Intermediate formation + target hydrocarbons

Compact
EC-reactor

Co-ionic
Electrolyte

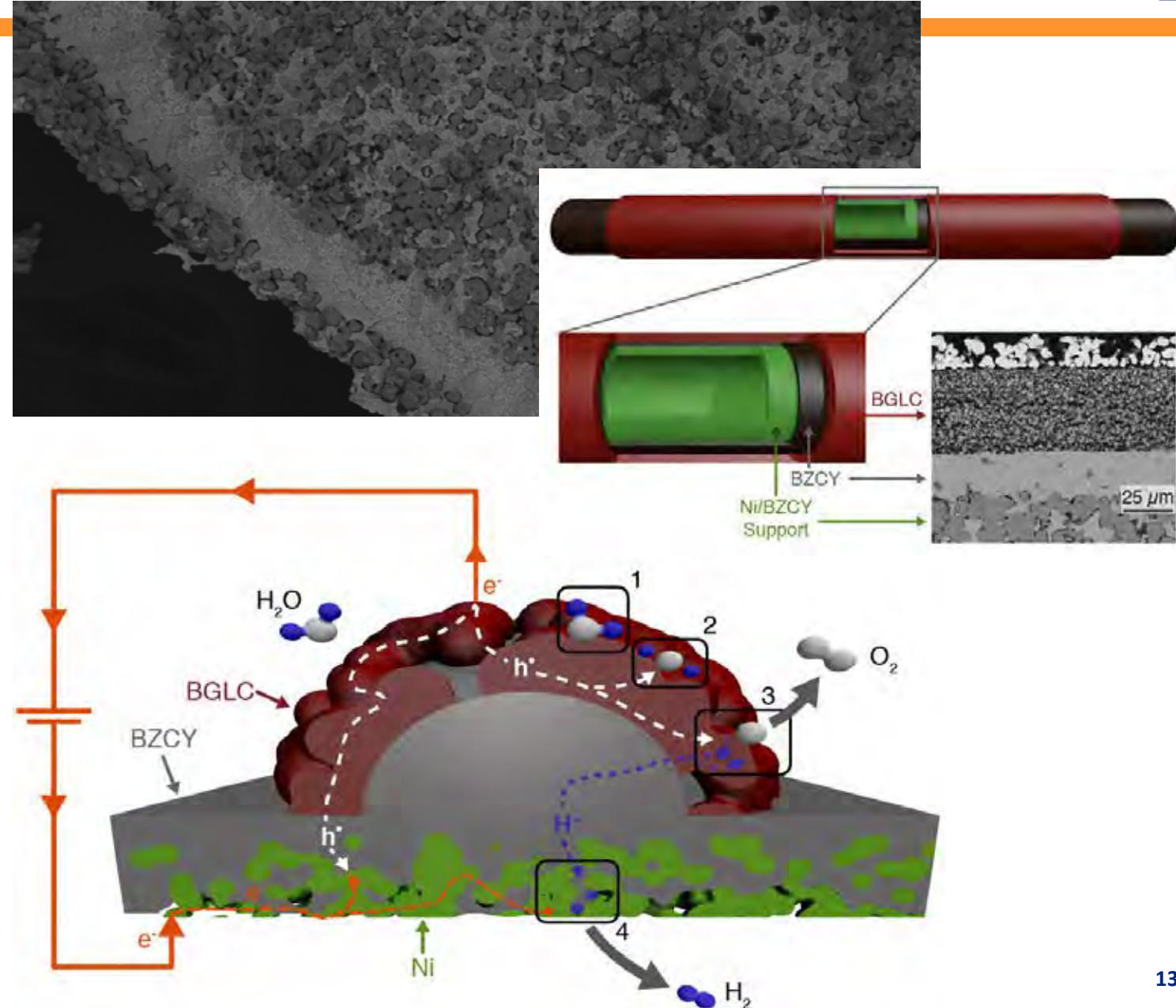
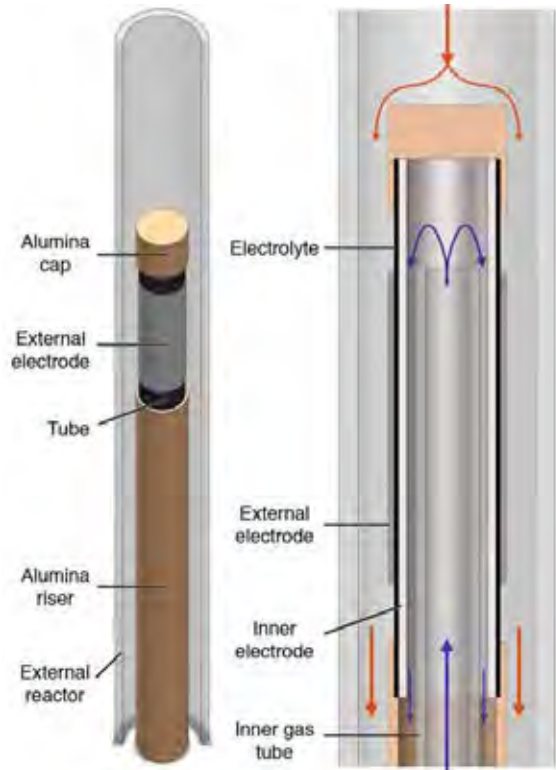
Hybrid
Catalyst





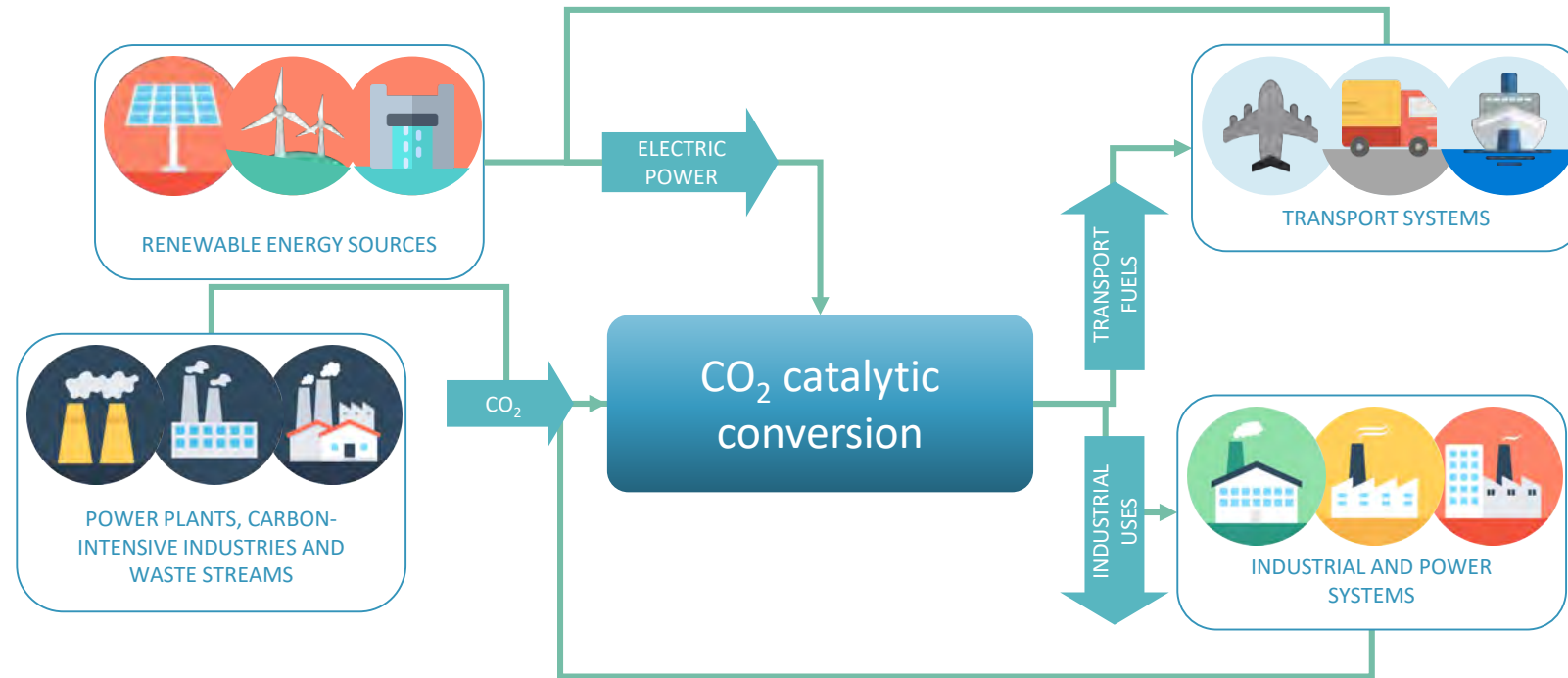
E. Vøllestad, et al. "Mixed Proton and Electron Conducting Double Perovskite Anodes for Stable and Efficient Tubular Proton Ceramic Electrolysers", **Nature Materials** 2019





E. Vøllestad, et al. "Mixed Proton and Electron Conducting Double Perovskite Anodes for Stable and Efficient Tubular Proton Ceramic Electrolysers", **Nature Materials** 2019

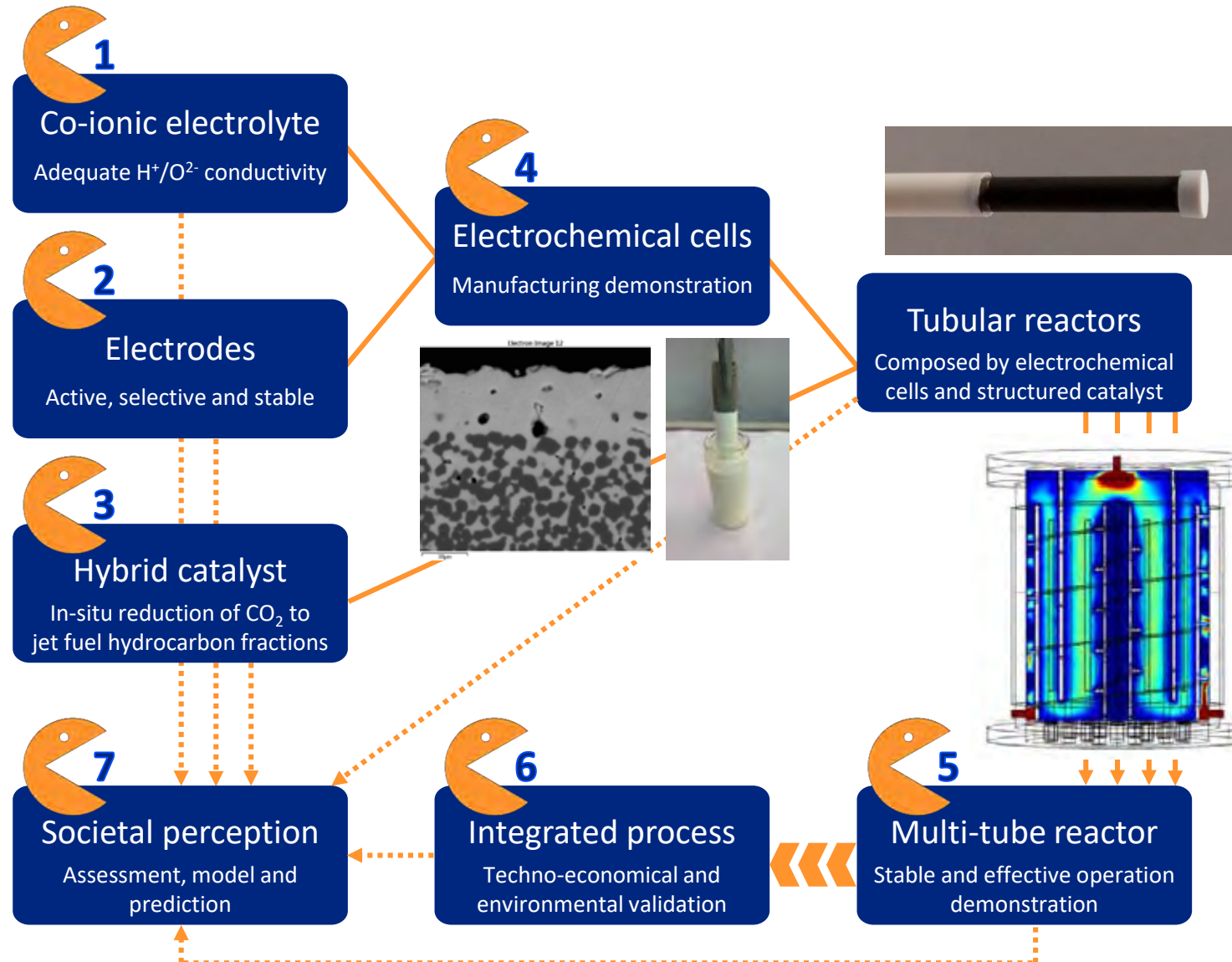




Challenges

- Couple Catalysis and Electrochemical Cell operation conditions
- Manufacture of large cells with novel components
- CO₂ streams: composition, conditions, capture&cleaning costs...
- Integration in industrial processes: TEA
- Social perception and acceptance





The consortium is formed by well balance of reference research and academic institutions:

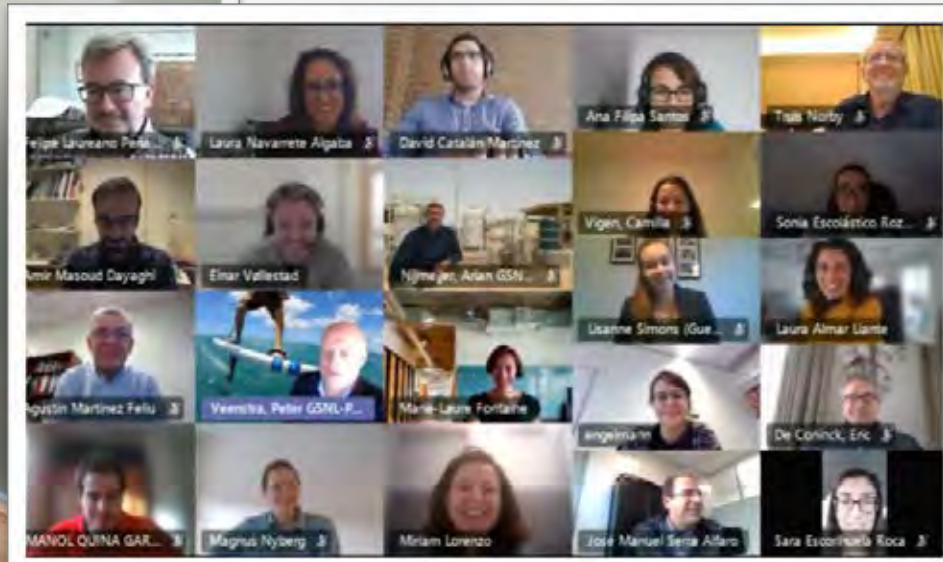


and leader companies:



Teams

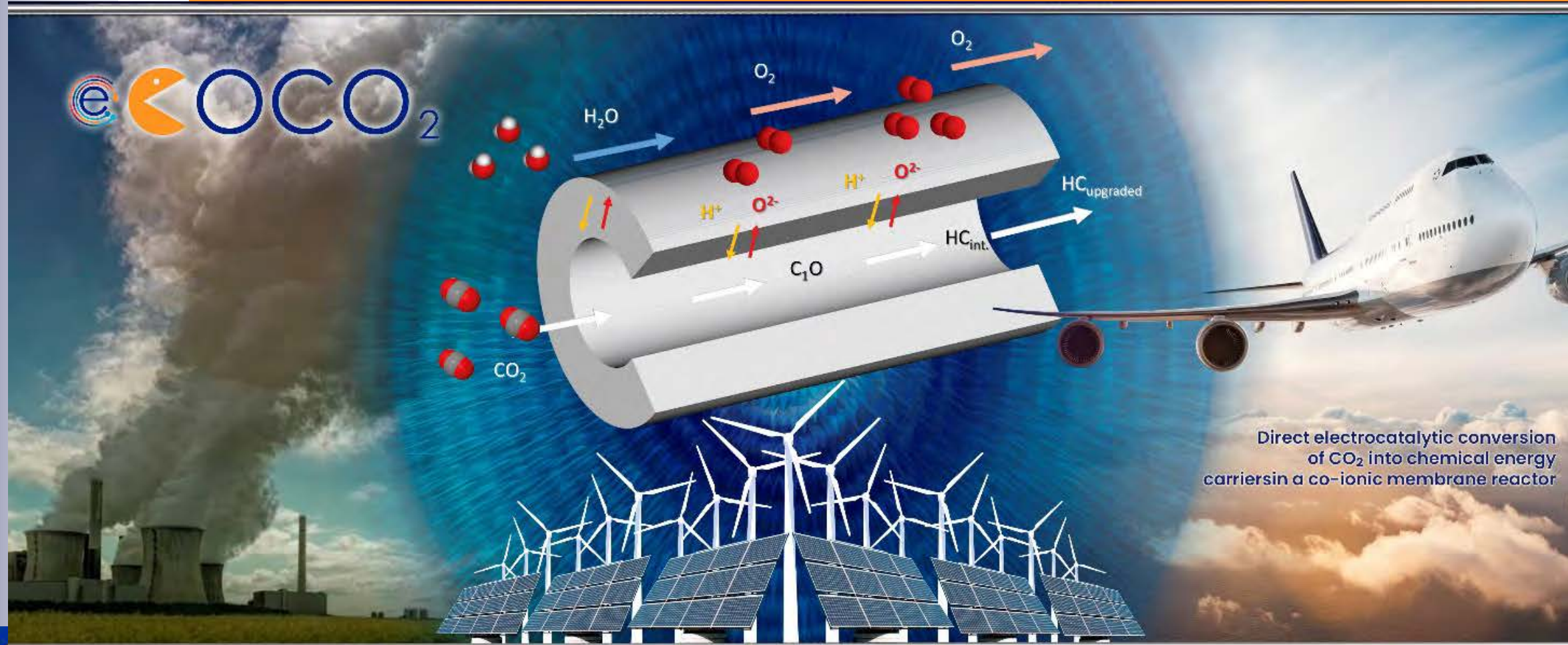
Equal opportunities between men and women in the implementation of the action are promoted. Gender balance at all levels of personnel assigned to the action, including at supervisory and managerial level.



5 Women
WP Leaders

- **Economic sustainability of the process**
 - Associated costs, including capital costs and operating costs (mainly energy consumption), and the expected savings and revenues.
- **Dependence on upstream technologies**
- **Availability of required associated infrastructure**
- **Public perception and acceptance of the technology**
- **Regulatory barriers**





Direct electrocatalytic conversion of CO_2 into chemical energy carriers in a co-ionic membrane reactor

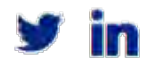


- ✓ Website ecocoo.eu
- ✓ Social networks
- ✓ Visual identity

- ✓ Press release and radio
- ✓ Project flyer
- ✓ Project video



FOLLOW US!





<https://ecocoo.eu>



twitter.com/eCOCO2/



linkedin.com/company/ecoco2/



YouTube channel: eCOCO2 H2020



INTERNATIONAL WORKSHOP ON CO₂ CAPTURE AND UTILISATION



CO₂ utilisation focused on market relevant
dimethyl ether production, via 3D printed reactor
and solid oxide cell based technologies

Vesna Middelkoop
16 February 2021



CO₂Fokus facts and figures



42
MONTHS



2019/07/01
STARTING DATE



8
COUNTRIES

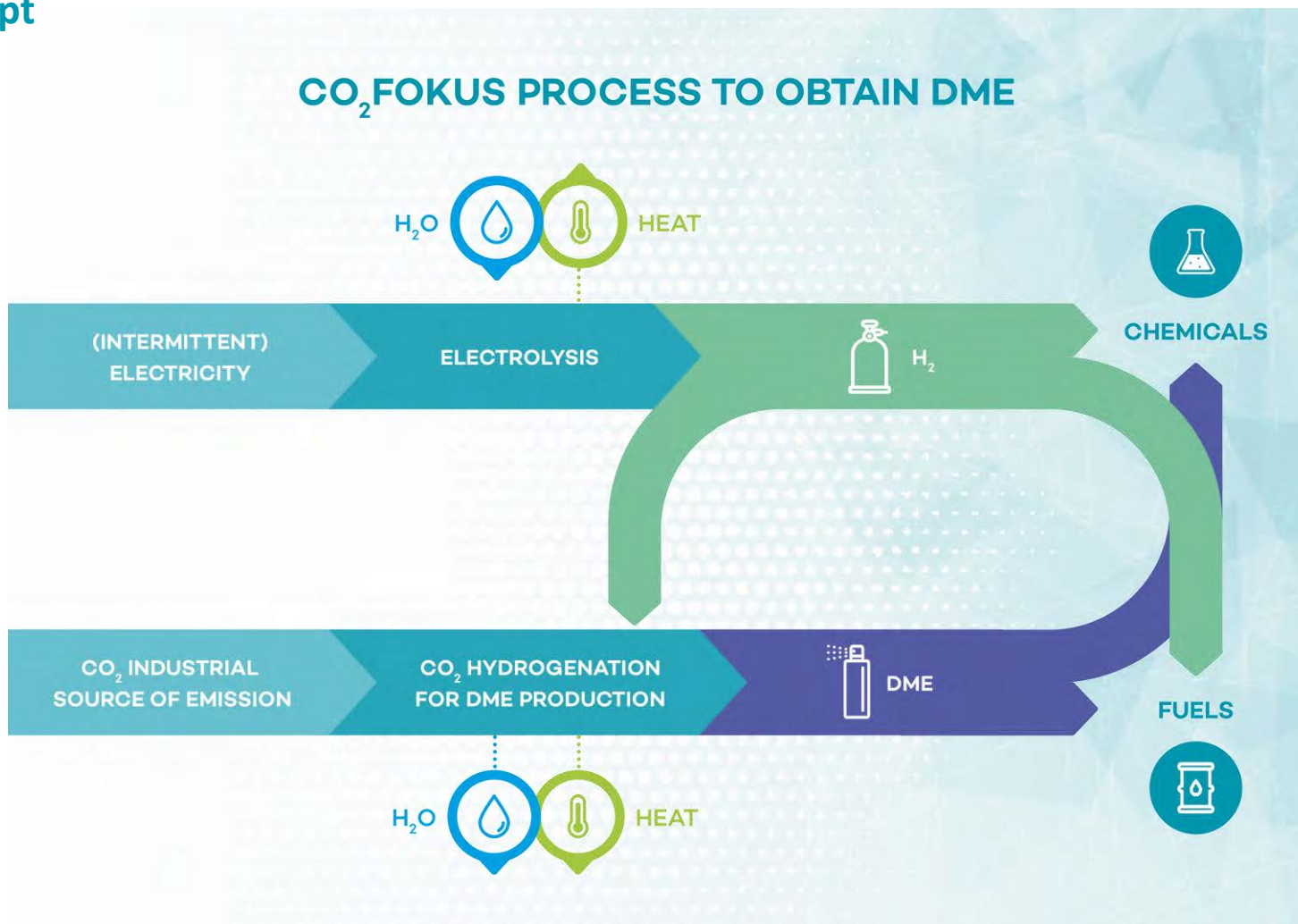
CO₂Fokus at a glance

The project will develop a cutting-edge technology to directly convert industrial CO₂ into DME (Dimethyl Ether), by:

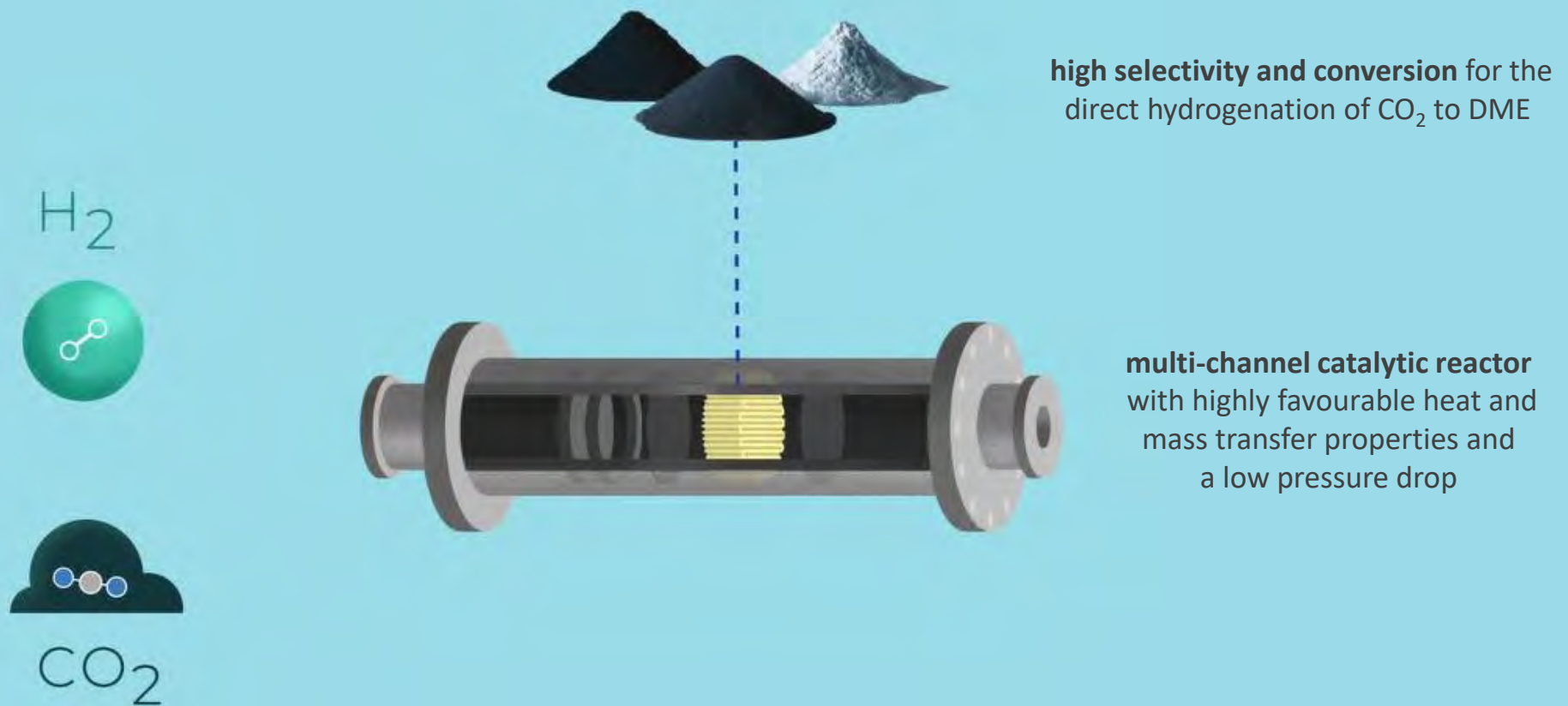
- employing innovative 3D printed multichannel catalytic reactors and solid oxide electrolyser cells
- integrating and testing them in an industrial environment of large industrial CO₂ point sources



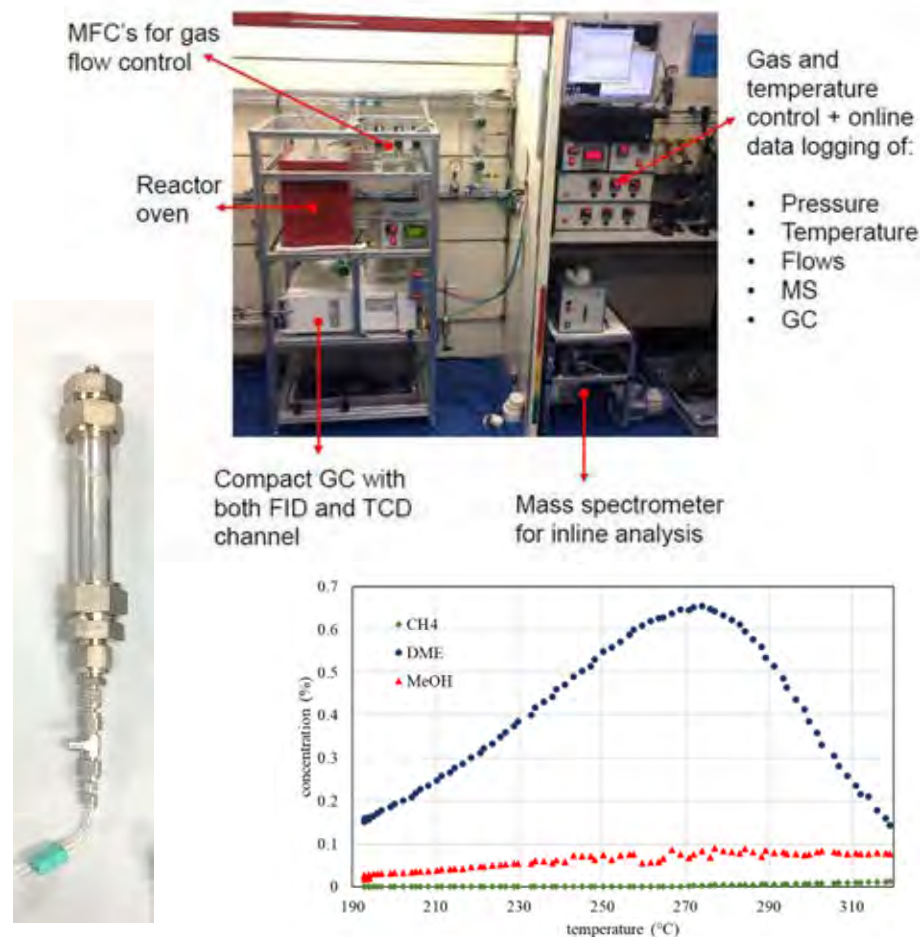
Concept



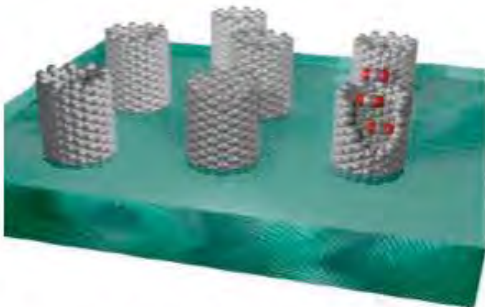
Catalyst formulation and single tube catalyst screening for DME production



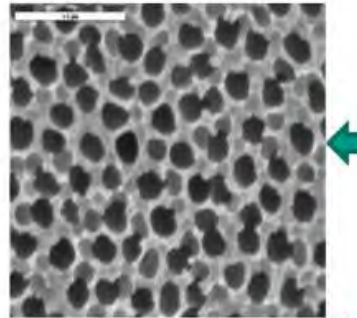
Catalyst formulation and single tube catalyst screening for DME production



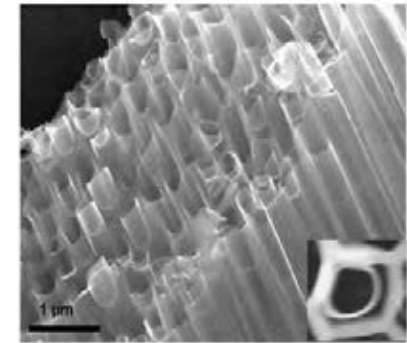
Single tube catalytic CNT membrane reactors for DME production



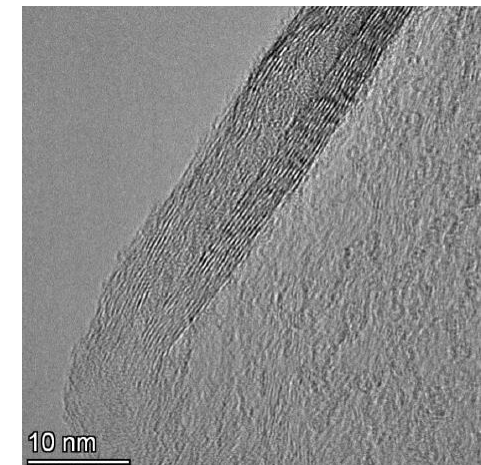
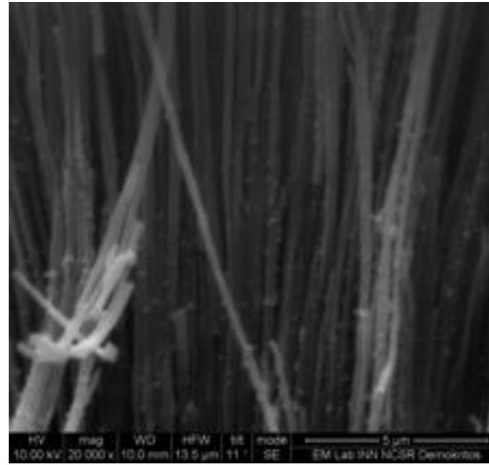
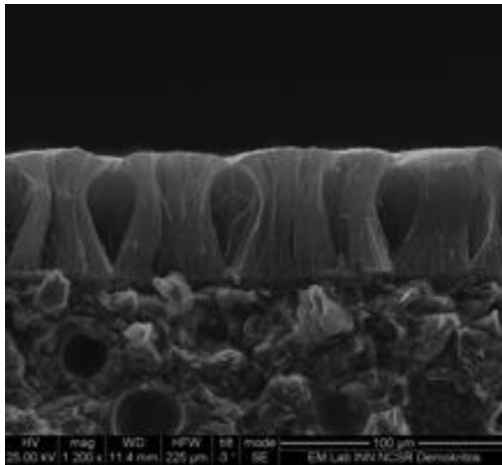
Aligned Carbon Nanotube (ACNT)s:



SWCNTs

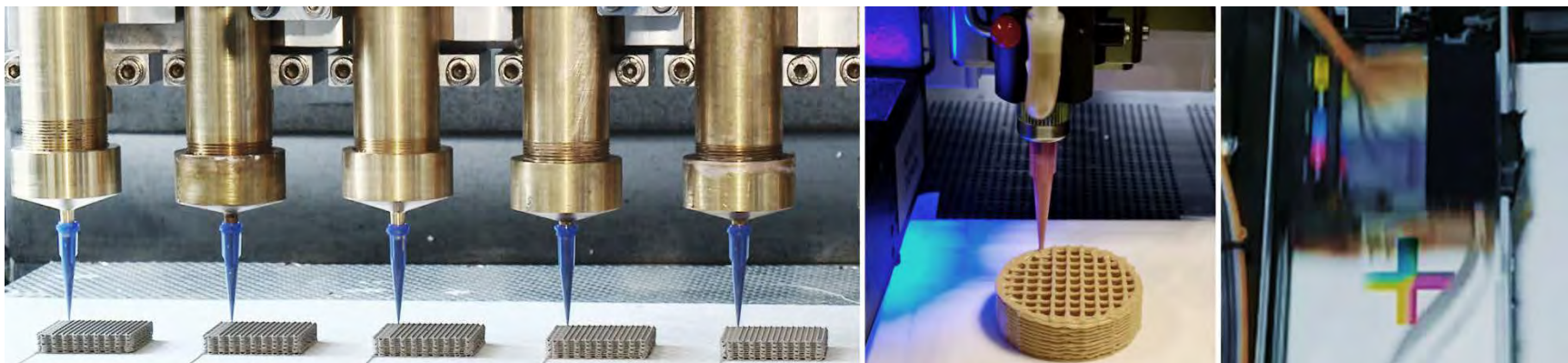


parallel catalytic nanoreactors



Tailored nano pore size by Atomic Layer Deposition (ALD)

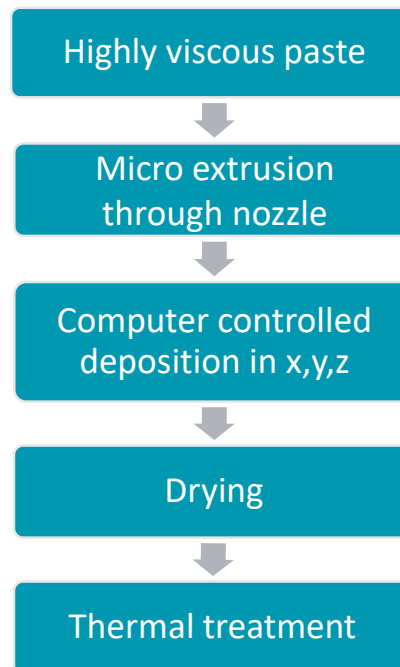
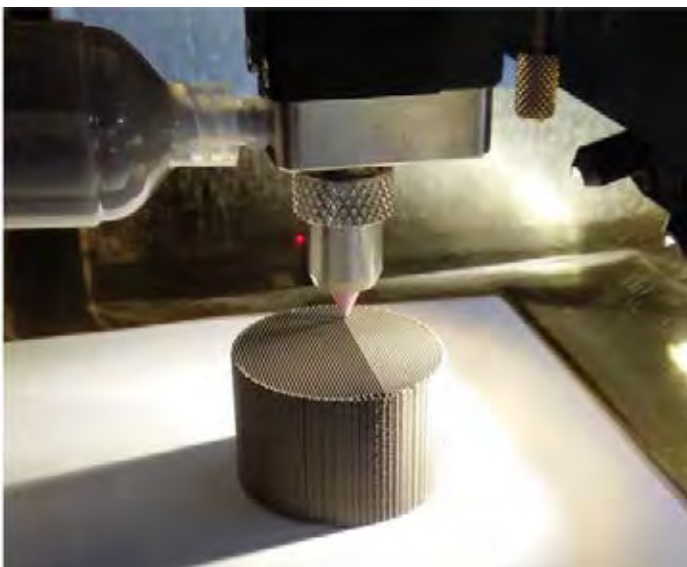
Why do 3D printing of catalysts and adsorbents?



Major advantages of 'direct write' (structuring reactors into multi-channel, multi-layer architectures) is that tailor-made multi-modal devices allow for:

- **precise and uniform distribution of active material over a high surface area**
- **highly adaptable and well-controlled design for optimal flow pathways**
- **low pressure drop**
- **improved mass- and heat-transfer**
- **easy (in-situ) regeneration and cost-effective product removal**
- **overall greatly improved productivity per cubic meter of reactor volume**

3D printing process - 'direct write'



Offers bespoke patterning of all-in-one structures in a variety of materials:

- ❖ **oxide ceramics** (e.g. Al_2O_3 , SiO_2 , ZrO_2 , CeO_2 , mixed metal oxides, nanocomposites)
- ❖ **metals** (e.g. titanium, copper, aluminium, silver) and **alloys** (e.g. stainless steel)
- ❖ **non-oxide ceramics** (e.g. silicon carbide, carbon, boron nitrate)
- ❖ **other functional materials**: zeolites, polymers, MOFs, graphene oxide

3D printed catalyst, adsorbents and reactor components at a glance



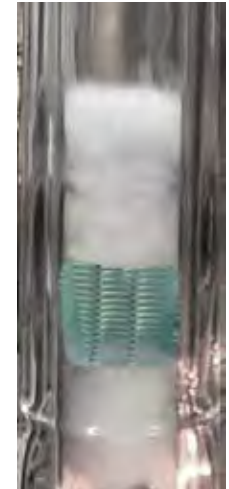
3D printed catalyst for DME production in CO2Fokus



CZA as-prepared



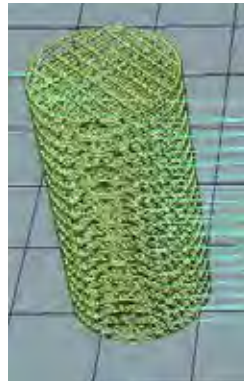
mixing the printing paste



calcination



CZA calcined



optimising the printing model

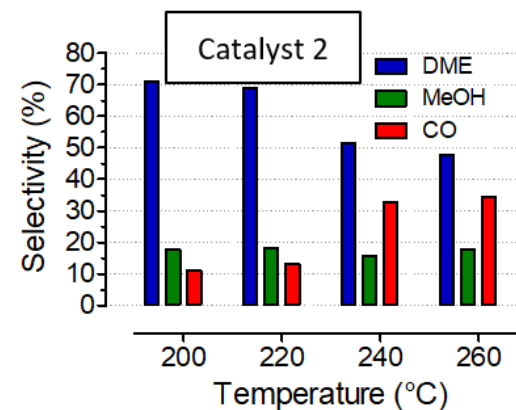
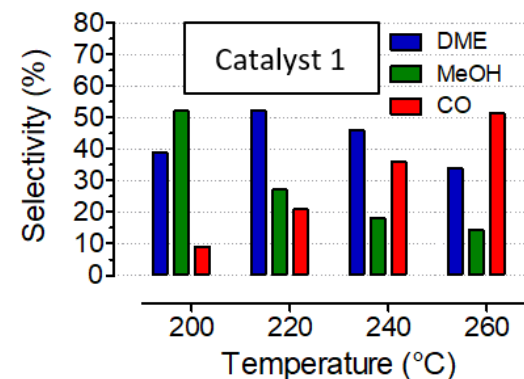
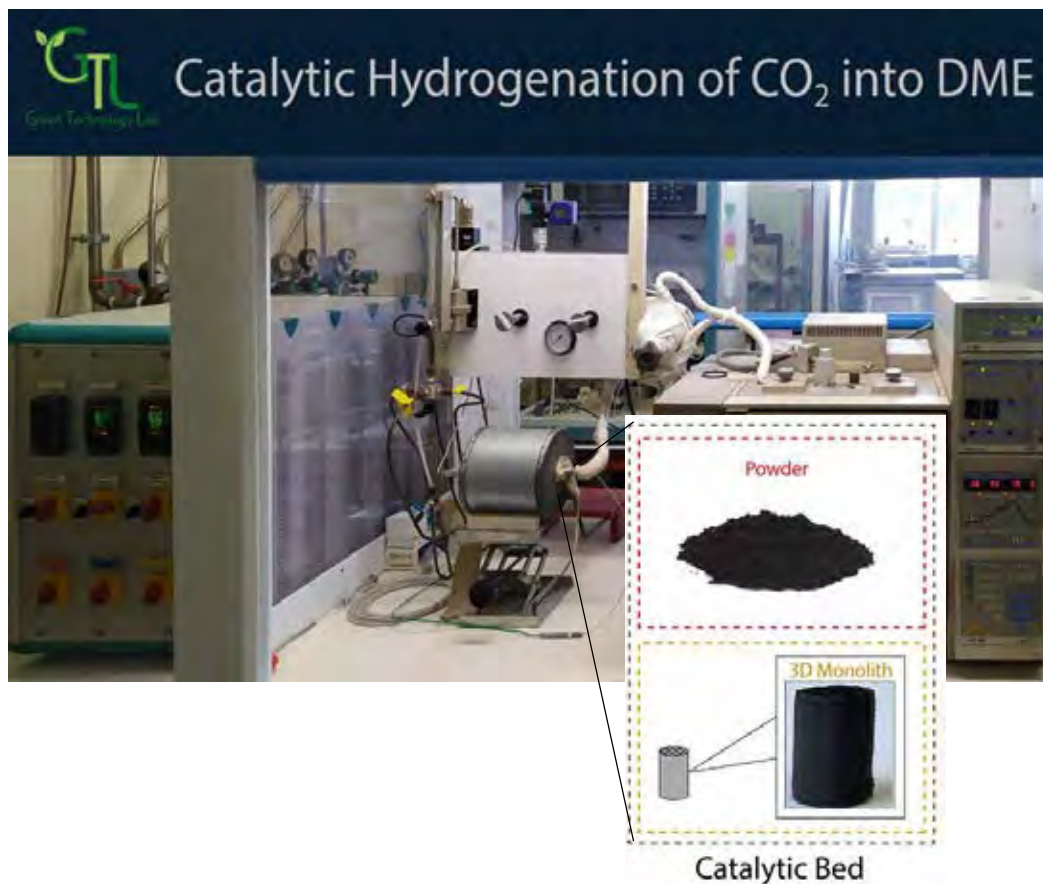


varying design and size



integration into the reactor

Single tube catalyst testing for DME production



For more details see further: Session 1B, Dr. G. Bonura

3D-printing in catalysis: Development of efficient hybrid systems for the direct hydrogenation of CO₂ to DME

Multi-channel millireactors TRL4-TRL6



PROCESS INTENSIFICATION

↑↑↑ A/V



Characteristics required of the reactor:

- Improve the mass transference
- Optimisation of heat dissipation
- Dimensional uniformity of the tubes
- Thermal and mechanical stability
- Ease of handling



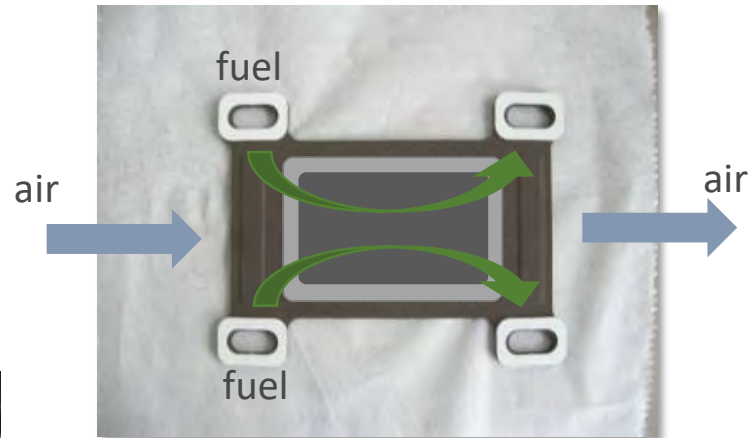
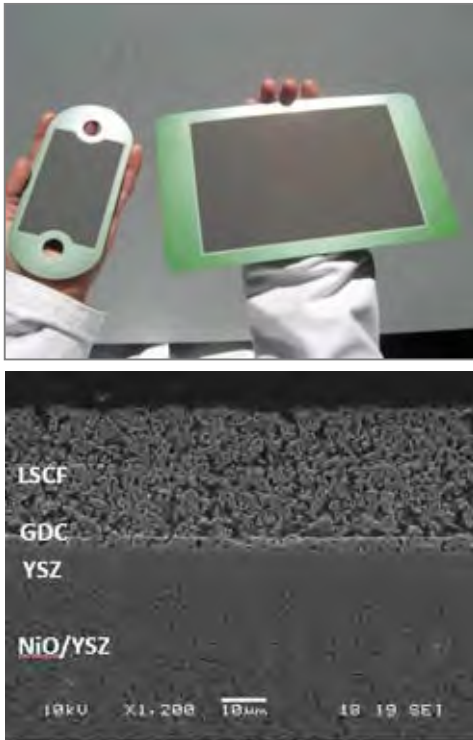
| 16 Millichannel Reactor | | | | |
|--|-------|----------------------------------|-----------------------|-----------------|
| Space velocity, ML/kg _{cat} /h | T, °C | CO ₂ Conversion, % | DME Selectivity, % | DME Yield, % |
| | 280 | 12.1 | 31.0 | 3.7 |

For more details see further: Session 3A, Dr. S. Perez

Process intensification in the conversion of CO₂ with a milli-structured reactor

Solid oxide electrolyser cell and design, development and build up for H₂ production

cell
design



- Thin (ca. 250 µm) anode support with GDC/LSCF cathode
- Low cost state-of-the-art materials
- High mechanical strength and reliability

| performances | unit | nominal |
|---------------------------|------|-----------|
| Conversion | % | 60 |
| H ₂ Production | NI | 0.30-0.32 |
| Stack power DC | kW | 4.5 |
| Thermal cycling | - | 100-200 |

Process design of CO₂Fokus prototype demonstration units and on site integration



Reactor and SOE units will be integrated into existing carbon-intensive industrial facilities for on-site recycling of CO₂



| Key Performance Indicators (KPI) | State-of-the-art | CO ₂ Fokus |
|--|-------------------|---------------------------------------|
| Energy efficiency (MJ/ton) DME | 2300 [#] | 20-30% reduction |
| Catalyst & reactor design | TRL 3-4 | TRL 6 |
| Catalyst durability (hrs) | 10 ² | 10 ³ |
| Pressure (bar) | 30-70 | 30 |
| Temperature (°C) | 280 | 250 |
| CO ₂ /H ₂ feed (N L/h) | 33/100 | 500/1500 or larger by numbering tubes |
| DME yield (%) | 20-25 | >30 (multichannel reactor) |
| CO ₂ conversion (%) | 30 | >30 |
| Overall H ₂ conversion (%) | 50 | 50 |

Conclusions

Advance beyond the state-of-the-art

- Effective controlled deposition of active catalyst particles
- Reactor design: large surface to volume ratio and controlled macrostructure; millichannel reactors offer enhanced mass and heat transfer and 10-20% increase in reaction performance
- Integration and operation at Petkim's facilities - industrial CO₂ point source

Technical acceptance enablers

- Tackle potential technological and industries' concerns
- Provide technical guidelines for companies based on CO2Fokus demo design
- Tasks are put in place to provide analysis of environmental, financial and regulatory requirements
- Join forces with other projects on common interest topics to amplify the impact of our activities

Thank you!



The project has received funding from the European Union's Horizon 2020 research and innovation programme under grant agreement n. 838061

This document reflects only the authors' view and the Innovation and Networks Executive Agency (INEA) and the European Commission are not responsible for any use that may be made of the information it contains.



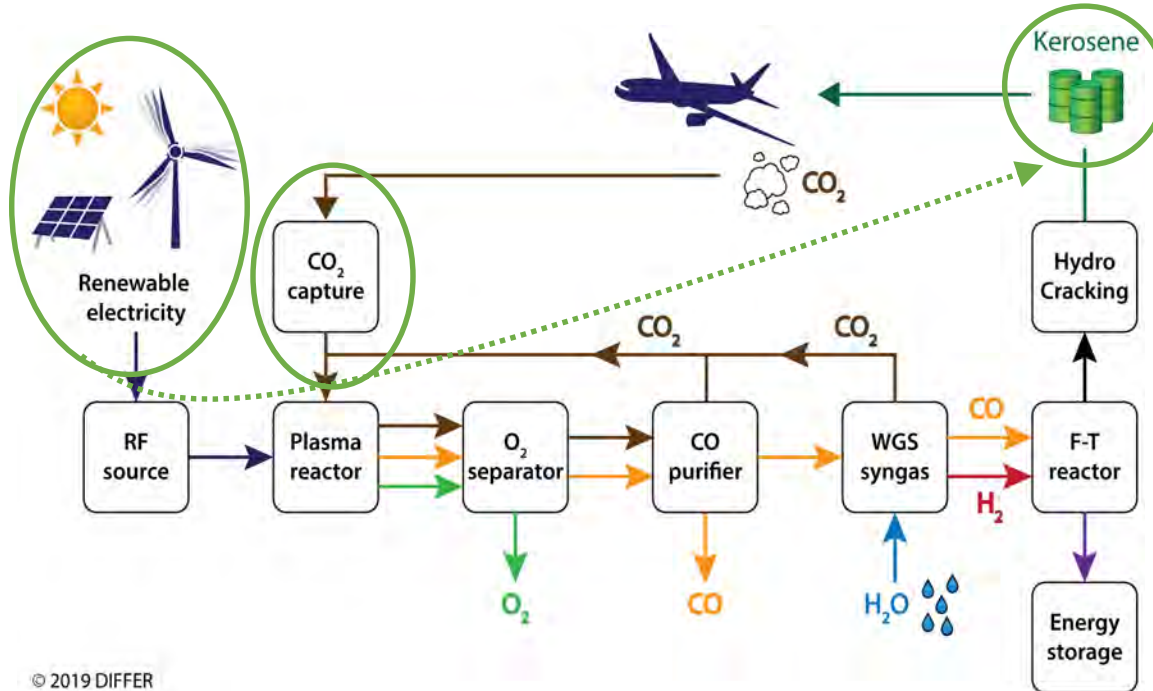


Production of Sustainable aircraft grade Kerosene from water and air powered by Renewable Electricity, through the splitting of CO₂, syngas formation and Fischer - Tropsch synthesis

The KEROGREEN CO₂ plasma route to CO and alternative fuels

A. Pandiyan, S. Welzel, A. Goede, M.C.M. van de Sanden, M.N. Tsampas

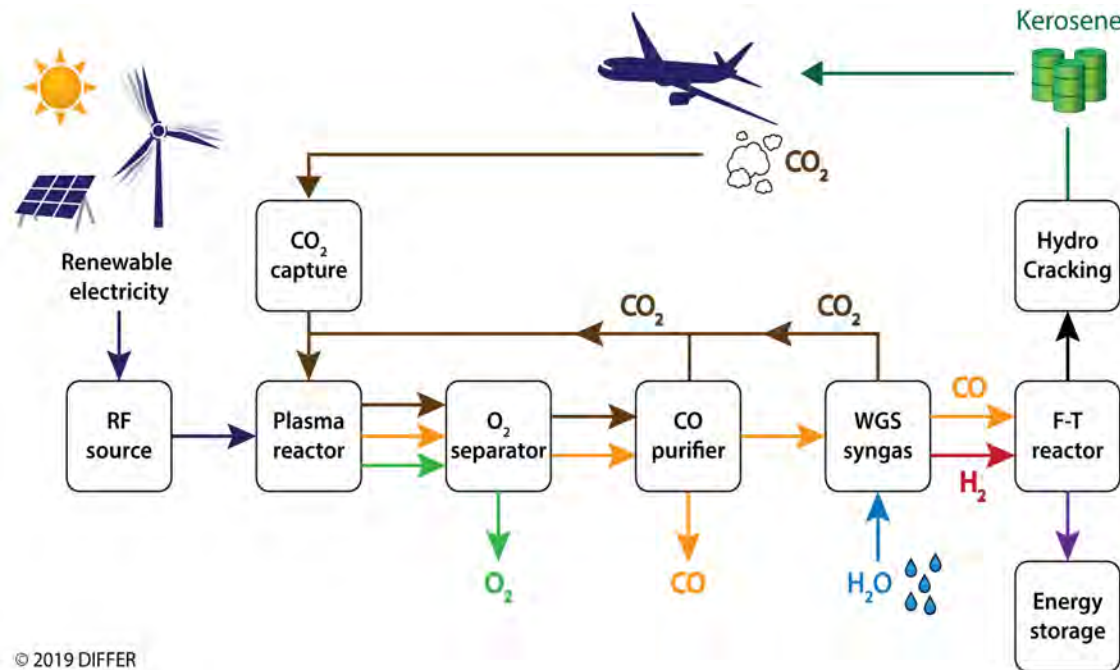
DUTCH **I**NSTITUTE **F**OR **F**UNDAMENTAL **E**NERGY **R**ESearch, EINDHOVEN, THE NETHERLANDS



Kerogreen aim: Demonstration of the full chain process from renewable electricity, CO₂ (captured) and H₂O to kerosene.

- Research and optimization of individual process steps TRL (1-3) → 4
- Integration phase at Karlsruhe Institute of Technology → 3 L per day
- Duration 2018-2022





KEROGREEN offers an innovative conversion route based on:

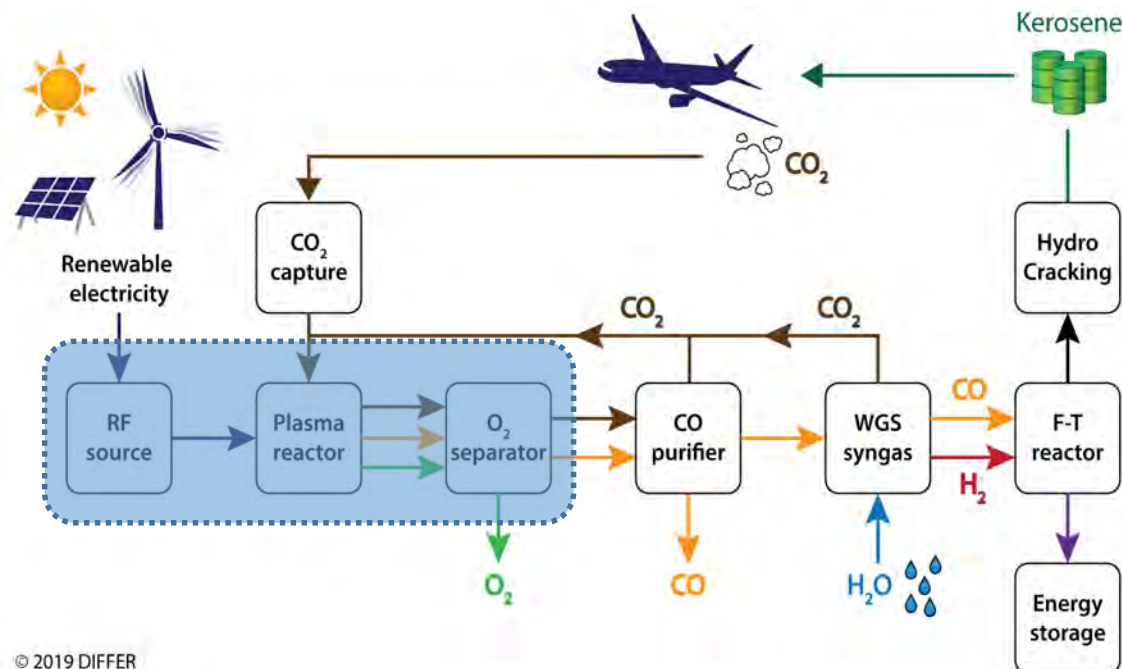
- CO₂ plasmolysis (DIFFER)
- Electrochemical O₂ separation (DIFFER, VITO, Cerpotech, Hygear)
- CO purification (HYGEAR)
- Water gas shift reaction reaction (KIT)
- Fischer-Tropsch synthesis (INERATEC)
- Heavy HC hydrocracking (KIT)

Main challenges

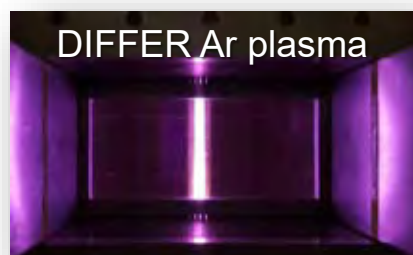
- Oxygen separation after plasmolysis by SOEC
- System integration of different technologies into one **container** sized assembly
- Maximization of the energy and carbon efficiency of the full chain

INERATEC



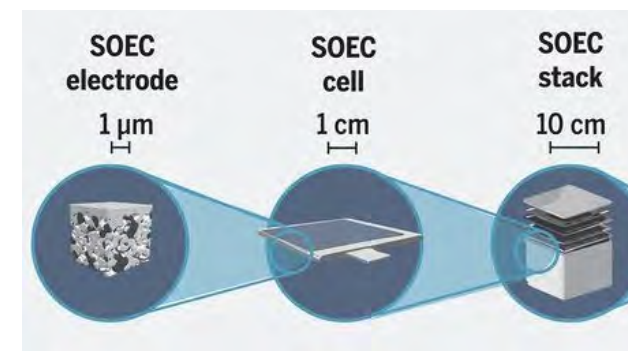


© 2019 DIFFER



DIFFER involvement

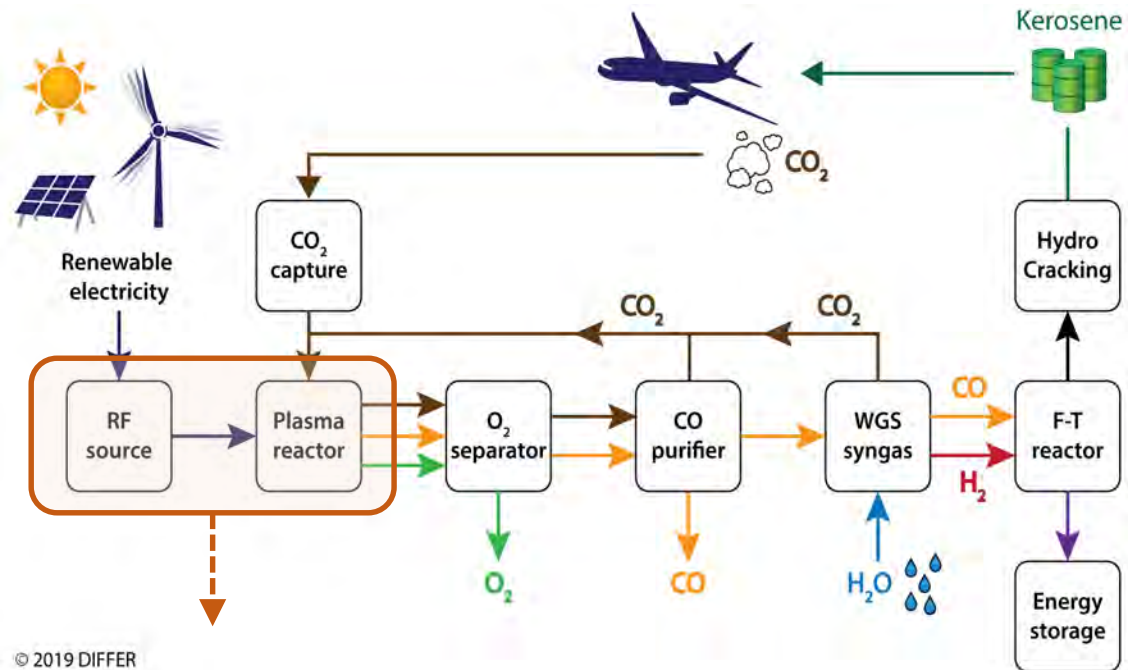
- Plasmolysis
 - Plasma modeling and optimization
 - Upscaling from 1 to 6 kW
- Electrochemical oxygen separation
 - Proof of concept
 - SOEC material requirements
 - Upscaling from 1W to 1.5 kW



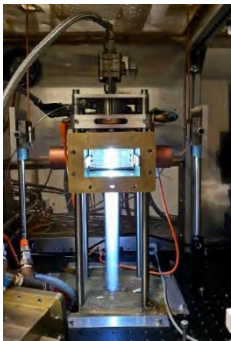
SOEC: Solid oxide electrolyte cells

[DOI: 10.1126/science.aba6118](https://doi.org/10.1126/science.aba6118)

Why CO₂ plasmolysis?

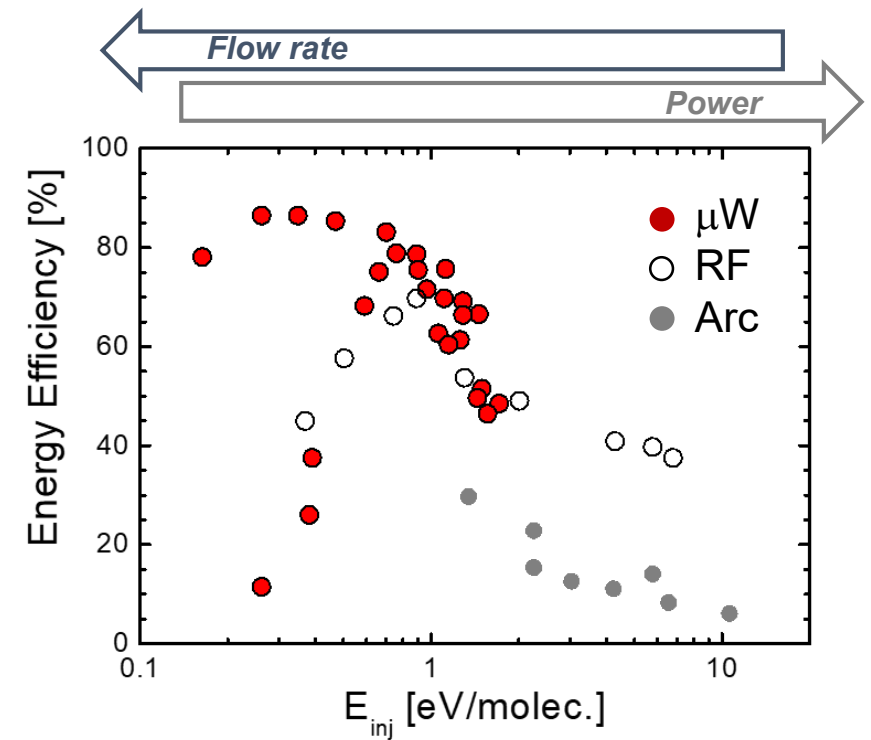


© 2019 DIFFER

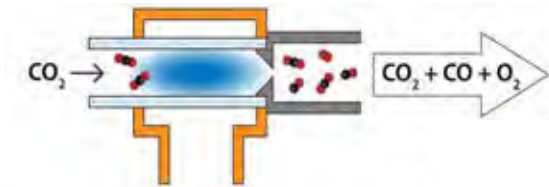


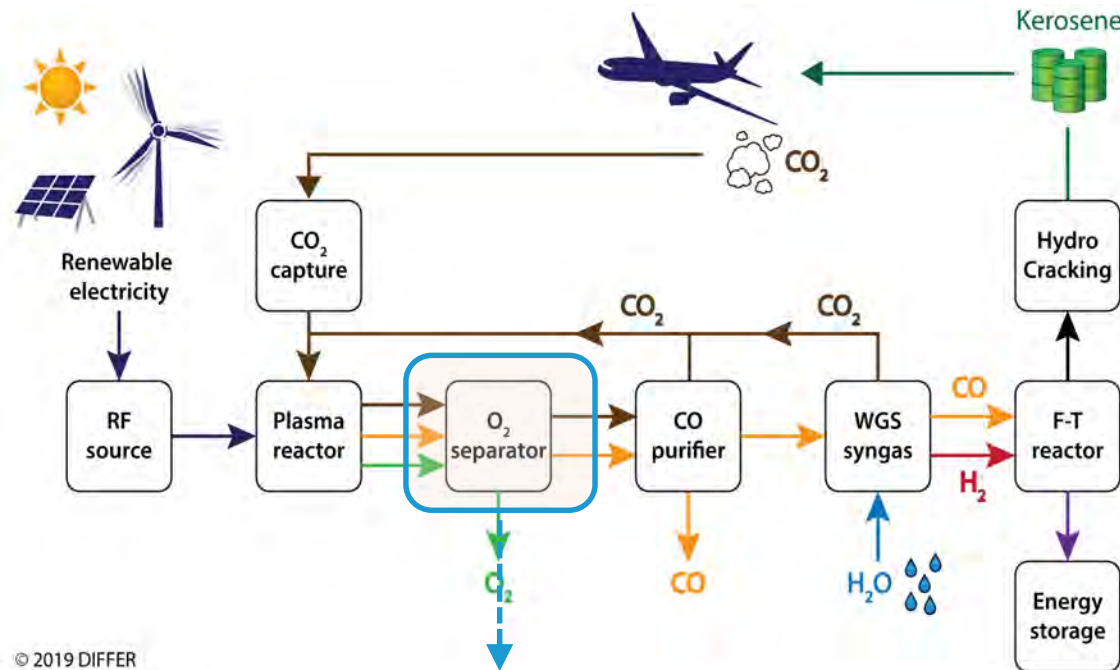
CO₂ plasmolysis: $2\text{CO}_2 \rightarrow 2\text{CO} + \text{O}_2$

- Input: CO₂ + renewable electricity
- Output: CO₂, CO and O₂
- High energy efficiency, ...
- Main challenge O₂ separation



DOI: 10.1017/CBO9780511546075



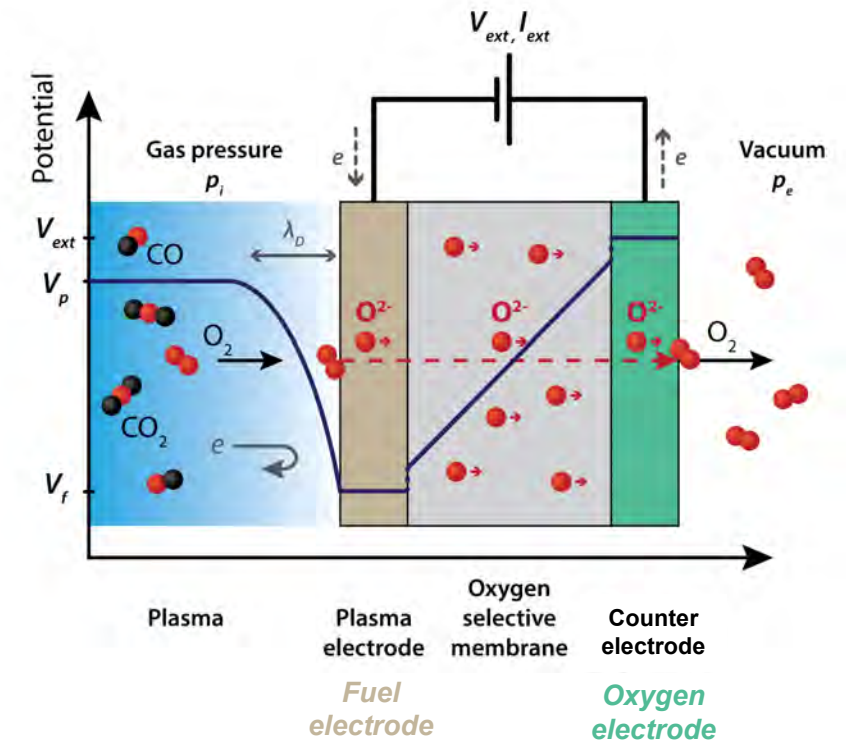


© 2019 DIFFER



O₂ separation

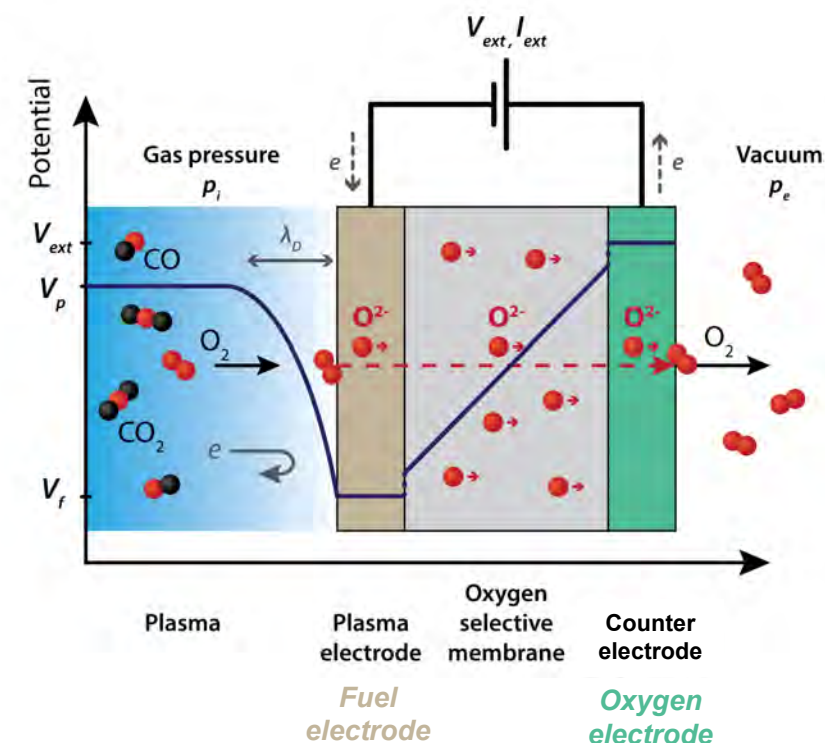
- Difficult process
- Lack of literature
- SOEC: Electrochemical O₂ pumping



*Conceptual design of
plasma integrated SOEC*

Material functionalities

- **For both electrodes:**
 - *Mixed electronic & ionic conductivity*
 - *Low overpotential losses*
- **Electrolyte**
 - *Oxygen ion conductivity*
 - *Low resistance → thin*
- **Key performance indicators**
 - *High oxygen fluxes*
 - *Stability*
- **Plasma (or fuel) electrode**
 - *Unconventional mixture ($\text{CO}_2, \text{CO}, \text{O}_2$)*
 - *Low CO oxidation activity*



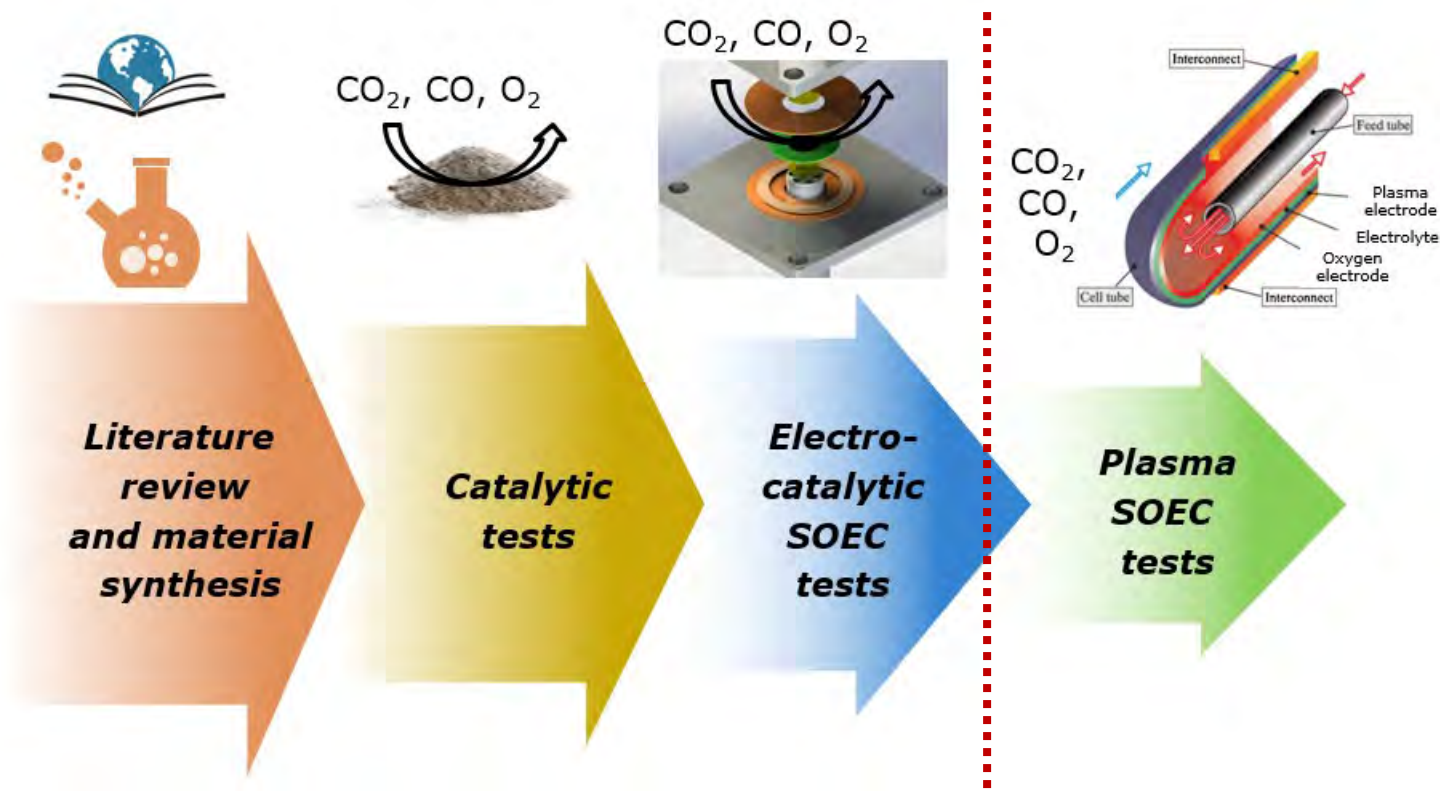
*Conceptual design of
plasma integrated SOEC*

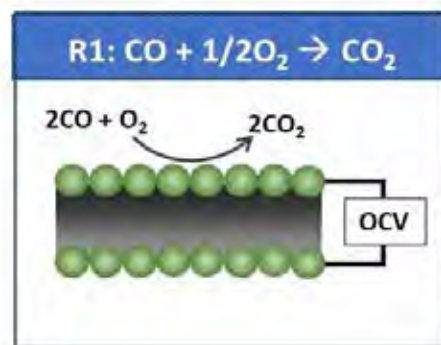
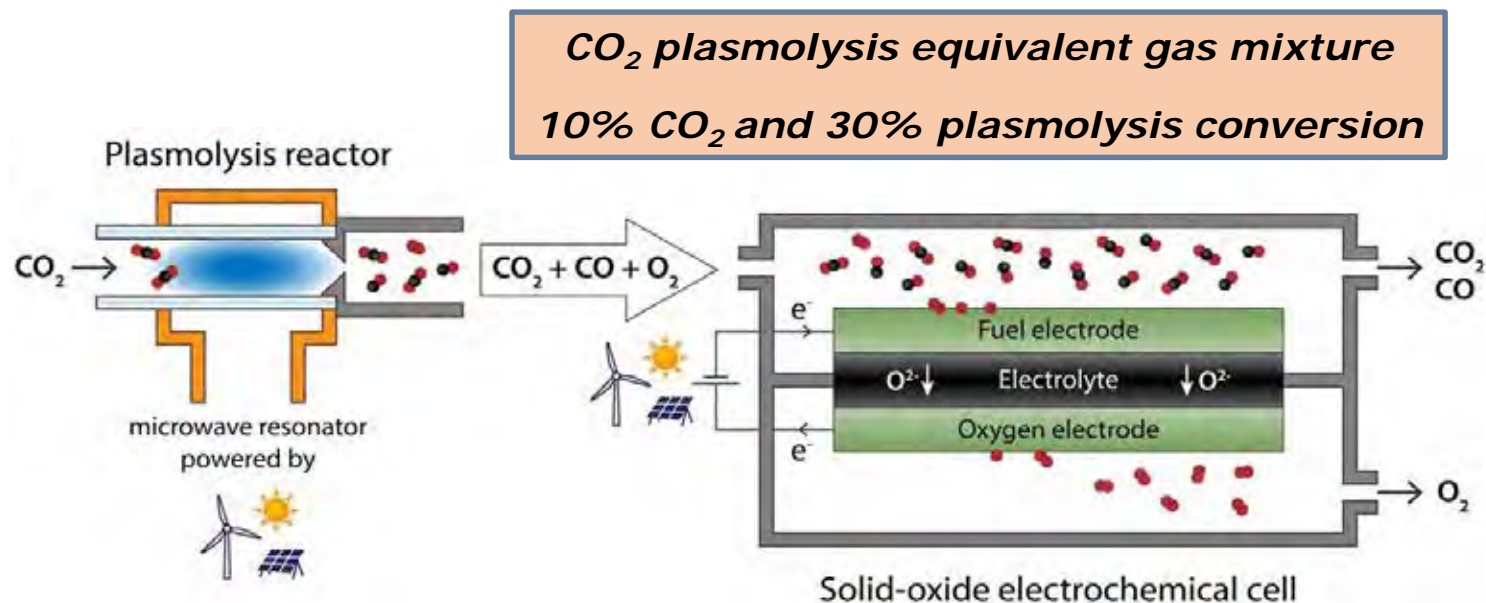
Plasma electrode development

- Literature review (redox properties)
- Material synthesis (Cerpotech)
- Catalytic tests

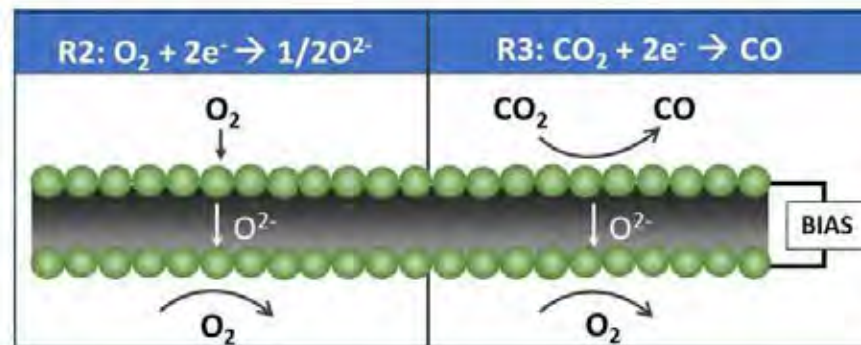
Testing

- SOEC electrocatalytic tests
- Plasma SOEC integrated tests





Unwanted

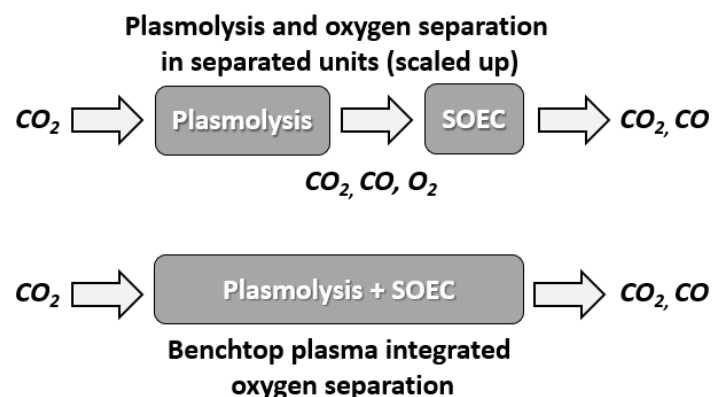
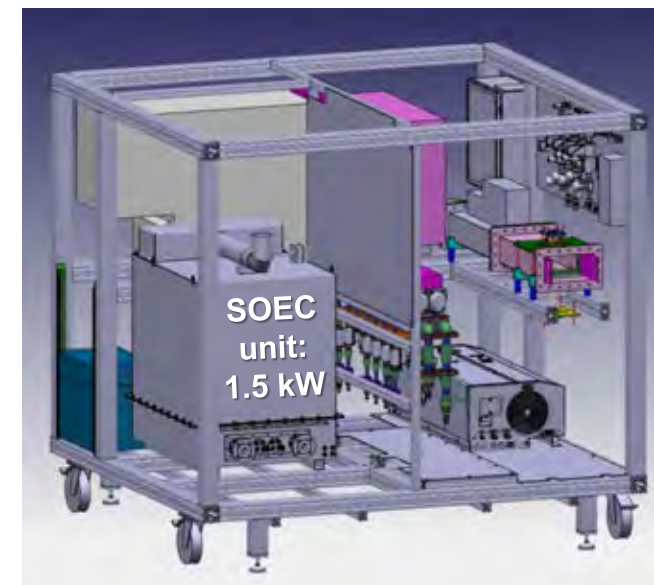


Desired

"Neutral"

Summary

- Oxygen separation from CO_2 plasmolysis equivalent mixtures has been demonstrated.
- Lowering operating temperature decreases CO oxidation losses but also oxygen separation.
- SOEC operation with CO_2 plasmolysis equivalent mixtures improves materials stability.



Outlook for integration phase

- Advance SOEC architectures will decreased ohmic losses:
 - allow operation at lower T (less CO losses),
 - while achieving high oxygen pumping rates.
- Integrated phase: Commercial vendor → 1.5 kW unit
- DIFFER studies: CO_2 plasma-integrated SOEC.

Thank you for your attention!





CO₂ utilisation focused on market relevant dimethyl ether production,
via 3D printed reactor- and solid oxide cell based technologies

3D-printing in catalysis: Development of efficient hybrid systems for the direct hydrogenation of CO₂ to DME

INTERNATIONAL WORKSHOP ON CO₂ CAPTURE AND UTILISATION

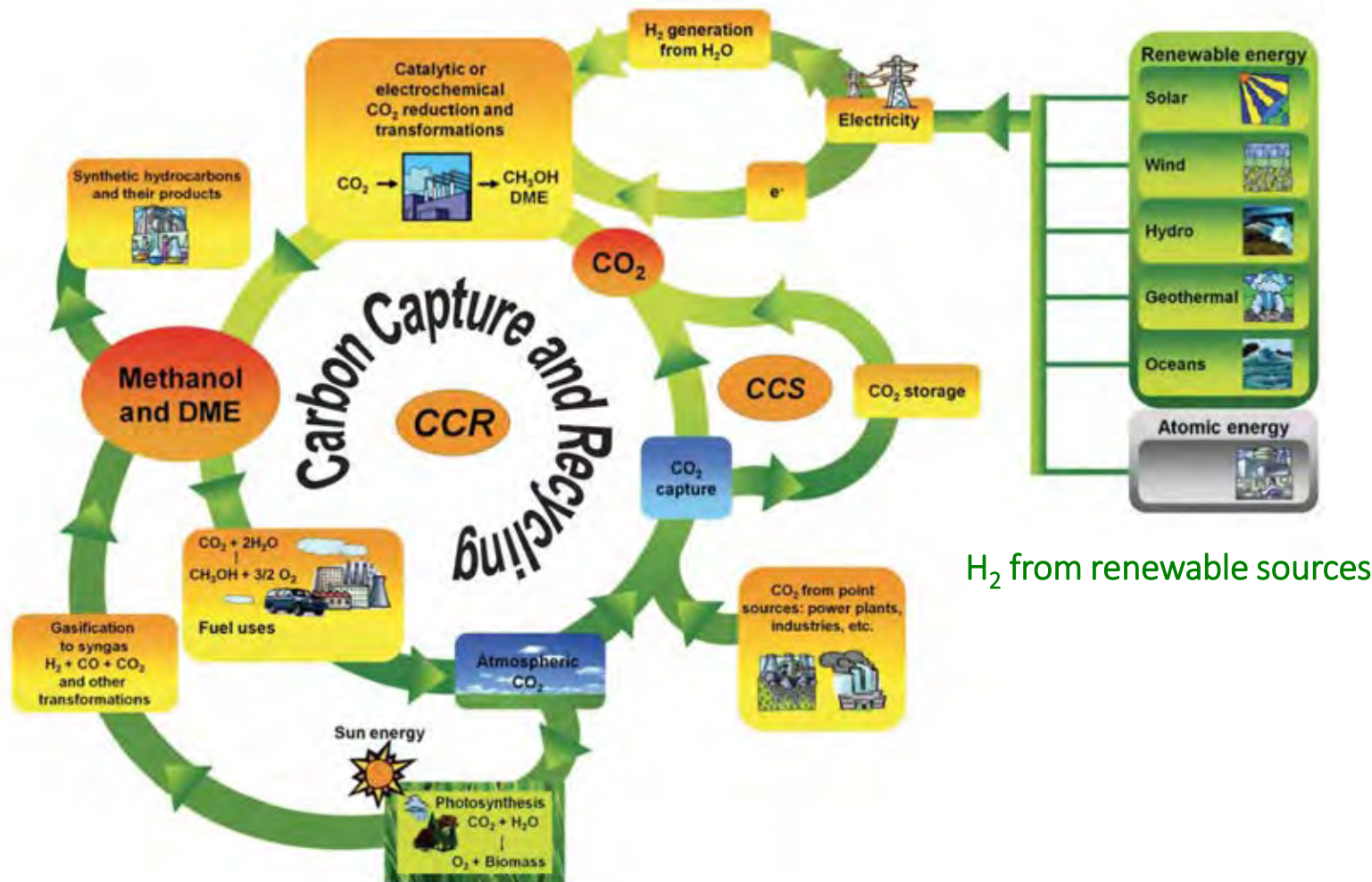
Giuseppe Bonura
16 February 2021



Overview

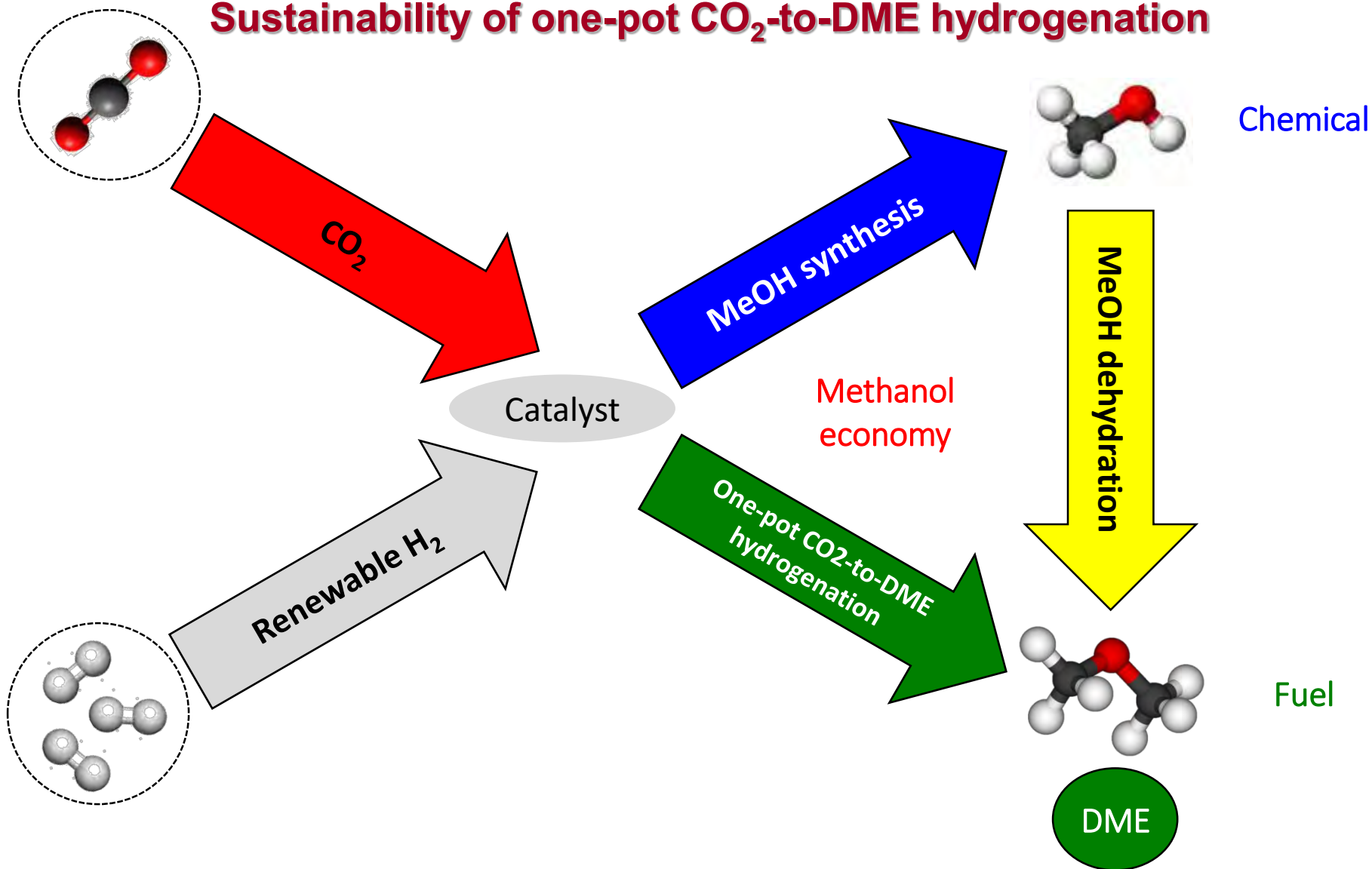
- Carbon Capture and Recycling
- DME: a multipurpose chemical & a fuel
- Conventional two-step processes
- Integrated one-step hydrogenation CO₂-to-DME
- 3D catalysis: a step forward
- Catalytic results
- Rationalization of the catalytic behaviour
- Conclusions

CO₂ as a substitute for toxic CO, derived from fossil carbon

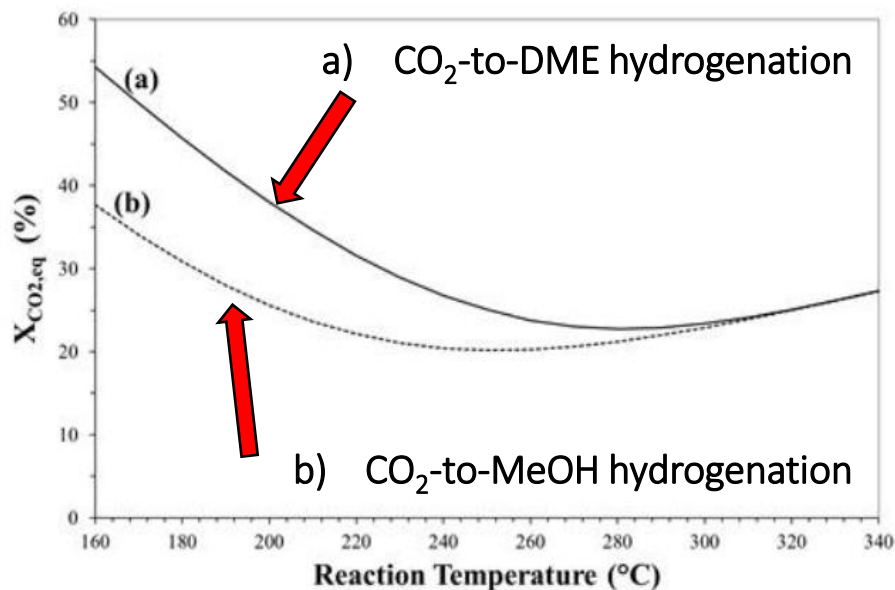


Olah et al.// Chem. Soc. Rev. 43 (2014) 7995

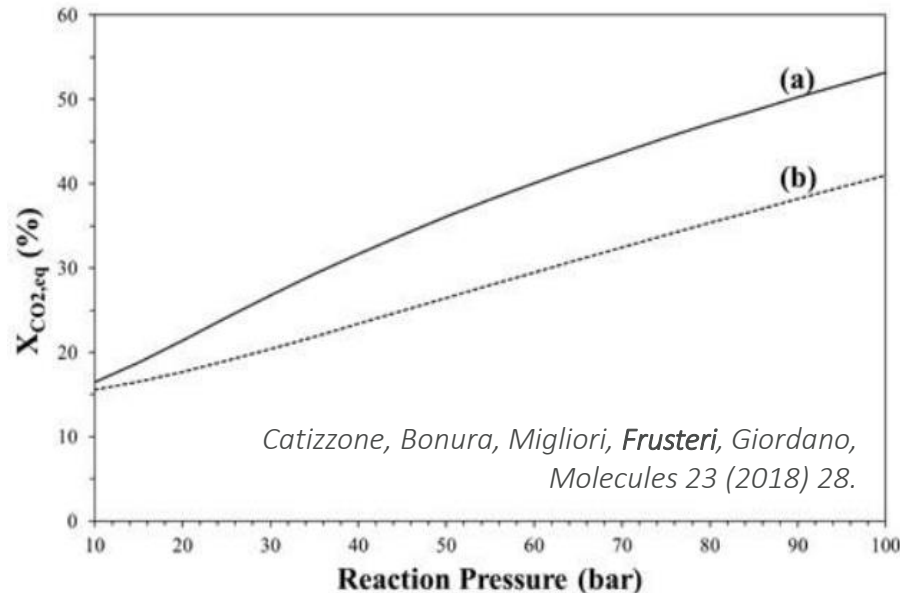
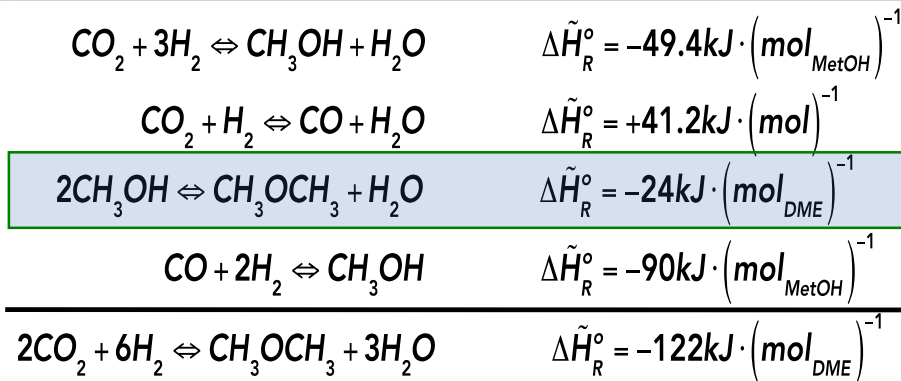
Sustainability of one-pot CO₂-to-DME hydrogenation



Thermodynamics of CO₂ hydrogenation



Due to methanol consumption by dehydration reaction, the one-step process is more efficient than the two-step process, with a main benefit at low temperature and high pressure.



Conventional two-step processes

1. Methanol synthesis from syngas

Cu-based catalysts (high activity and selectivity)

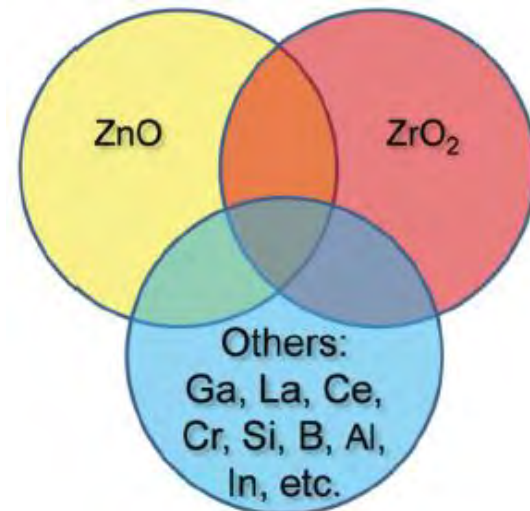
- Catalyst composition

- a) **Support** \Rightarrow
 - High SA_{BET}
 - Cu^+ stabilization

- a) **Promoter** \Rightarrow
 - High MSA_{Cu} and D (%)
 - High Poisoning resistance

- Catalyst preparation

- Co-precipitation [Jingfa *et al.*, 1996]
 - Sol-Gel [Köppel *et al.*, 1998]
 - Incipient-Wetness [Toyir *et al.*, 2001]
 - Combustion [Arena *et al.*, 2004]
 - Reverse coprecipitation under ultrasounds [Arena *et al.*, 2007]
 - Gel-oxalate coprecipitation [Bonura *et al.*, 2014]



OPEN ISSUES

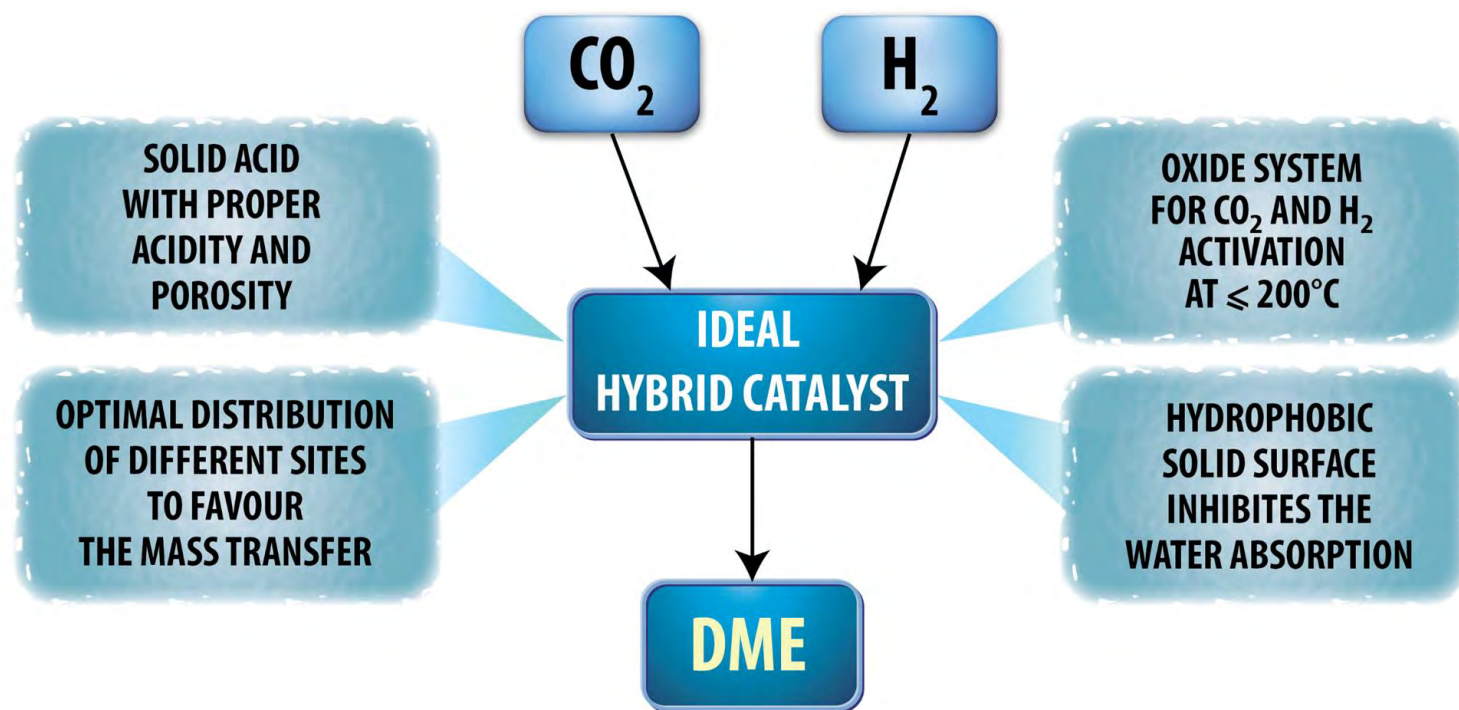
- a) Metal/Support interaction
- b) Metallic Dispersion
- c) “Water Poisoning”
- d) REACTION MECHANISM**

2. Dehydration of methanol

γ -Al₂O₃, zeolites, heteropolyacids, ...

Integrated one-step process: new hybrid catalysts

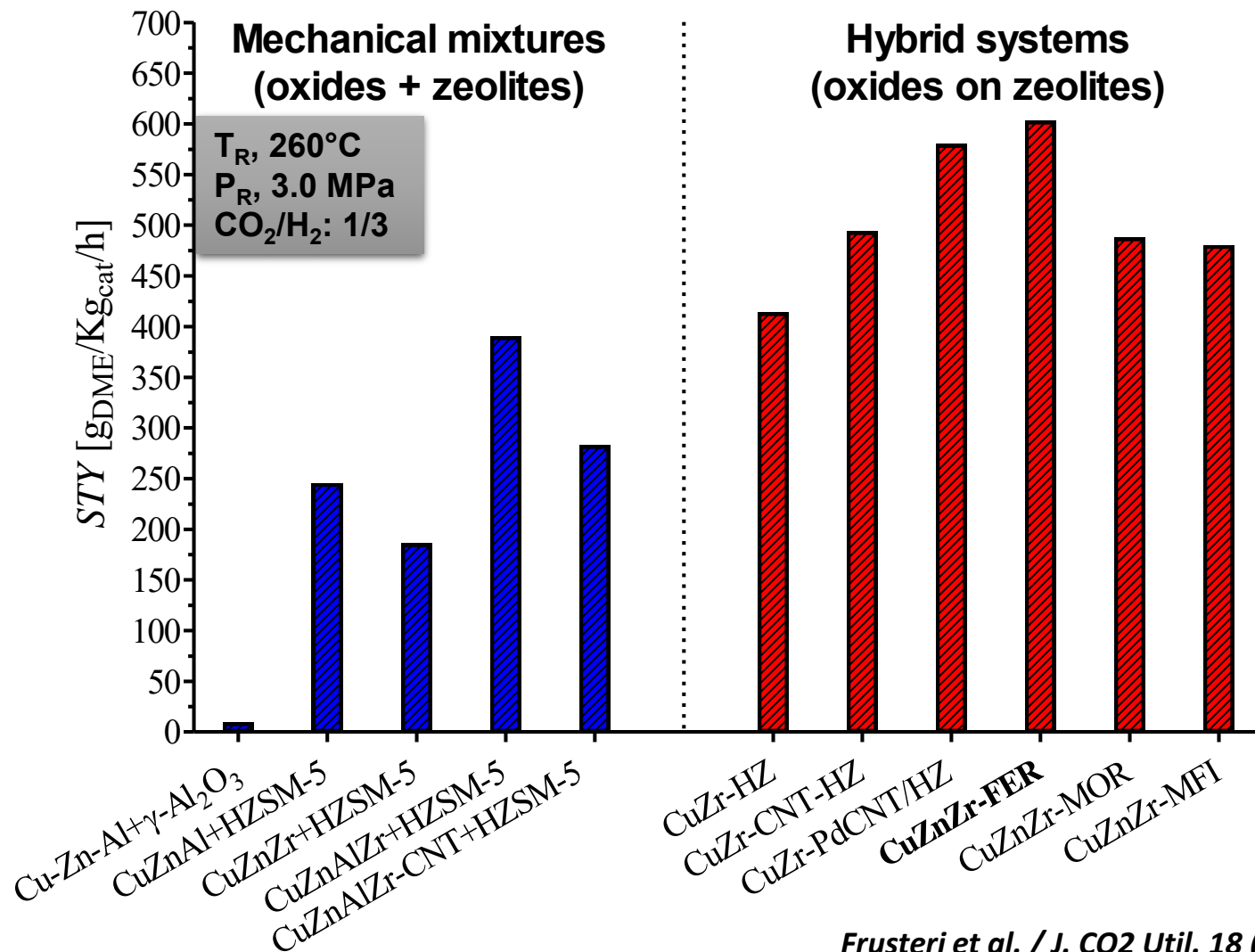
CATALYST CONCEPT



Frusteri et al. // *Catal. Today* 277 (2016) 48–54.

Frusteri et al. // *Catal. Today* 281 (2017) 337–344.

Mechanical Mixtures vs. Single Grain Hybrid Systems



Frusteri et al. / J. CO₂ Util. 18 (2017) 353–361

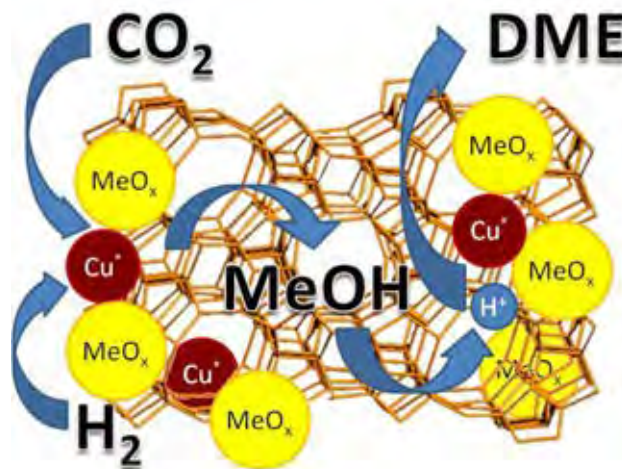
Integrated one-step process: new 3D hybrid catalysts

Preparation of 3D hybrid catalysts with reproducible properties at long radius

Combination of metal/oxide(s) and acidic functionalities in a single solid system

The parent catalysts are not distinguishable anymore

3D printing (VITO)



Coprecipitation of metal precursors by oxalic acid in a slurry solution containing a finely dispersed zeolite / binder paste / printing / drying / calcination



Not only uniform distribution...
exposure vs. accessibility of surface sites

- Reproducibility
- Properties controlled
 - Texture
 - Structure
 - Morphology
 - Surface

Experimental setup

CO₂-to-DME hydrogenation

Reactor id: 4.0 mm

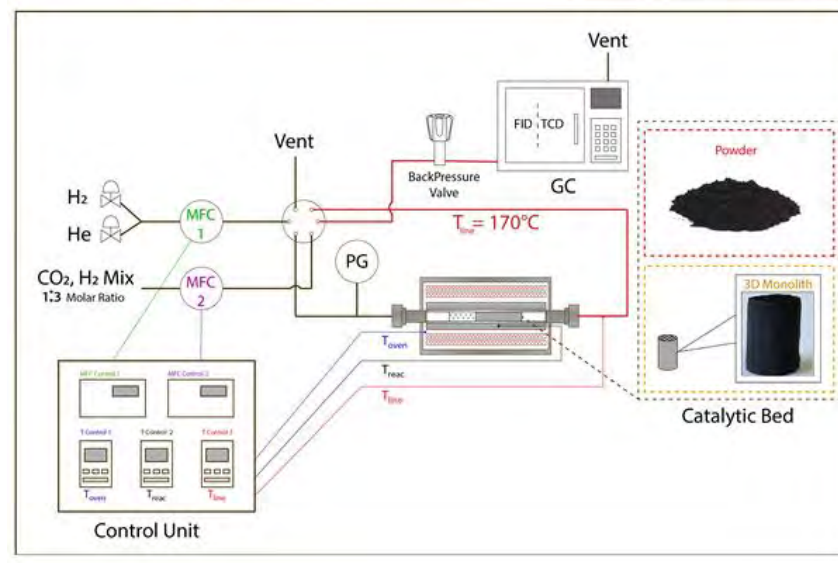
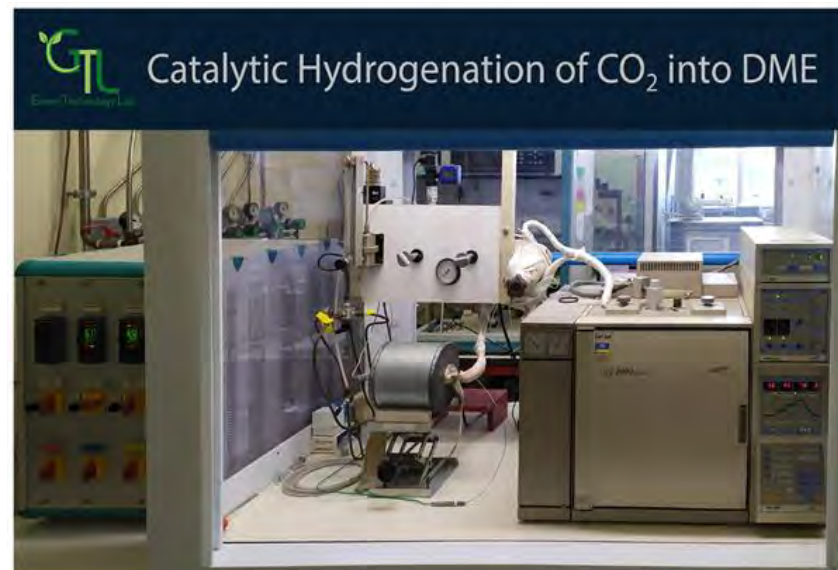
$wt_{cat} = 0.25 \text{ g}$

$H_2:CO_2:N_2 = 69:23:8$

GHSV: 8,800 ml_n/g_{cat}/h

$P_R = 30 \text{ bar}$

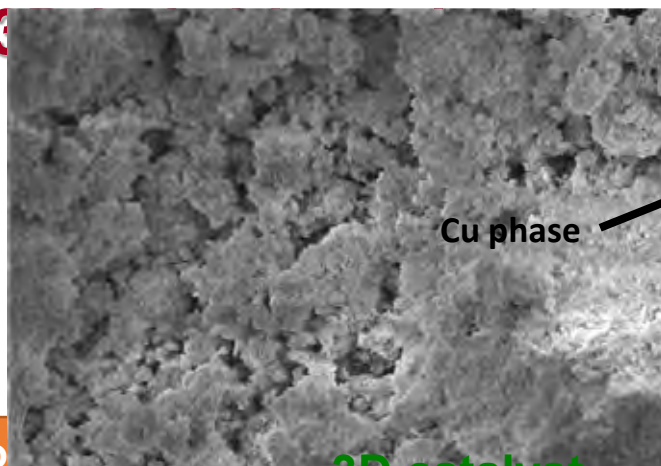
$T_R = 200\text{-}260 \text{ }^\circ\text{C}$



Synthesis of a 3D catalyst

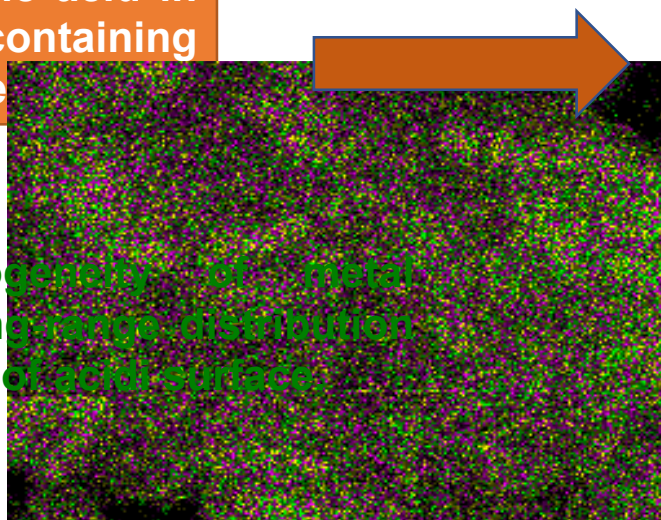
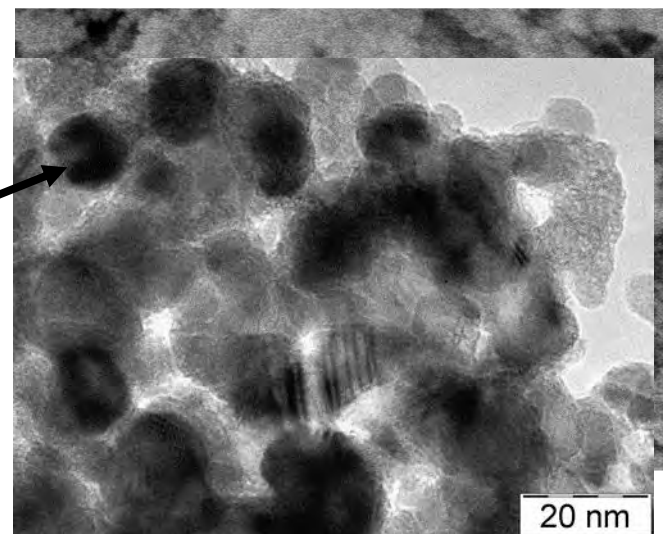
Coprecipitation of metal precursors by oxalic acid in a slurry solution containing the solid acid carrier

Very good homogeneity of metal precursors, with long-range distribution of elements per unit of acid surface

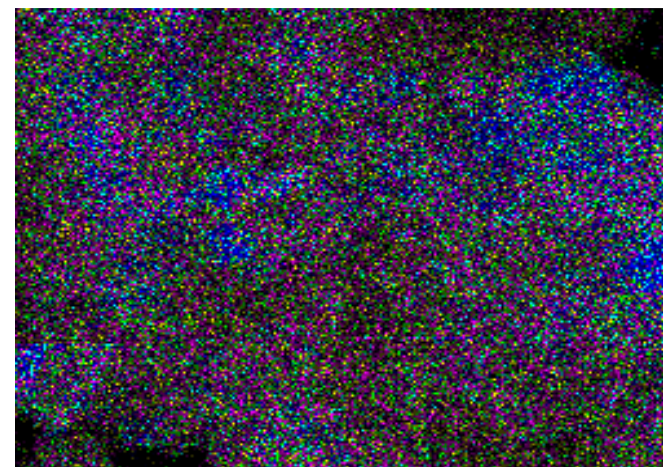


3D catalyst

SEM: 2000x

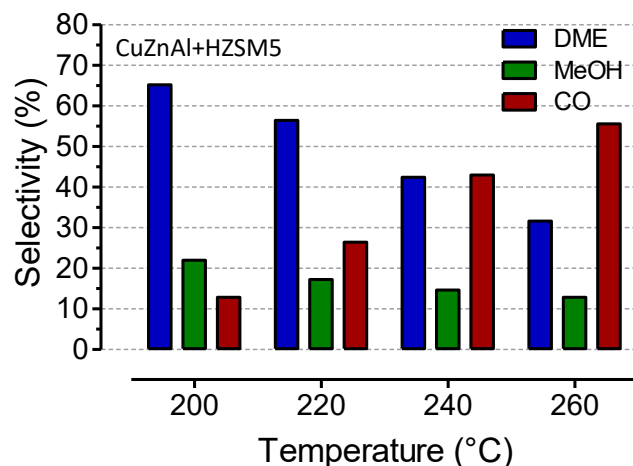
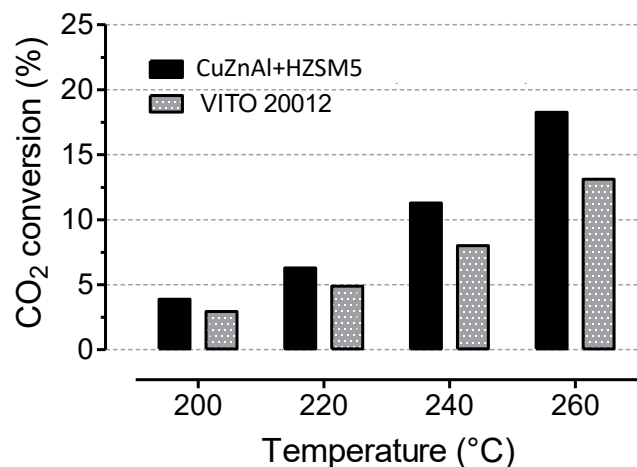


EDAX: CuZnZr



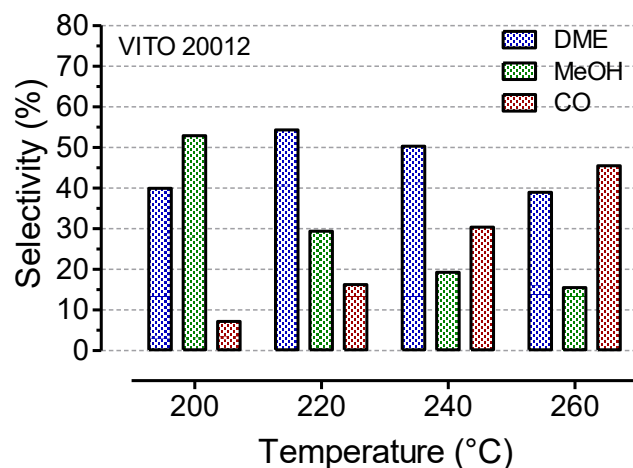
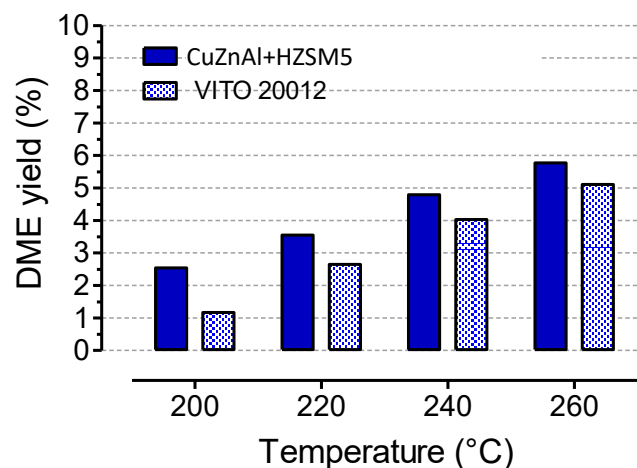
EDAX: CuZnZr:SiAl

Conventional powdered vs. 3D printed catalysts (VITO)



Conventional catalyst exhibits a better performance than the 3D printed crushed monolith

20012



Selectivity pattern quite different between conventional and 3D catalyst

Textural properties

A lower activity of the 3D catalysts is mainly ascribable to a dramatic loss of microporosity during printing

| SAMPLE | SA _{Lang} (m ² /g) (a) | PV (cm ³ /g) (b) | MV (cm ³ /g) (c) | APD (Å) (d) |
|--------------------|---|--------------------------------|--------------------------------|----------------|
| CZA+HZSM5 - fresh | 233.3±1.5 | 0.146 | 0.081 | 25 |
| VITO 20013 - fresh | 30.5±1.2 | 0.140 | 0.008 | 184 |
| VITO 20013 - used* | 175.6±1.5 | 0.173 | 0.060 | 39 |

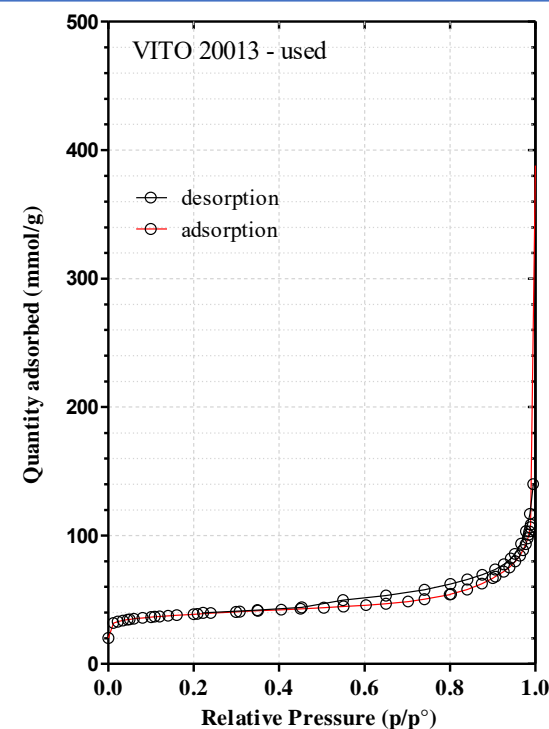
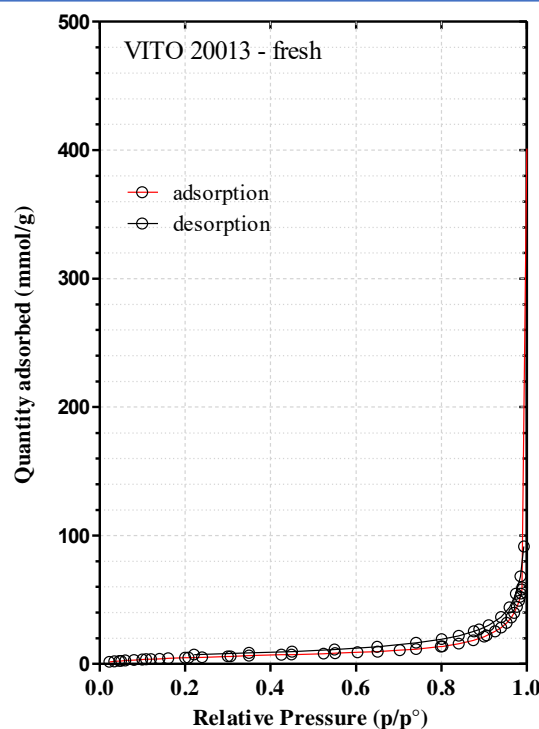
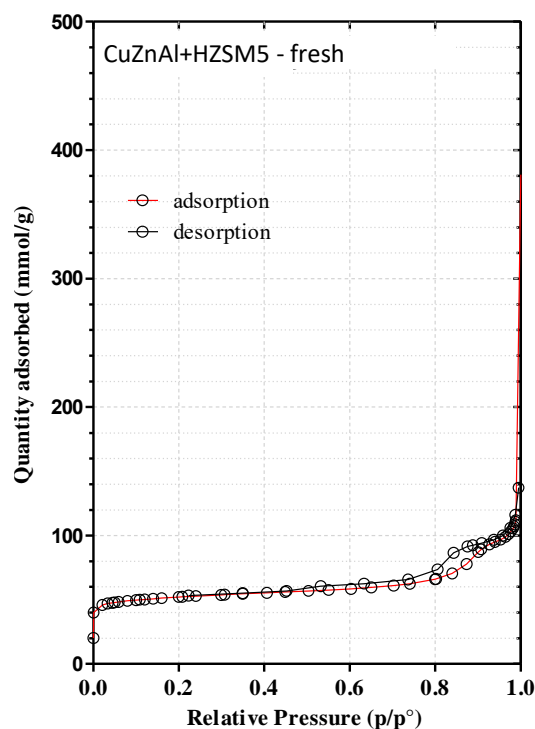
*Sample recovered after run at 30 bar and 260 °C, upon cooling at r.t.

(a) Surface area determined according to the Langmuir model

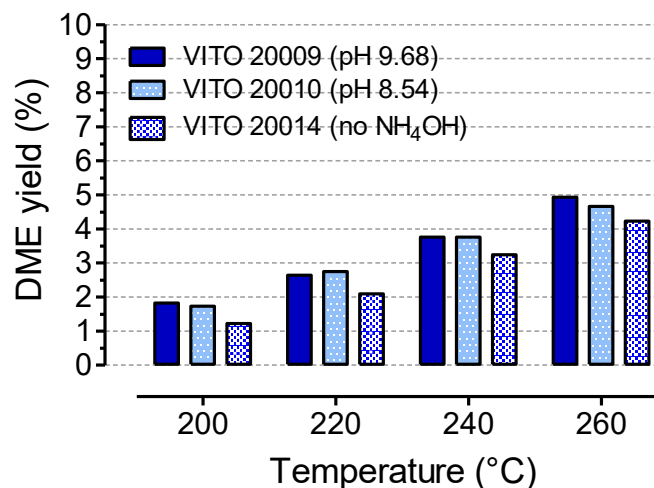
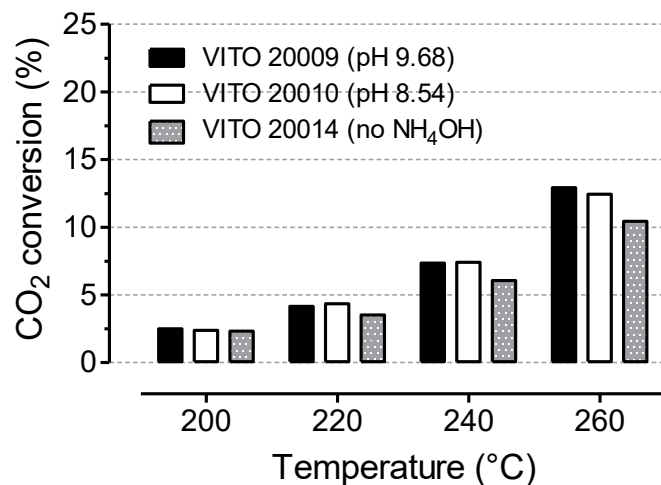
(b) BJH desorption cumulative pore volume

(c) Micropore volume from Horvath-Kawazoe at relative pressure ≈ 0.2

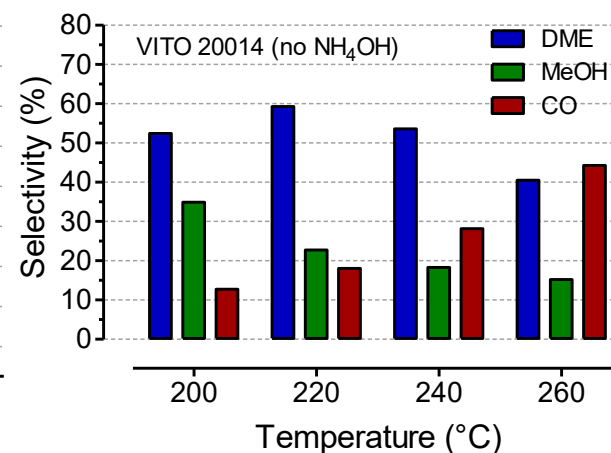
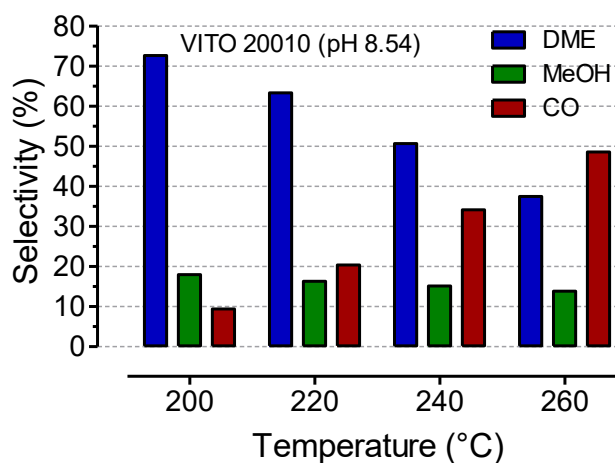
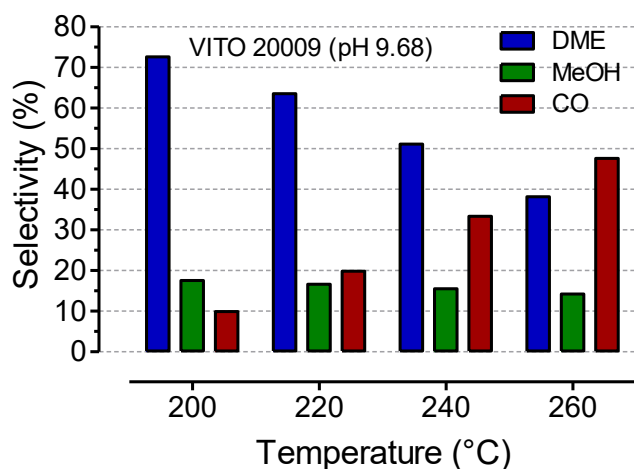
(d) Average pore diameter determined from the geometrical formula: $4PV/SA$



Influence of pH on 3D printing

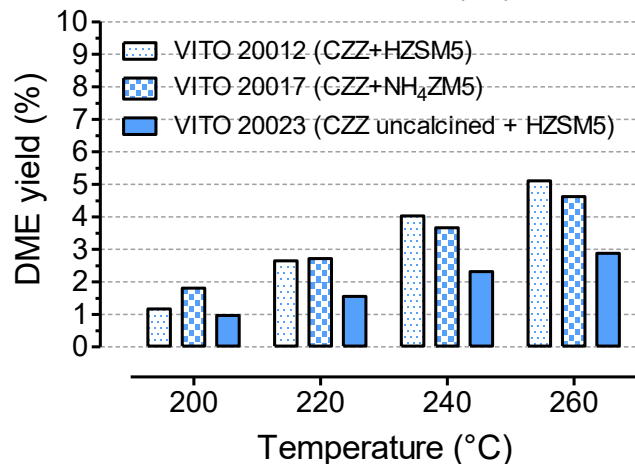
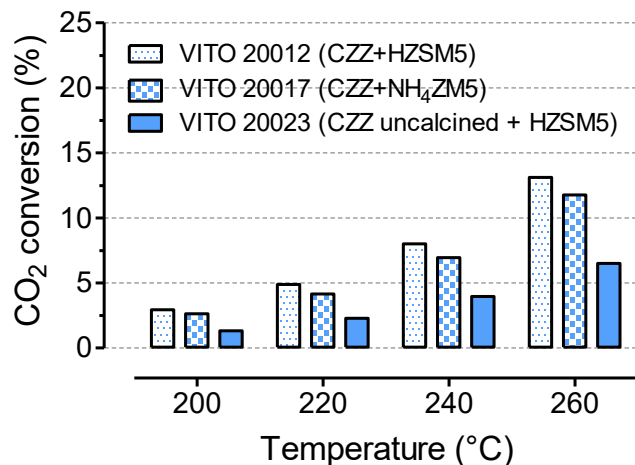


The preparation of the paste for 3D printing benefits from a higher pH

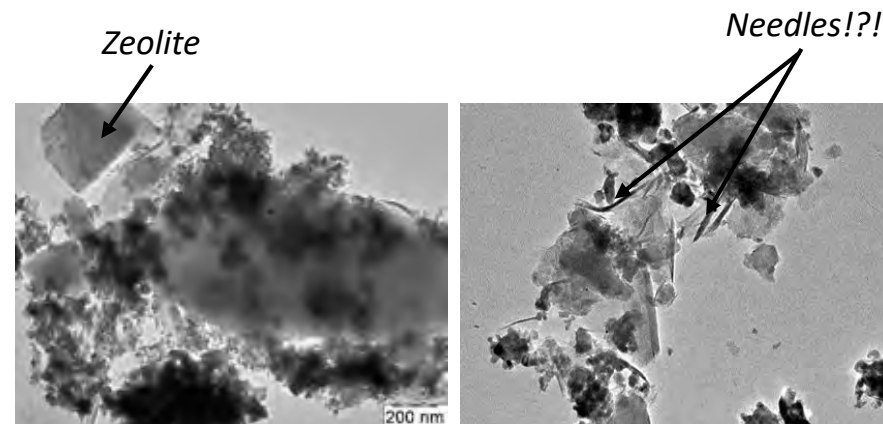


Influence of pre-calcination of the phases :

**VITO 20012 (precalcined phases before printing) vs.
VITO 20017 (CZZ+ NH₄ZSM-5, co-catalyst not calcined) vs.
VITO 20023 (CZZ uncalcined + HZSM-5)**



1. On VITO 20017, printing before stabilization of the zeolite phase prevents the shift of equilibrium as the result of a significant inhibition or reduction of acid sites (NH₃-TPD !), not available/activable anymore even after further calcination.
2. On VITO 20023, the activation of CO₂ is significantly depressed on a poor stabilized Cu phase (XRD!), demonstrating as the extent of metal-oxide interface during preparation/calcination is crucial for addressing catalytic behaviour.



VITO 20017 – TEM images on the fresh sample (calcined at ITAE @ 500 °C)

Key messages

- ❑ The development of a catalytic process for the direct conversion of CO₂ to DME with 3D hybrid systems is feasible.
- ❑ Very promising results were obtained using 3D hybrid system consisting of a mixed oxide phase supported on an acidic preformed carrier.
- ❑ 3D printing before stabilization of the acid phase prevents the shift of equilibrium as the result of a significant inhibition or reduction of acid sites, not available/activable anymore even after further calcination.
- ❑ 3D printing before calcination of methanol phase showed that the activation of CO₂ is significantly depressed on a poor stabilized metal phase, confirming as the extent of metal-oxide interface during preparation/calcination is crucial for addressing catalytic behaviour.
- ❑ High selectivity to DME can be achieved at reaction temperature lower than 250 °C and the current limit is related to CO₂ activation.

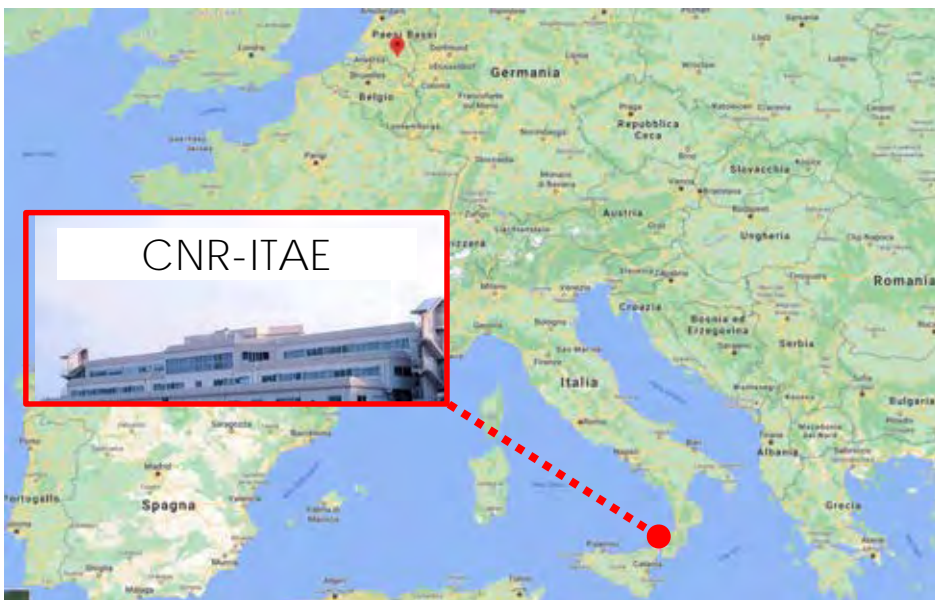
Open Issues

- Novel active phase suitable to activate CO₂ at low temperature taking a direct advantage on DME selectivity (see thermodynamics)
- New binders for a full control of texture/structure/surface properties
- Innovative stacked and alternating 3D reactors for increasing DME productivity from CO₂ hydrogenation in one step
- Optimization of catalyst stability and regeneration

Acknowledgements

❑ EU H2020 - Grant agreement N. 838061 – CO2Fokus

<http://www.itae.cnr.it>



Dr. Francesco FRUSTERI Dr. Catia CANNILLA Mr. Aldo MEZZAPICA



Dr. Giuseppe BONURA

Dr. Serena TODARO

Dr. Leone FRUSTERI

Thank you!



The project has received funding from the European Union's Horizon 2020 research and innovation programme under grant agreement n. 838061

This document reflects only the authors' view and the Innovation and Networks Executive Agency (INEA) and the European Commission are not responsible for any use that may be made of the information it contains.



INTERNATIONAL WORKSHOP ON CO₂ CAPTURE AND UTILIZATION

TU/e - EINDHOVEN - 16-17 FEBRUARY 2021

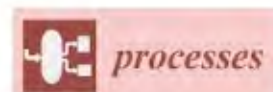
Plenary session (chairperson Fausto Gallucci)

14:00-15:00 Dr. Angels Orduna (Spire 2030)

ORGANIZED BY



SPONSORED BY



Processes4Planet

*Transforming the European Process Industry
for a sustainable planet & a prosperous society*



INTERNATIONAL WORKSHOP ON CO₂ CAPTURE AND UTILIZATION

TU/E - EINDHOVEN

16 February 2021

WHO ARE WE

A vibrant community ...

A.SPIRE – European Cross-Sectoral association



DG R&I
DG Grow



Industrial Associations & Clusters
Industries, incl SME's, New Sectors ...

RTO's & Higher Education Institutions

Consultancies, NGO's,
KIC's, Innovation Agencies, ...

MS & Regional Representatives
Financial Partners

PROCESS INDUSTRY: INDISPENSABLE

- **€ 1.8** turnover
- **4,7%** of EU 28 GDP
- **+ 25 million jobs** (direct & indirect)
- **+ €78 billion (CAPEX) investments** in the EU
- Crucial in an **exceptionally large number of value chains**
- Strongly resilient and **strategically key to relaunch the EU economy post-COVID19**

OPEN APPROACH: inclusive of different stakeholders and welcoming Newcomers

Processes4Planet

Process Industries

From primary & secondary resources
to materials with
required properties and functionalities



Circular
Bio-based EU

Clean Steel

Chemicals Risk Assessment

Clean Energy
Transition

Resources



Clean H2

Water4All

Minimized input
of primary
resources

Enablers

EIT Digital KIC
AI, Data & Robotics
Key Digital Technologies

EIT Raw
materials KIC

EIT Inno
Energy KIC

EIT Climate KIC

EIT Manufacturing KIC

Manufacturing industries and contractors

Manufacturing of
consumption goods or capital goods
enhancing quality of life of citizens



Built4People

Made in Europe

Batteries

Driving Urban Transition
for a Sustainable Future

Society



Waste management,
regions and cities



Accelerating Innovation and Maximising sustainable impact accross sectors and borders



- First Partnership ever gathering **8 Process Industry sectors. Currently 10**
- **Continuous dialogue on R&I and trust relation** across SPIRE sectors and beyond
- **Enhanced voice** to shape the framework of process innovation and competitiveness through the dialogue with the public sector

THE VOICE OF
10 SECTORS

JOINT
SOLUTIONS

- **Collaboration** with the innovation ecosystem, the value chain, society and the public sectors (RTOs, NGOs, EC, MS, regions...)
- Development of **joint solutions** through **125 SPIRE projects** funded from **2014 to 2019**, always respecting the Intellectual Property

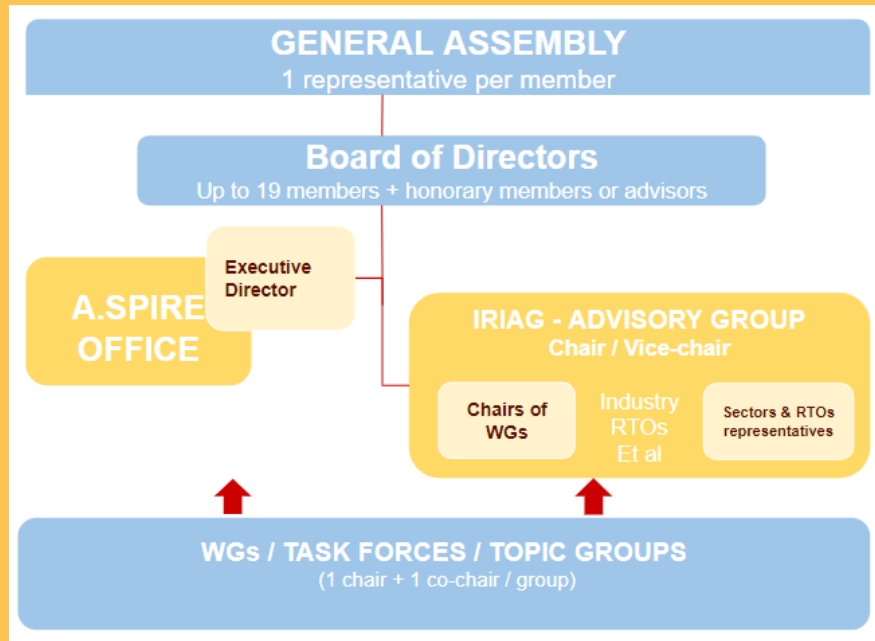
- Direct access to a **pool of knowledge, talent** and applied research services through the RTOs
- Direct access to specialised SME providers
- Direct access of **SMEs** to growth opportunities, customers and new markets

OPPORTUNITIES

GOVERNANCE SPIRE cPPP

PRIVATE PARTNER ASSOCIATION SPIRE

- Discuss priorities
- Propose call topics
- Form consortia
- Apply to calls



PARTNERSHIP BOARD

- Discuss priorities & call topics H2020/HEU
- Assess progress



PUBLIC PARTNER

- Develop work programme
- Publish open calls

European
Commission

TRENDS REPORT 2020 – SPIRE PROJECTS OUTCOMES

In 2014-2019 SPIRE cPPP has supported a total of **125 projects**.

1775

organisations participating in SPIRE granted projects

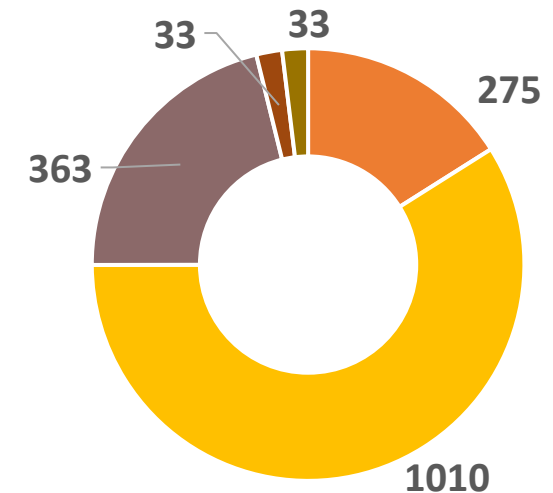
30%

of the participating organisations are **SMEs**

EUR 205 million

EC contribution to SPIRE projects **SME participants**

Organisations in granted projects per category



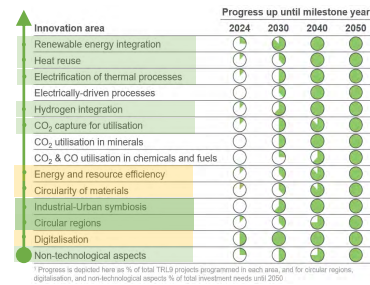
- Higher or Secondary Education Establishments
- Private for-profit entities
- Research Organisations
- Public Bodies
- Others

Transformation levers and tools to enable P4Planet to achieve its ambitions





Unique cross-sectoral community



36 innovation programmes to FILL the GAP

+ Skills, Jobs, Competitive gap analysis, Framework/Standards



First-of-a-kind plants

Hubs for Circularity



Ambitions to enable Prosperity for all



Climate neutrality

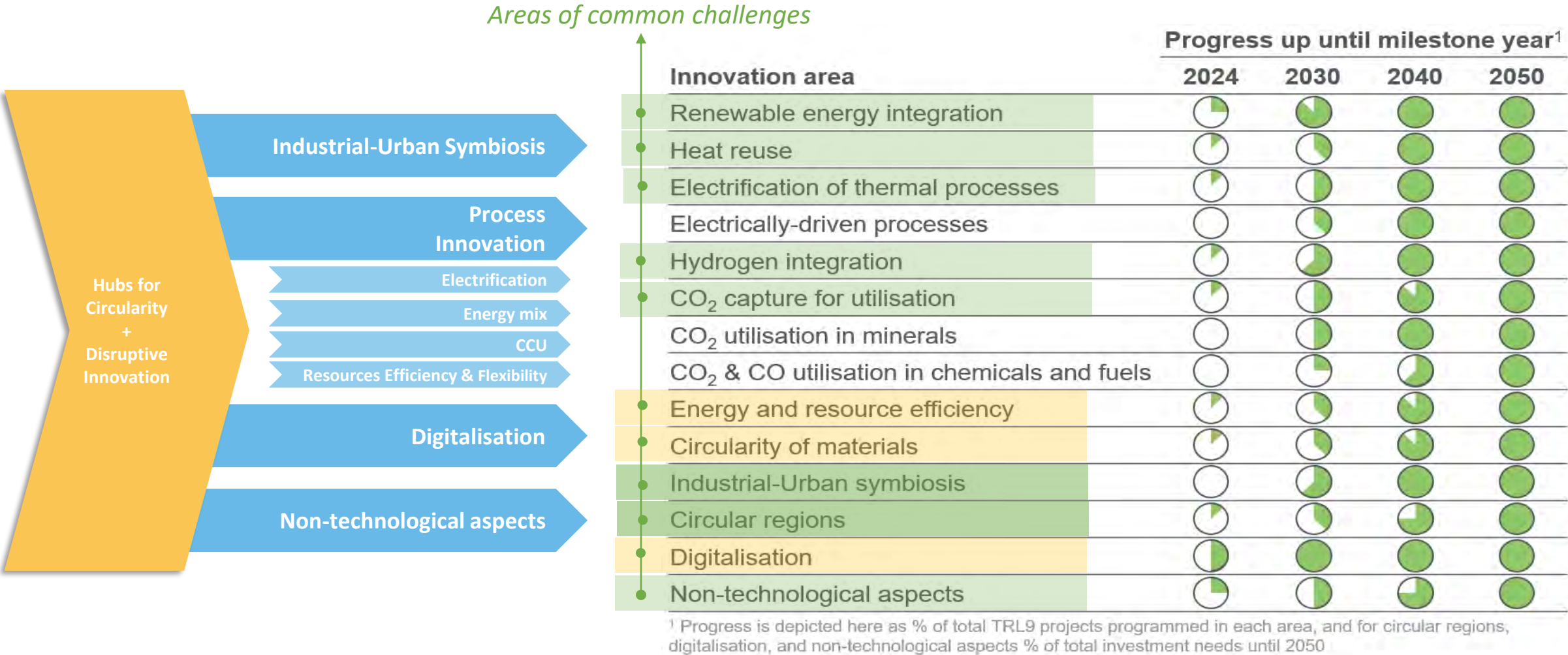


Near zero landfilling and near zero water discharge

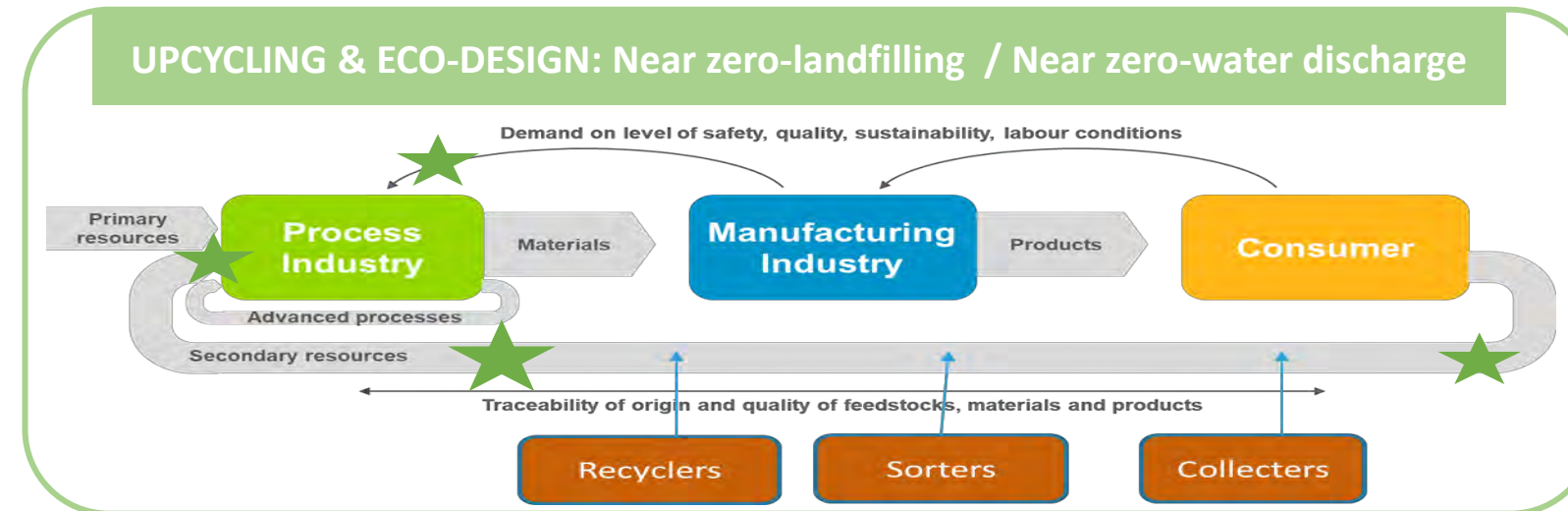
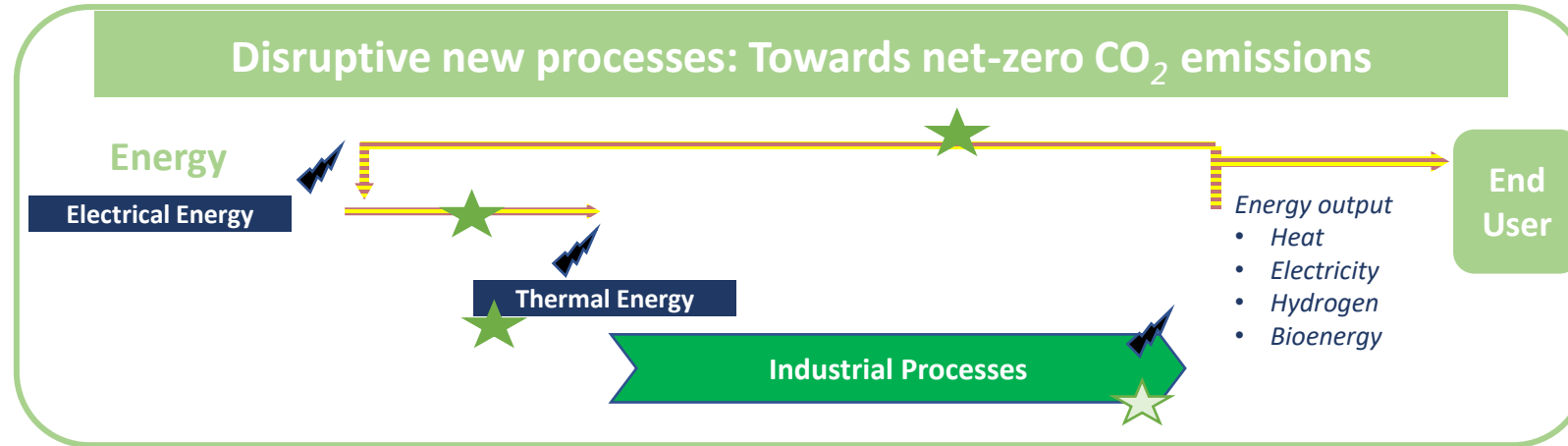


Competitive EU process industries

Processes4Planet Innovation Areas progress towards 2050



Combining efforts & ideas will accelerate innovations



36 innovation programmes



CARBON CAPTURE AND USE STORIES



P4Planet roadmap

Building on the results of SPIRE projects

- **CLIMATE AMBITION:** towards the net-zero emissions scenario
- **Focus on:** process CO₂ emissions and indirect emissions
- **Specific Objective 2:** Reduce emissions through CO/CO₂ capture and use.
 - Develop new efficient CO/CO₂ capture and purification technologies
 - Develop efficient CO₂ valorisation routes to chemicals, minerals and fuels
- **KPI 2:** co₂ eq. emissions reduction potential through CO₂ Capture and Use measured through a relevant number of demonstrators. (Target: 100% reduction trajectory at TRL7)

| 14 IAs Innovation area | | 36 IPs | Innovation programme |
|------------------------|--|--------|--|
| 1 | Renewable energy integration | 1a | Integration of renewable heat and electricity |
| | | 1b | Integration of bioenergy, waste and other new fuels |
| | | 1c | Hybrid fuel transition technologies |
| | | 1d | Flexibility and demand response |
| 2 | Heat reuse | 2a | Advanced heat reuse |
| 2 | Electrification of thermal processes | 3a | Heat pumps |
| | | 3b | Electricity-based heating technologies |
| 4 | Electrically-driven processes | 4a | Electrochemical conversion |
| | | 4b | Electrically driven separation |
| 4 | Hydrogen integration | 5a | Alternative hydrogen production routes |
| | | 5b | Using hydrogen in industrial processes |
| | | 5c | Hydrogen storage |
| 6 | CO2 capture for utilisation | 6a | Flexible CO2 capture and purification technologies |
| 7 | CO2 utilisation in minerals | 7a | CO2 utilisation in concrete production |
| | | 7b | CO2 utilisation in building materials mineralisation |
| 8 | CO2 & CO utilisation in chemicals and fuels | 8a | Artificial photosynthesis |
| | | 8b | Catalytic conversion of CO2 to chemicals or fuels |
| | | 8c | Utilisation of CO2 and CO as building block in polymers |
| | | 8d | Utilisation of CO to chemicals or fuels |
| 9 | Energy and resource efficiency | 9a | Next-gen catalysis |
| | | 9b | Breakthrough efficiency improvement |
| 10 | Circularity of materials | 10a | Innovative materials of the process industries |
| | | 10b | Inherent recyclability of materials |
| | | 10c | Upgrading secondary resources |
| | | 10d | Wastewater valorisation |
| 11 | Industrial-Urban symbiosis | 11a | Demonstration of Industrial-Urban Symbiosis |
| 12 | Circular regions | 12a | European Community of Practice |
| | | 12b | Development of Hubs for Circularity |
| 13 | Digitalisation | 13a | Digital materials design |
| | | 13b | Digital process development and engineering |
| | | 13c | Digital plant operation |
| | | 13d | Intelligent material and equipment monitoring |
| | | 13e | Autonomous integrated supply chain management |
| | | 13f | Digitalisation of industrial-urban symbiosis |
| 14 | Non-technological aspects | 14a | Integration of non-technological aspects in calls |
| | | 14b | Human resources, skills and labour market |

UNLOCKING PRIVATE INVESTMENTS & BARRIERS TO MARKET FOR CLIMATE NEUTRAL & CIRCULAR SOLUTIONS

- ★ De-risk investments
- Financial Flow up to TRL9
- Define framework conditions for market uptake
- Available & affordable green energy as enabler
- Holistic digital process innovation 4.0 as accelerator
- ★ Hubs for Circularity to accelerate innovation

★ **P4PLANET**



★ **Competitive
Process Industry**

- ★ Jobs
- Skilled workforce
- Sustainable Processes
- Sustainable Materials
- Shift to a real circular economy
- Circular Regions
- Export innovations worldwide
(CO2 has no borders)

**36 innovation
programmes**



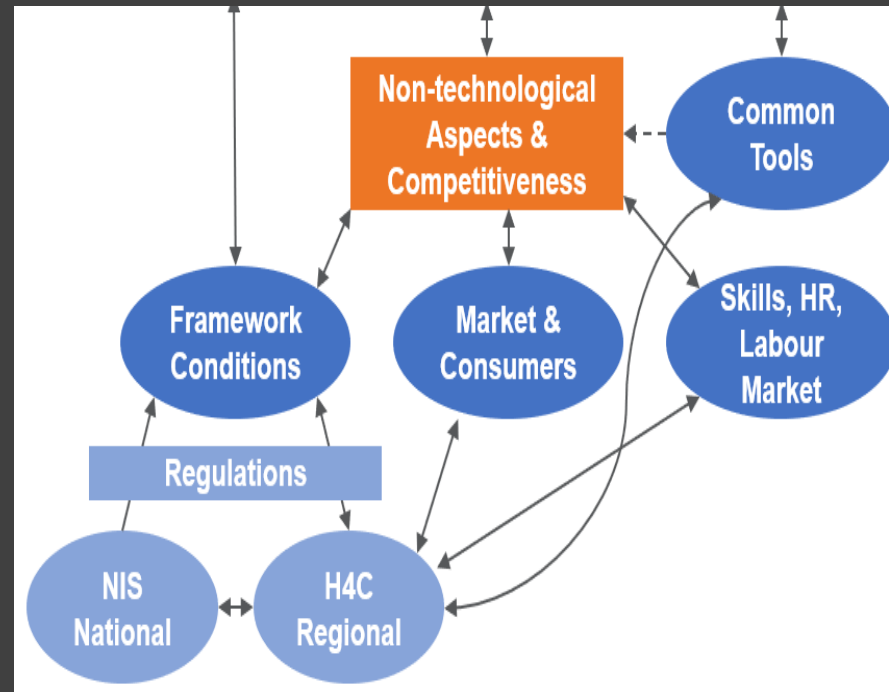


**“European Energy Intensive Industry
Skills Agenda and Strategy”
Erasmus+ Project**



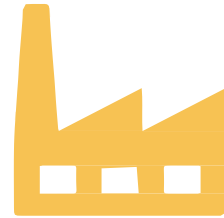
SPIRE/P4PLANET sectors and innovation eco-system
working together for the skills of the future
on Industrial-Urban Symbiosis
and the Process Industry 4.0

NON-TECH & SOCIAL INNOVATION Delivering more societal, economic and market impact.

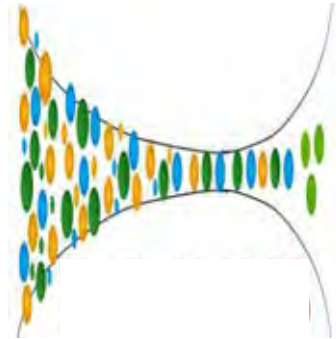


- EU, national & regional framework conditions
- Management of market & consumer demands & changes
- Effective common tools: LCA, business models, digital methodologies...
- Gender balance
- Human Resources, skills and labour market

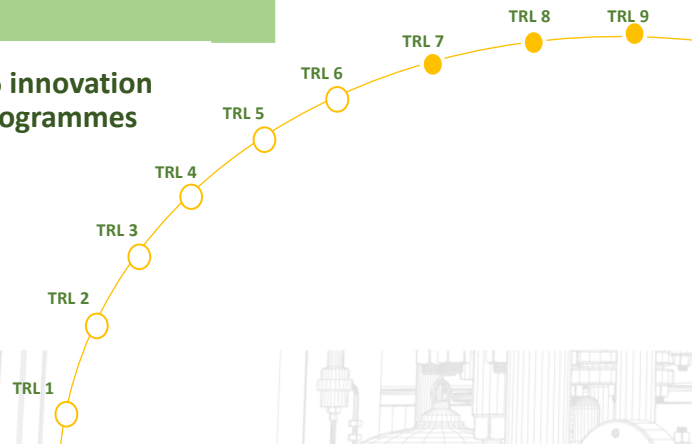
MARBLES: a showcase of the Process Industry transformation



FIRST OF A KIND
FOAK Plants
FOAK Units within a plant



36 innovation
programmes

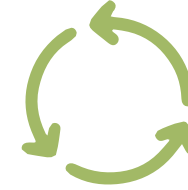


- **First-of-a-kind Large scale plants in operation**
- Combine one or several P4Planet Innovations towards the 2030/2050 ambitions to reach Climate neutrality and circularity
- Acting as Hubs of bulk amounts of resources from industry and the municipalities.
- Several marbles will likely connect to reach together the targets of the partnership's KPIs
- **50+ Marbles** identified of which ca. We aim to **launch 15 in the period 2021 – 2030**, responding to the green-deal plan, and enabled by the P4planet innovation portfolio

PRIVATE INVESTMENTS

- Industry leader commitment
- when technical and economic feasibility is proved through Horizon Europe programs.
- Public support needed to de-risk and accelerate





FIRST OF A KIND

Hubs for Circularity

36 innovation programmes



SRL 1

SRL 2

SRL 3

SRL 4

SRL 5

SRL 6

SRL 7

SRL 8

SRL 9

Starting Hubs

Intermediate Hubs

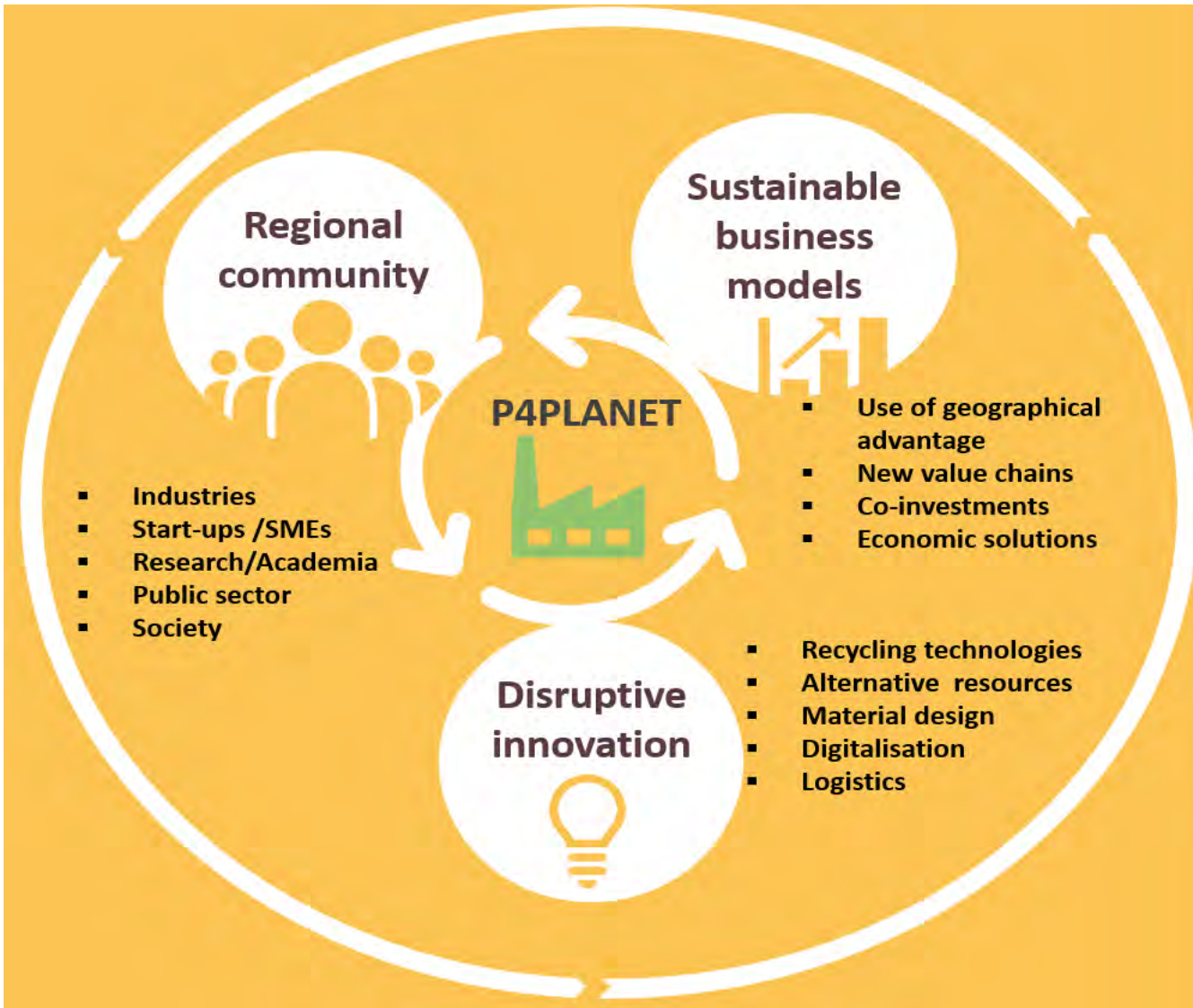
Advanced Hubs

Mature Hubs

SRL: Symbiosis Readiness level

Based on the *"Study and portfolio review of the projects on industrial symbiosis in DG Research and Innovation: findings and recommendations"* by Klaus H. Sommer

Systemic geographical proximity connected across EU regions

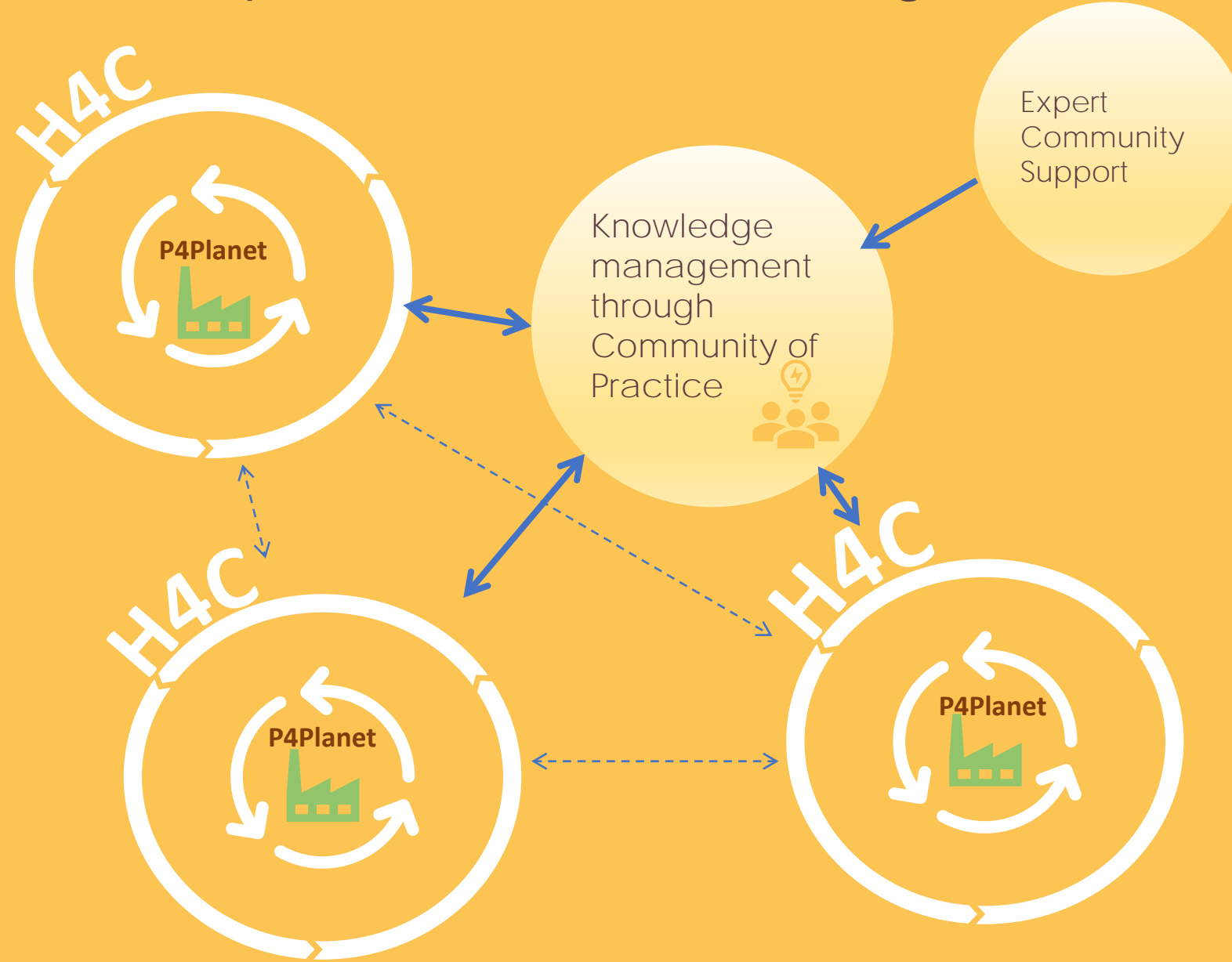


THE H4Cs CONCEPT

Self-sustaining economic industrial ecosystems for full-scale Industrial-Urban Symbiosis and Circular Economy, closing energy, resource and data loops and bringing together all relevant stakeholders, technologies, infrastructures, tools and instruments necessary for their incubation, implementation, evolution and management.

- Territorial systemic solutions (regional approach)
- Processes4Planet inside!
- Facilitation necessary to overcome non-technological barriers to symbiosis

European Community of Practice



Platform for non-competitive exchange of knowledge and best practices

- Practical toolbox: technologies and tools
- Innovation programmes for finding the missing pieces in the puzzle of symbiosis
- Modelling circular concepts and plants of the future
- Enhancing replicability
- Communication and transfer of technologies and solutions
- Education and training
- Sustainability of the network

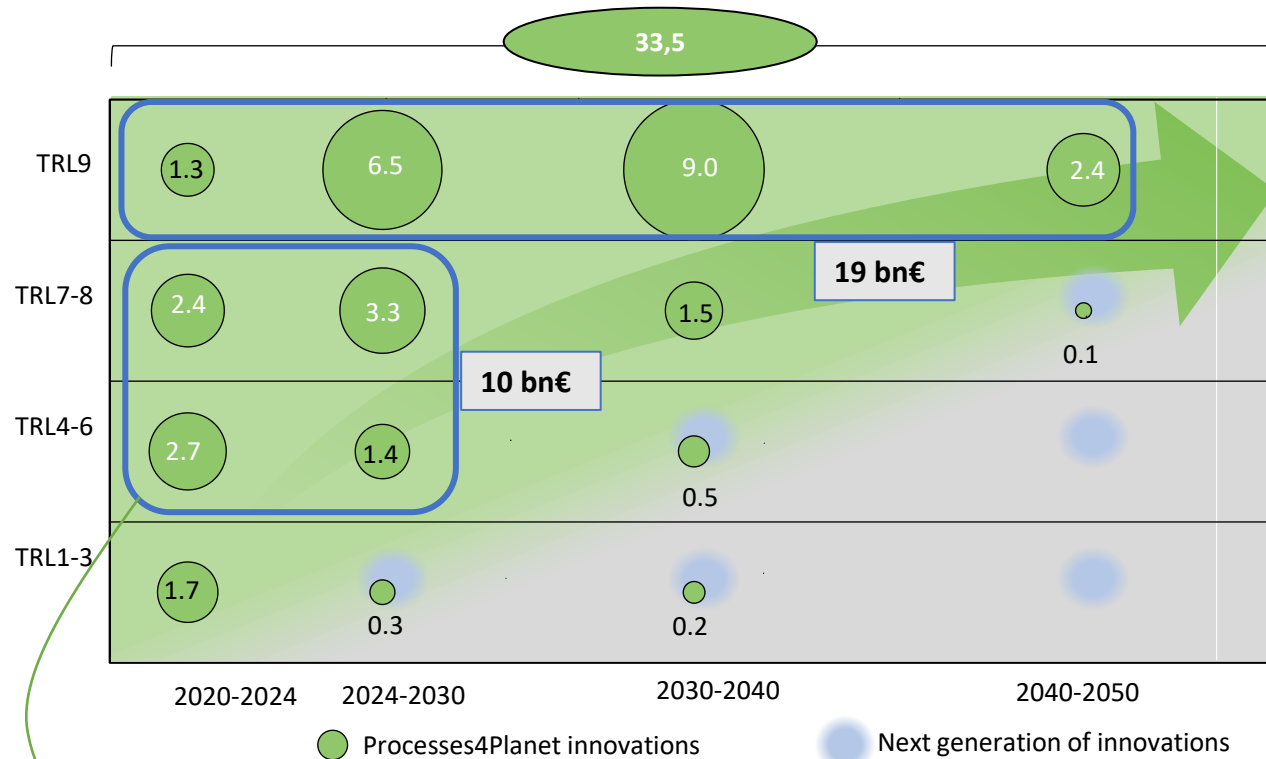
MASSIVE INVESTMENTS NEEDED TO REACH IMPACT

JOINING FORCES WILL HELP

R&I Investment needs (TRL 1- 9), € billion

Roll out investments

2050 impacts



- Estimated in trillions €
- Two rounds of investments for PI before 2050



Climate neutrality



Near zero landfilling and near zero water discharge



Competitive EU process industries

R&I Investments can be optimized if we avoid redundancies

WHY JOIN A.SPIRE

Teaming up to address the challenges of Climate Change, Circular Economy and Competitiveness together

LARGER INDUSTRIES:

- Continuous dialogue on R&I across SPIRE sectors and beyond
- Channel to raise your voice on R&I for HEU & other programmes
- Access to a pool of knowledge & talent (in Universities, research centres....)
- Direct access to SME providers
- Collaboration with the innovation ecosystem and value chain
- Access to developments by other projects, SMEs, universities...
- Protection of intellectual property
- Dialogue with the EC, MS, regions, MePs & other stakeholders

Further benefits to other members

SMEs:

- Direct Access to growth opportunities
- Direct Access to new markets
- Direct Access to large industry customers

RTOs, NGOs Innovation agencies et al.:

- Direct Access to applied innovation
- Link to deliver impact to society and regions
- Collaboration for disruptive innovations



SMEs in SPIRE: A Success Story



Growing above the EU-28 average

- 7 new employees / SME (higher than EU average = 2)
- 40% growth in turnover (+double than EU average)
- 27% of SMEs won new business through SPIRE contacts



Key to Process Innovation

- Innovative SMEs delivering innovations for the Process Industry
- They develop the solutions with their customers
- The roadmap signals their market opportunities

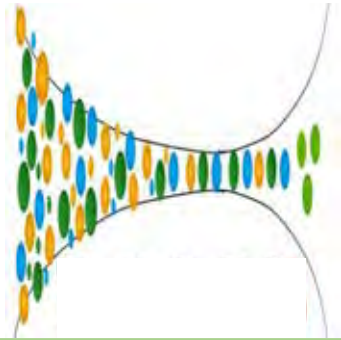
SMEs ARE PARTNERS IN +100 SPIRE PROJECTS like Dryficiency, Dream, Reslag, Liberate, etc...

SMEs COORDINATE + 17 SPIRE ROJECTS like Scaler, Sharebox, Maestri, IdB, Spring, MultiCycle, etc...

Ceramics awarded as the most successful small sector in SPIRE projects



SMEs in P4PLANET: Key players & opportunities



**36 innovation
programmes
to FILL the GAP**



First-of-a-kind plants

Hubs for Circularity



SPECIALISED ON DIFFERENT AREAS:

- Process Innovation for the Process Industry
- Engineering
- IT
- Waste Management
- I-U Symbiosis
- Etc.

**KEY PARTNERS
IN P4PLANET
PROJECTS**

RAISE THE SMEs VOICE

- In Working Groups
- In the Advisory Group
- In the Board

**Key players in the
HUBS4CIRCULARITY**

WHAT'S NEXT

- **February –March 2021:**
 - A.SPIRE members finalise topics and negotiations for P4Planet's MoU
 - Define new working structure within A.SPIRE
 - 8 to 17 Feb: **P4PLANET's ideation/brokerage event**
 - March (tbc): **follow up P4Planet's Brokerage event**
 - 19 March (A.SPIRE BoD) + 31st March (A.SPIRE General Assembly)
- **April 2021: Signature of Processes4Planet MoU with the European Commission**
- **May 2021: Processes4Planet launch event (Process Industry conference)**
- **April – June 2021:**
 - Kick-off of new working structure of A.SPIRE: engagement of our members
 - Kick-off of the new governance and advisory structures of Processes4Planet: Partnership Board, Feedback Panel and Impact Panel
 - 19 June: A.SPIRE BoD meeting
- **September - November 2021: Projects & H4Cs Forum** + Board meeting



Connected across borders and to citizens

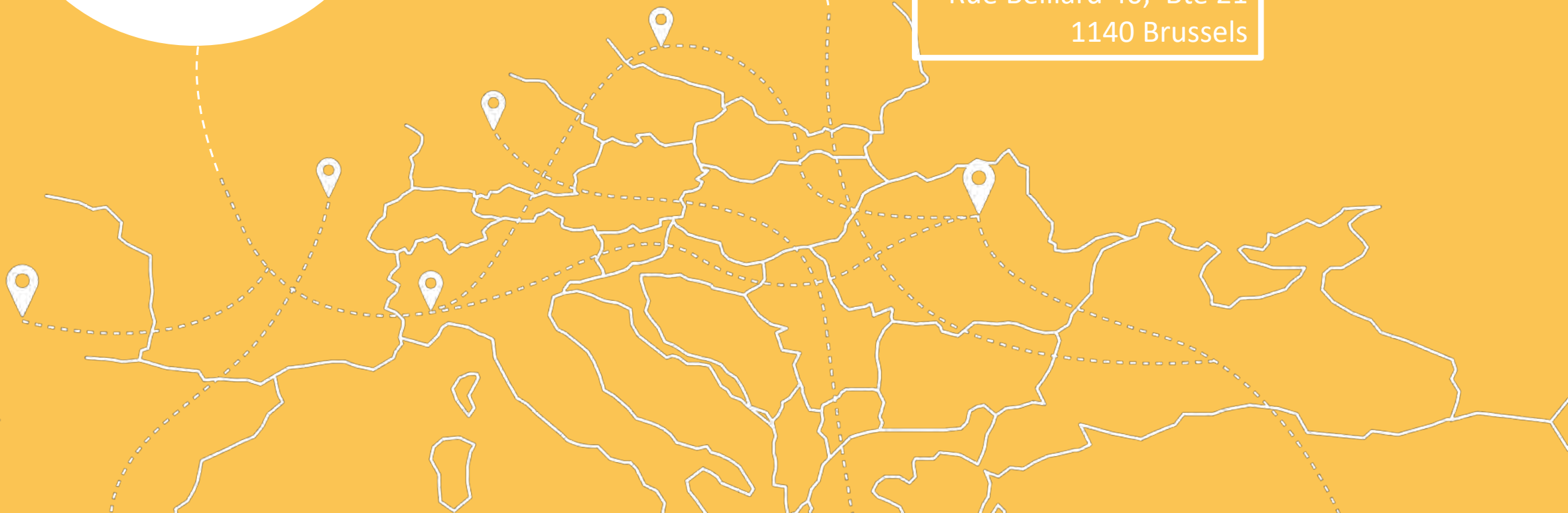
CONTACT US: Àngels Orduña

aor@spire2030.eu

info@spire2030.eu

www.spire2030.eu

Rue Belliard 40, Bte 21
1140 Brussels



INTERNATIONAL WORKSHOP ON CO₂ CAPTURE AND UTILIZATION

TU/e - EINDHOVEN - 16-17 FEBRUARY 2021

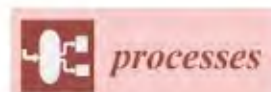
Session 2A (chairperson Giampaolo Manzolini)

- 15:00-15:20 Dr. G. Garcia - LCA and TEA of the COZMOS technology
- 15:20-15:40 Dr. A. Mattos or Dr. A. Mitchell - How can public policy and business model innovation be developed to address challenges of CCUS and realise the opportunity?
- 15:40-16:00 Dr. L. Engelmann - Perception of CO₂-based fuels and their production in international comparison
- 16:00-16:20 Dr. N. Dunphy - Social studies in REALISE project

ORGANIZED BY



SPONSORED BY



LCA and TEA of the CO2MOS technology

Guillermo Garcia-Garcia

G.Garcia-Garcia@Sheffield.ac.uk

UK Centre for Carbon Dioxide Utilisation

The University of Sheffield

International Workshop on CO2 Capture and Utilization

16-17 February 2021



COZMOS: Efficient CO2 conversion over multisite Zeolite-Metal nanocatalysts to fuels and OlefinS.

This project has received funding from the European Union's Horizon 2020 research and innovation programme under Grant Agreement No. 837733.

Contents

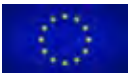
- Introduction to LCA and TEA methodologies
- Literature review of LCA studies of CCU products
- Environmental analysis of catalysts
- Initial stages of the full LCA and TEA for COZMOS
- Conclusions



LCA and TEA methodologies

- As research in CCU matures, investors and funders require clarification on the credentials of these technologies
- Governments and regional authorities are creating roadmaps and require clarity on CCU options
- Companies are trying to choose between bio-based, CCU and other waste routes to create their products and need data for comparisons
- Life-Cycle Assessment (LCA) can help us to analyse environmental consequences of decisions
- Techno-Economic Assessment (TEA) can help us to analyse economic consequences of decisions
- Both LCA and TEA allow technologies to be compared

What are the environmental and economic consequences of CCU?
Can CCU reduce CO₂ emissions and be economically profitable?



Definition of LCA

Life-cycle assessment is a methodology to account for the environmental impacts of a product, service, process, company, etc. throughout its entire life cycle



Structure of LCA studies

INTERNATIONAL STANDARD

**ISO
14040**

Second edition
2006-07-01

Environmental management — Life cycle assessment — Principles and framework

*Management environnemental — Analyse du cycle de vie — Principes
et cadre*

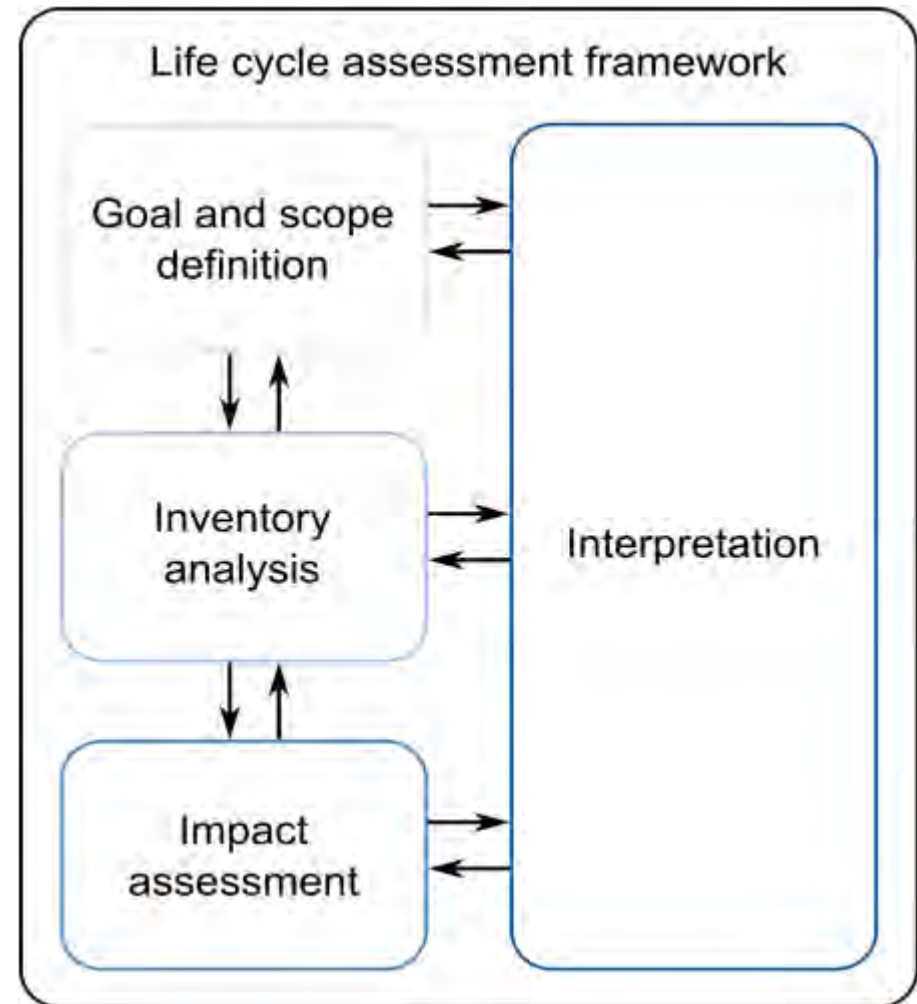
INTERNATIONAL STANDARD

**ISO
14044**

First edition
2006-07-01

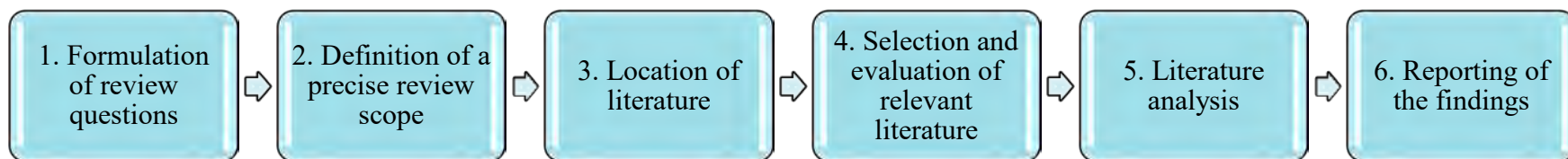
Environmental management — Life cycle assessment — Requirements and guidelines

*Management environnemental — Analyse du cycle de vie — Exigences
et lignes directrices*



Literature review

- Following CCU products studied:
methanol, methane, DME, DMC, propane and propene



Methodology for analytical review

Research questions

1. What are the most promising products that could be produced from CO₂?
2. What are the potential environmental impacts and/or benefits of producing these products from CO₂, in comparison with traditional methods?
3. What is the level of application of the LCA methodology to study CCU?



Literature review – general findings

- Large potential from CCU for a number of feedstocks
- Main constraints:
 - Availability of green hydrogen. If hydrogen is from fossil sources or current grid mix, the environmental benefits can be reduced or disappear
 - The origin of electricity has a key role in determining the final environmental impact of the process. Current grid mix is unfavourable, future scenarios need to be realistic
 - CO₂ capture, separation, purification and transport needs have a high impact
- Need for full LCAs to assess the environmental impacts
 - Not only look at Global Warming Potential or carbon footprint, but also other impacts
 - All life cycle stages have to be considered for a consistent, robust analysis
- A strong value chain is required to support the production of CO₂-based products



Literature review – use of LCA to analyze environmental impacts of CCU technologies

- Few LCA studies of CCU systems have been undertaken so far
- Often, significantly different results are obtained for LCA studies carried out for the same CO₂-based product manufactured by the same route
- Main reasons behind this are different assumptions about the supply of feedstocks (e.g. CO₂, H₂ and electricity), definition of the system boundaries, and the way to allocate products and co-products (i.e. multi-functionality issues)
- Most studies focus on climate change or global warming only, omitting the rest of the environmental impact categories
- A common framework for LCA of CCU is needed: in addition to generic LCA standards (e.g. ISO 14040, ILCD Handbook) we are using The Guidelines for LCA and TEA of CCU



More information in our journal article

- “Analytical review of Life Cycle Environmental Impacts of Carbon Capture and Utilization Technologies”
- Published in ChemSusChem in January 2021
- Open Access, free to download at:
<https://chemistry-europe.onlinelibrary.wiley.com/doi/abs/10.1002/cssc.202002126>

doi: 10.1002/cssc.202002126

Analytical Review of Life-Cycle Environmental Impacts of Carbon Capture and Utilization Technologies

Guillermo Garcia-Garcia,^[a] Marta Cruz Fernandez,^[a] Katy Armstrong,^[a] Steven Woolass,^[a] and Peter Styring^{*[a]}

[a] UK Centre for CO₂ Utilization, Department of Chemical and Biological Engineering, The University of Sheffield, Sir Robert Hadfield Building, Sheffield, S1 3JD, UK

[b] Tata Steel, Unit 2, Meadowhall Business Park, Carbrook Hall Road, Sheffield S9 2EQ, UK

*Corresponding author. E-mail: p.styring@sheffield.ac.uk

Abstract

Carbon capture and utilization (CCU) has been proposed as a sustainable alternative to produce valuable chemicals by reducing the global warming impact and depletion of fossil resources. To guarantee that CCU processes have environmental advantages over conventional production processes, thorough and systematic environmental impact analyses must be performed. Life-Cycle Assessment (LCA) is a robust methodology that can be used to fulfil this aim. In this context, this article aims to review the life-cycle environmental impacts of several CCU processes, focusing on the production of methanol, methane, dimethyl ether, dimethyl carbonate, propane and propene. A systematic literature review is used to collect relevant published evidence of the environmental impacts and potential benefits. An analysis of such information shows that CCU generally provides a reduction of environmental impacts, notably global warming/climate change, compared to conventional manufacturing processes of the same product. To achieve such environmental improvements, renewable energy must be used, particularly to produce hydrogen from water electrolysis. Importantly, we identified different methodological choices being used in the LCA studies, making results not comparable. There is a clear need to harmonize LCA methods for the analyses of CCU systems, and more importantly, to document and justify such methodological choices in the LCA report.

Keywords

Carbon capture and utilization • environmental analysis • life-cycle analysis • sustainable chemistry • renewable resources

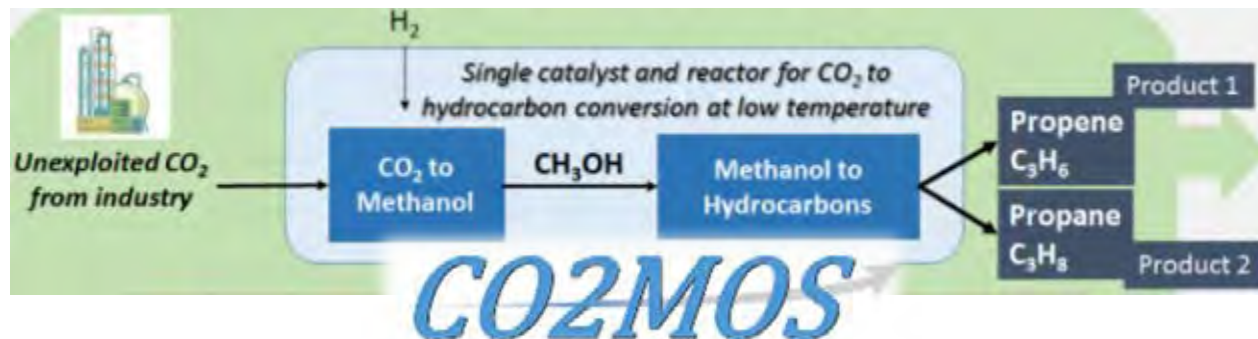
1 Introduction

Global anthropogenic fossil CO₂ emissions have continuously increased over the last decades, peaking at 37.9 Gt in 2018 [1]. They represent over 75% of the total anthropogenic greenhouse gas (GHG) emissions [1], causing global warming and therefore affecting the Earth's climate system. IPCC [2] estimates that, if these emissions keep growing at the current rate, global

Page 1 of 54



Environmental impacts of catalysts



- Catalyst compared:
 - ✓ ZnO:ZrO₂ / ZSM-5
 - ✓ PdZn@ZrO₂ / SAPO-34
 - ✓ ZnCeZrO_x / H-RUB-13
- Cradle to gate comparison
- The comparison was initially done in terms of 1 g of catalyst produced

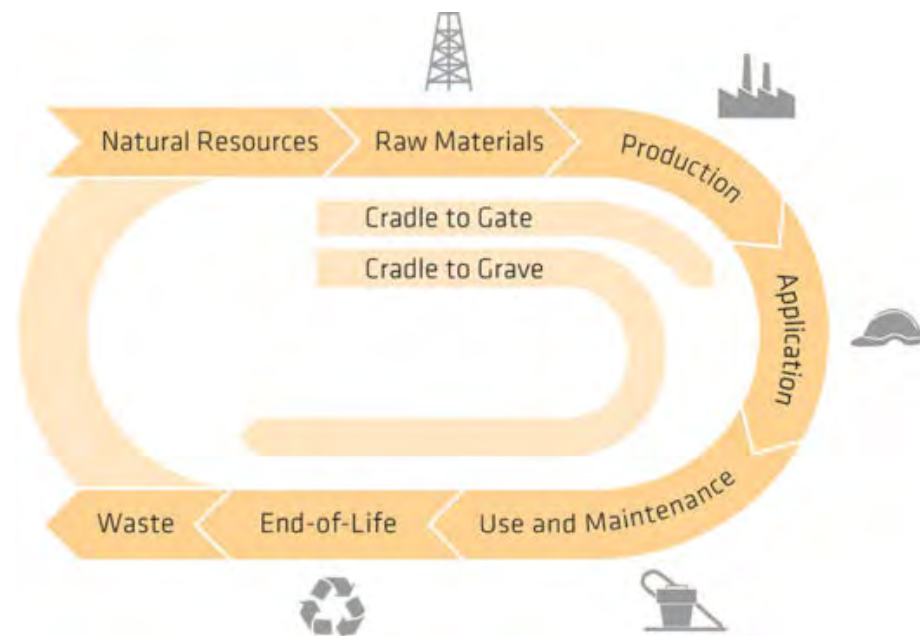
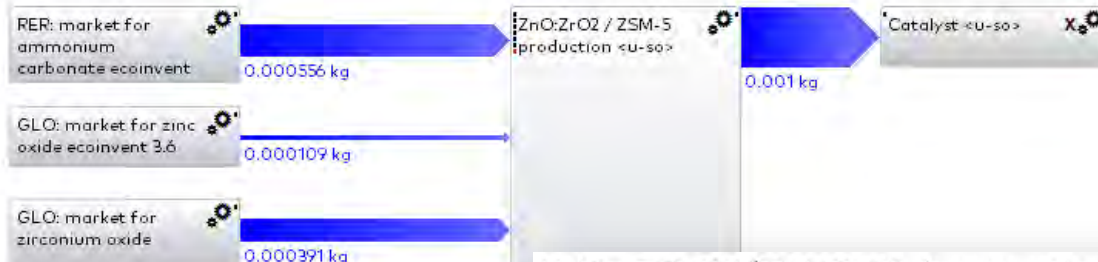


Diagram source: Silka Concrete

GaBi models

ZnO:ZrO₂ / ZSM-5

Process plan: Mass [kg]



PdZn@ZrO₂/SAPO-34 (conventional impregnation)

Process plan: Mass [kg]

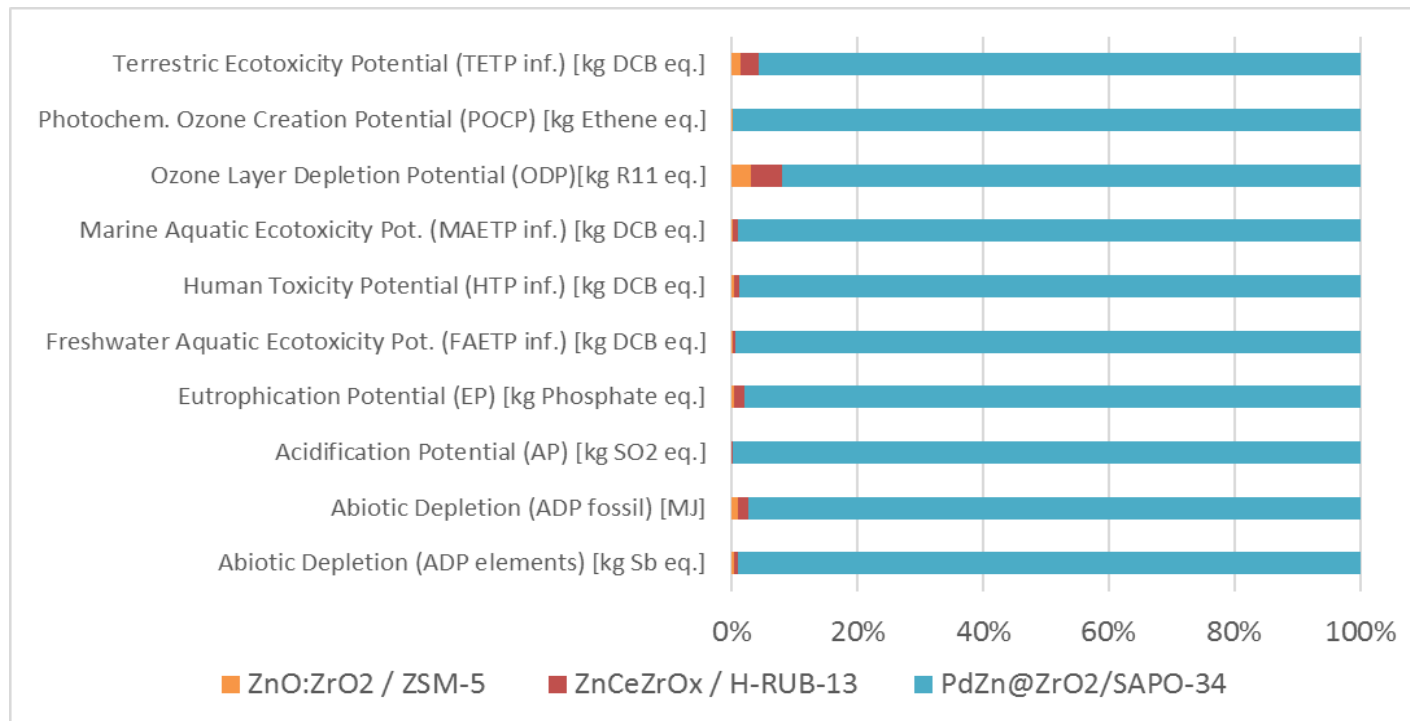


thinkstep
GaBi



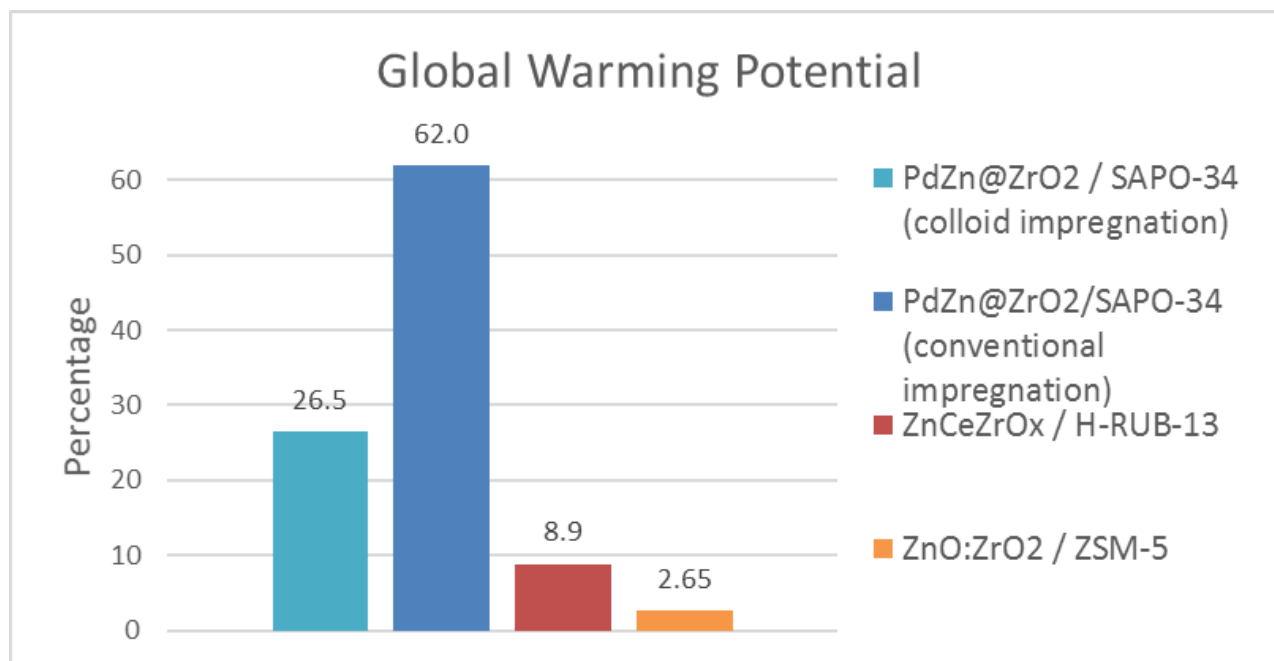
Environmental impact results

- With the assumptions of the study, the catalyst with palladium had the largest global warming potential, most of it coming from the palladium content
- The catalyst with the lowest GWP is ZnO:ZrO₂/ZSM-5



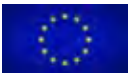
Sensitivity analysis

- We also did sensitivity analysis for the catalyst preparation method and the reaction yield
- Including the increased yield, reduced the relative impact of the catalyst compared to the other ones, but remained the highest one

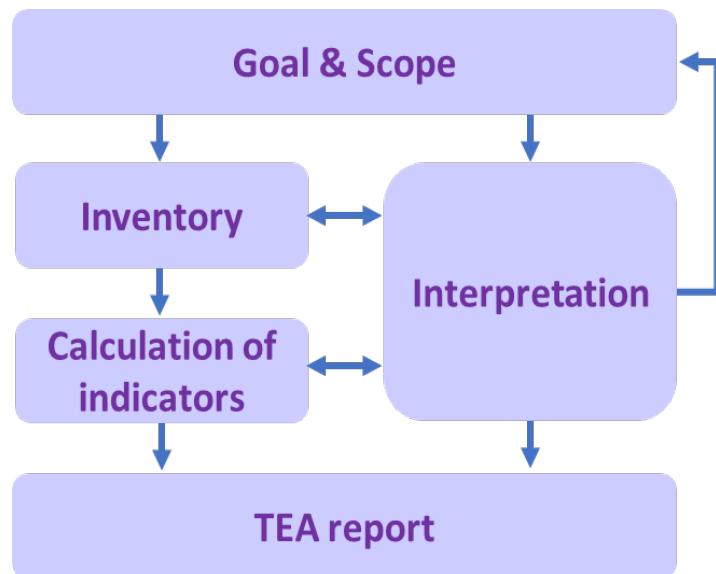


Definition of TEA

- Techno-Economic Assessment (TEA) is a **methodology to analyze the technical and economic** performance of a process, product or service
- TEA integrates **cost, revenue and technical criteria** with a general focus on the production phase (but not always) – typically gate to gate type studies
- TEA is an assessment methodology that can aid in making decisions
- TEA can be used to feed back recommendations during the design phase
- TEA results are specific to a scenario/context



Structure of TEA studies



TEA is built on the framework outlined in the LCA ISO

- **Goal** provides guidance for the overall study
- **Scope** defines the system boundary
- **Inventory** collects the relevant data
- **Calculation** produces results
- **Interpretation** assesses the quality of results, provides recommendations & conclusions
- **Reporting** captures the outputs of the study in a form that can be communicated consistently and transparently

TEA is an iterative process – we often go back and make adjustments



Scope of LCA and TEA studies

- Both **LCA** and **TEA** will be aligned
- **The main goal** is to assess whether the use of carbon intensive gases from the steel industry and the petrochemical refinery to produce propane and propene would have an economic and/or environmental benefit when compared to the conventional production of those products

- **Gate to gate** study

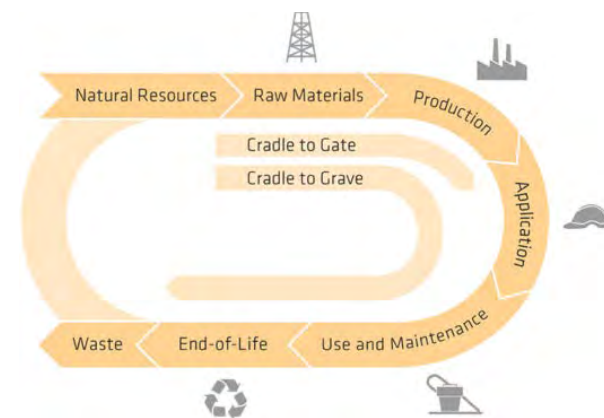
Upstream operations are unchanged in the different scenarios so they are not included

- **Functional unit:**

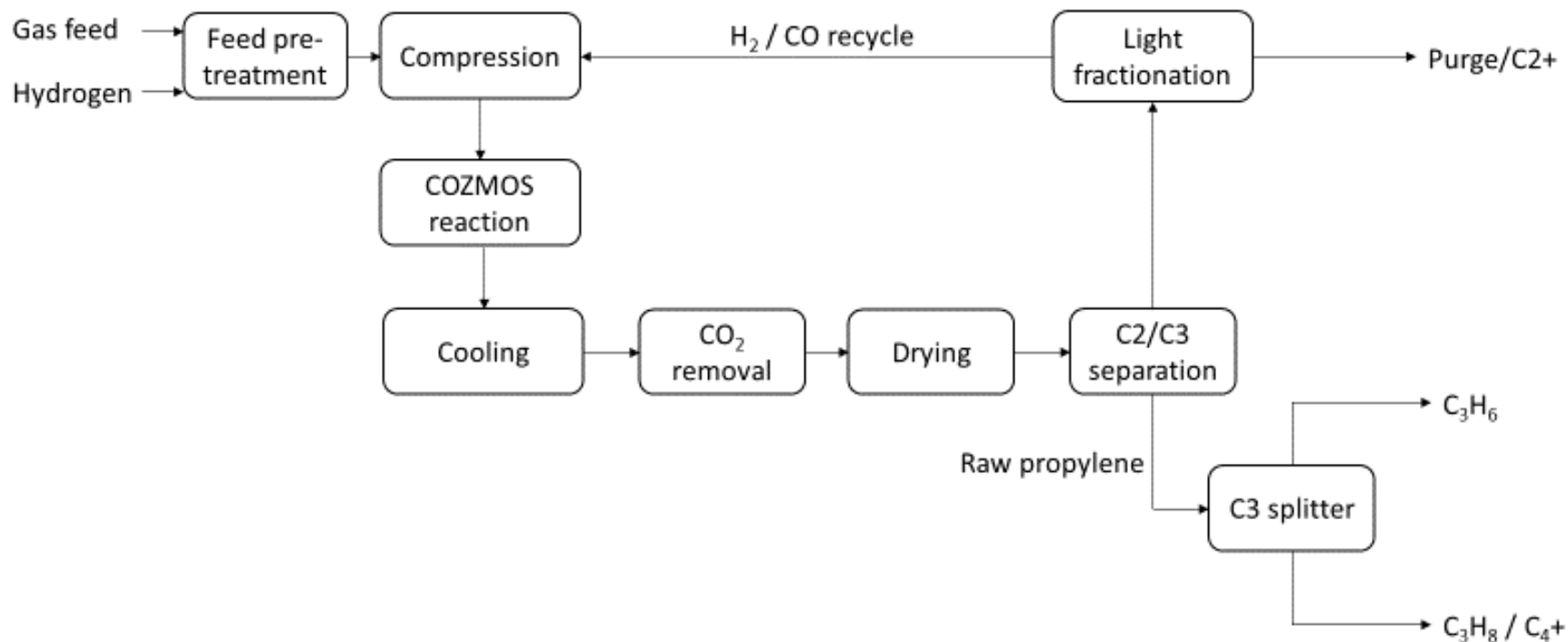
Production of 1 kg of propane

All the products will be considered in the study even if they are not part of the functional unit

The product distribution can be adjusted with the reactor conditions



COZMOS process



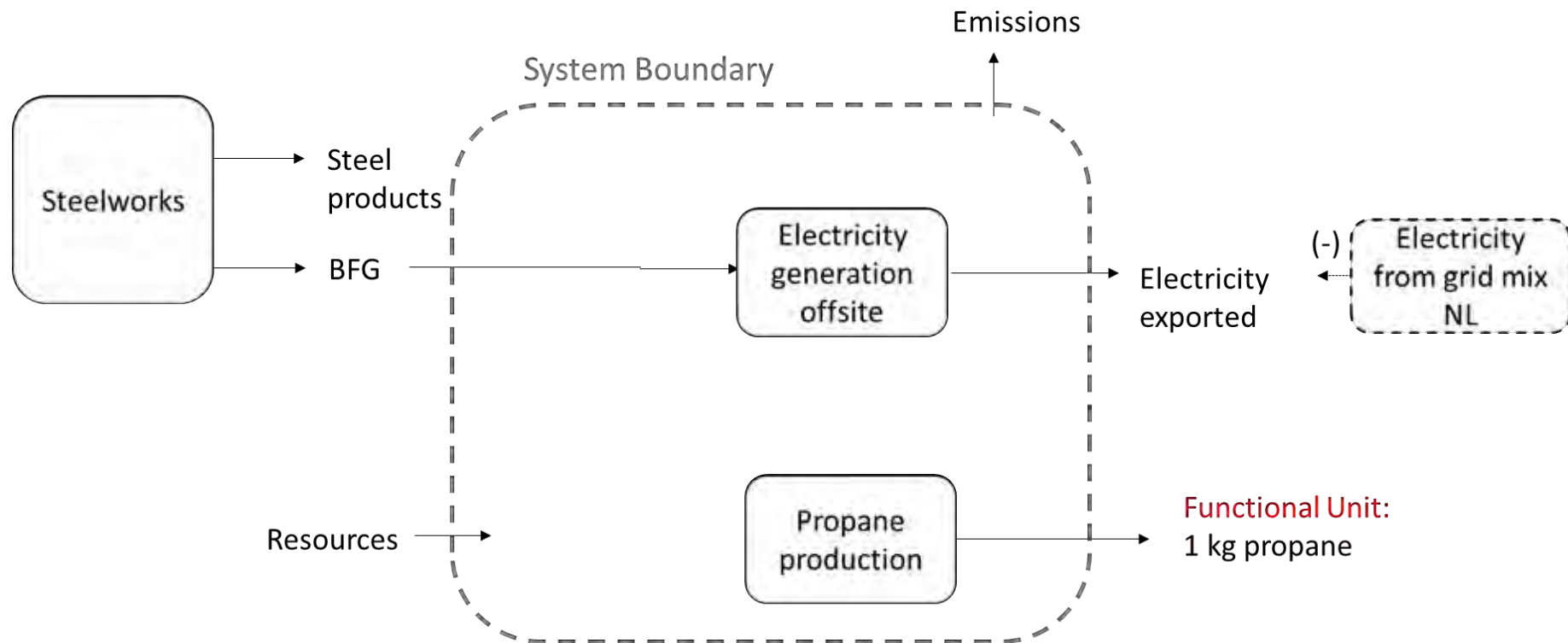
LCA and TEA scenarios

4 main scenarios considered:

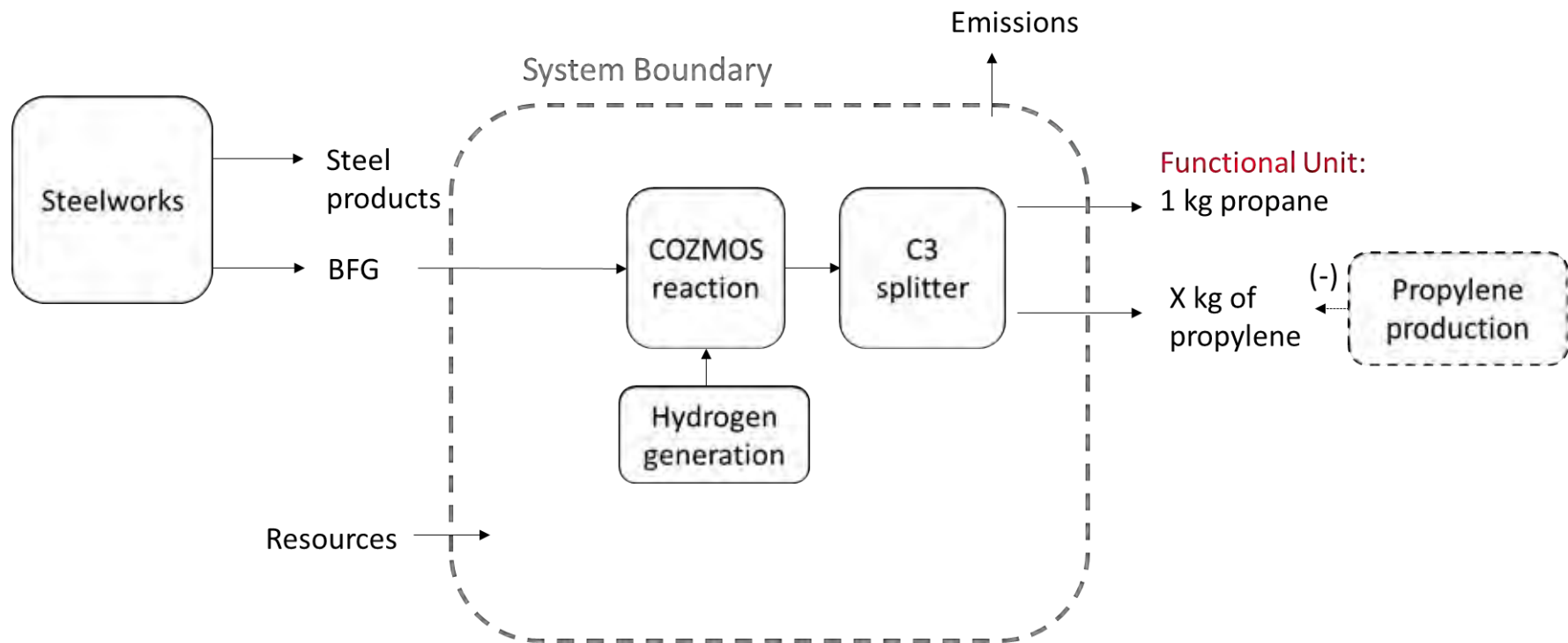
1. Tata Steel reference or baseline case, where the BFG is sent offsite for electricity generation
2. Tata Steel COZMOS scenario, where BFG is used within COZMOS
3. Tupras reference case, where the PSA tail gas is used for heating
4. Tupras COZMOS scenario, where the PSA tail gas is used for the COZMOS process



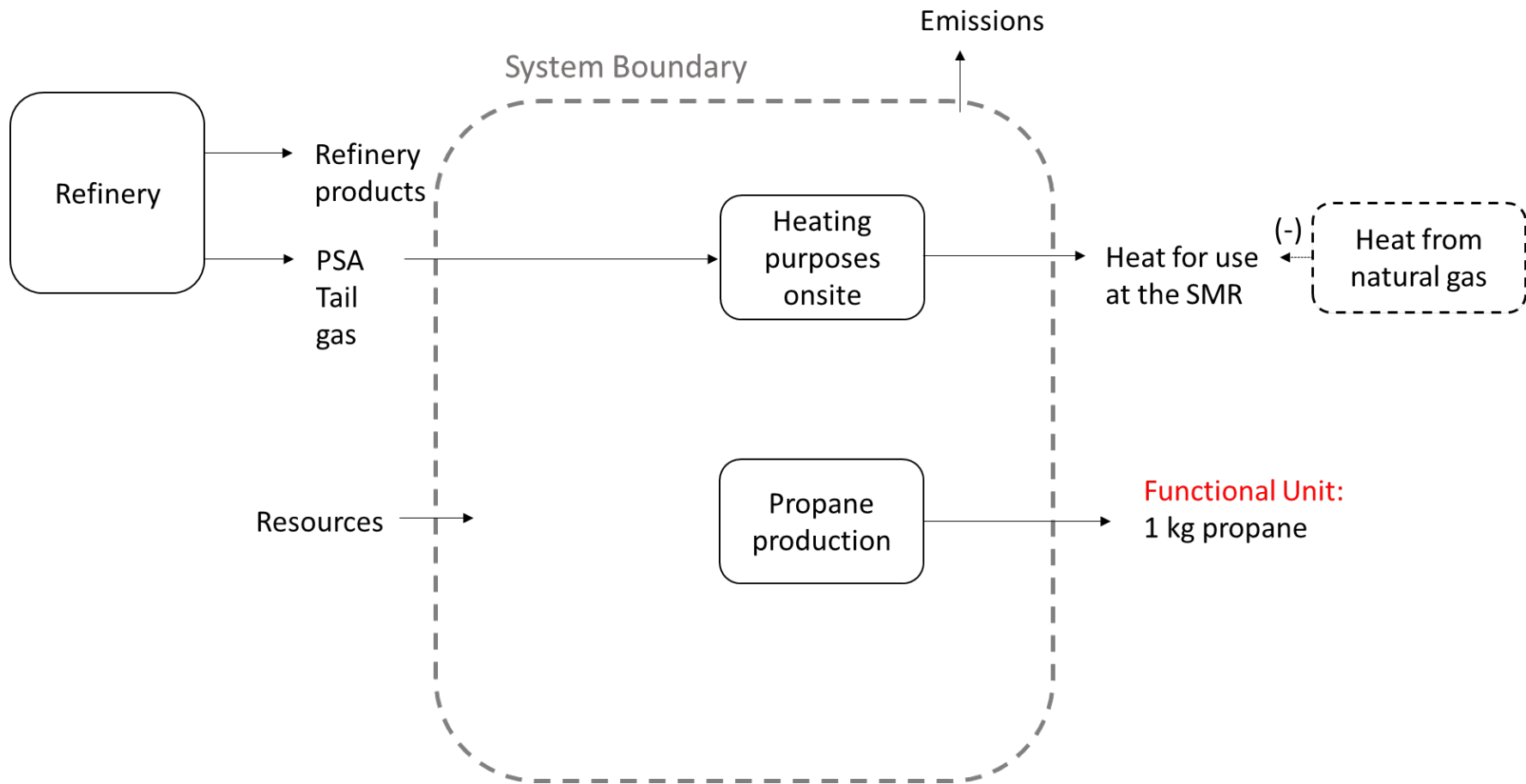
Scenario 1: Reference case, Tata Steel



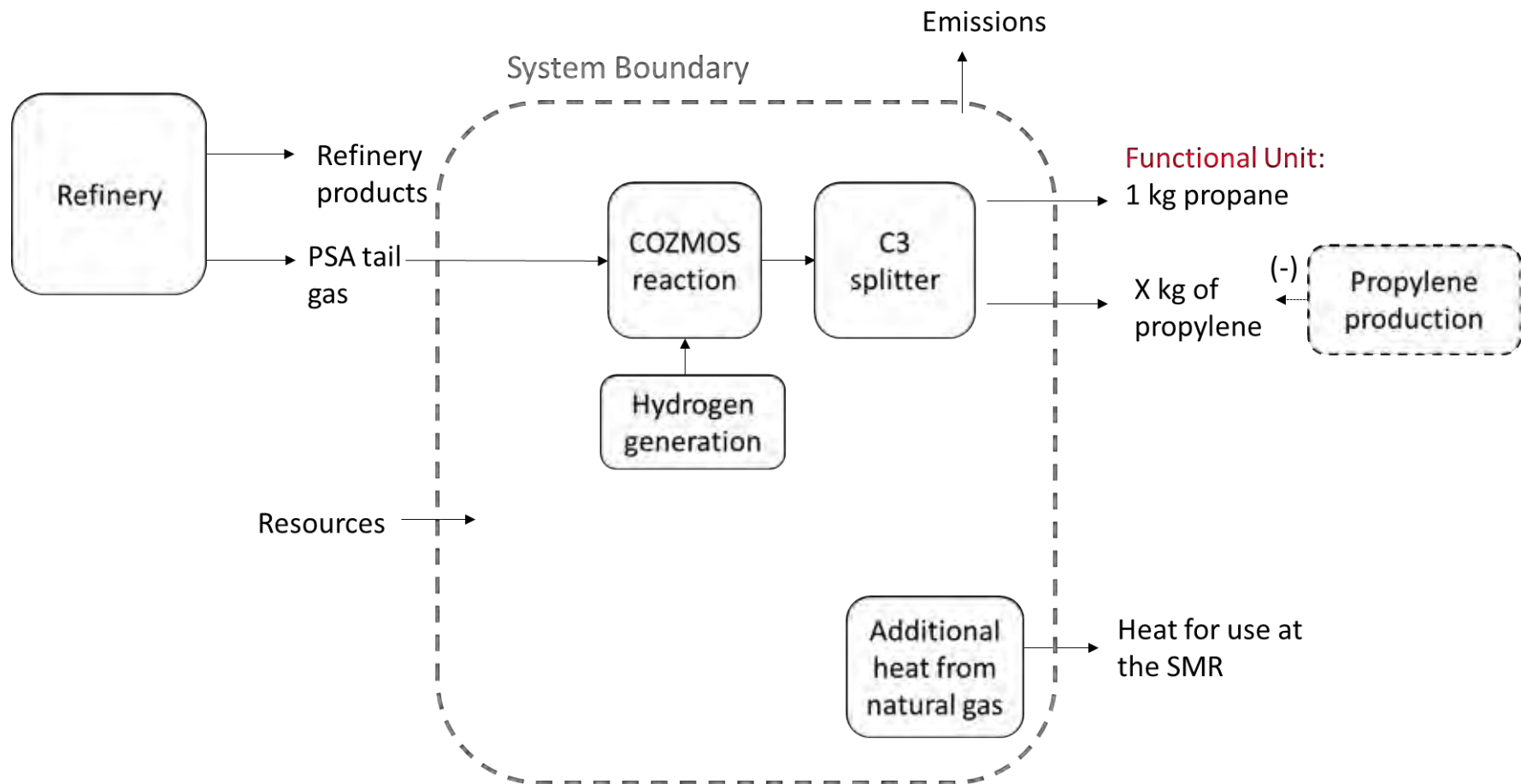
Scenario 2: COZMOS scenario, Tata Steel



Scenario 3: Reference case, Tupras



Scenario 4: CO2MOS scenario, Tupras



The Guidelines for LCA & TEA of CCU

Project goal:

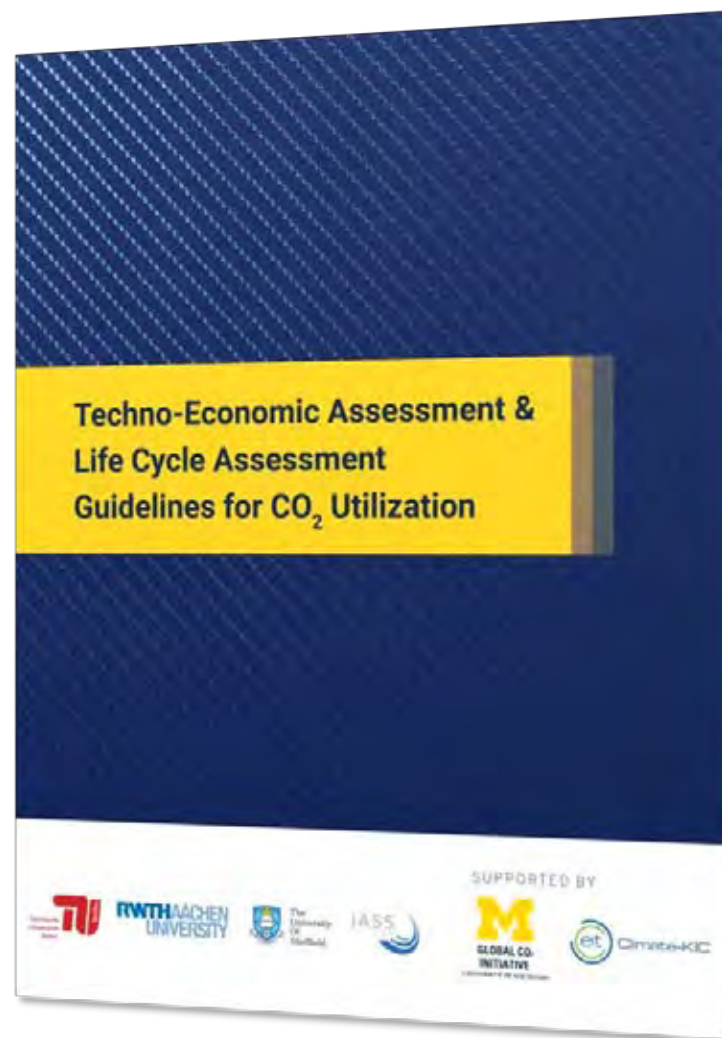
- Define a common assessment language to push R&D, investment and commercialization of CCU
- Align LCA and TEA
- Enhance transparency and comparability
- Enable strong acceptance and adoption of guidelines

Available at:

<http://umlib.us/CO2Guidelines>

DOI: 10.3998/2027.42/145436

ISBN: 978-1-916 4639-0-5



Conclusions

- LCA allows you to calculate the environmental impacts throughout a product or process life time
- TEA allows you to analyze the technical and economic performance of a process or product
- LCA and TEA can support decisions based on environmental and techno-economic performance
- We are using LCA to identify possible bottlenecks in the process
- We applied a streamlined LCA to potential catalysts to rank them according to their environmental impact
- We are undertaking full LCA and TEA of the COZMOS process in accordance with existing standard references and guidelines



Acknowledgments

CO2MOS



This project has received funding from the European Union's Horizon 2020 research and innovation programme under Grant Agreement No. 837733.

Katy Armstrong, Stephen McCord, Peter Sanderson, Peter Styring
Department of Chemical & Biological Engineering, The University of Sheffield



The
University
Of
Sheffield.

Marta Cruz Fernandez, Steven Woollass
Tata Steel



Thank you for your attention

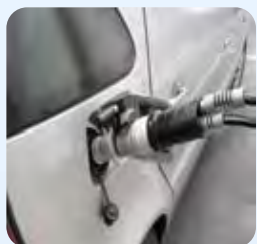
Guillermo Garcia-Garcia
G.Garcia-Garcia@Sheffield.ac.uk

UK Centre for Carbon Dioxide Utilisation
Department of Chemical & Biological Engineering
The University of Sheffield



The
University
Of
Sheffield.





CCUS business models & public policy support

Addressing challenges and realizing opportunities for CCUS



February 2021

elementenergy

Antonia Mattos:
Amelia Mitchell:

antonia.mattos@element-energy.co.uk
amelia.mitchell@element-energy.co.uk

Element Energy, a consultancy focused on the low carbon energy sector

Element Energy covers all major low carbon energy sectors:



Selected clients:

Public sector



NGOs



Public-Private Partnerships



Private Sector



Agenda

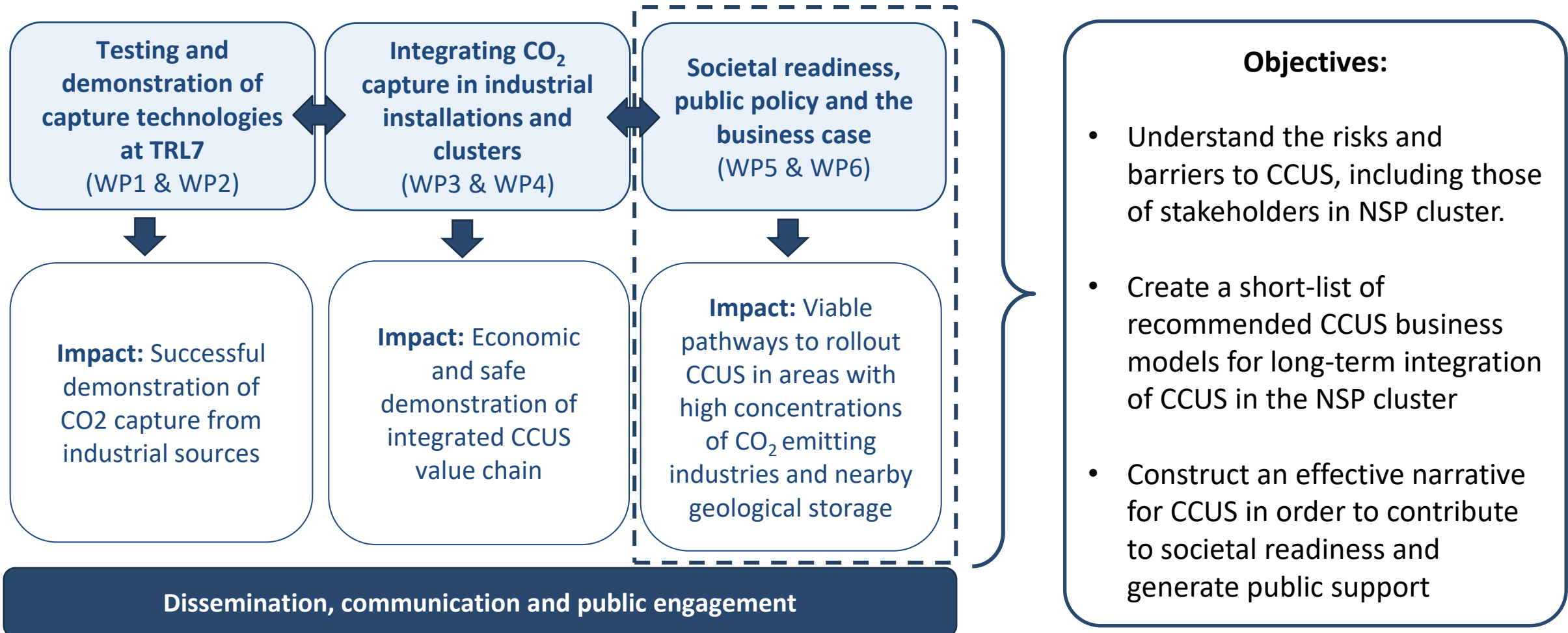
Introduction

Risks policy must address

Business model example

CCU policy requirements

C4U: Advanced Carbon Capture for Steel Industries Integrated in CCUS Clusters (Horizon 2020 Funded Project)

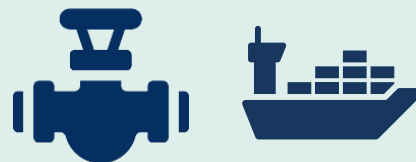


Why are policies and business models needed?



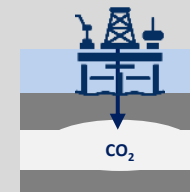
CO₂ capture from industrial emitters

Need to remain financially competitive with sites w/o CCS – need strong revenue model and protection from some risks.



CO₂ transport operators

Need certainty of CO₂ volumes and transport fees, from emitters and/or storers (or protection from cross-chain default risks).



CO₂ storage operators

Need certainty of CO₂ volumes and storage fees. Early projects need support with CO₂ leakage liability.



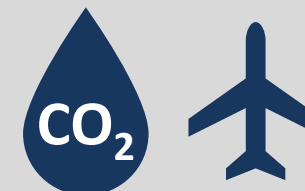
CO₂ capture from power emitters

Need to have certainty on future role in power market and a guaranteed revenue from services provided.



Government and society

Need decarbonisation at lowest cost to society and minimum environmental impact. Need to understand the benefits of CCUS.



CO₂ utilisation

Need regulatory framework for CO₂ accounting and verification of climate benefits. Need development of end-use markets and likely financial support or end-use standards.

Agenda

Introduction

Risks policy must address

Business model example

CCU policy requirements

Identified risks, challenges & failure factors

| Recurring factors contributing to project failures |
|---|
| Lack of long-term economic viability |
| Poor risk management |
| Technical integration and compatibility when scaling up from demonstration to commercial scale |
| Over-reliance on Government subsidies |
| Additional factors specific to full-chain CCUS projects |
| Poor management of cross-chain liabilities and poor risk ownership allocation among project stakeholders |
| Poor coordination of construction timescales or poor integration design between the interfaces of each CCUS segment |

Legend:

C Capture
 T Transportation
 U Utilisation
 S Storage



Segment predominantly affected



Segment less affected

| Category | Associated risks and challenges | C | T | U | S | WIP |
|---------------------------|---|---|---|---|---|-----|
| Technical and operational | Technology performance uncertainty | | | | | |
| | Technology lock-in | | | | | |
| | Site-specific challenges | | | | | |
| | Increased operational complexity | | | | | |
| | Variation in CO ₂ purity grade | | | | | |
| | Maintenance of pipelines | | | | | |
| | CO ₂ storage well damage | | | | | |
| Economic and market | High capital investment | | | | | |
| | Capital cost uncertainty | | | | | |
| | Opportunity cost (technology lock-in) | | | | | |
| | Poor finance opportunities | | | | | |
| | Energy cost uncertainty | | | | | |
| | Long investment timescales | | | | | |
| | Insufficient value proposition | | | | | |
| | Reduced competitiveness | | | | | |
| | Carbon leakage (offshoring of emissions) | | | | | |
| | Revenue volatility | | | | | |
| | T&S monopoly and fee uncertainty | | | | | |
| | Long-term CO ₂ storage liability | | | | | |
| Political | Policy and regulatory uncertainty | | | | | |
| | Carbon leakage and employment loss risk | | | | | |
| | CO ₂ price level and uncertainty | | | | | |
| | Stringent conditions of government support | | | | | |
| | Complex permitting processes | | | | | |
| Cross chain | Integration risk | | | | | |
| | Operational interface risk | | | | | |
| | Risk allocation | | | | | |
| | Cross-border | | | | | |
| | Cluster / hub coordination | | | | | |

Agenda

Introduction

Risks policy must address

Business model example

CCU policy requirements

Project example - Business model characterisation & assessment

| Revenue* | Funding source | Risk Management | Capital |
|---|---|--|---|
| <p><i>Main revenue model:</i></p> <ul style="list-style-type: none"> • CfD-like mechanism (or CPF) • RAB-like mechanism • Cost plus: public operational payments (open book) • CO₂ abatement payments (fixed or variable) • Green product premium or product CO₂ taxes • CCS certificates tradeable, obligated • Tax credits tradeable • Public procurement of low-carbon products <p><i>Supporting only:</i></p> <ul style="list-style-type: none"> • CO₂ price avoidance or credits • CO₂ utilisation & EOR • Energy performance standards • Obligation (CCS or industrial decarbonisation) | <ul style="list-style-type: none"> • Exchequer (taxpayer) • All industrial emitters • All national emitters • Fossil fuel suppliers • Gas and/or electricity consumers • Purchasers of low carbon products (price premium) <p><i>Supporting</i></p> <ul style="list-style-type: none"> • CO₂ sales for utilisation eg EOR • CO₂ tax avoidance | <ul style="list-style-type: none"> • Public loan guarantees • Public underwriting of operational risks e.g. opex • Stable policy / long term contracts • Insurer / buyer of last resort • Price floor / ceiling • Compensation for BAU disruption • Revenue guarantees* • Border adjustments <p><i>Supporting cross-chain requirements:</i></p> <ul style="list-style-type: none"> • Contractual arrangements eg take-or-pay, interface agreements, T&S fee regulation • Public backstops on cross-chain default • Multiple emitters and stores | <ul style="list-style-type: none"> • Public grants • Public loans • Public equity • Emitter equity • Investor / JV equity • Debt / loans (inc Green bonds) • Multilateral funds <p>Ownership</p> <ul style="list-style-type: none"> • Private - emitter • Private – other eg JV • PPP • Public – direct • Public – through state-owned enterprise or SPV |

Build additional elements and instruments around revenue model to mitigate risks not addressed by *revenue model* itself. Assess complete business model using step 1 & 2 criteria.

Step 1 criteria: industrial acceptability

1. Capital availability or low cost financing
2. Strength of revenue incentive
3. Industry competitiveness and carbon leakage
4. Flexibility for operational cost uncertainties
5. CO₂ price level and uncertainty
6. Simplicity and transparency for industry

Step 2 : government acceptability

1. Cost: efficiency promotion
2. Cost: ability to pass costs on
3. Policy track record
4. Speed and simplicity of implementation
5. Ongoing simplicity for government
 - Applicability to industrial sectors
 - Applicability to CCS phases

Business model summary example – CfD_c CO₂ certificate strike price

Revenue

- CfD_c on strike price £/tCO₂ for abated CO₂, via tradeable CO₂ certificates
- Offered contract fixed for duration but set annually for new joiners¹

Funding source options

- Government: general taxation or levies eg fossil fuel suppliers

Risk mitigation

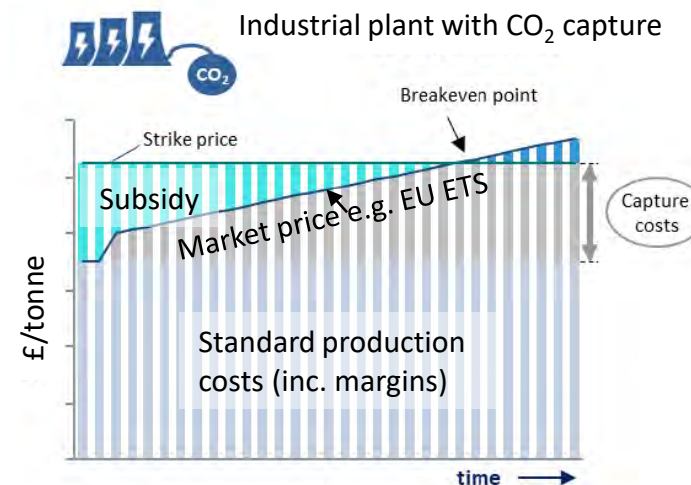
- Capital loan guarantee in scale-up
- Long term contract on strike price²
- ICC cost backstops/pain-gain sharing

Capital

- *Roll-out*: Emitter equity & low-cost loans
- *Scale up*: grants or loan guarantees

Description & discussion

- The emitter is paid the difference between the CO₂ strike price contractually agreed (that needed to cover capture costs) and the prevailing CO₂ market price (e.g. EU ETS). For early projects, strike price may need to be high due to higher risks.
- Cost to government, if well designed, is only that required above the carbon price avoidance to compensate the emitter and protect competitiveness. Efficiency is incentivised, but costs are not passed on to consumers.
- Policy track record and applicability is high, although power CfD is on product price.



Industry criteria

Capital availability
Revenue strength
Competitiveness
Opex uncertainty
CO₂ price
Simplicity



Government criteria

Cost: efficiency
Cost: pass on
Track record
Implementation
Administration
Sectors
Phases
CCS specific?



Source: Element Energy for BEIS, industrial carbon capture business models 2018

1: Scale-up: negotiation on site by site basis. Roll-out: competitive bidding process.

2: Annual adjustments including linked to fuel prices or CPI-linked <https://lowcarboncontracts.uk/payments>

CCUS deployment: Several promising business models were identified for industrial carbon capture, drawing on comparable existing policies

Contract for difference:

CfD on CO₂ price relative to market CO₂ price (e.g. EU ETS) to provide guarantee of revenue

Cost plus:

All properly incurred ICC operational costs are reimbursed through taxpayer funding

Regulated asset base:

Public regulation allows costs to be recovered through product prices e.g. of Hydrogen

Tradeable tax credits:

CCS tax credits awarded \$/tCO₂ to reduce firms tax liability (e.g. 45Q) or trade with other firms.

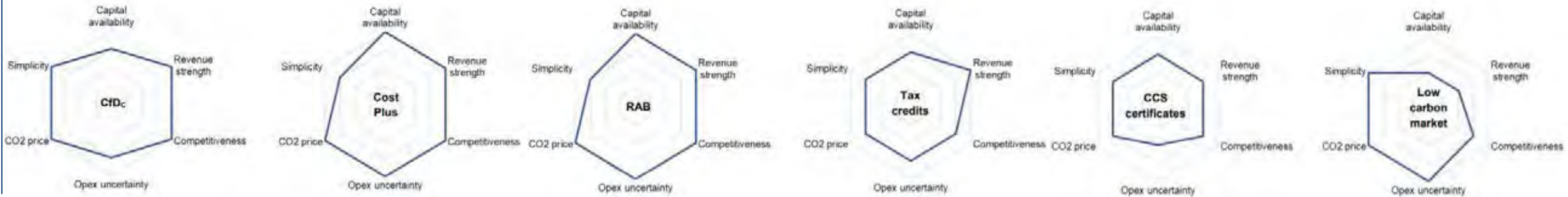
CCS certificates:

Certificates representing tCO₂ abated through CCS, which can be traded and emitters have an obligation.

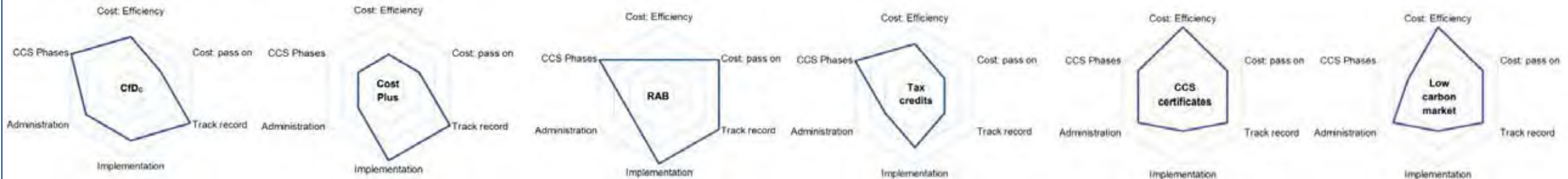
Low carbon market:

End-use regulation e.g. on buildings to create a low carbon market & achieve product premium

Acceptability to industry evaluation



Acceptability to government evaluation



Key messages

Industrial carbon capture

- The key challenge for industrial carbon capture is providing the **revenue level and certainty** to incentivise industry to decarbonise and unlock capital whilst protecting it from carbon intensive competition, and therefore prevent carbon leakage.
- **There are a number of available mechanisms** to support the deployment of industrial carbon capture. The key to a successful mechanisms is balancing the private and public sector requirements. A number of key learnings can be taken from projects such as Longship, Lake Charles Methanol and Porthos e.g. financial structure, CCUS value chain construction and use of existing assets.
- **Each of the revenue models requires support from a suite of risk management instruments** to ensure risks are addressed where possible. This is particularly important for incentivising deployment of early projects where the private sector cannot bear these risks.

CCUS

- In the longer term as CCUS clusters grow and costs and risks reduce, **CCUS may be able to transition to an unsubsidised end-state**. This assumes either global action on climate or border adjustments for product carbon intensity.
- CCUS requires a business model for the other aspects of the chain, such as CO₂ transport and storage or utilisation. **The integration of these business models is key**, with cross-chain risks significant for early or isolated projects.
- **The Netherlands has implemented a mechanisms in SDE++¹** (similar to a CfD), which is likely to form part of the North Sea Port business models. The NSP will be explored in more detail in our work in the coming 2 years.

¹ the government pays the difference between the cost price of a technology and the market price of carbon abatement, expressed in euros per metric tonne of CO₂. It guarantees to do this for 12 or 15 years.

Agenda

Introduction

Risks policy must address

Business model example

CCU policy requirements

**Revenue from CCU products:
challenges of market uptake & enabling interventions**

Competitiveness & Market Potential: products from CO₂ utilisation need to compete with existing products and penetrate markets

Challenges to successful uptake of CCU products

Demonstrating product suitability:

- Technologies need to be demonstrated at scale to gain investor confidence
- Products need to meet existing standards and regulations. This can be a lengthy and expensive process. Prescriptive standards may prevent approval.
- Some markets are highly conservative needing further demonstrations over many years.

Developing market interest and product demand:

- Procurers may lack awareness or engagement with their Scope 3 emissions.
- Procurers may not have awareness of CCU products or the benefits of CCU. There may be a lack of clarity on how these benefits may be realized through carbon accounting.
- Consumer perception could be a barrier if not managed well, or a driver.
- Market drivers are typically not sufficient to justify cost premiums for CCU products.

Achieving cost-competitiveness:

- CCU products can be significantly more expensive than conventional fossil-based products (which may be in receipt of subsidies).
- However, a select few routes are driven by cost-savings or improving the value of products.
- Avoidance of fees or compliance with regulations could become a driver if more ambitious incentives or targets are imposed.

Interventions to enable success

- **Funding for innovation & demonstration projects.**
- **Facilitating testing & approvals processes.**
- **Updating of standards to be performance based.**

- **Increasing awareness and reporting of lifecycle & Scope 3 emissions.**
- **Clarifying carbon accounting for CCU products.**
- **Use of mandates or standards to increase demand for lower emission products.**

- **Funding of linked projects such as renewables, green hydrogen and carbon capture to lower costs.**
- **Introducing policies to level the field by recognizing sustainability benefits (performance based).**

Support for CCU: examples of existing or adaptable support mechanisms



Research & Demonstration Funding

- Funding programmes in the EU (H2020, Innovation Fund), US and member states.
- Private investment initiatives and competitions such as Carbon Xprize



Low Emission Fuels Standards / Targets

- Blending obligations for road transport (EU RED II) and aviation fuels (e.g. Norway)
- Minimum standards (e.g. Californian Low-Carbon Fuel Standard)



Level Field Mechanisms & Subsidies

- Carbon pricing (ETS or carbon tax)
- Operational subsidies such as Contract for Difference (e.g. Netherlands SDE++)



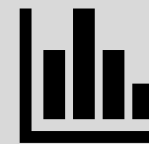
Testing, Approvals & Certifications

- US Clearing House facilitating aviation fuel approvals
- Sustainability Certification Schemes & product labelling



Procurement Guidelines

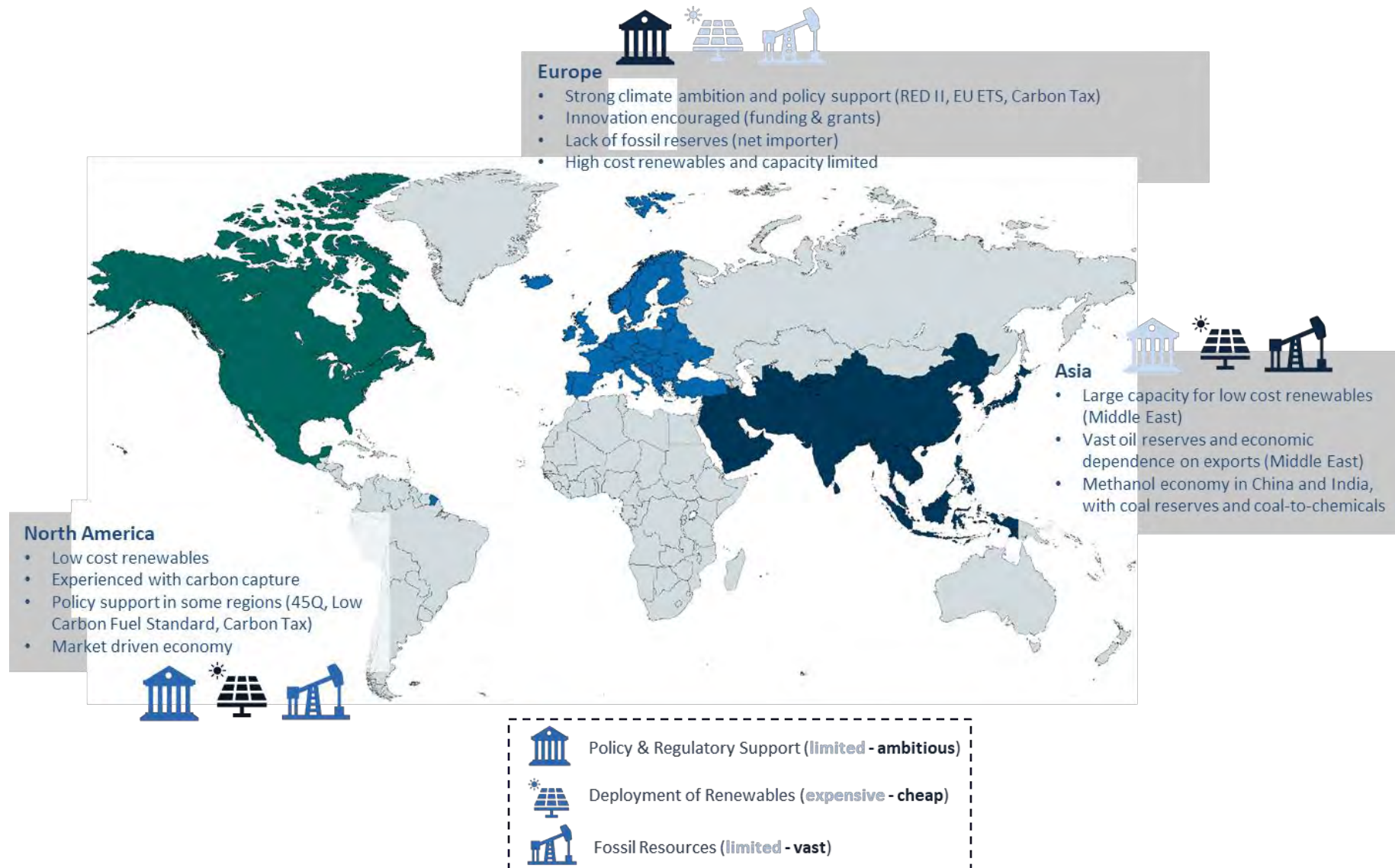
- Standards for public infrastructure projects (e.g. UK BREEAM rating)
- Tender evaluation (e.g. Netherlands CO₂ performance ladder)



Company Monitoring & Reporting

- Emission reporting obligations (government & investor driven)
- Knowledge sharing & guideline development

Drivers, barriers and enablers for CCU can vary regionally. There may be local niche opportunities where CCU becomes favourable.



Thank You!

Thank you for your listening!

Any questions?



This project has received funding from the European Union's Horizon 2020 research and innovation programme under grant agreement No 884418

Element Energy is a leading low carbon energy consultancy working in a range of sectors including industrial decarbonisation, carbon capture utilisation and storage (CCUS), hydrogen, low carbon transport, low carbon heat, renewable power generation, energy networks, and energy storage. Element Energy works with a broad range of private and public sector clients to address challenges across the low carbon energy sector.

For further information please contact:
CCUSindustry@element-energy.co.uk



elementenergy

www.element-energy.co.uk

Perception of CO₂-based fuels and their production in international comparison

Linda Engemann, M.A.
HCIC | Chair of Communication Science
RWTH Aachen University

engemann@comm.rwth-aachen.de



Introducing the project



Closing the loop: from CO₂ to fuel

Direct electrocatalytic conversion of CO₂ into chemical energy carriers in a co-ionic membrane reactor

ecocoo.eu

Project aim

- set up a CO₂ conversion process using renewable electricity and water steam to directly produce synthetic jet fuels with balanced hydrocarbon distribution to meet the stringent specifications in aviation
- process is compact, modular – quickly scalable – and flexible, thus, process operation and economics can be adjusted to renewable energy fluctuations
 - technology will enable to store more energy per processed CO₂ molecule and therefore to reduce GHG emissions per jet fuel ton produced from electricity at a substantial higher level

Consortium



1

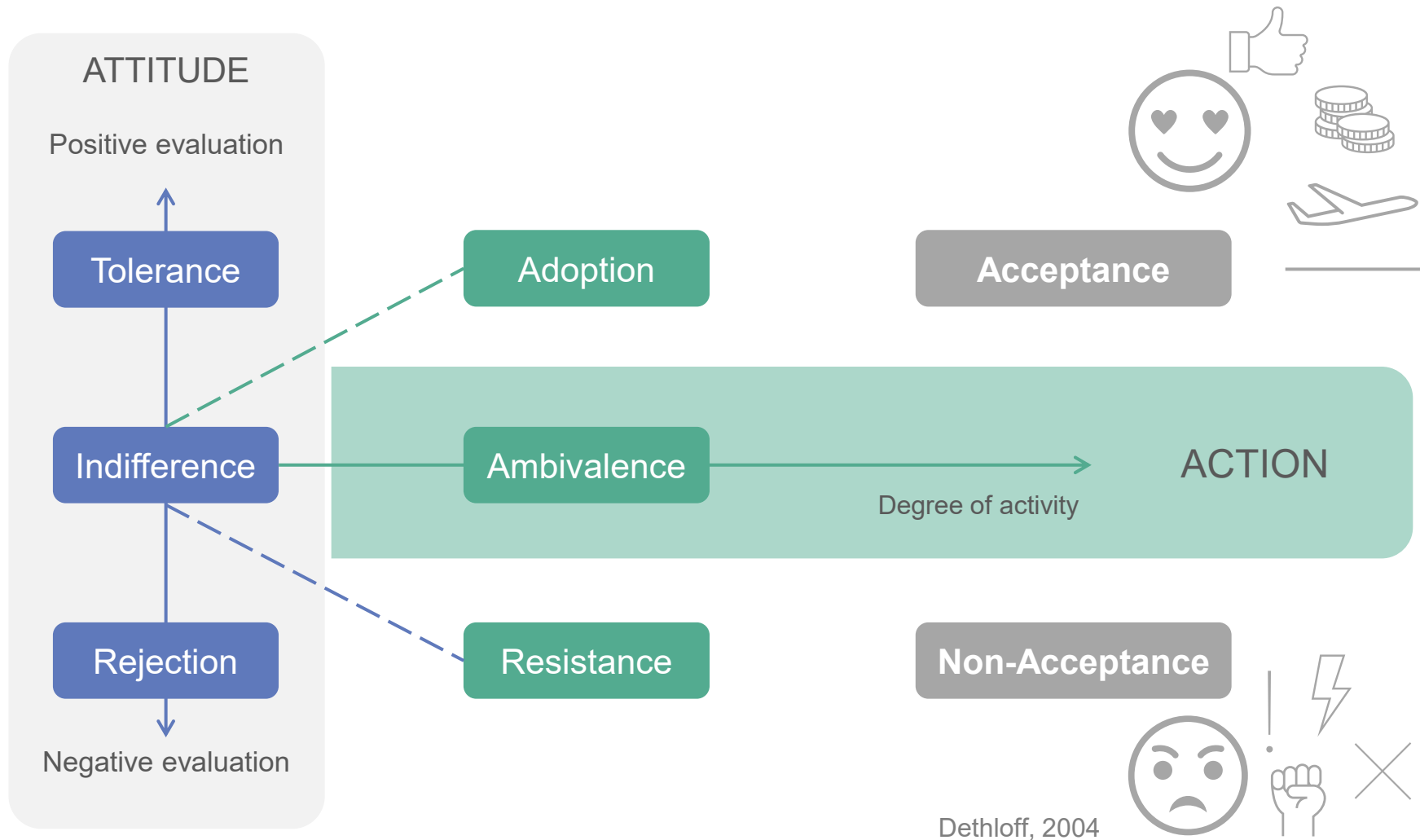
Consideration of public perceptions and acceptance from the very beginning of the developmental process

Informing technical designers about acceptance barriers

Education of the public and increase of awareness

Development of communicative strategies

How do we define acceptance?



Dethloff, 2004

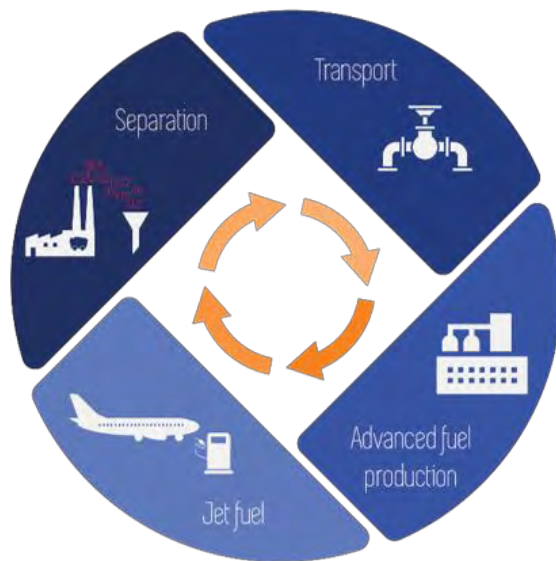
3

Objects of investigation

– Societal perception of CO₂-based fuels

Previous Research

- Protest potential against CCS is impacted by risk and benefit perceptions of CCS (Wallquist et al., 2012)
- Perception of mattresses as a CO₂-based product is linked to health and environmental risk perception (Arning et al., 2018)



- Technical *infrastructure* and *production processes*
- CO₂-based jet fuel as *end-product*



Target groups

laypeople, technical experts,
industrial stakeholders, policy
makers



Methods

Mixed method approach
interviews, surveys

International survey on CO₂-based aviation fuels

Sample (***N* = 2.187**)

Germany (*n* = 543)



M = 45 years
SD = 15.2 years



49.9% female
50.1% male

Netherlands (*n* = 549)



M = 44.8 years
SD = 15 years



50.8% female
49.2% male

Spain (*n* = 545)



M = 45.4 years
SD = 12.9 years



54.9% female
45.1% male

Norway (*n* = 550)



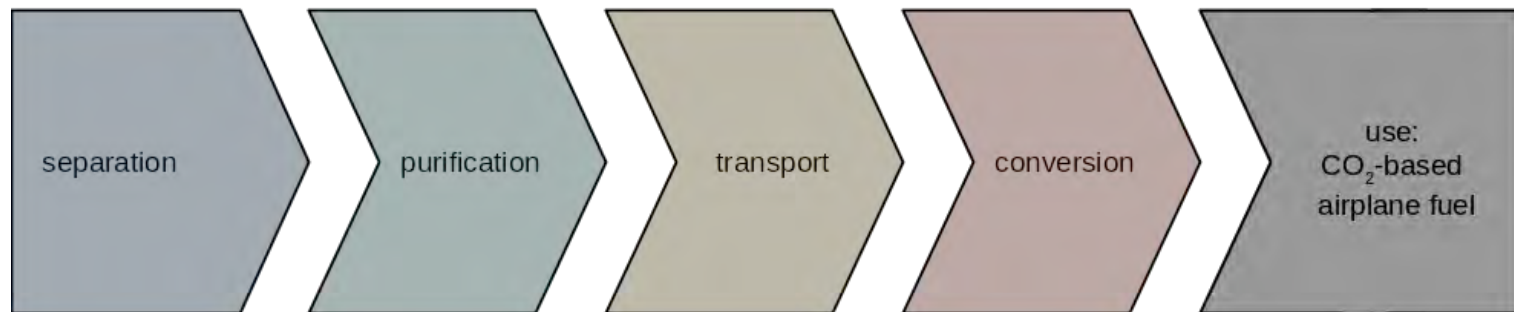
M = 45 years
SD = 14.4 years



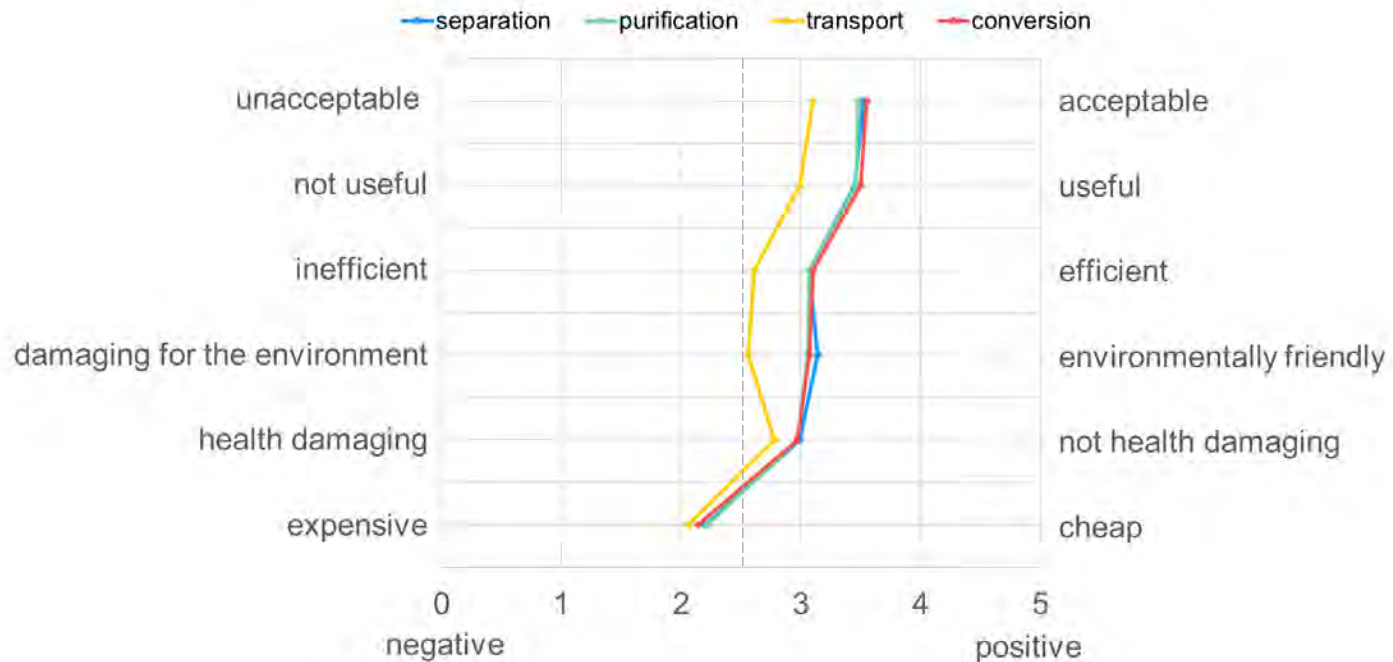
52% female
48% male



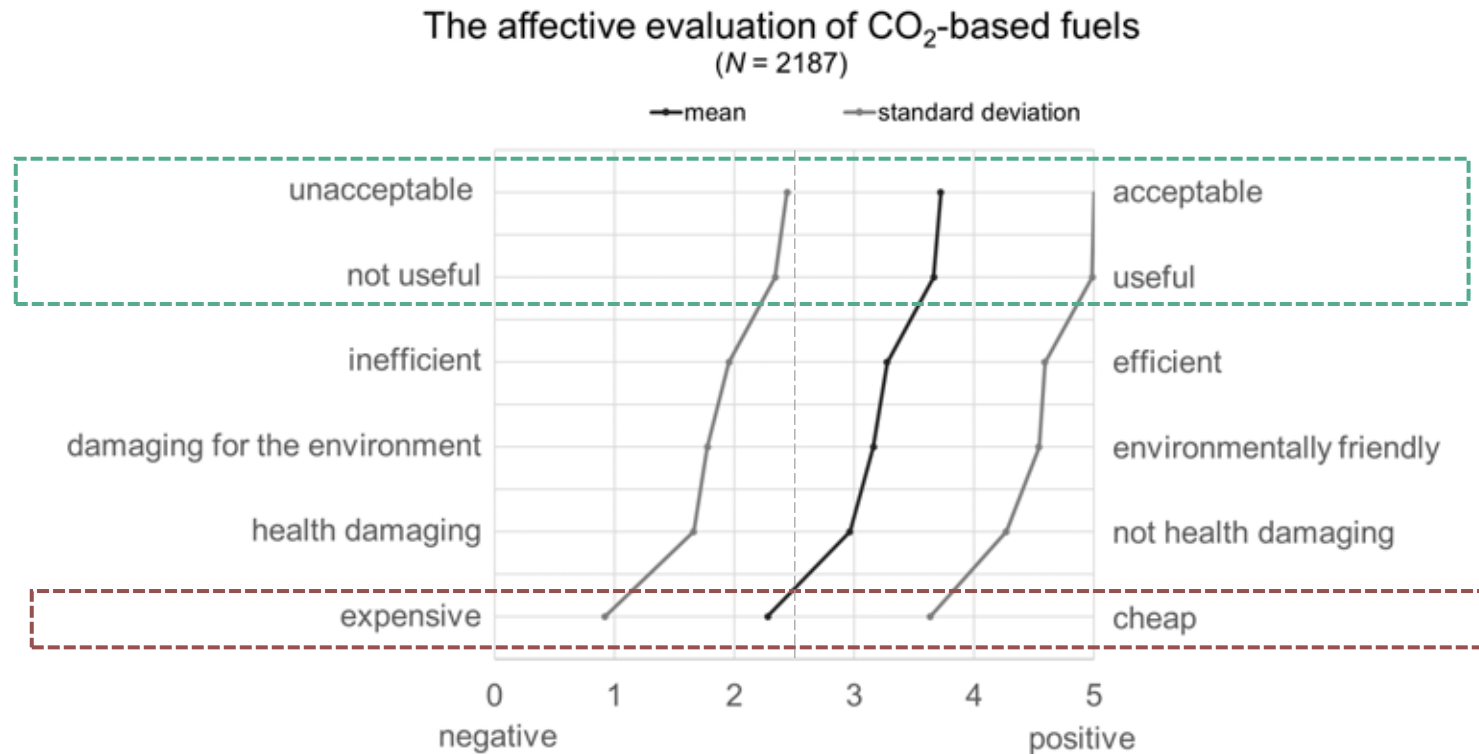
Production CO₂-based fuel using CCU



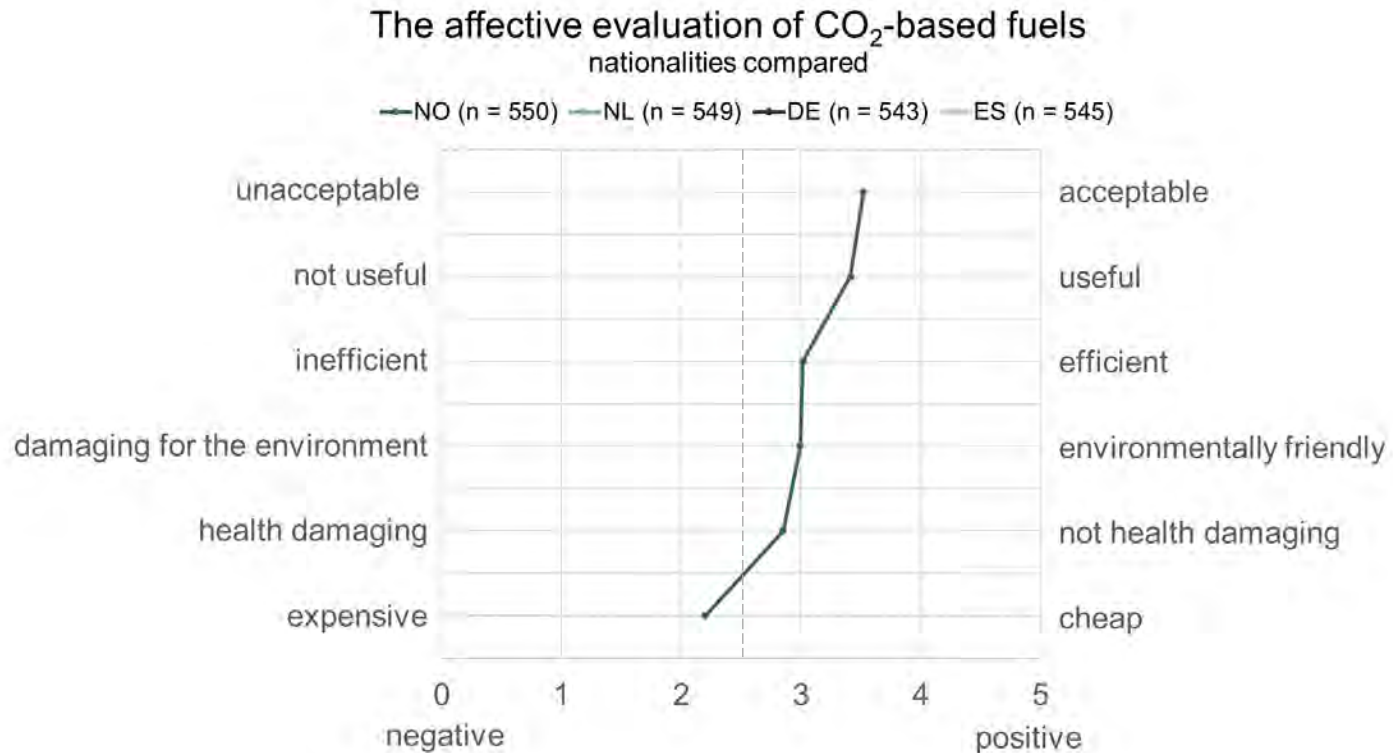
The affective evaluation of the different CCU production steps
(N = 2187)



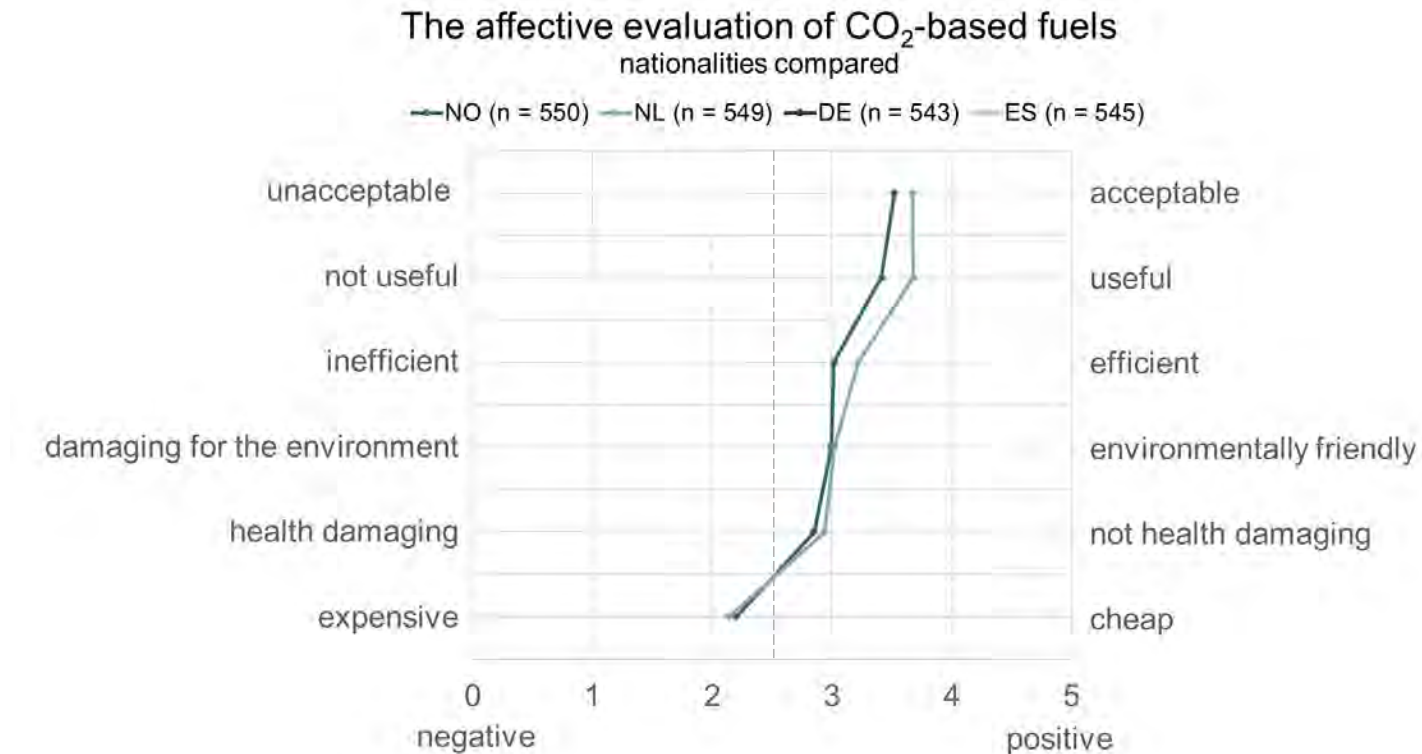
»» Generally, the production steps are perceived as being acceptable and useful. However, people do think it will be expensive.



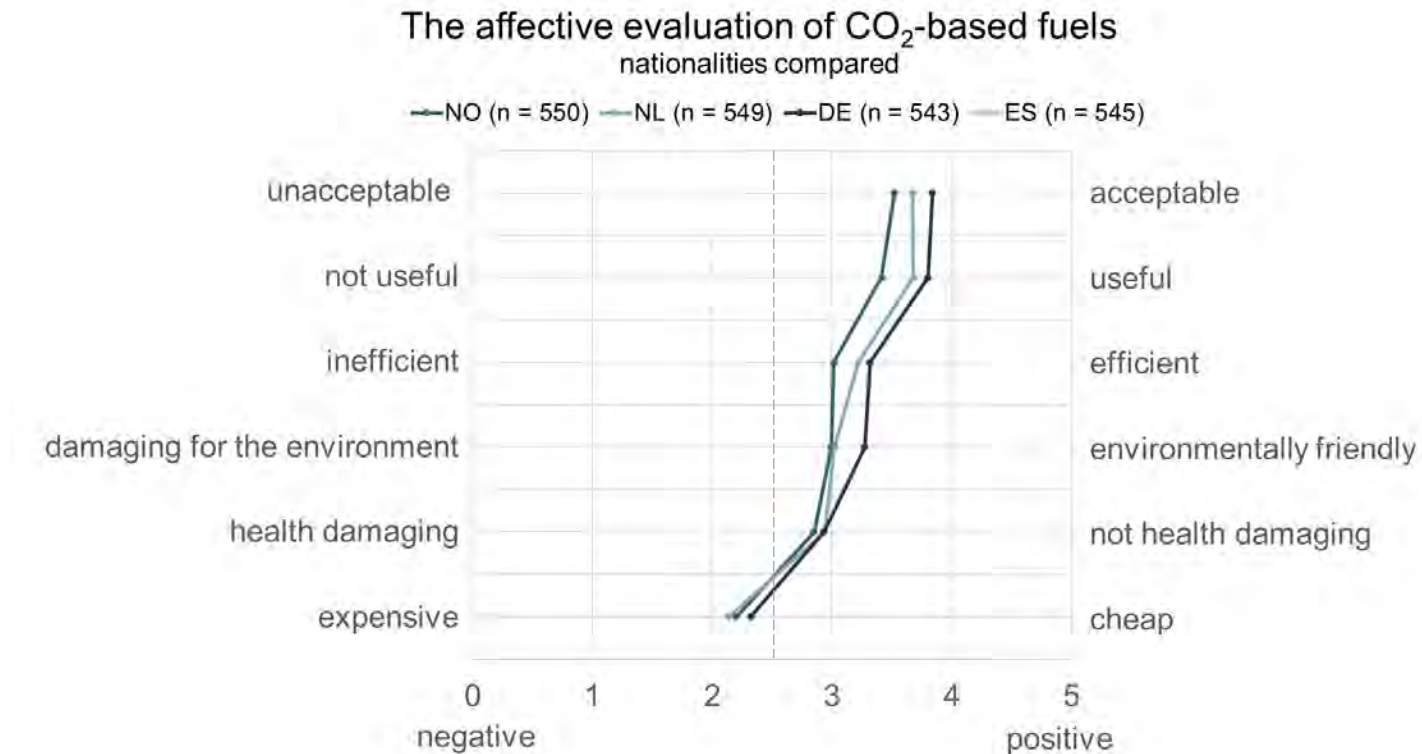
Perception of CO₂-based fuel:
Rather **acceptable**, **useful**, **efficient**, **environmentally** and **health friendly**,
assessment of price as **rather expensive**



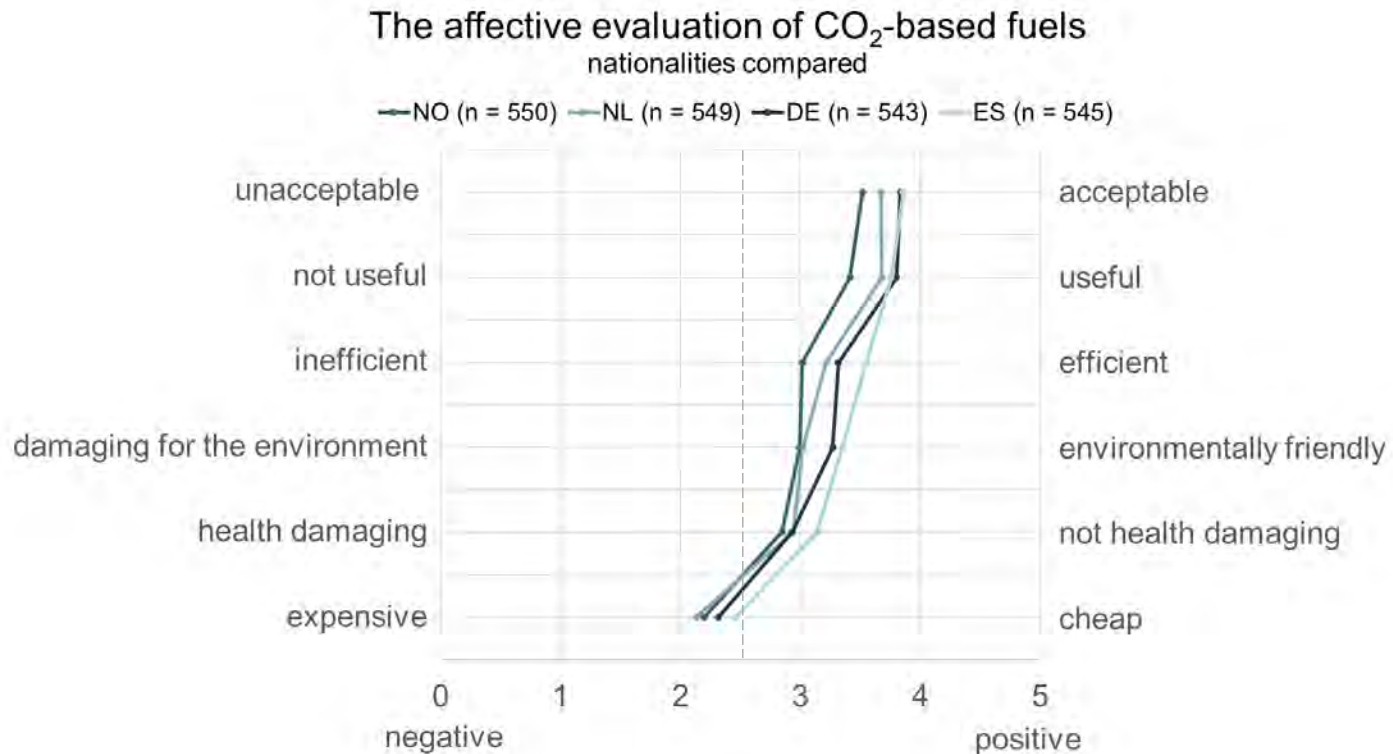
»» The affective evaluation of the end-product of CO₂-based fuels was least positively perceived by the Norwegians,...



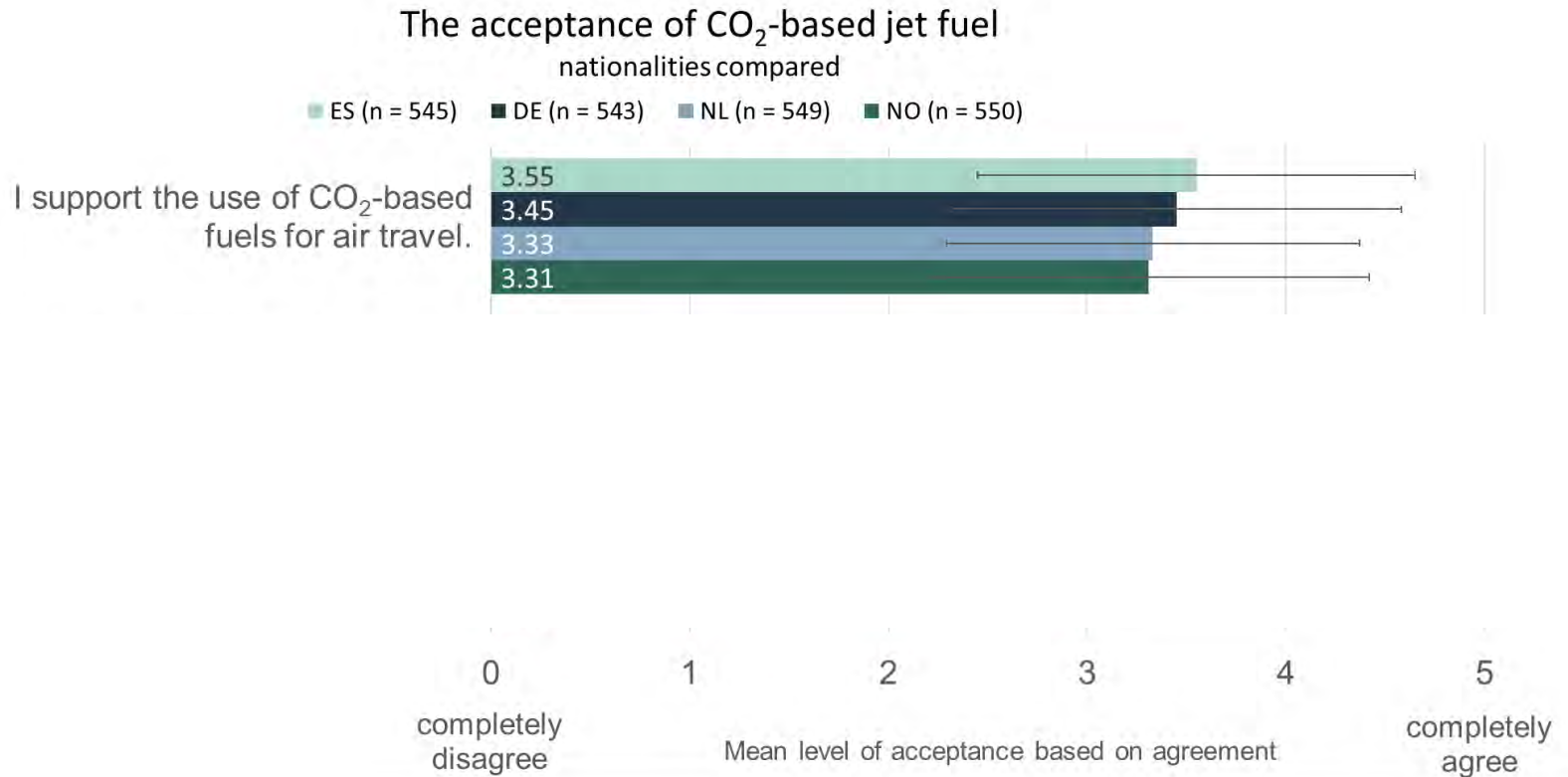
»» The affective evaluation of the end-product of CO₂-based fuels was least positively perceived by the Norwegians, followed by the Dutch,...



The affective evaluation of the end-product of CO₂-based fuels was least positively perceived by the Norwegians, followed by the Dutch, the Germans,...

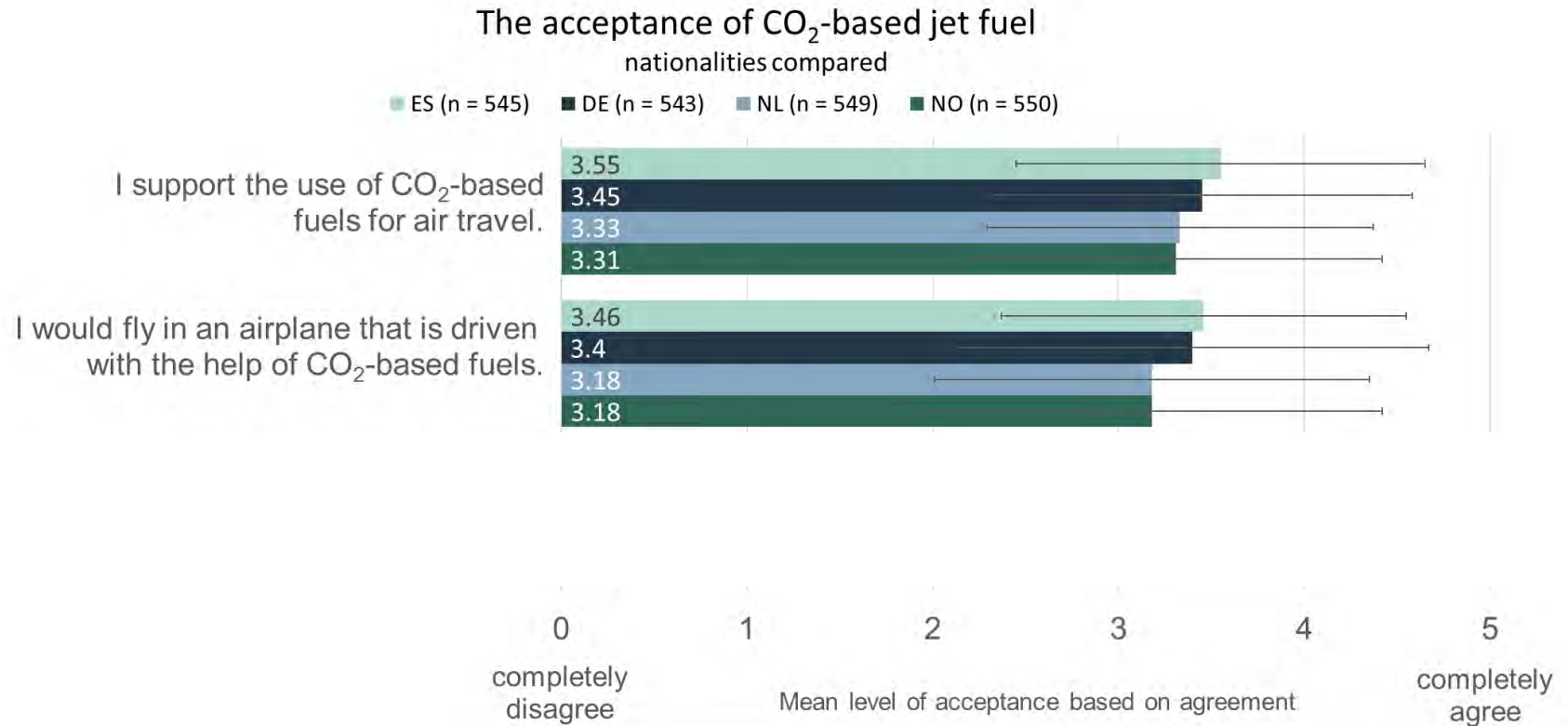


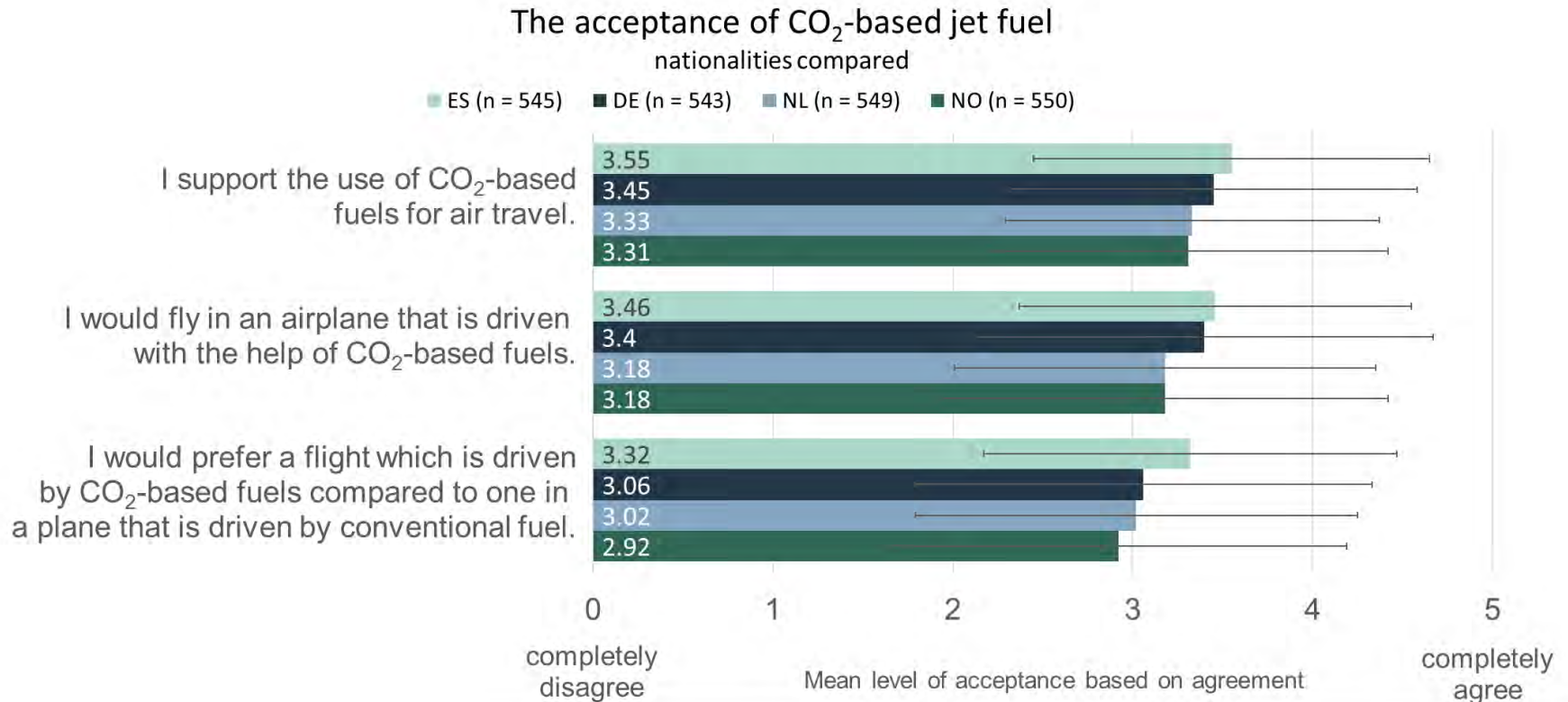
»» The affective evaluation of the end-product of CO₂-based fuels was least positively perceived by the Norwegians, followed by the Dutch, the Germans, and finally the Spaniards.



Acceptance of CO₂-based jet fuel

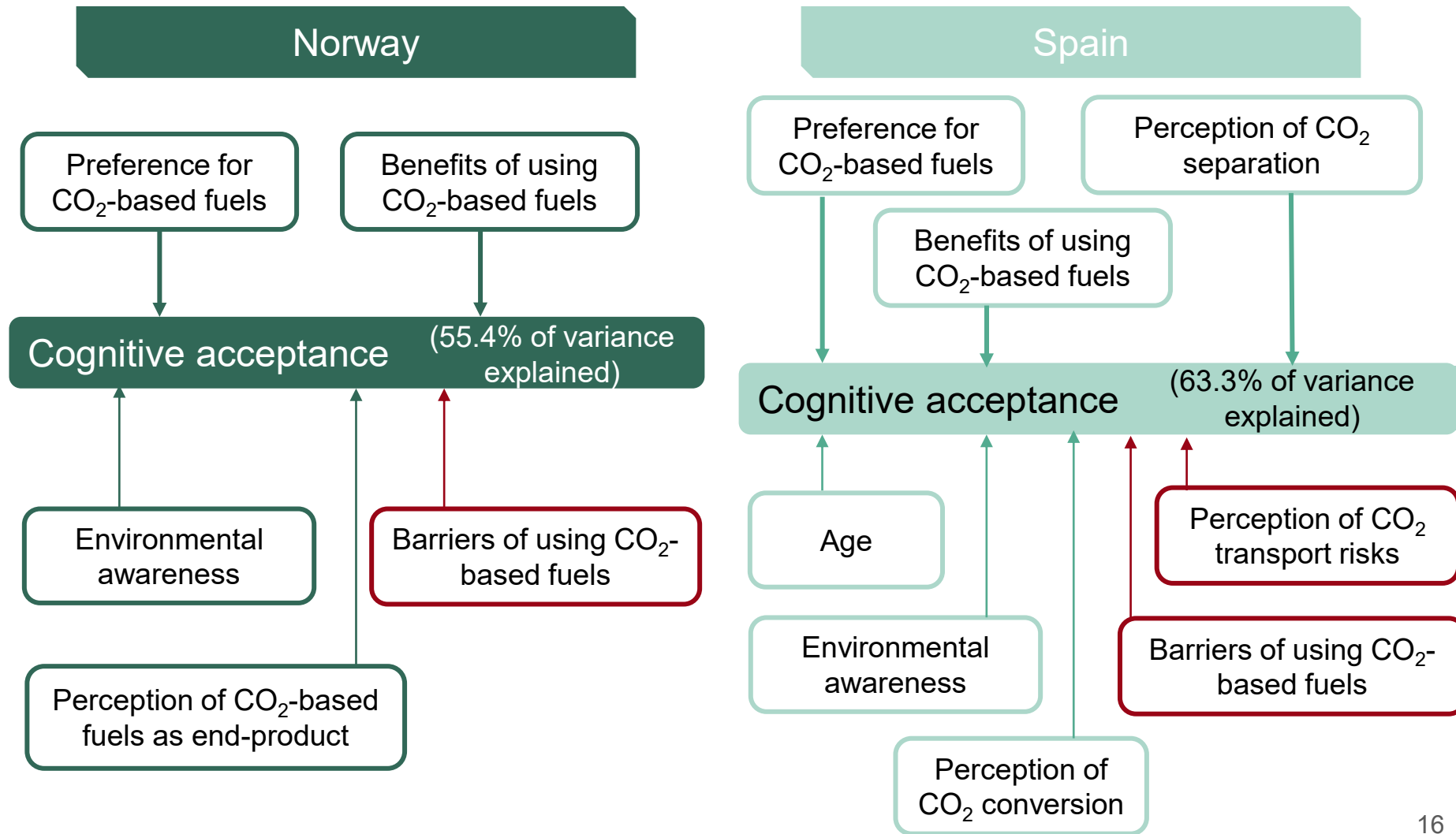
National differences



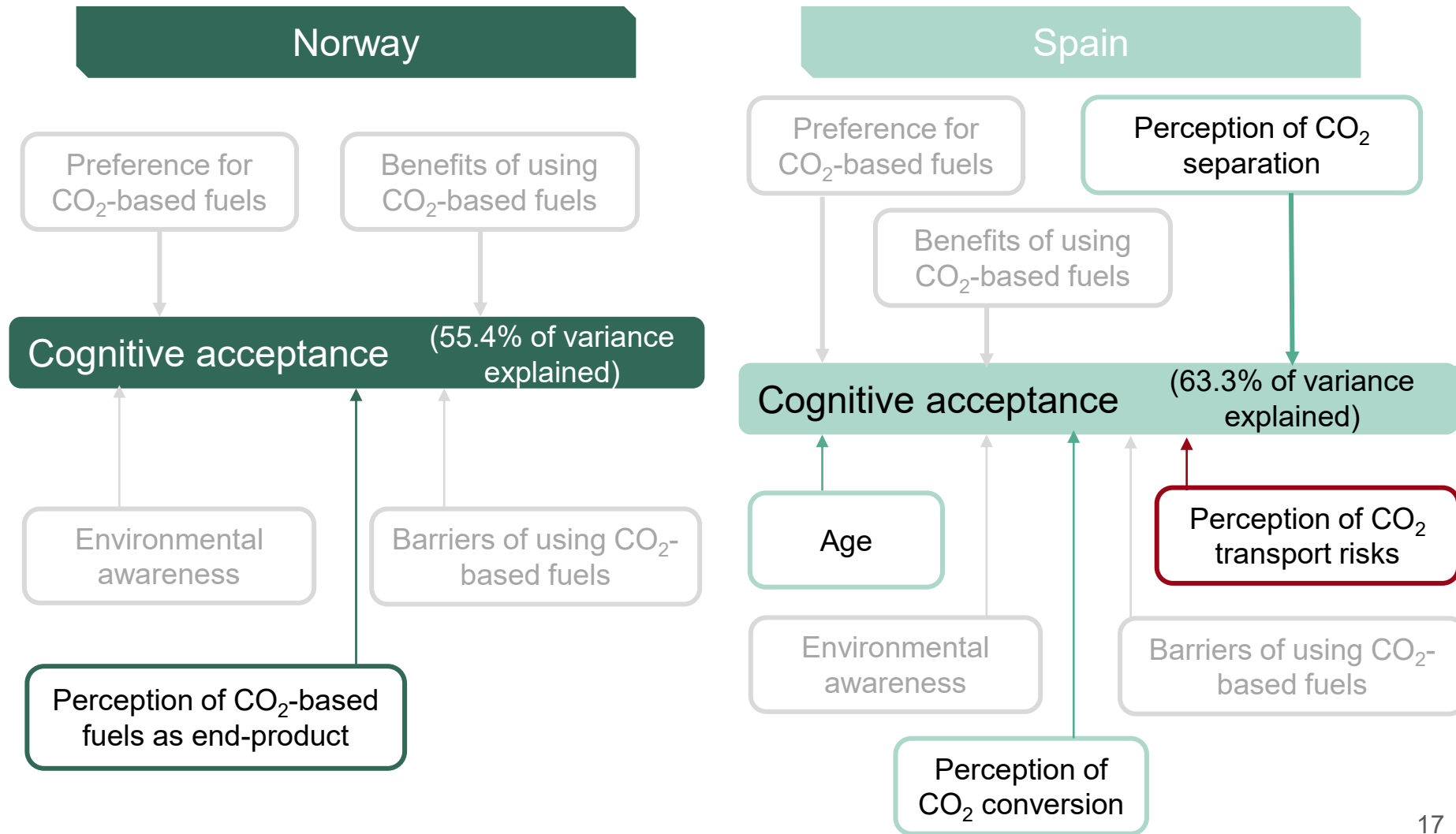


»» The greatest approval and willingness to use CO₂-based fuel existed among Spanish participants, followed by Germans, Dutch and Norwegian people.

Differences in acceptance influencing factors

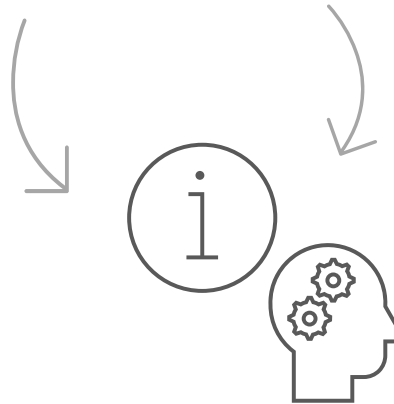


Differences in acceptance influencing factors

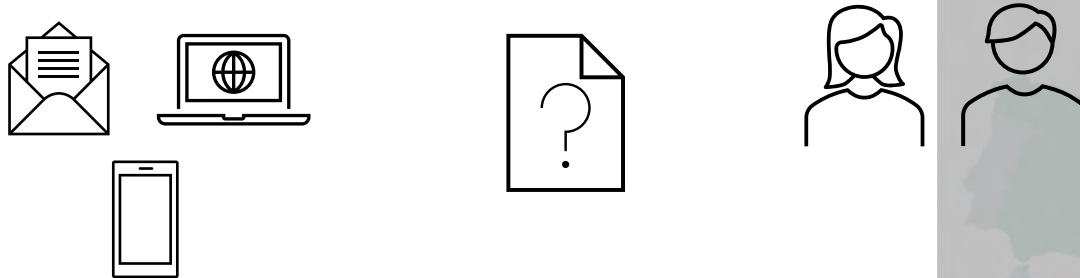


Outlook: Communication and information strategies

What increases or decreases acceptance?



What informative and communicative needs do different groups have?



**Thank you
for your attention!**

Human and societal dimensions



Dr Niall Dunphy, University College Cork  @NPDunphy



This project has received funding from the European Union's Horizon 2020 research and innovation programme under grant agreement No 884266

INTERNATIONAL WORKSHOP ON CO₂ CAPTURE AND UTILIZATION
TU/E - EINDHOVEN - 16-17 FEBRUARY 2021



REALISE project overview

- Demonstrating a refinery-adapted cluster-integrated strategy to enable full-chain CCUS implementation
- Horizon 2020 funded project (LC-SC3-NZE-5-2019-2020)
- 3-year duration – commenced May 2020
- Working to develop means to capture up to 90 % of CO₂ from multiple sources in operating refineries



www.realiseccus.eu



[@realise-ccus](https://twitter.com/realise-ccus)



This project has received funding from the European Union's Horizon 2020 research and innovation programme under grant agreement No 884266

Socio-political dimension of decarbonization

- Achieving the decarbonization of Europe is a key goal of the European Green deal.
- The required energy and industrial transition will both necessitate, and result in, a substantial societal transformation.
- Citizens have a crucial role to play in this transition, indirectly by accepting, supporting or resisting changes and thus influencing other policy actors or directly by consenting or refusing policy options in democratic decision-making processes.



Socio-political considerations within REALISE

- The technical and geological aspects of a CCS project are of course the primary focus of the planning and implementation phases.
- However, REALISE recognizes the importance of understanding (and appreciating) the social context of prospective CCS projects.
- Specific package of work which seeks to develop and in-depth understanding of the societal, socio-political and commercial contexts of CCS deployment.



WP4 Societal, socio-political and commercial context

Task 4.1 Education and public engagement best practice

Review of EPE practices

Task 4.2 Social acceptability, societal impact

Co-development and trialing of EPE programme

Task 4.3 Socio-political context analysis

Exploring socio-political lessons learned from global CCS projects

Task 4.4 Industrial context analysis

Engagement of key CCS actors through an industry club

Task 4.5 Public outreach activities and life-long learning

Contribute to improved societal readiness through outreach

Task 4.6 Synthesis report on societal readiness



T4.1 Education & public engagement best practice

- Comprises a critical review of education and public engagement (EPE) associated with large energy and related infrastructure.
- It is intended to work towards development of a framework for social acceptance of deploying CCS at an industrial site.
- Key examples of EPE identified through a literature search and via partners' networks using a snowballing approach.



T4.1 Education & public engagement best practice

- Seven EPE case studies characterised through a comprehensive desk study coupled with use of targeted informants.
 - CO2CRC Otway Project, Australia
 - Jämschwalde CCS Project, Germany
 - San Cristóbal Mine, Bolivia
 - Block Island Wind Farm, USA
 - Portsmouth Energy Recovery Facility, UK
 - Barendrecht CCS Project, Netherlands
 - Tomakomai CCS Demonstration Project, Japan
- The resultant report details the case studies, outlines methods adopted, explores key challenges, and presents best practices.



Need for acceptance

- The deployment of the major infrastructure needed to realise the required energy and industrial transition can only be successful with social acceptance.
- This means acceptance by the public generally (of the technology), but also, and critically acceptance by the community which will play host to the infrastructure.
- However, the strong public opposition faced by many projects threatens to significantly slow down this transition



Social acceptance ... (or)

- The term '*social acceptance*' with respect to infrastructure deployment, often implies (whether by design or otherwise) a passive acquiescence of a decision that has already been made.
- Such activities are usually concerned more with advocacy rather than decision-making or decision-making processes.
- So called DAD Model - Decide, Announce, Defend
- (or Decide, Announce Defend, Abandon ... DADA !)



(or) ... societal acceptability

- On the other hand, '*social acceptability*' refers to a project itself, it infers an effort to design (and implement) a project to be (more) agreeable to social stakeholders.
- It suggests (and arguably requires) a more participatory approach.
- This is an implied acknowledgement of societal stakeholders' legitimacy, provision for them to be earlier, and understanding that they would (be allowed to) provide real input into decision-making.



Acceptability ... ‘fairness’

Perceptions of fairness play a crucial role in determining the social acceptability of infrastructure projects.

- Procedural justice: the way in which the process is structured and implemented.
- Distributional justice: how benefits and ills of the project are distributed .
- Recognition justice: acknowledgement, recognition and respect.



Lennon, B., Dunphy, N. P., & Sanvicente, E. (2019). Community acceptability and the energy transition: a citizens' perspective. *Energy, Sustainability and Society*, 9(35). <https://doi.org/10.1186/s13705-019-0218-z>

Jenkins, K., McCauley, D., Heffron, R., Stephan, H., & Rehner, R. (2016). Energy justice: A conceptual review. *Energy Research & Social Science*, 11, 174–182. <https://doi.org/10.1016/j.erss.2015.10.004>

Examples of lessons from T4.1 ...

1. You cannot engage too early

- Early and open channels of communication with the public helps build mutual trust between process leaders and the community.
- Projects benefit when stakeholders across all groups are involved in the process.
- Ideally, the local community should be involved in the process of location selection, permitting, and policy-making, as soon as a project is proposed



Examples of lessons from T4.1 ...

2. Value of community liaisons

- Useful to hire staff who either already have good relations with local communities, or who have the skills to develop trusting relationships with communities.
- Having someone who is a 'known entity' with at least some members in the local community is vital in building trust.
- Can also ensure issues can be dealt with promptly and before they evolve into problems.



Examples of lessons from T4.1 ...

3. Advantages of blended approach to communication

- Complement official formal communication with informal modes to ensure effective outreach and build/maintain trust with communities
- A blended approach to communication can contribute to fostering what Dwyer and Bidwell (2019) describe as a “chain of trust” between the process leaders and local stakeholders.



Examples of lessons from T4.1 ...

4. First impressions count

- Build trust through early, open & responsive communication with communities.
- Actions are interpreted through the lens of relationships – a poor relationship could lead actions to be seen as hostile, whereas a hands-off approach might lead to perceptions of having something to hide.



Examples of lessons from T4.1 ...

5. Provide good quality information

- Availability of high-quality tailored information builds trust and pre-empts issues.
- Effective (and trusted) communications promotes credibility of both the project itself and the developer.
- Important to develop an understanding of target audiences and implement a communications strategy which reflects their cultural and other specificities.



Examples of lessons from T4.1 ...

6. Listening is also part of communication

- Educating and informing can help improve understanding on particular issues, however on its own it is a very limited strategy and minimizes the values of the process.
- Real engagement requires a two-way flow of information, as it encourages the public to voice their views and interests to inform decisions.



Next steps

- Building on the developed knowledge, an EPE programme will be co-designed with community stakeholders for the Cork Harbour case study.
- The approach will take an intersectional approach, considering the socio-demographic specificities of the relevant communities, *e.g.*, gender, life stage.
- Key elements will be trialed in local communities to evaluate effectiveness, to identify areas of potential improvement, and to ascertain transferability of the programme.



Dr Niall Dunphy
Director, Cleaner Production Promotion Unit
University College Cork



n.dunphy@ucc.ie



[@NPDunphy](https://twitter.com/NPDunphy)



INTERNATIONAL WORKSHOP ON CO₂ CAPTURE AND UTILIZATION

TU/e - EINDHOVEN - 16-17 FEBRUARY 2021

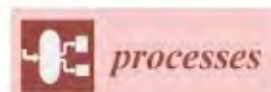
Session 2B (chairperson Vesna Middelkoop)

- 15:00-15:20 Dr. M. Slezekowski and Dr. Pablo Ortiz - Turning gas separation membranes green with biobased block copolymers
- 15:20-15:40 Dr. A. Benedito - CARMOF Project: a CO₂ capture demonstrator based on membrane and solid sorbents hybrid process
- 15:40-16:00 Dr. R.H. Heyn - Introduction to the COZMOS project
- 16:00-16:20 Dr. L. Petrescu - Converge technology for efficiency methanol production with negative CO₂ emissions: energy and environmental analysis

ORGANIZED BY



SPONSORED BY



Bio-based copolymers for membrane end products for gas separations



This project has received funding from the Bio Based Industries Joint Undertaking (JU) under the European Union's Horizon 2020 research and innovation programme, under grant agreement No 887075.

The JU receives support from the European Union's Horizon 2020 research and innovation program and the Bio Based Industries Consortium

Turning gas separation membranes green with biobased block copolymers

International workshop on CO₂ capture and utilization

TU/e Eindhoven, 16-17th February 2021

Dr. Marcin Ślęczkowski and Assoc. Prof. dr. Katrien Bernaerts

m.sleczkowski@maastrichtuniversity.nl

katrien.bernaerts@maastrichtuniversity.nl

Dr. Pablo Ortiz

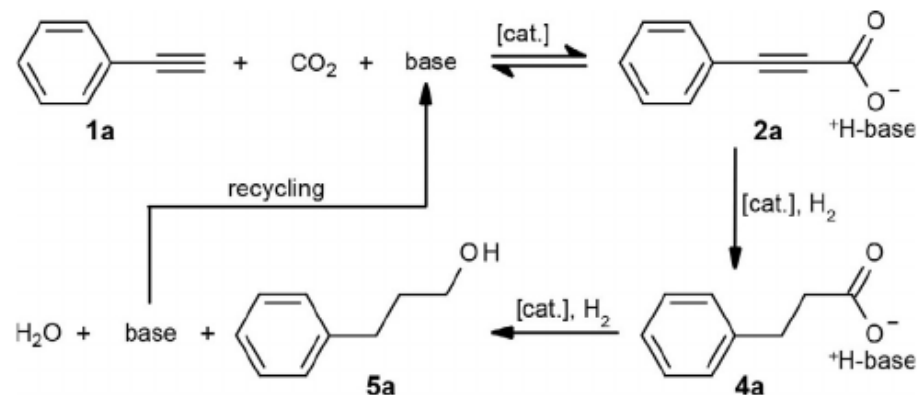
pablo.ortiz@tecnalia.com

The present publication reflects only the author's views. The Commission is not responsible for any use that may be made of the information contained therein.

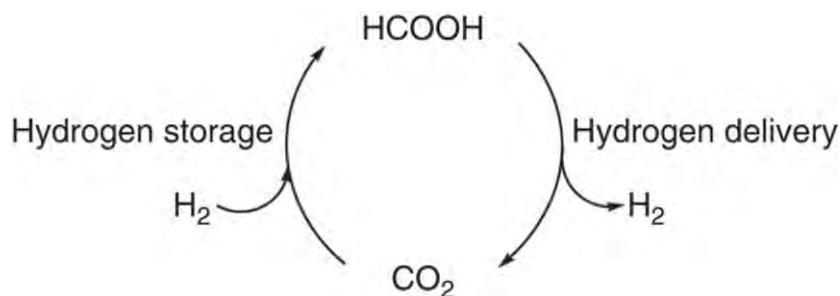
CO₂ recognized as useful raw material.



<https://www.covestro.com/en/sustainability/lighthouse-projects/co2-dreams>



T. Wendling et al, *Chem. Eur. J.*, 24, **2018**, 6019-6024



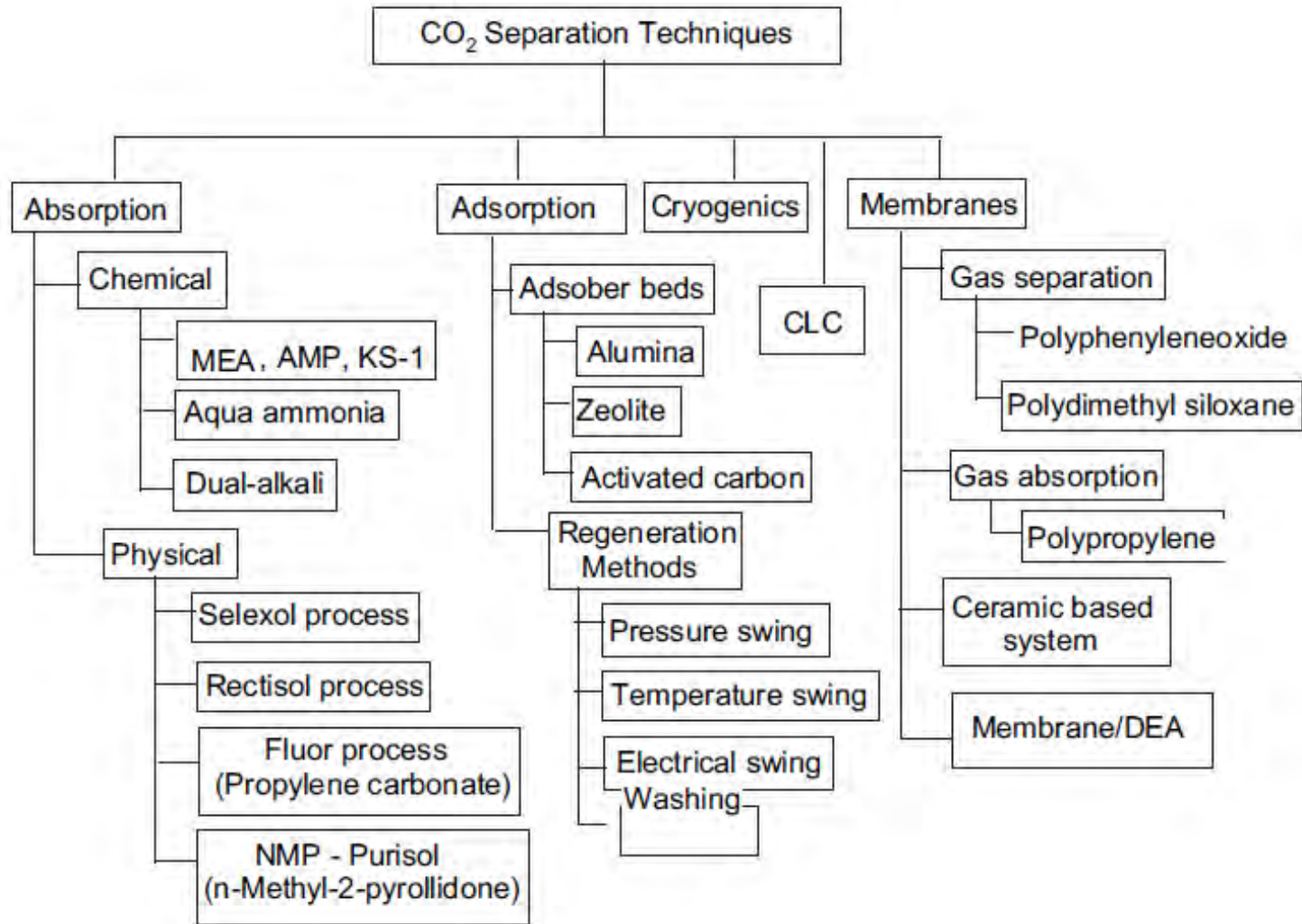
S. Moret et al, *Nat Commun.*, 5, **2014**, 4017

De Novo metabolic conversion of electrochemically produced formate into hydrocarbons



www.eforfuel.eu

Multiple separation techniques are available.

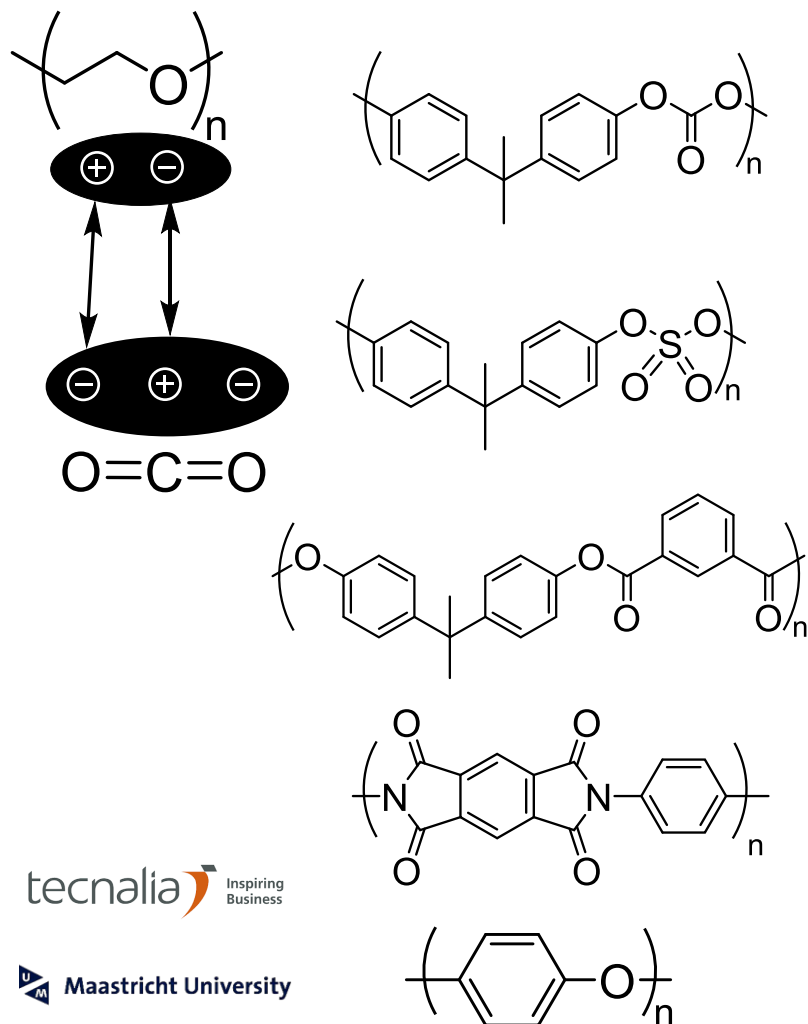


A. A. Olajire, *Energy*, 35, **2010**, 2610-2628

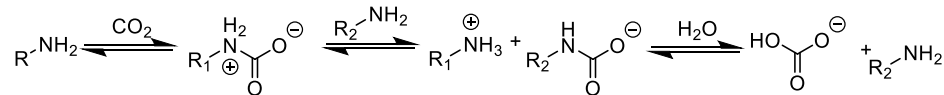
Membranes utilize dipole or ionic interactions

MTR Polaris®

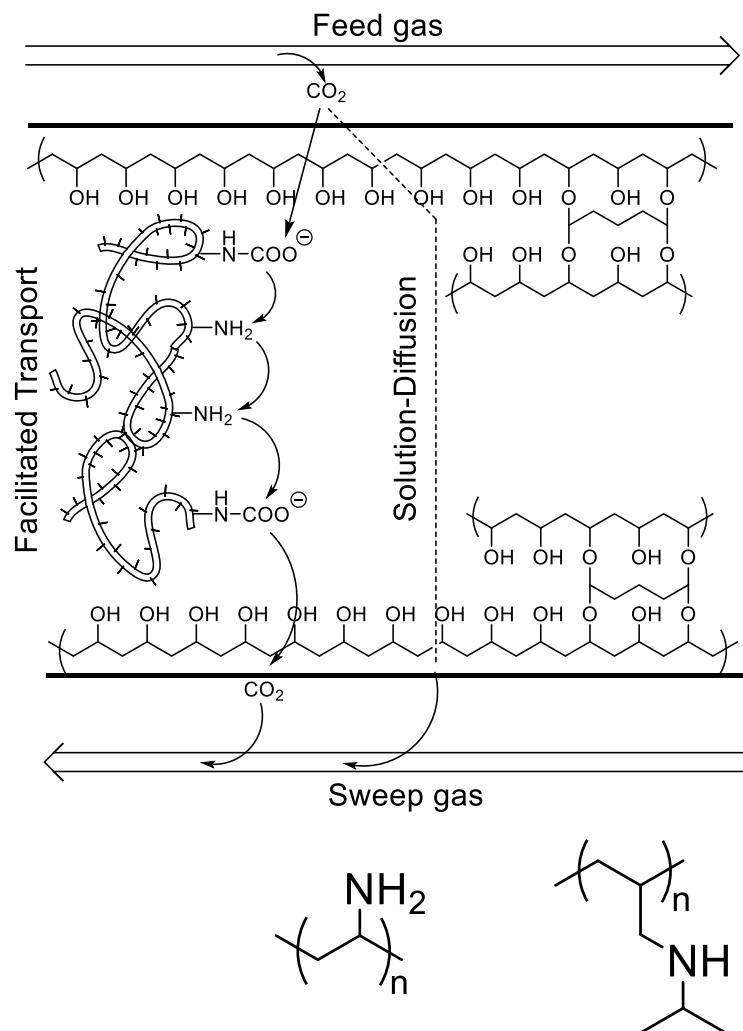
Cross-linked PEO of $\sim 700 \text{ g mol}^{-1}$

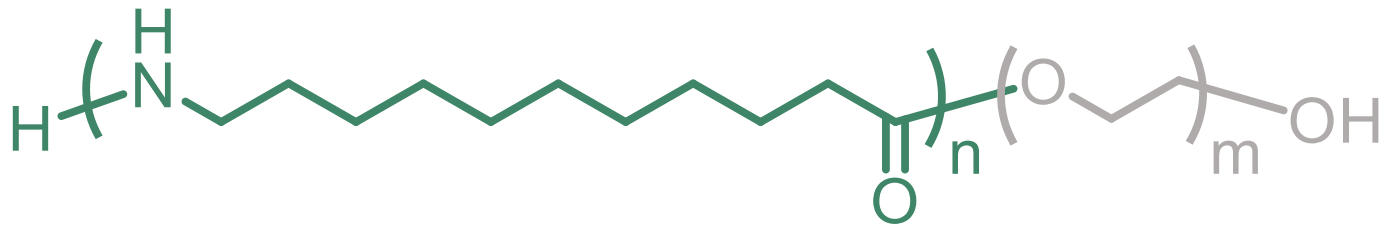
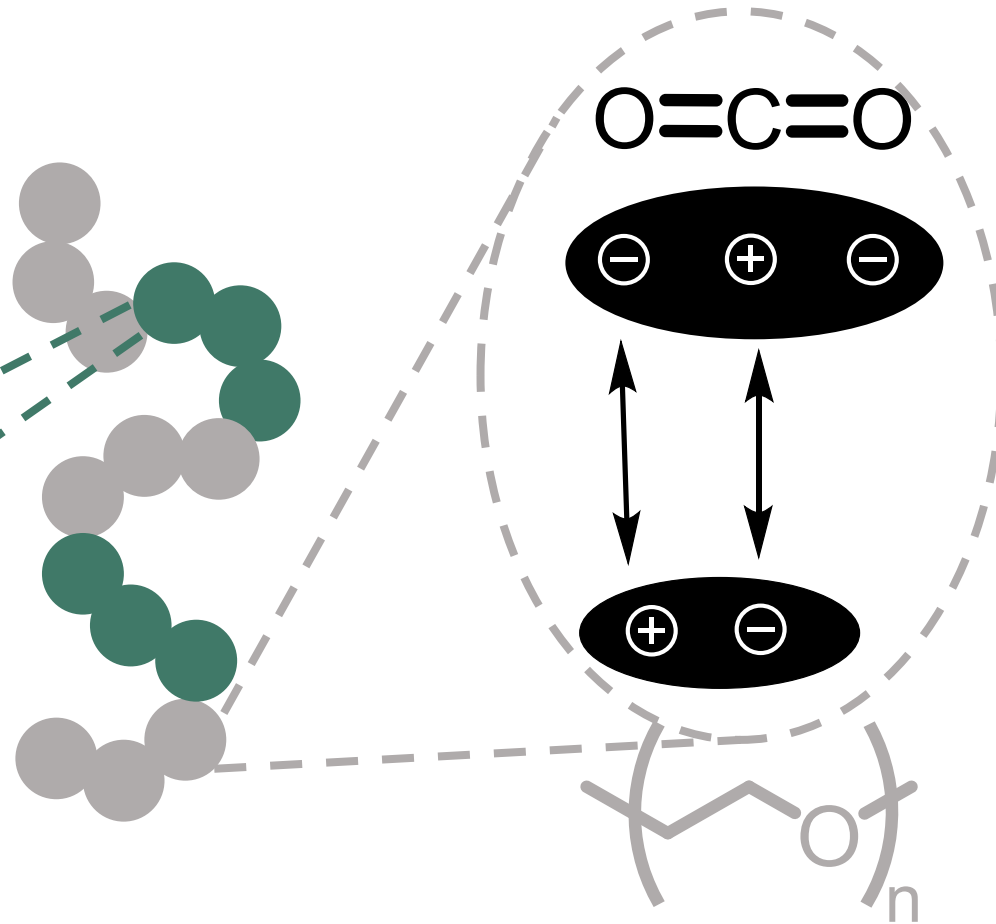


a)



b)

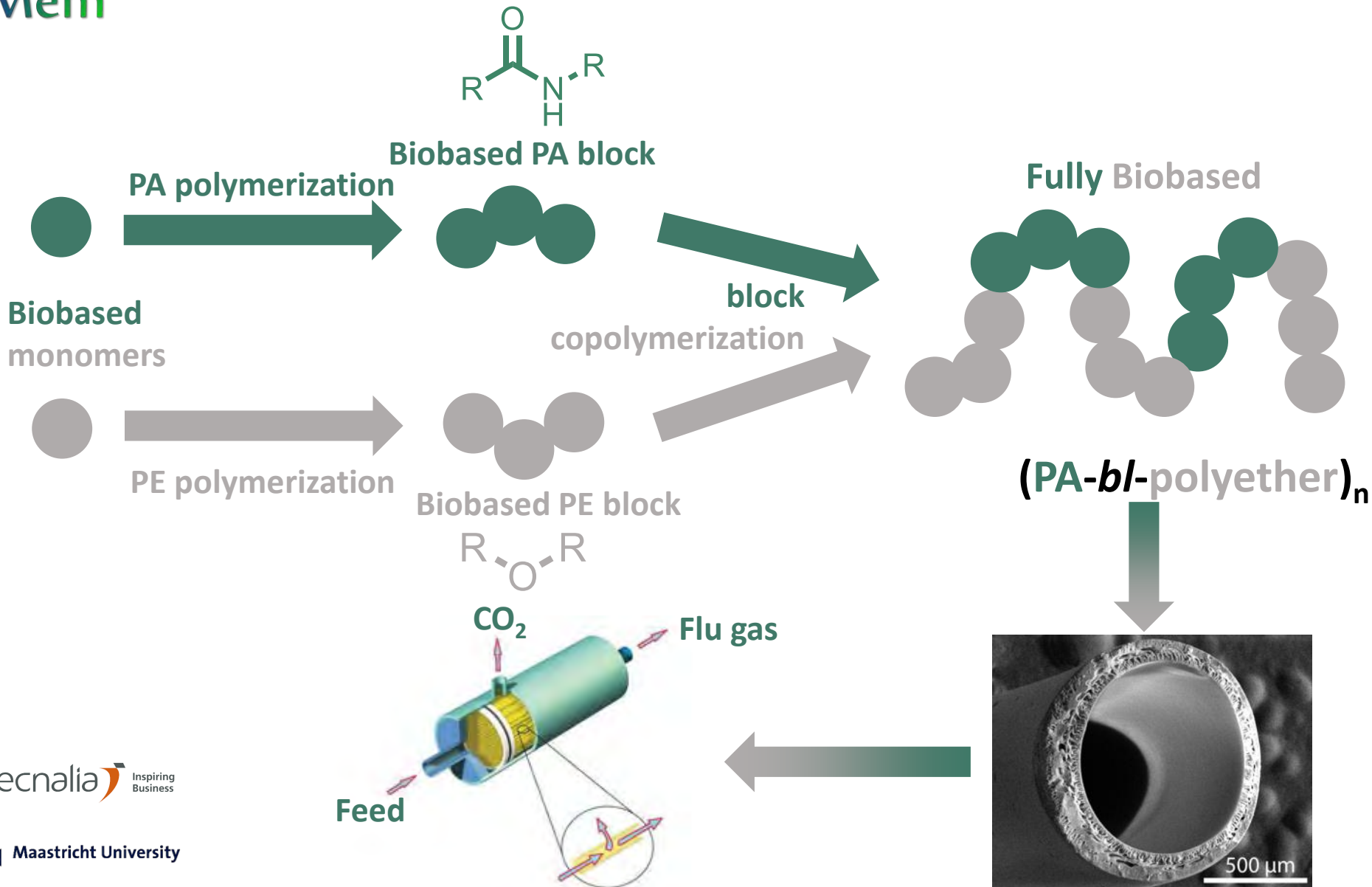




Develop bio-based polyether-b-polyamide (PEBA) copolymers as precursors for gas separation membranes at TRL 5, with

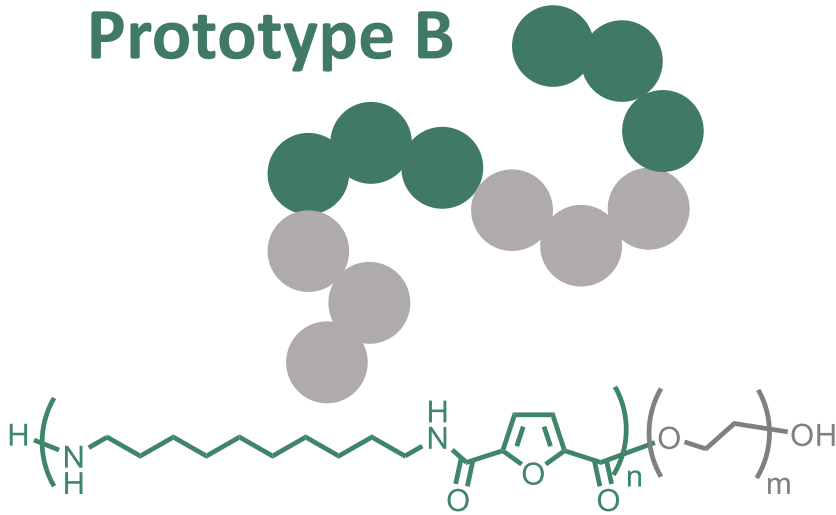
- compared to commercially available PEBA PA₁₁-b-PEO
 - higher processability into monolithic hollow fiber membrane (i.e. solubility)
 - higher bio-based content
- additional performance, like
 - higher gas separation performance and/or
 - higher resistance to chemical attack (reversible crosslinking)

New, biobased block copolymers

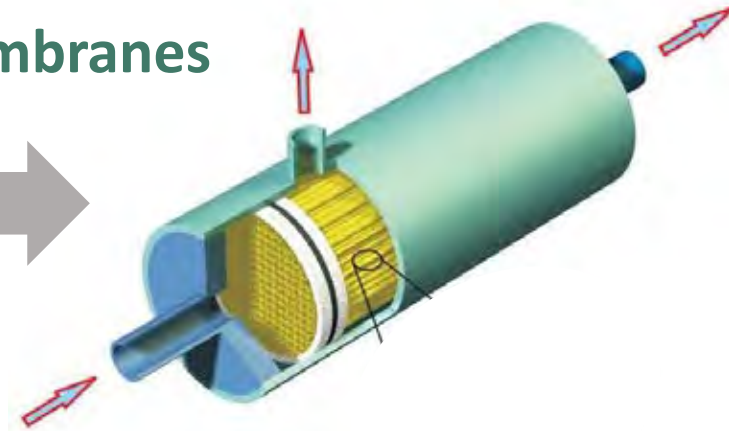


Two new scalable prototypes

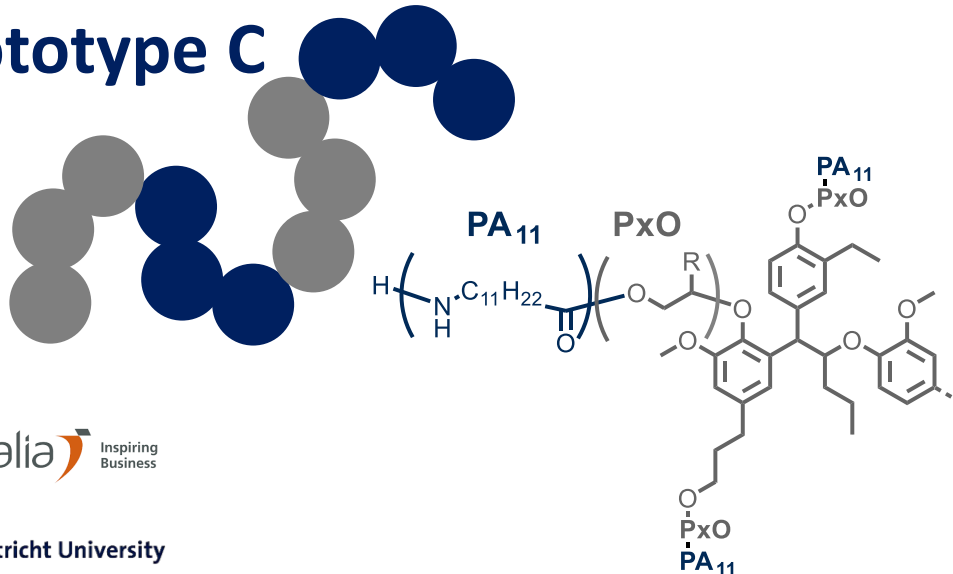
Prototype B



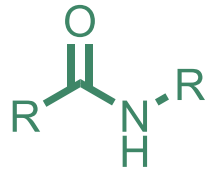
Two new PEBA copolymers suitable for HF membranes



Prototype C



Challenge: synthesis of polymer building blocks



polymerization

tecnalia

Inspiring Business

Biobased monomers



polymerization

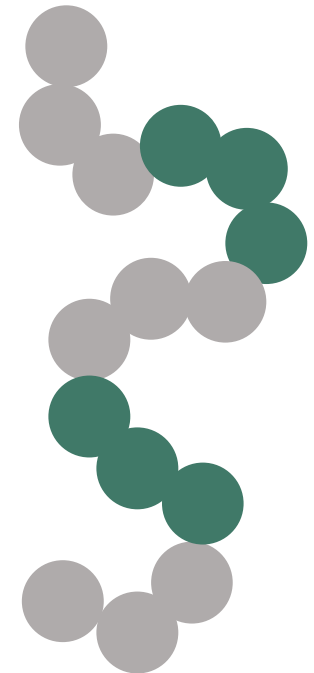


Biobased PE block
hydroxy functionalized



copolymerization

block

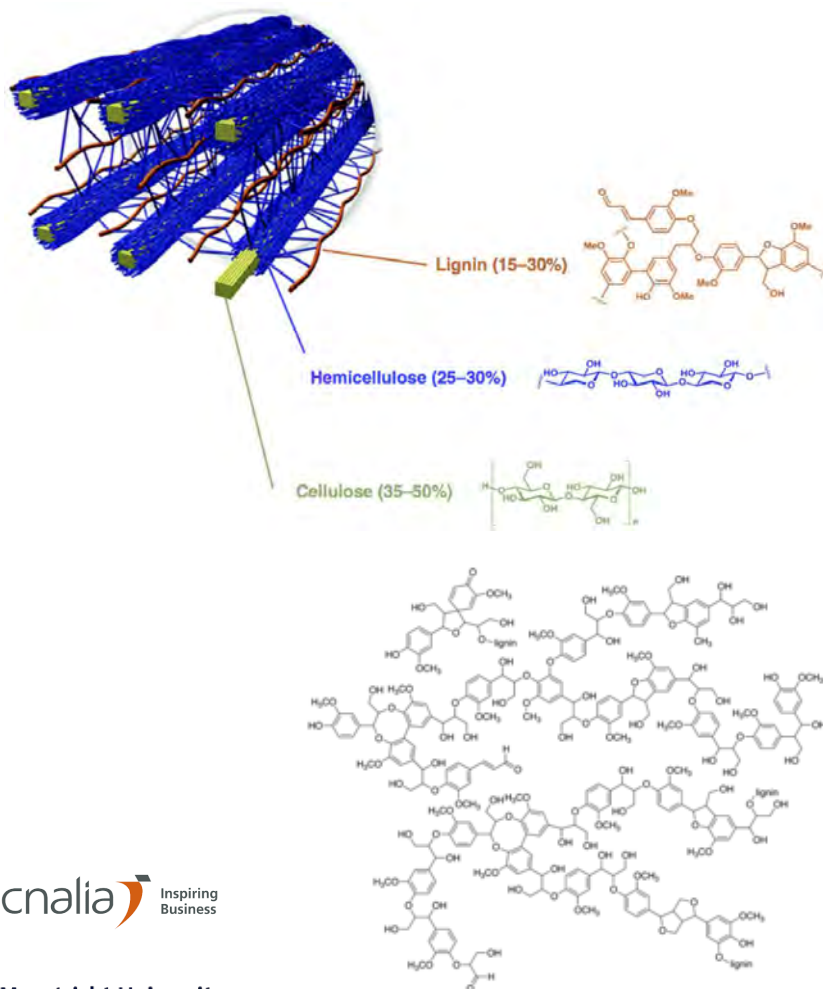


Fully Biobased
(PA-bi-polyether)_n

- Synthesis and characterization of both PA and PE blocks
- Synthetic methodology choice / optimization
- Structure – property screening / optimization

Lignin-based polyols

Lignin overview



Characteristics:

- Availability
- Aromatic content

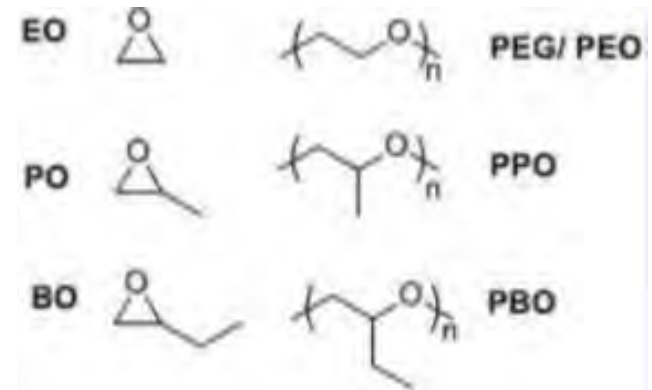
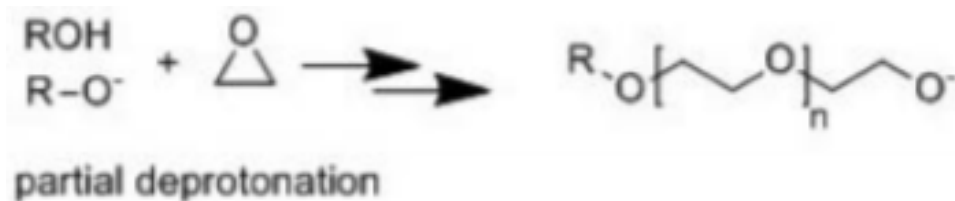
Currently lignin:

- Low solubility in organic solvents
- Low compatibility with other reagents
- Heterogeneous
- Polydisperse
- Low reactivity

Ways to overcome drawbacks:

- Using mild isolation techniques
- Depolymerizing lignin
- Fractionating lignin (solvent extraction)
- Chemically modifying it

Anionic ROP of oxiranes



Anionic ROP of oxiranes using lignin as initiator

150-330°C

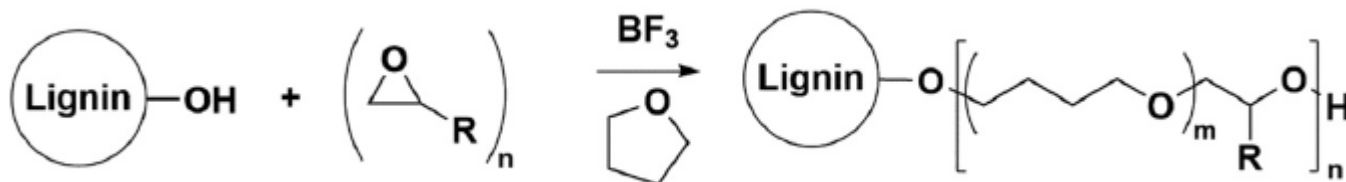
6-40 bar

Side products

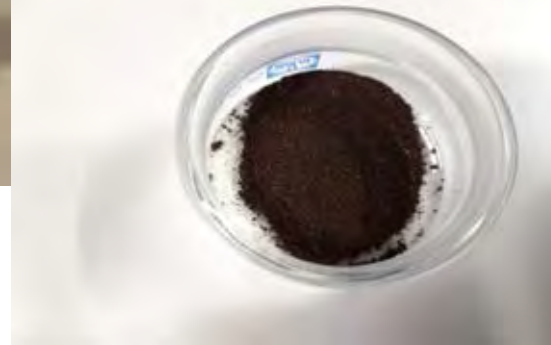
Bad odor

Lignin-based polyols

Cationic ROP of oxiranes using lignin as initiator

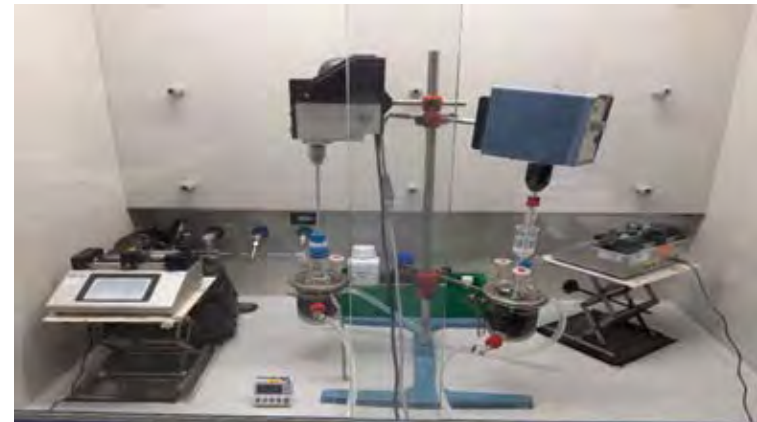
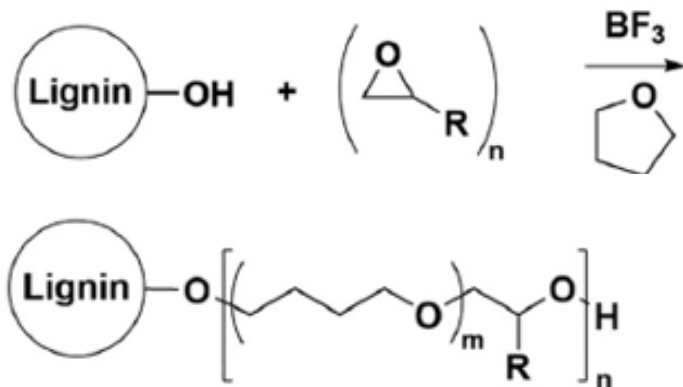


Lignin screening



$M_w \approx 1000$

Initial screening of the reaction conditions



Parameters

- Oxirane
- Concentration of lignin
- Ratio butylene oxide/lignin OH

Results

- Reproducibility
- Viscosity
- Molecular weight
- Polydispersity
- OH number

Characteristics

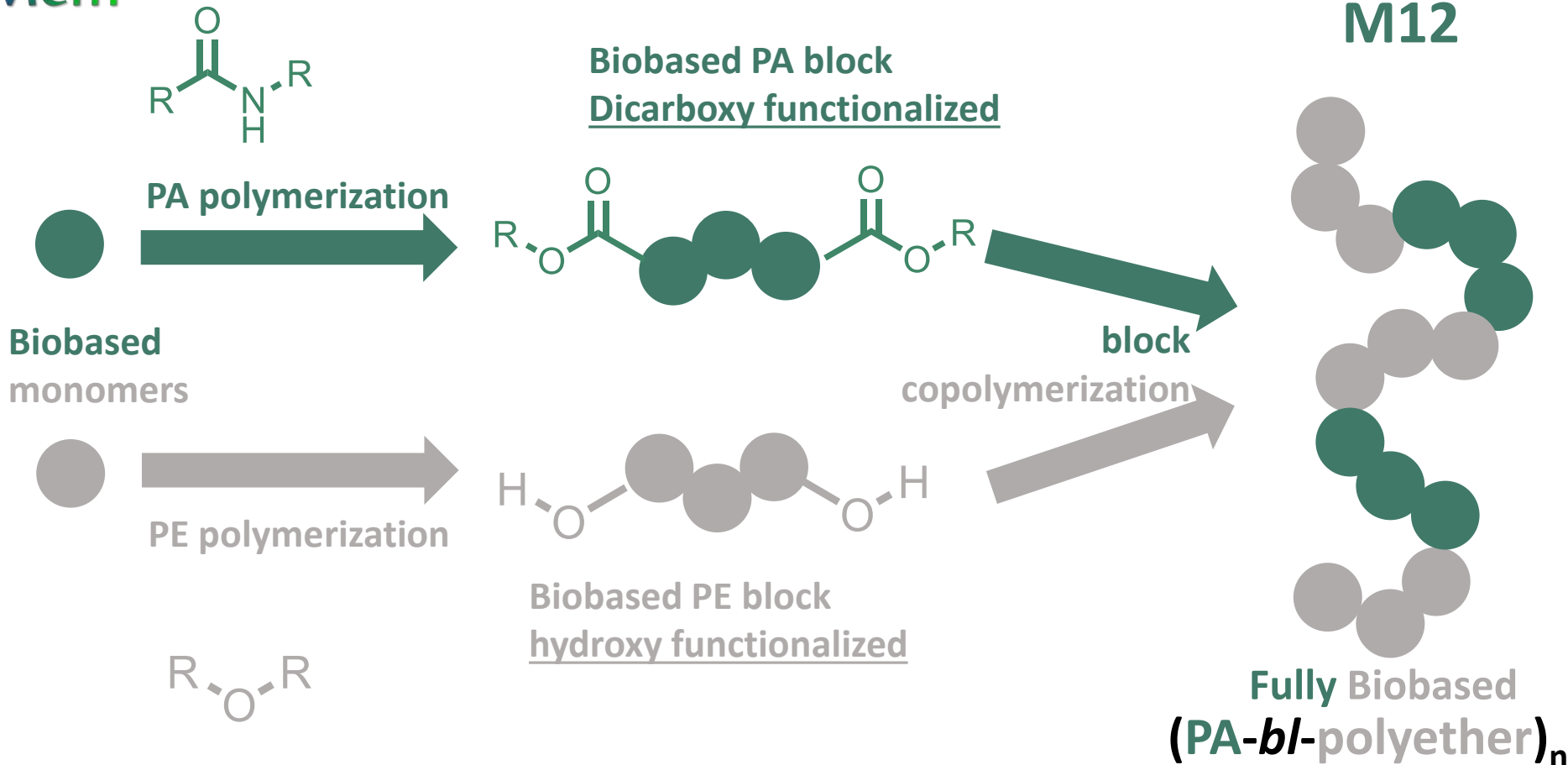
Delivery of 3 LBP to the University of Maastricht

- 3x 50g
- Liquid/viscous
- From 2 different lignins
- M_w : 4000-10000 g/mol
- Lignin content (%): 20-28
- OH number: 86-110 mg KOH/g



Challenge: synthesis of polymer building blocks

M12



- Synthesis and characterization of both PA and PE blocks
- Synthetic methodology choice / optimization
- Structure – property screening / optimization

R-C(=O)-N(R)-R

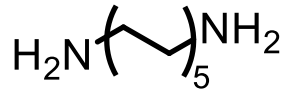
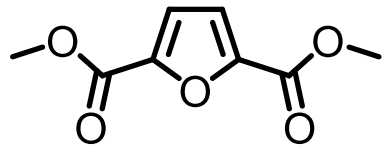
PA polymerization


$$\text{H}-(\underset{\text{H}}{\overset{|}{\text{N}}}(\text{CH}_2)_6-\text{NH}-\text{C}(=\text{O})-\text{furan}-\text{C}(=\text{O}))_n-[\text{O}(\text{CH}_2)_m\text{OH}]_m$$

Fully Biobased
(PA-*bi*-polyether)_n

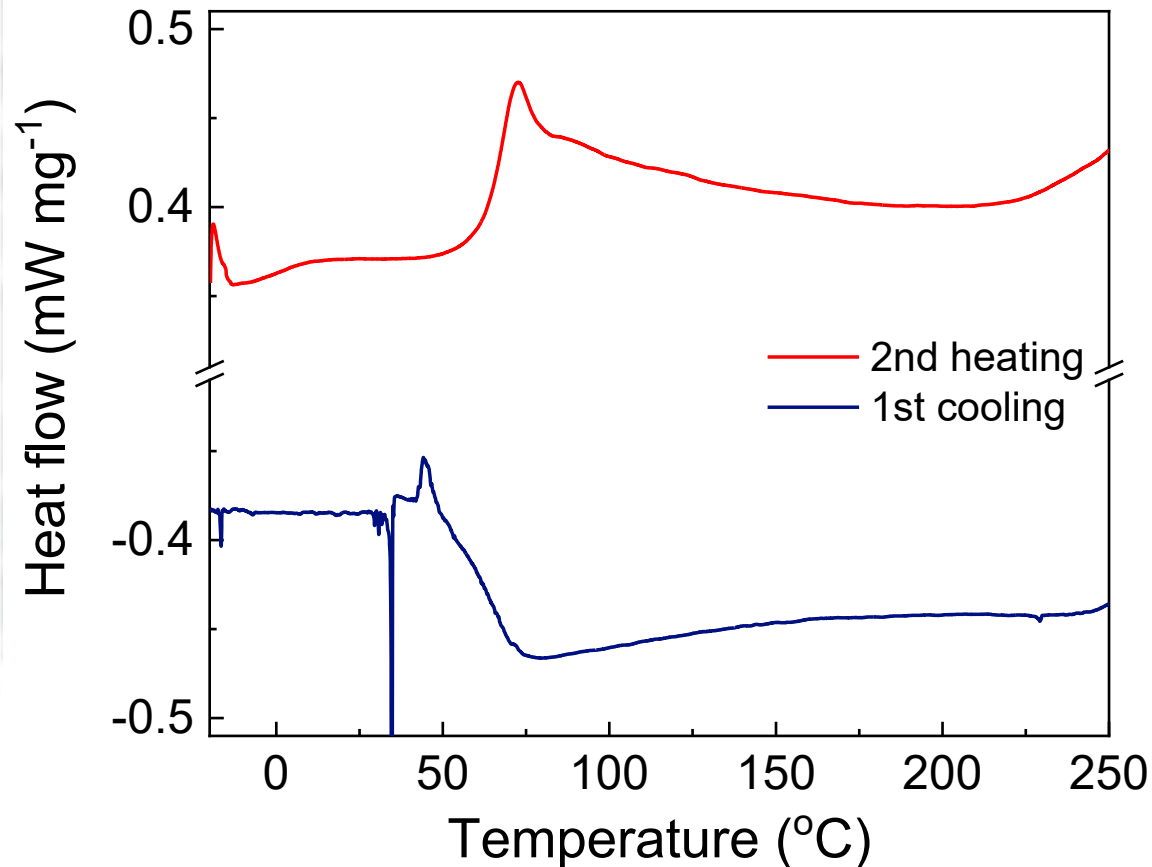
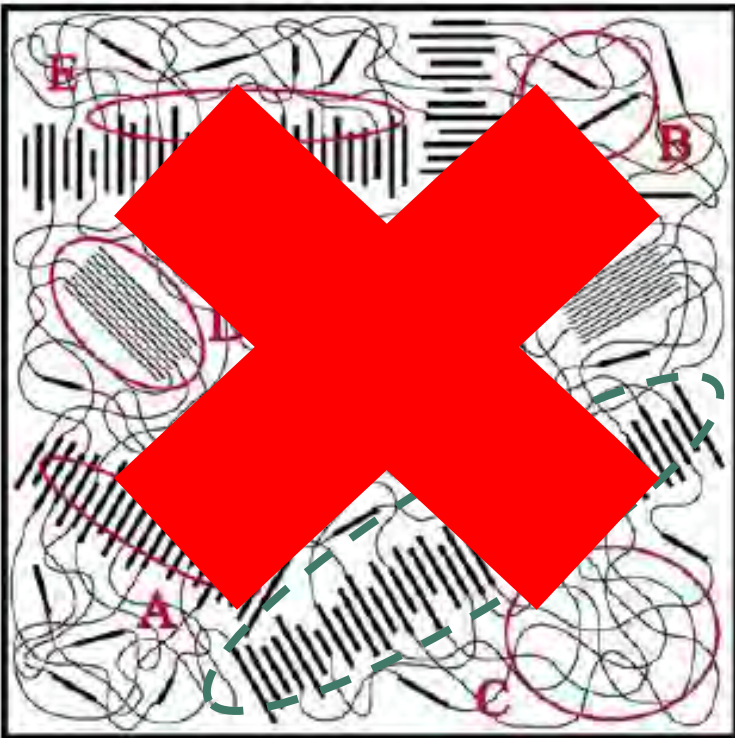
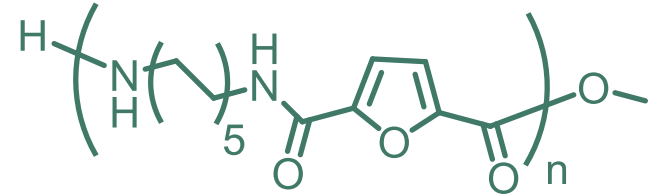
- Synthesis and characterization of PA
- Synthetic methodology choice / optimization
- Structure – property screening / optimization

No melting transitions in furan-only polyamide

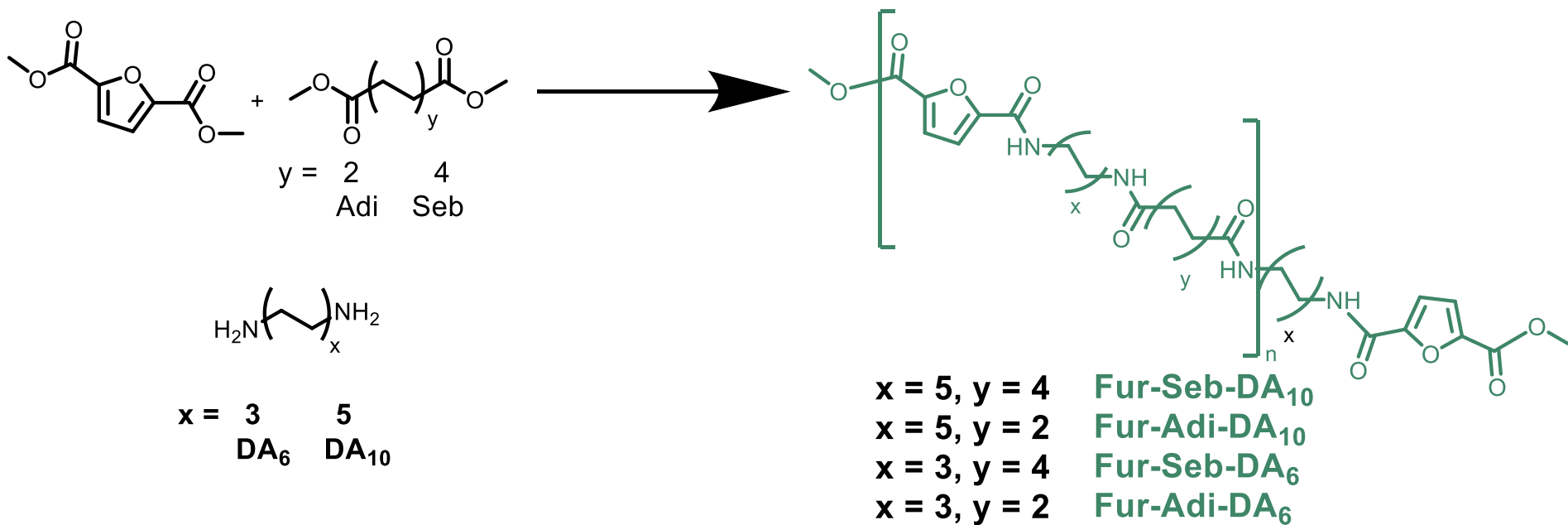


T: 150 to 220 °C

p: atm to 5 mbar

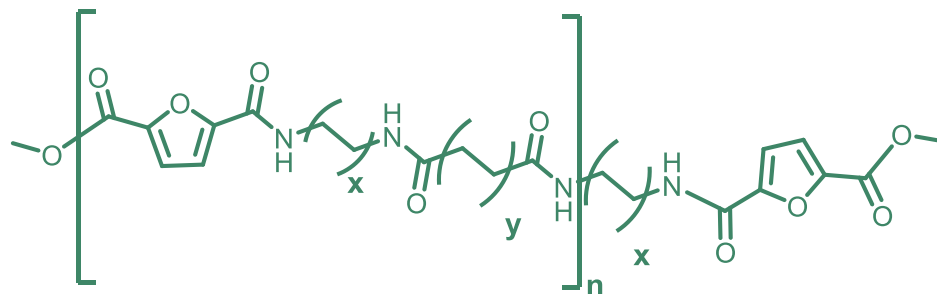


Library of copolyamides with linear comonomers



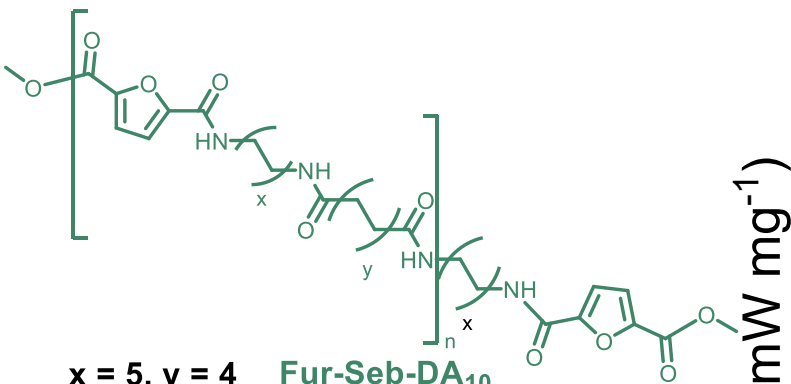
Desired molecular weight and AV are achieved

| Feed | | | Results | | | |
|-------|----------|---------|---------|----------------------------|-------------|-----------------|
| Furan | Sebacate | Adipate | AV | Calculated M_n [g / mol] | M_n (GPC) | \bar{D} (GPC) |
| 1 | 0 | 0 | 92 | 950 | | |
| 0.8 | 0.2 | 0 | 112 | 900 | 4500 | 1.8 |
| 0.6 | 0.4 | 0 | 93 | 1000 | 3500 | 1.9 |
| 0.4 | 0.6 | 0 | n/a | n/a | 2500 | 2.1 |
| 0.2 | 0.8 | 0 | 91 | 950 | 2000 | 2.2 |
| 1 | 0 | 0 | 92 | 950 | | |
| 0.8 | 0 | 0.2 | 98 | 950 | 3000 | 2.1 |
| 0.6 | 0 | 0.4 | 93 | 950 | 2000 | 2.2 |
| 0.4 | 0 | 0.6 | 102 | 1000 | 3000 | 2.3 |
| 0.2 | 0 | 0.8 | 94 | 1050 | 2000 | 2.4 |



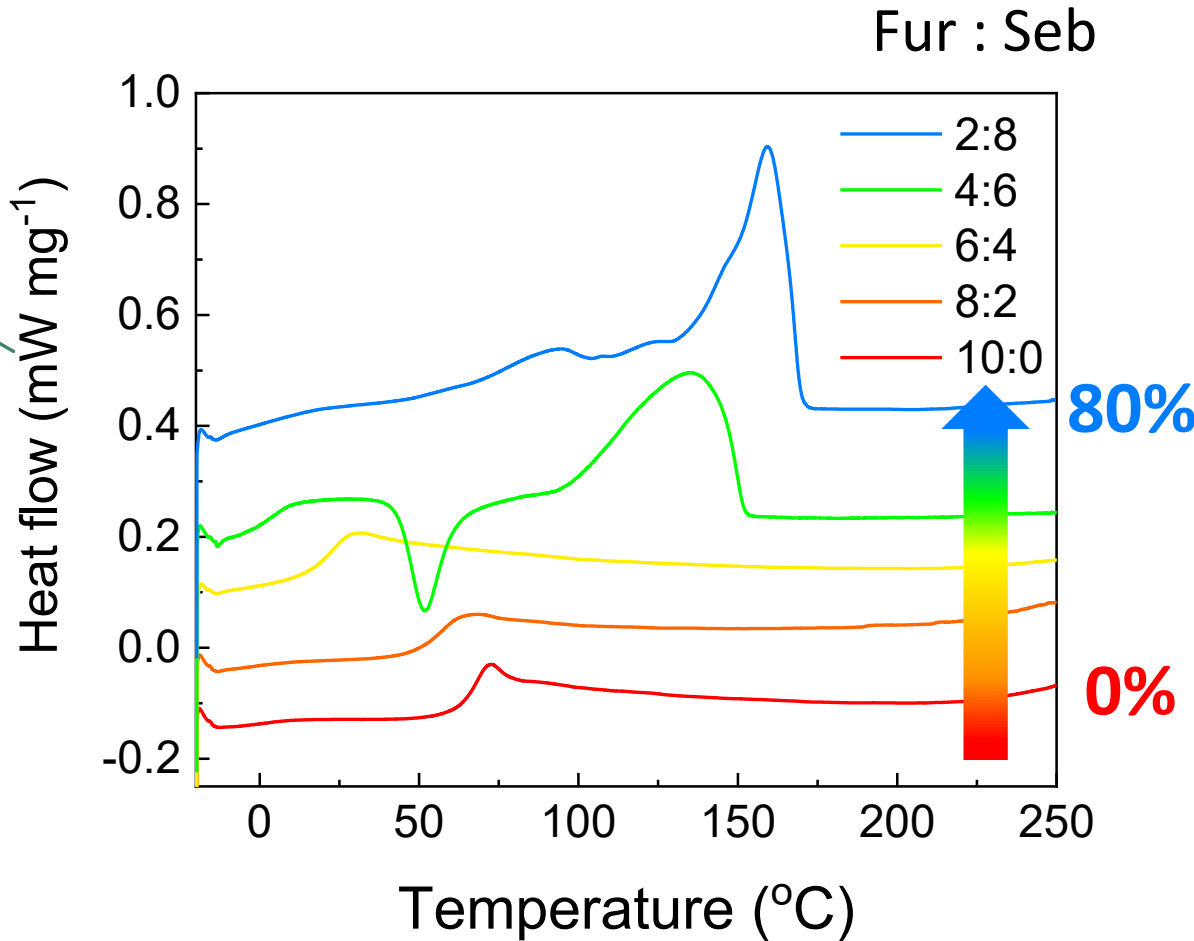
$x = 5, y = 4$ Fur-Seb-DA₁₀
 $x = 5, y = 2$ Fur-Adi-DA₁₀
 $x = 3, y = 4$ Fur-Seb-DA₆
 $x = 3, y = 2$ Fur-Adi-DA₆

Melting transitions recognized in copolyamides

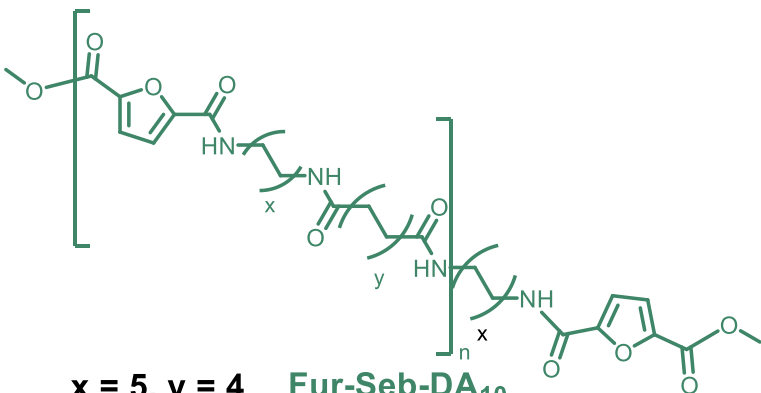


$x = 5, y = 4$ Fur-Seb-DA₁₀
 $x = 5, y = 2$ Fur-Adi-DA₁₀
 $x = 3, y = 4$ Fur-Seb-DA₆
 $x = 3, y = 2$ Fur-Adi-DA₆

add data for PA11 reference



DA10



x = 5, y = 4 Fur-Seb-DA₁₀
x = 5, y = 2 Fur-Adi-DA₁₀
x = 3, y = 4 Fur-Seb-DA₆
x = 3, y = 2 Fur-Adi-DA₆

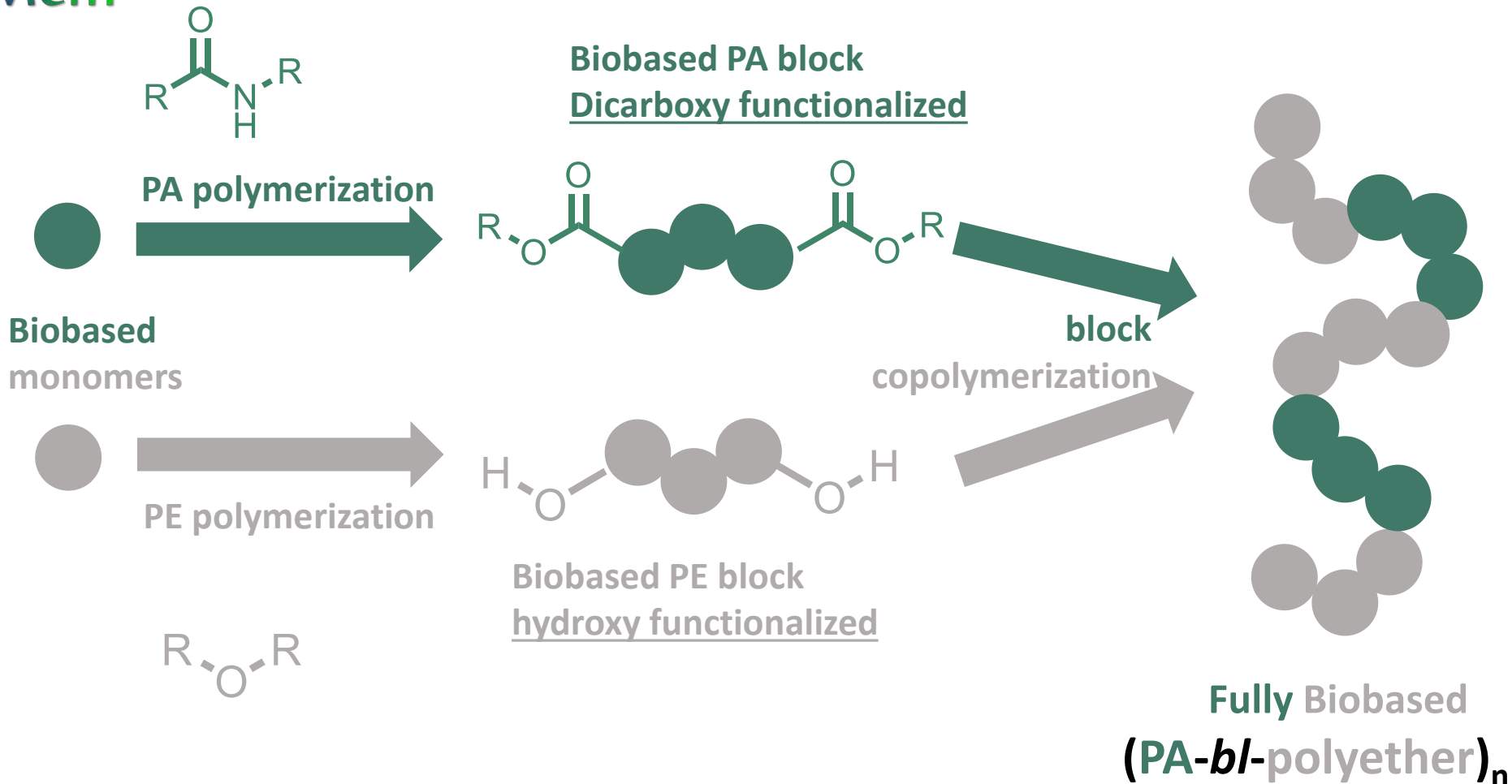
add data for PA11 reference

DA6

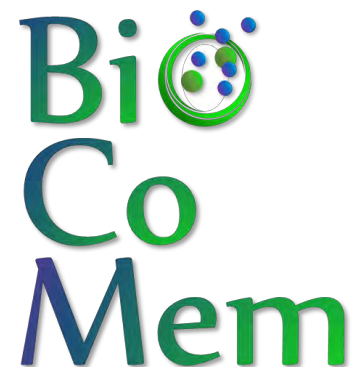
| Furan | Sebacate | Adipate | T_g [°C] | T_m [°C] |
|-------|----------|---------|------------|------------|
| 1 | 0 | 0 | 57 | n |
| 0.8 | 0.2 | 0 | 52 | n |
| 0.6 | 0.4 | 0 | 15 | n |
| 0.4 | 0.6 | 0 | 1 | 136 |
| 0.2 | 0.8 | 0 | ? | 159 |
| 1 | 0 | 0 | 57 | n |
| 0.8 | 0 | 0.2 | 30 | n |
| 0.6 | 0 | 0.4 | 17 | 149 |
| 0.4 | 0 | 0.6 | 0 | 168 |
| 0.2 | 0 | 0.8 | ? | 218 |

| | | | | |
|-----|-----|-----|----|-----|
| 1 | 0 | 0 | 90 | n |
| 0.8 | 0.2 | 0 | 43 | n |
| 0.6 | 0.4 | 0 | 36 | n |
| 0.4 | 0.6 | 0 | 9 | 148 |
| 0.2 | 0.8 | 0 | ? | 174 |
| 1 | 0 | 0 | 90 | n |
| 0.8 | 0 | 0.2 | 57 | n |
| 0.6 | 0 | 0.4 | 38 | n |
| 0.4 | 0 | 0.6 | 28 | 164 |
| 0.2 | 0 | 0.8 | ? | 212 |

Outlook: synthesis of block copolymers



Bio-based copolymers for membrane end products for gas separations



This project has received funding from the Bio Based Industries Joint Undertaking (JU) under the European Union's Horizon 2020 research and innovation programme, under grant agreement No 887075.

The JU receives support from the European Union's Horizon 2020 research and innovation program and the Bio Based Industries Consortium

Turning gas separation membranes green with biobased block copolymers

International workshop on CO₂ capture and utilization

TU/e Eindhoven, 16-17th February 2021

Dr. Marcin Ślęczkowski and Assoc. Prof. dr. Katrien Bernaerts

m.sleczkowski@maastrichtuniversity.nl

katrien.bernaerts@maastrichtuniversity.nl

Dr. Pablo Ortiz

pablo.ortiz@tecnalia.nl

The present publication reflects only the author's views. The Commission is not responsible for any use that may be made of the information contained therein.



Adolfo Benedito
AIMPLAS
(16&17 February)

New process for efficient CO₂ capture by innovative adsorbents based on modified carbon nanotubes and MOF materials.

H2020-NMBP-20-2017

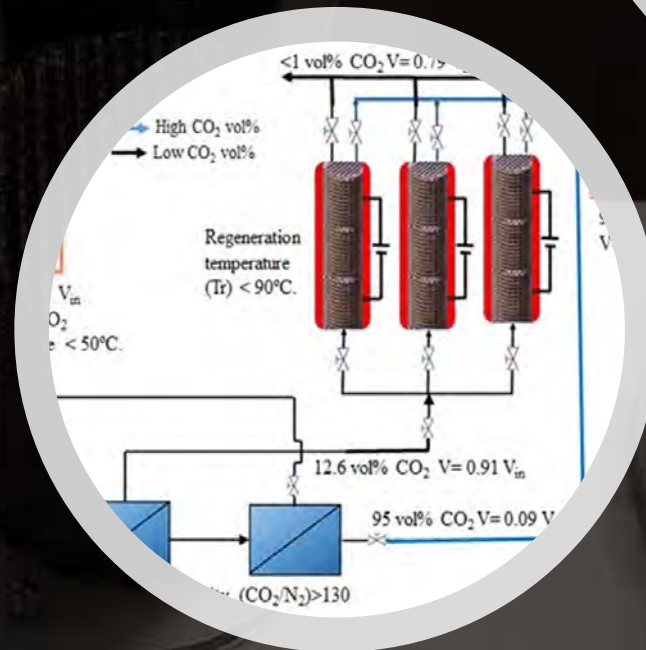


*This project has received funding from the European Union's Horizon 2020 research and innovation programme under grant agreement No 760884.
This publication reflects only the author's view and that the Commission is not responsible for any use that may be made of the information it contains.*

CARMOF Project

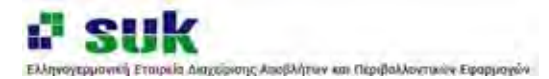
TAILOR-MADE 3D PRINTED STRUCTURES BASED ON
CNT AND MOF MATERIALS FOR EFFICIENT CO₂
CAPTURE

CARMOF is developing a hybrid CO₂ process combining **VTSA modules** based on 3D printed monoliths with thermoelectric regeneration and "in cascade" **membranes system**. The goal is to achieve high purity CO₂ streams from synergetic effects from both technologies

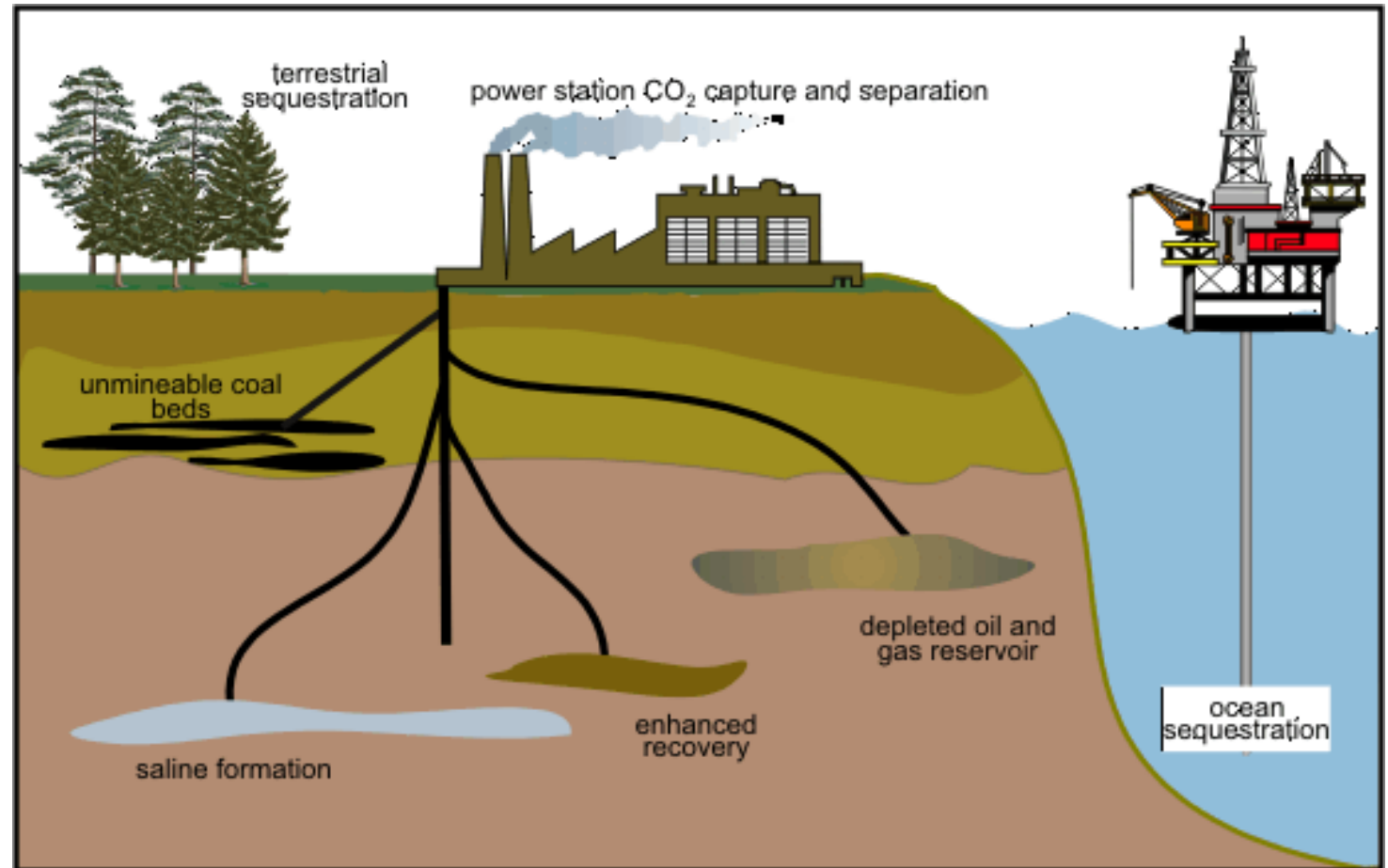


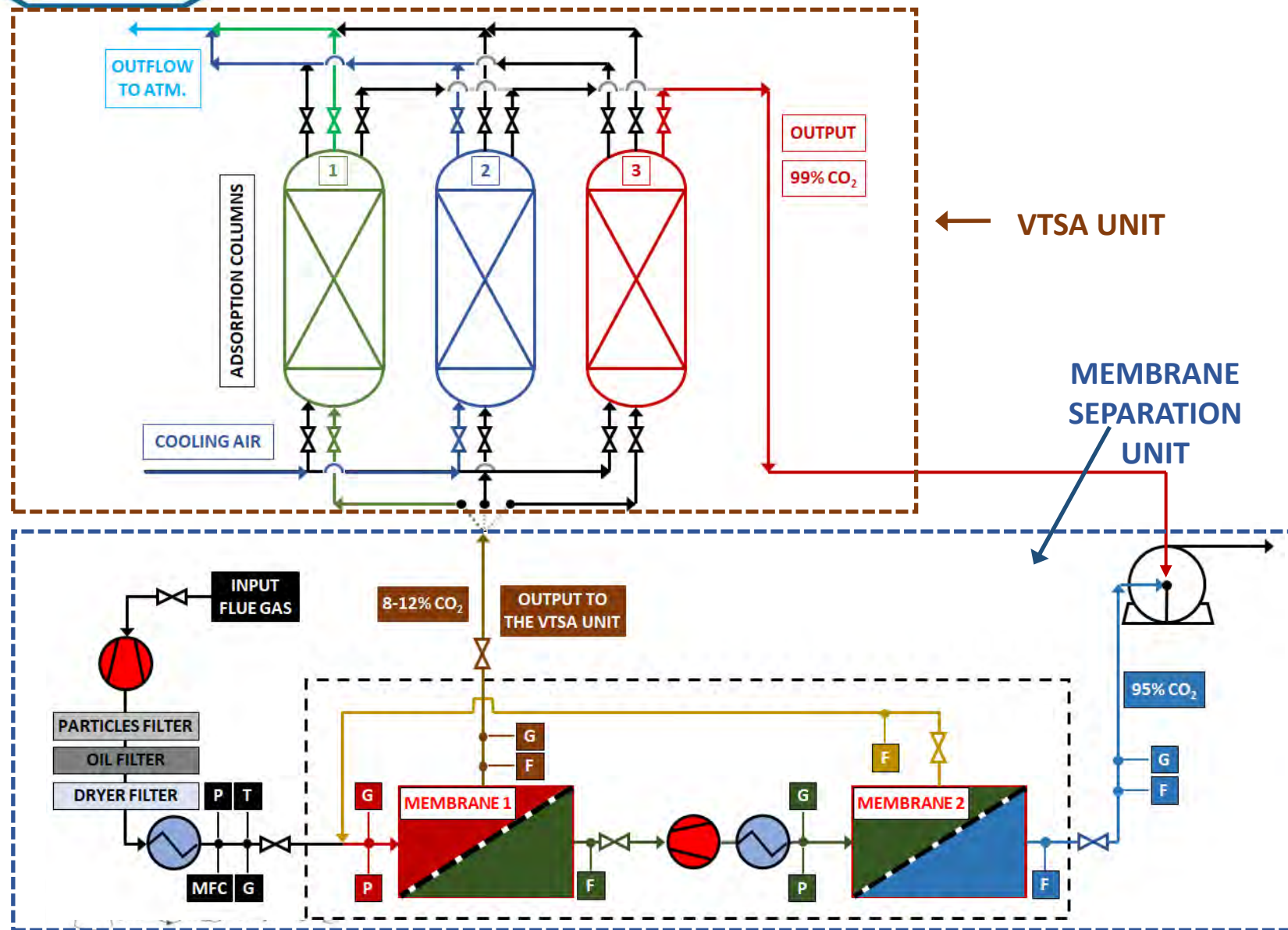


- Consortium consists of 15 partners from 9 countries
- Up to seven industrial pilot plants are proposed across the project – includes both manufacture and capture facilities
- €7.4 M overall budget



- Increasing levels of atmospheric CO_2 are a major contributor to anthropogenic climate change
- CCS aims to capture CO_2 from power plants and industry and sequester it underground
- Current capture and separation technologies use organic amines
- Regeneration of these sorbents is inefficient – it can consume up to 30% of the energy produced by a power station!





CARMOF is a hybrid system based on:

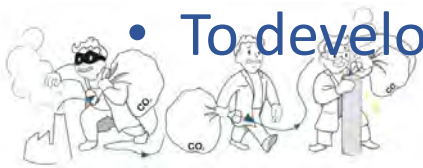
1. VTSA Unit.
2. Membrane Separation Unit.

Two full ***demo pilot plants*** are planned for 2022 with a capacity of up to 350 tonnes CO₂/year.



The **Key Objectives**:

- Industrial scale-up to a **full demonstrator** consisting on hybrid membrane combined with VTSA and Joule Swing (JS) regeneration processes.
- To develop a complete two-stage separation membrane system to couple with VTSA system.
- **Innovative dry sorbents** for post-combustión CO₂ capture based on combinations of MOFs, rGO and CNTs, supported by PEI as binder.
- To enhance **manufacturing processes** for these materials combination.
- To develop customized and packed monolith structures based on **3D printing**.

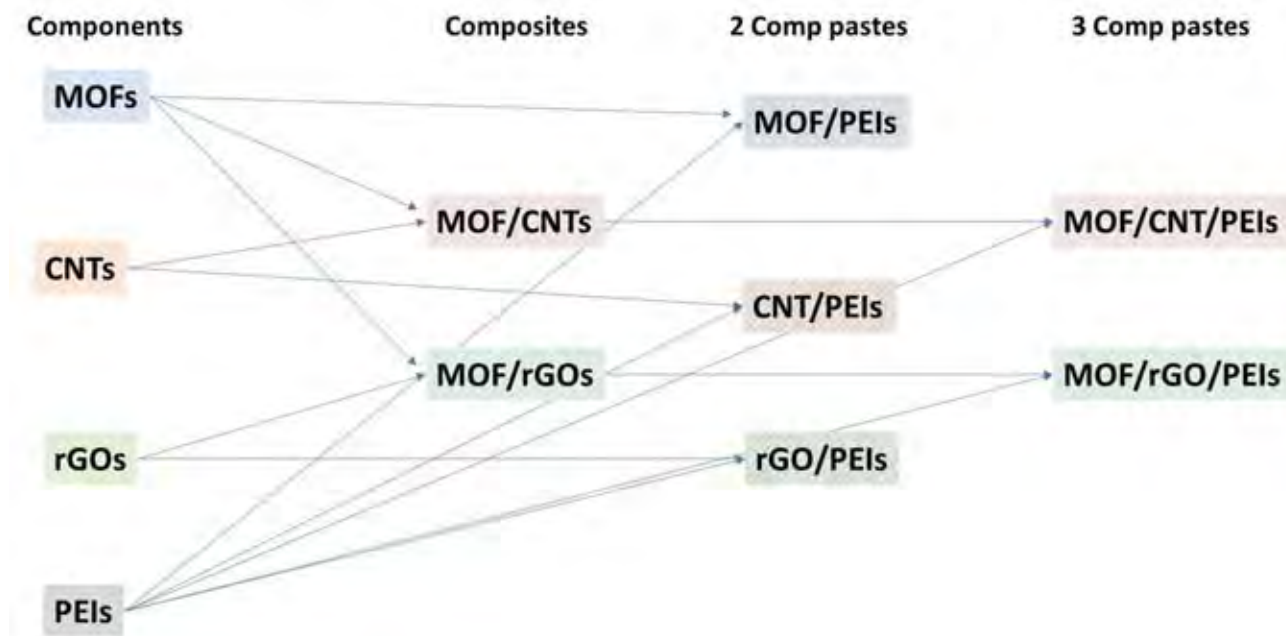


Innovative **dry sorbents**: Production of 3D printed monoliths of porous hybrid nanomaterials for solid phase CO₂ absorption.

- Hybrid materials based on MOF, carbon nanotubes and reduced graphene oxide.
- 3D printing used to obtain monolithic structures, high packing density and low pressure drop.
- It allows efficient regeneration of saturated sorbents by heating by Joule effect and absorption at vacuum temperature (VTSA).



Innovative **dry sorbents**: Production of 3D printed monoliths of porous hybrid nanomaterials for solid phase CO₂ absorption.



- Production optimization and **upscaling of MOF** component.
- Production of **functionalized CNT** component
MWCNTs, functionalization by oxidation (-OH, -COOH. Etc)
- Production of **functionalized rGO**
rGO, carboxylic groups
- MOF/CNT and MOF/rGO **chemical composites**



MOFs for CCS

Requirements:

- High volumetric and gravimetric CO₂ capacity
- High CO₂ selectivity (Power station flue gas is not pure CO₂)
- High chemical and physical stability
- Minimal loss of porosity over many heating/cooling cycles
- Low cost!



**Lab scale reactor system:
100 g MOF/day**



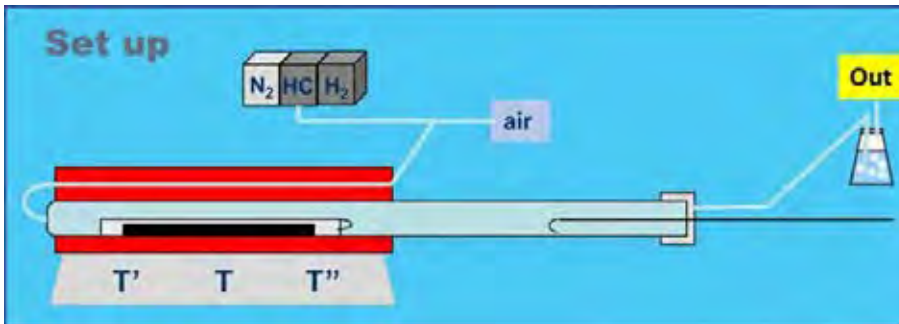
**Pilot scale reactor
system: 5 Kg MOF/day
STY = 266 Kg m³ day⁻¹**



Solution: CPO-27

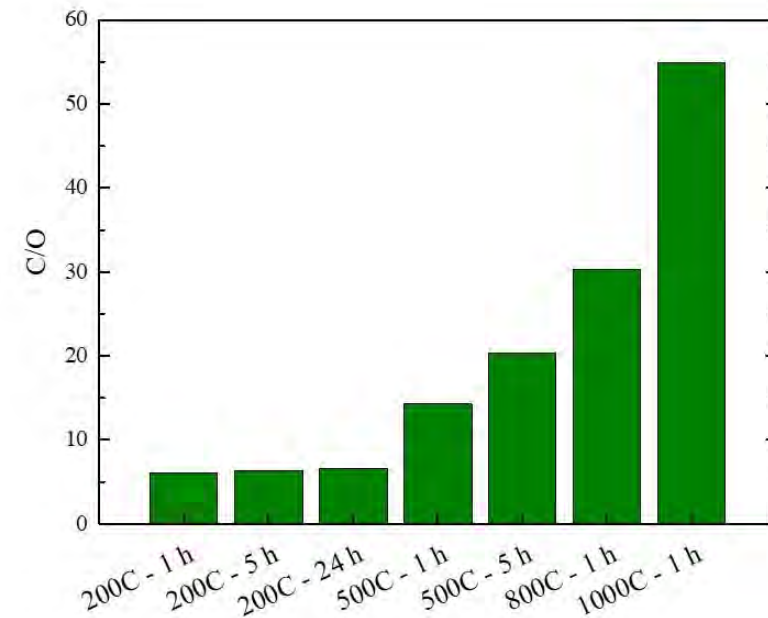
MWCNTs for CCS

- Oxidation of NC7000 in batch CNT synthesis unit by air/N₂ mixtures.
- Effect of temperature, oxidation time, air concentration, gas Flow rate, CNT mass.
- Use of statistical tool: design of experiments.
- Characterization and analysis of results.



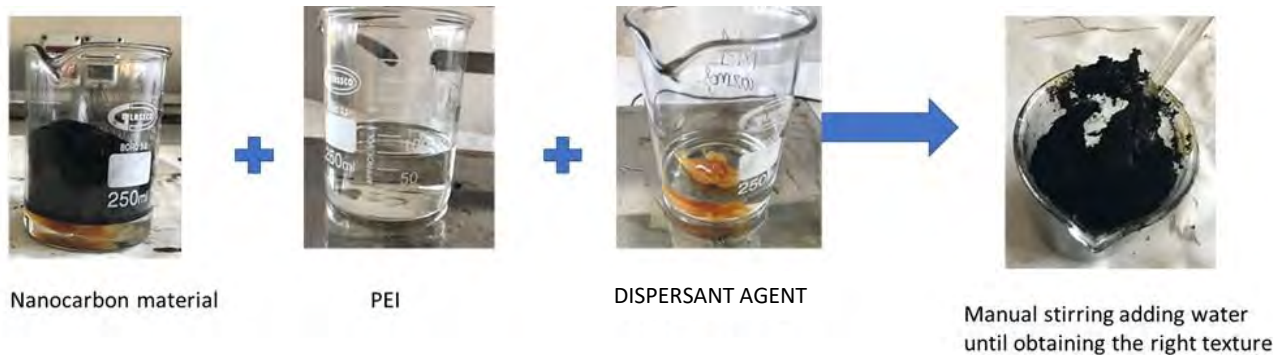
rGOs for CCS

Preparation of rGO with different C/O ratios.

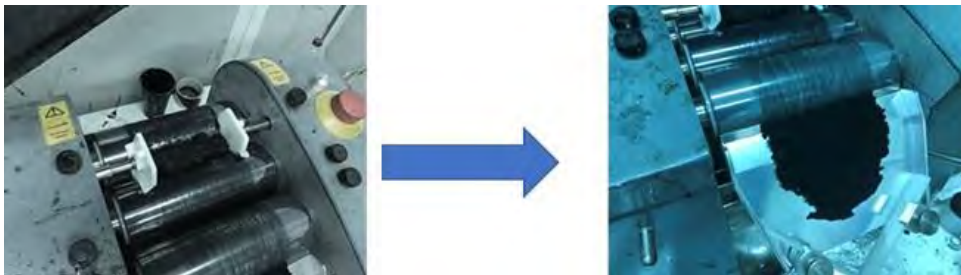


Pastes Preparation (Mixing Process)

STEP 1



STEP 2

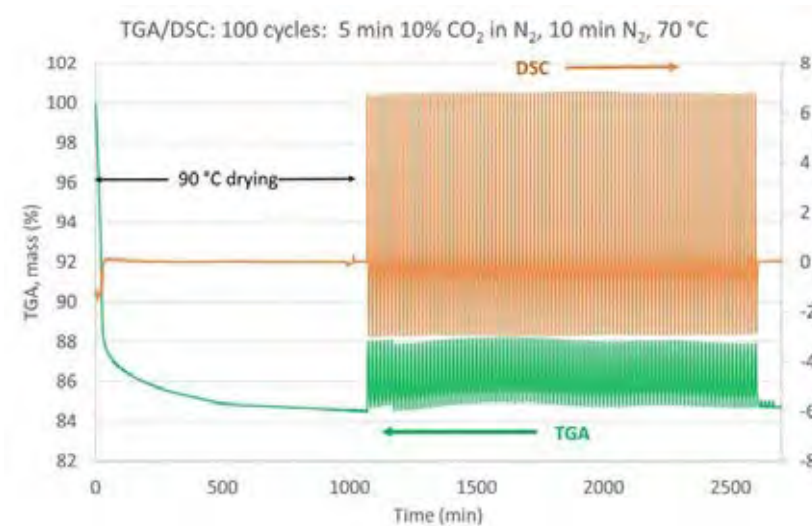
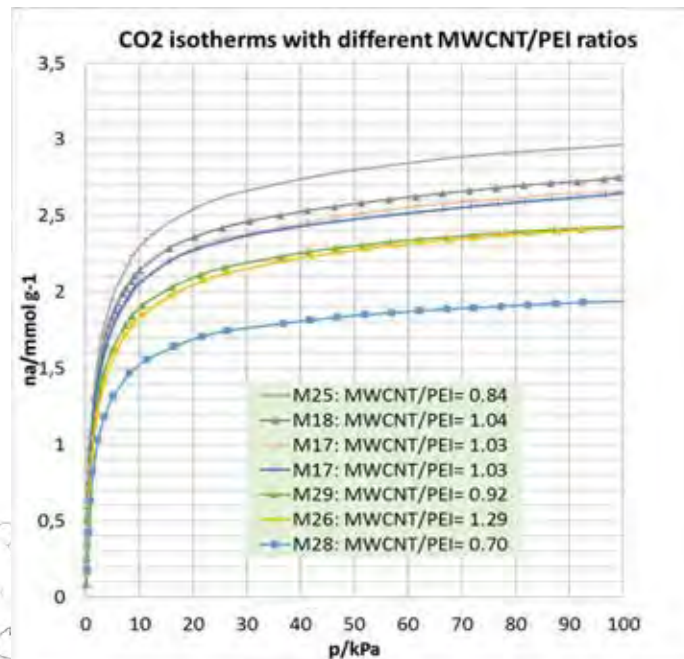


MAIN ISSUES:

- CO₂ adsorption values of the material and then after monolith 3D printing process.
- Suitable viscosity for 3D printing.
- To avoid water segregation.
- To control shrinkage through a strong optimization work.
- Homogeneous heating by thermoelectric effect (Joule Effect).

Pastes Preparation (Mixing Process)

Until now best samples are MWCNT/PEI pastes, instead of 3 component. Combinations with rGO are giving promising results.



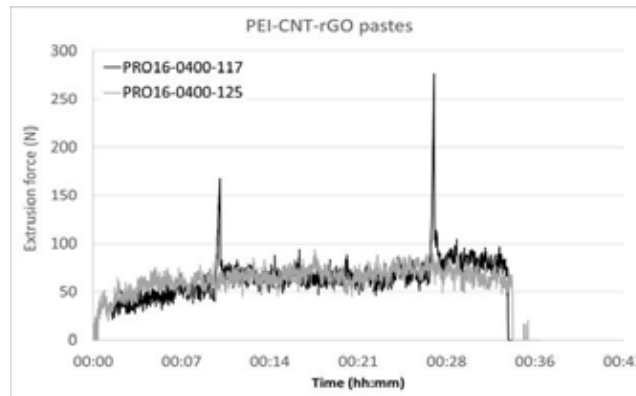
High selectivity to CO₂ over other gases as well as stable performance over high number of sorption/desorption cycles.

For the MWCNT/PEI composite, MWCNT may act in two ways:

- facilitating the diffusion of CO₂ into the sorbent structure by diffusion through or along its surface, and
- As spacer, avoiding thick aggregates of PEI leading to long diffusion paths through polymeric medium to reach sorption sites.

3D Printing (monoliths)

Optimization work related to avoid unstable Flow, phase segregation, bad cohesion of the paste and inhomogeneous shrinkage.



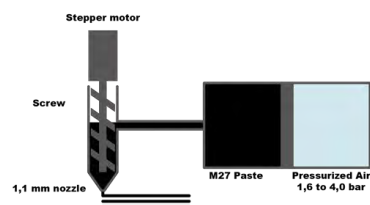
Improvements have been observed with different linkers and dispersing agents. Drop in sorption but to a lesser extent.



3D Printing (scale-up)



Delta 2040



Delta 3MT



Delta 40100



Printing volume

1000 mm

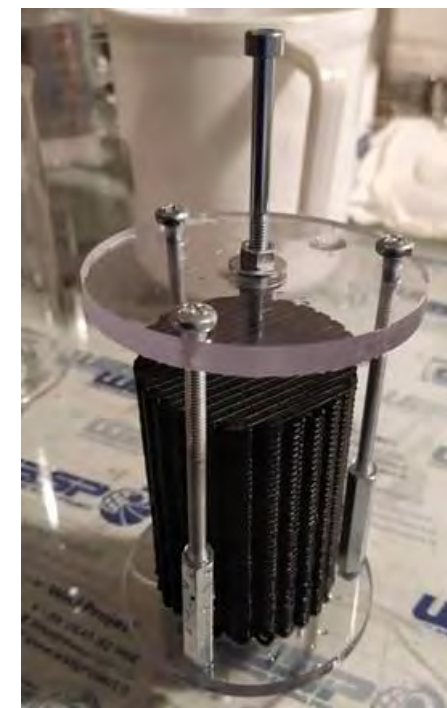


1000 mm

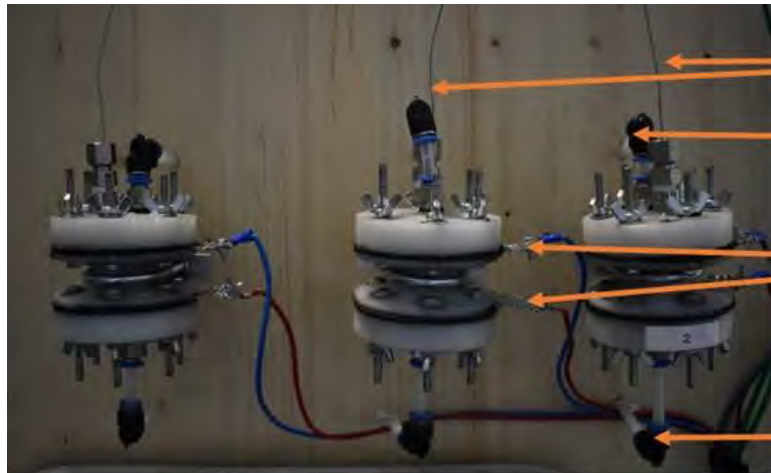
400 mm



1000 mm



VTSA Benchmark. Joule Effect and sensing process.

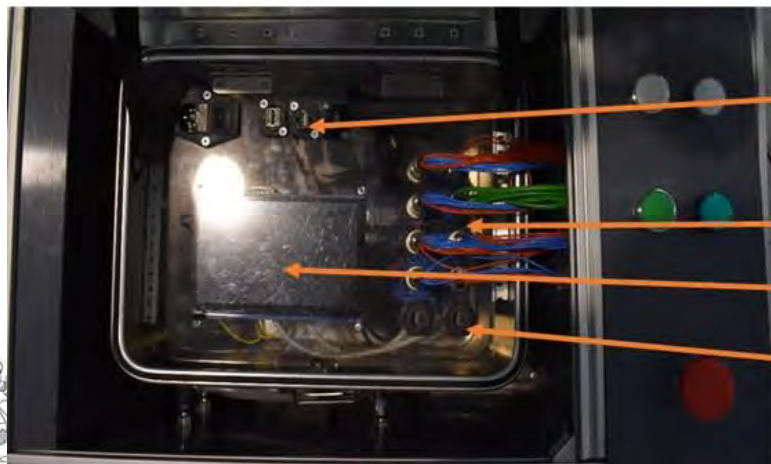


Temperature sensor

Output gas

Electrodes

Input gas



Second screen connector and usb connector

Electro-valves and sensor connector

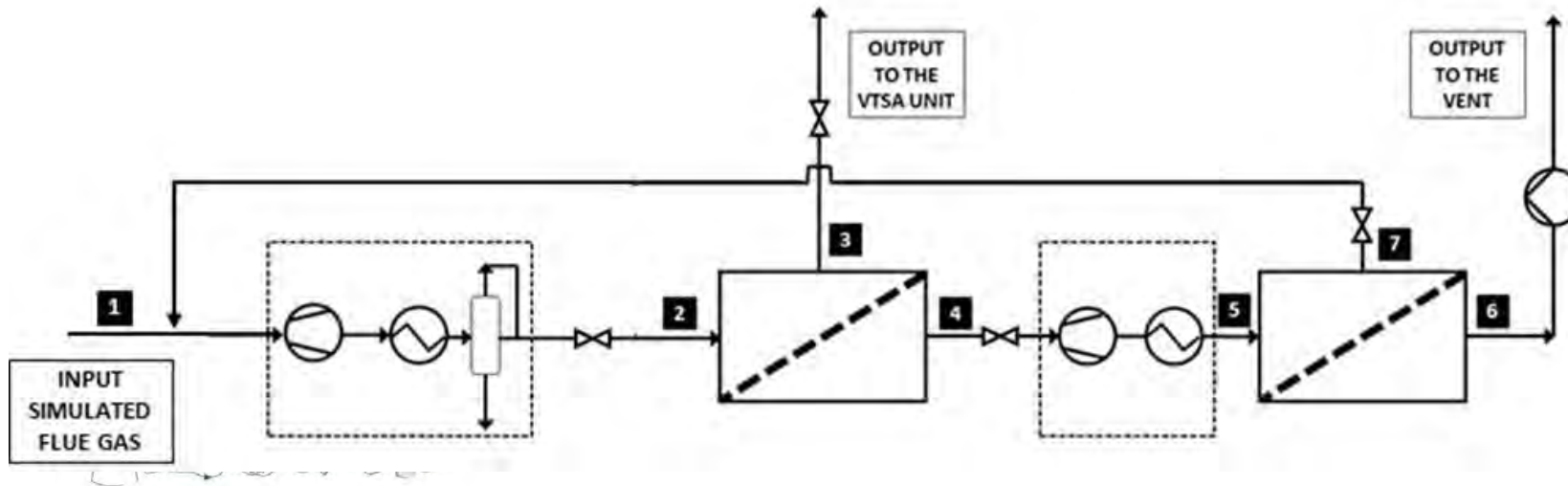
Direct screen controller

Ethernet connector + Wifi



Evaluation of the separation performance of the membrane unit

- Investigation of the effect of **recycling the retentate output of the 2nd membrane module into the gas feed** introduced into the membrane cascade by conducting experimental runs using two commercial membrane modules in series and a dry mixture of 15.6 v/v% CO₂ – 84.4 v/v% N₂ as a feed.



The two-stage membrane section has been tested successfully according to work programme using polyimide commercial membranes



Thank you



*This project has received funding from the European Union's Horizon 2020 research and innovation programme under grant agreement No 760884.
This publication reflects only the author's view and that the Commission is not responsible for any use that may be made of the information it contains.*

Introduction to the COZMOS project

Richard H. Heyn, COZMOS Dissemination and Communication Manager
SINTEF Industry, Oslo, Norway



COZMOS - Efficient CO₂ conversion over multisite Zeolite-Metal nanocatalysts to fuels and Olefins

- Four year project (01.05.2019 – 30.04.2023)
- Coordinator: Prof. Unni Olsbye, University of Oslo



- Industry partners



- RTO partners



- Foreign partners



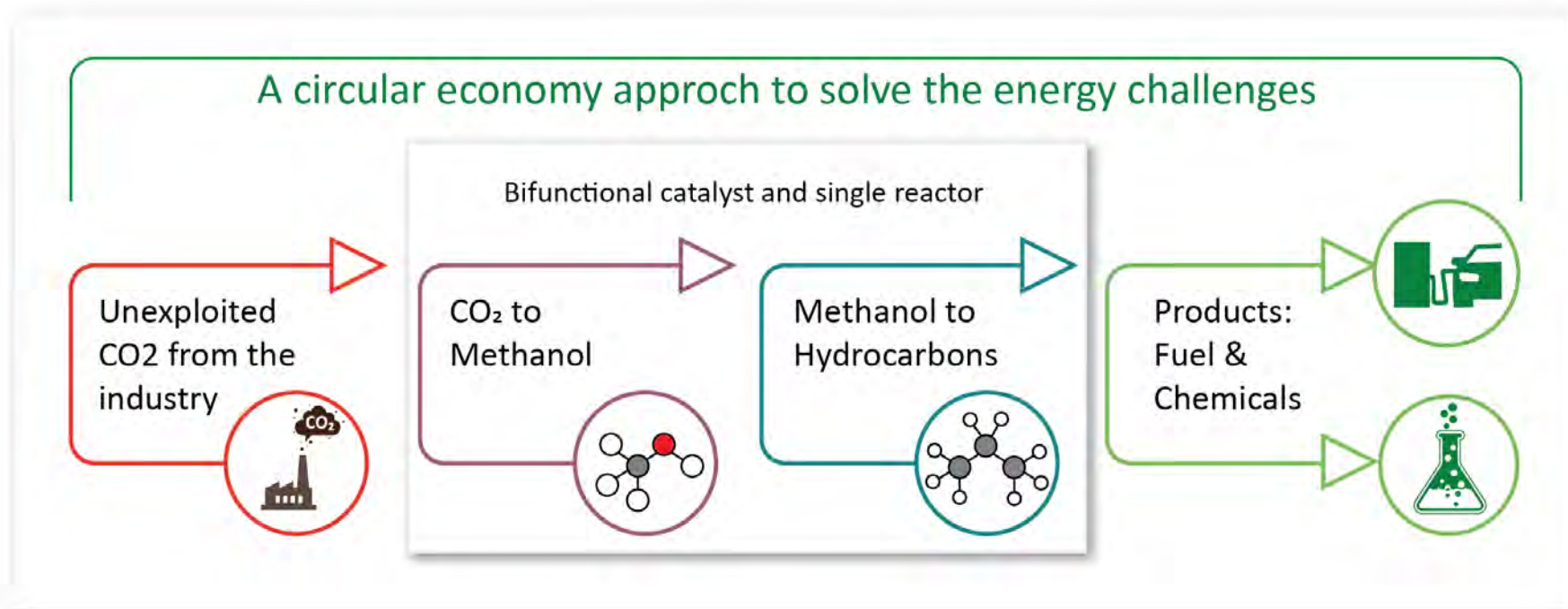
Institute for Coal
Chemistry (ICC) - China



King Abdullah University of
Science and Technology
(KAUST) – Saudi Arabia



CO2MOS in a nutshell



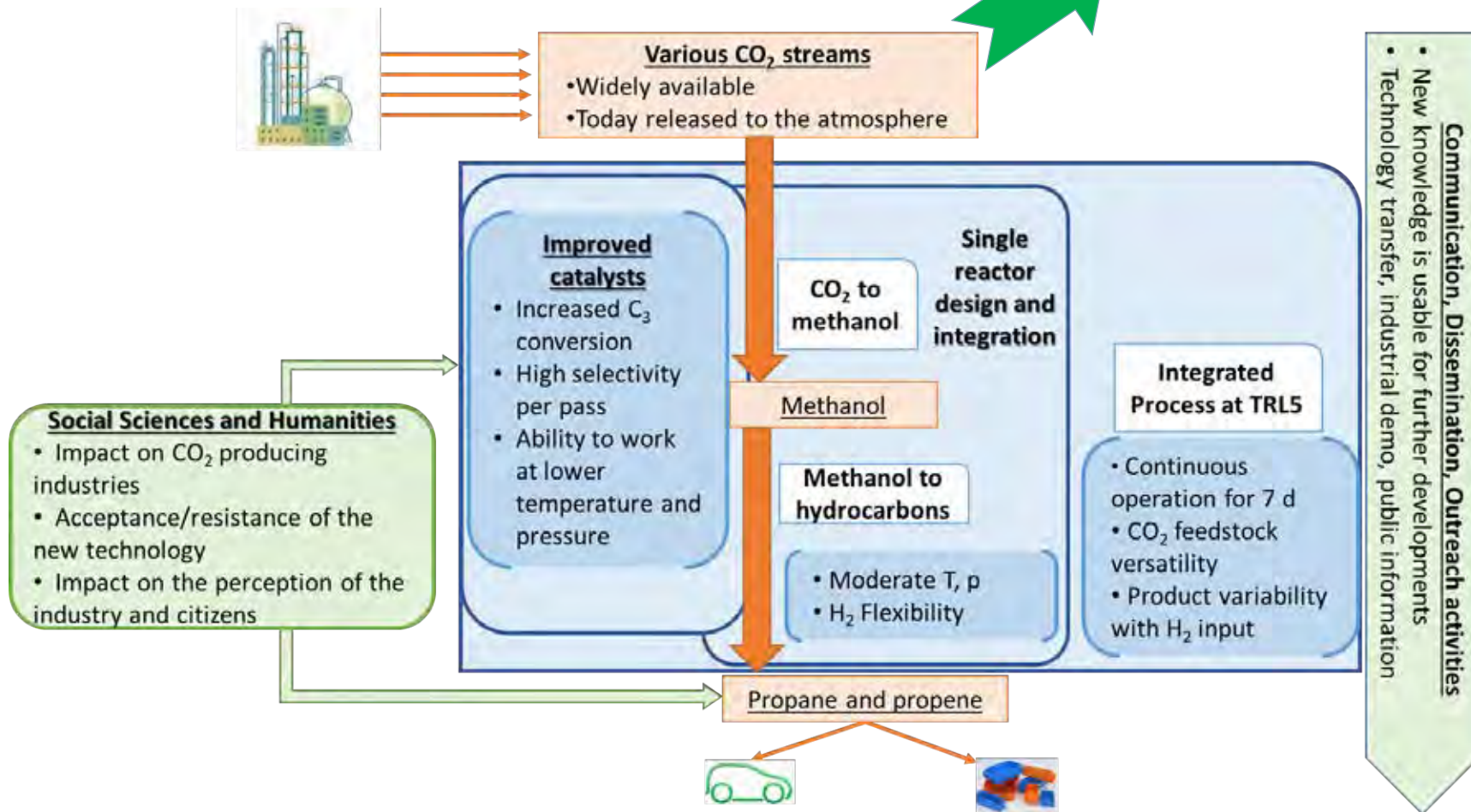
COZMOS Work Packages

- WP1 – Optimization of catalysts (and process conditions) for cascade reactions
 - Partners: **Univ. Oslo**, Haldor-Topsoe, CNRS, SINTEF, Univ. Torino, ICC, KAUST
- WP2 – Process design and optimization
 - Partners: **Linde**, Haldor-Topsoe, Tata Steel, Tüpraş
- WP3 – Demonstration (TRL5)
 - Partners: **Tüpraş**, Univ. Torino, Tata Steel, Linde, Haldor-Topsoe
- WP4 – LCA, TEA and social aspects
 - Partners: **Tata Steel**, Univ. Sheffield, Tüpraş
- WP5 – Communication, dissemination, outreach and exploitation
 - Partners: **SINTEF**, Tata Steel, Linde, Univ. Sheffield
- WP6 – Ethics
- WP7 – Management



Project overview

CO₂ emissions
from two sectors:
Steel and refining



Project Objectives and Innovations

- Development of an energy efficient, economically viable, environmentally friendly and socially acceptable process
- Development, optimization and upscaling of a combined catalyst for hydrogenation of CO₂ to C₃ products
- Determination of optimal process conditions, *i.e.*, optimal heat and pressure management with minimal separation
- Overall integration and validation in a relevant environment (TRL 5)
- Innovation 1: Tailor-made bifunctional catalysts for maximizing the yield, working at low temperature and pressure for both steps, with feeds with various compositions
- Innovation 2: Single reactor and optimized global process design for operation under conditions that are optimal from an energetic and techno-economic perspective, with efficient heat and pressure management, minimized separation and optimized recycling



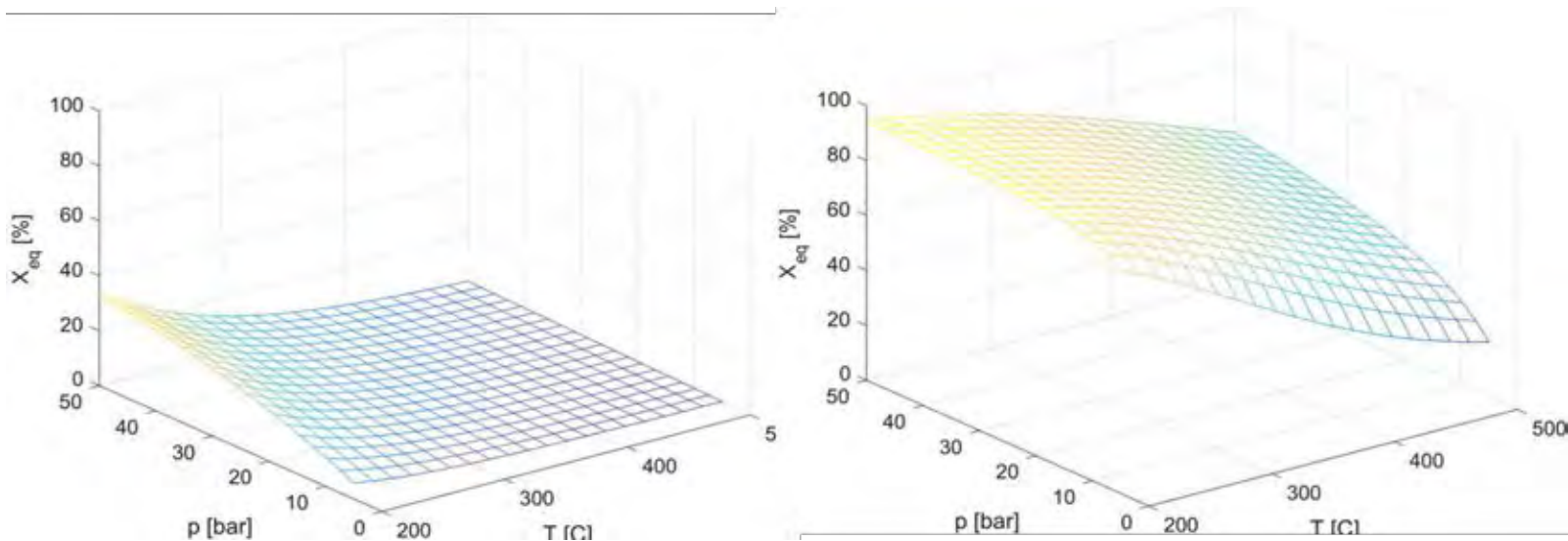
Impact

- Decrease in CO₂ emissions by 1.9 t_{CO2} / t_{C3 product}
 - DECHEMA Gesellschaft für Chemische Technik und Biotechnologie e.V., *Low carbon energy and feedstock for the European chemical industry*, 2017
- Convert 0.4 Mt CO₂/yr in 2030, 2.2 Mt CO₂/yr from 2034
- Flexible solutions for local requirements and different industries.
- Key aspect is availability of H₂
 - Must be made from renewable energies with no (appreciable) carbon footprint
- Scenario 1 – Lots of renewable energy and CO₂, but remotely located
 - Utilize excess renewable energy and make propane, which is a transportable energy vector (heating, cooking, transport)
- Scenario 2 – Limited renewable energy/high demand for H₂, located within established process industry infrastructure
 - Synthesize propene for use within the chemical industry



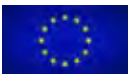
Thermodynamics – Le Chatelier is our friend

- All CO₂ chemistry has thermodynamic limitations
 - Hydrogenation of CO₂ to MeOH included
- If a second reaction converting MeOH is combined with CO₂ hydrogenation, CO₂ conversion should increase

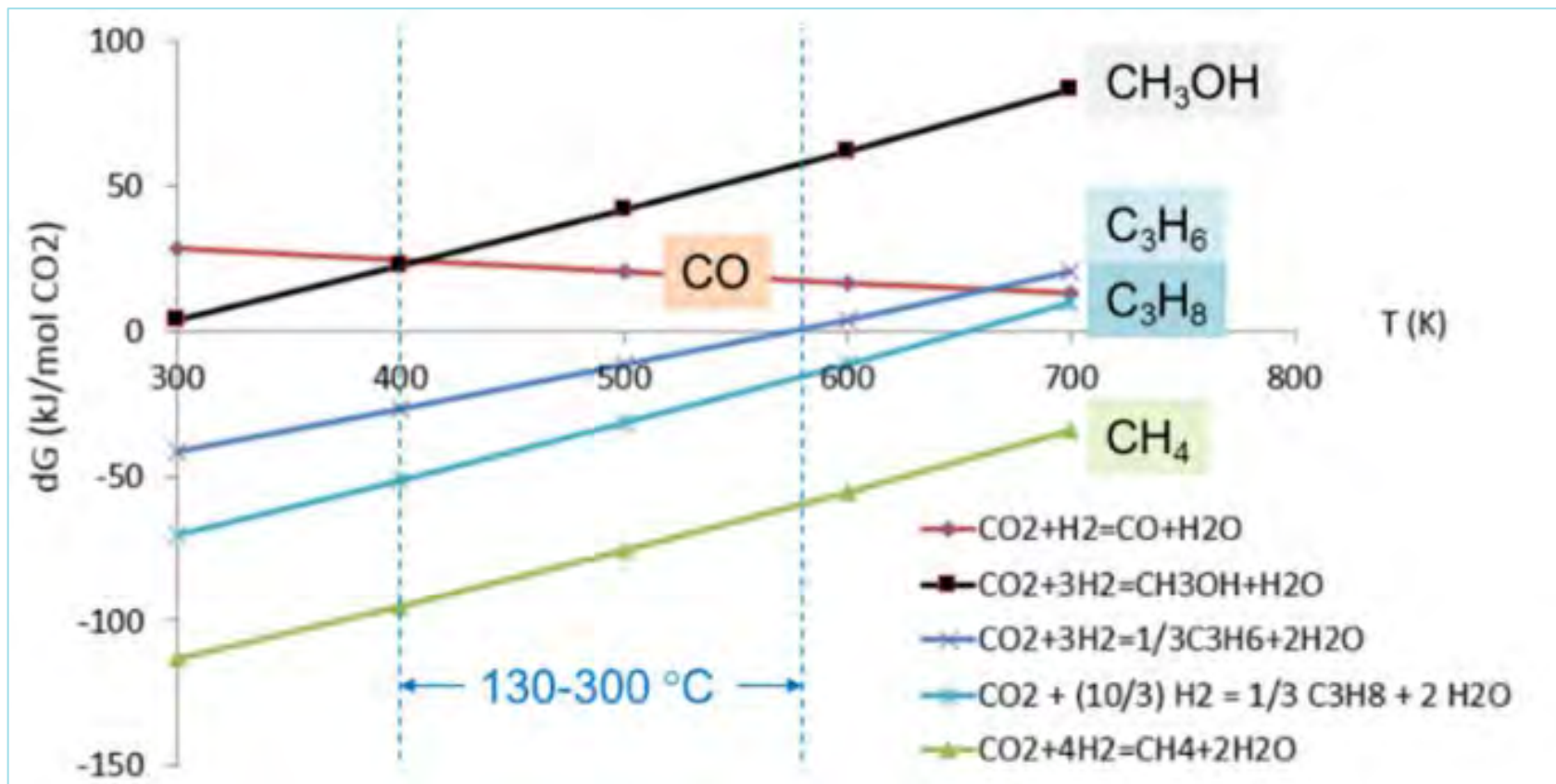


Maximum achievable per-pass (equilibrium) conversion of CO₂ to C₃ products

Left: Conventional two-reactor system. Right: CO2MOS one-reactor process



Thermodynamics is our favor



Gibbs free energy vs. Temperature for CO_2 hydrogenation reactions

- Hydrogenation of CO_2 to C_3 products is thermodynamically favorable in a readily accessible temperature/pressure window



Publications thus far

- On the conversion of CO₂ to value added products over composite PdZn and H-ZSM-5 catalysts: excess Zn over Pd, a compromise or a penalty?
 - From Univ. Oslo, Univ. Torino, CNRS
 - *Catal. Sci. Technol.* **2020**, 10, 4373-4385
- A toroidal Zr70 oxysulfate cluster and its diverse packing structures
 - From Univ. Oslo
 - *Angew. Chem. Int. Ed* **2020**, 48, 21397–21402
- Selective Conversion of CO₂ into Propene and Butene
 - From ICC and Univ. Oslo
 - *Chem* **2020**, 6, 3344-3363
- CO₂ hydrogenation to methanol and hydrocarbons over bifunctional Zn-doped ZrO₂/Zeolite catalysts
 - From Univ. Torino, KAUST, Univ. Oslo
 - Accepted, *Catal. Sci. Technol.*
- Analytical Review of Life-Cycle Environmental Impacts of Carbon Capture and Utilization Technologies
 - From Univ. Sheffield, TATA Steel
 - Accepted, *ChemSusChem*



Conclusions

- The COZMOS project aims to combine two catalytic processes into a single catalyst and process for the conversion of CO₂ into C₃ hydrocarbons
- The goal is to exploit Le Chatelier's principle to drive equilibrium-limited CO₂ conversions to higher, industrially relevant levels.
- The conversion of CO₂ to C₃ products is thermodynamically accessible in an industrially relevant temperature window.
- Important to optimize process conditions to minimize recycle and energy requirements
- Vision is a flexible process that can vary the C₃ product to fit the needs and limitations of different locations.





CONVERGE technology for efficient methanol production: Energy and Environmental analysis

Petrescu Letitia



Objectives

- » Green methanol for biofuel production using waste feedstock as raw-material



- » The waste feedstock (from 4 different regions) will be characterized and used in process modeling and simulation tasks; its supply chain will represent important data for LCA
- » The optimum economic layout will be identified for CONVERGE technology
- » LCA will compare the environmental impacts of CONVERGE to other green methanol production processes
- » Evaluation of social impact

CONVERGE concept

» Combines five innovative processes

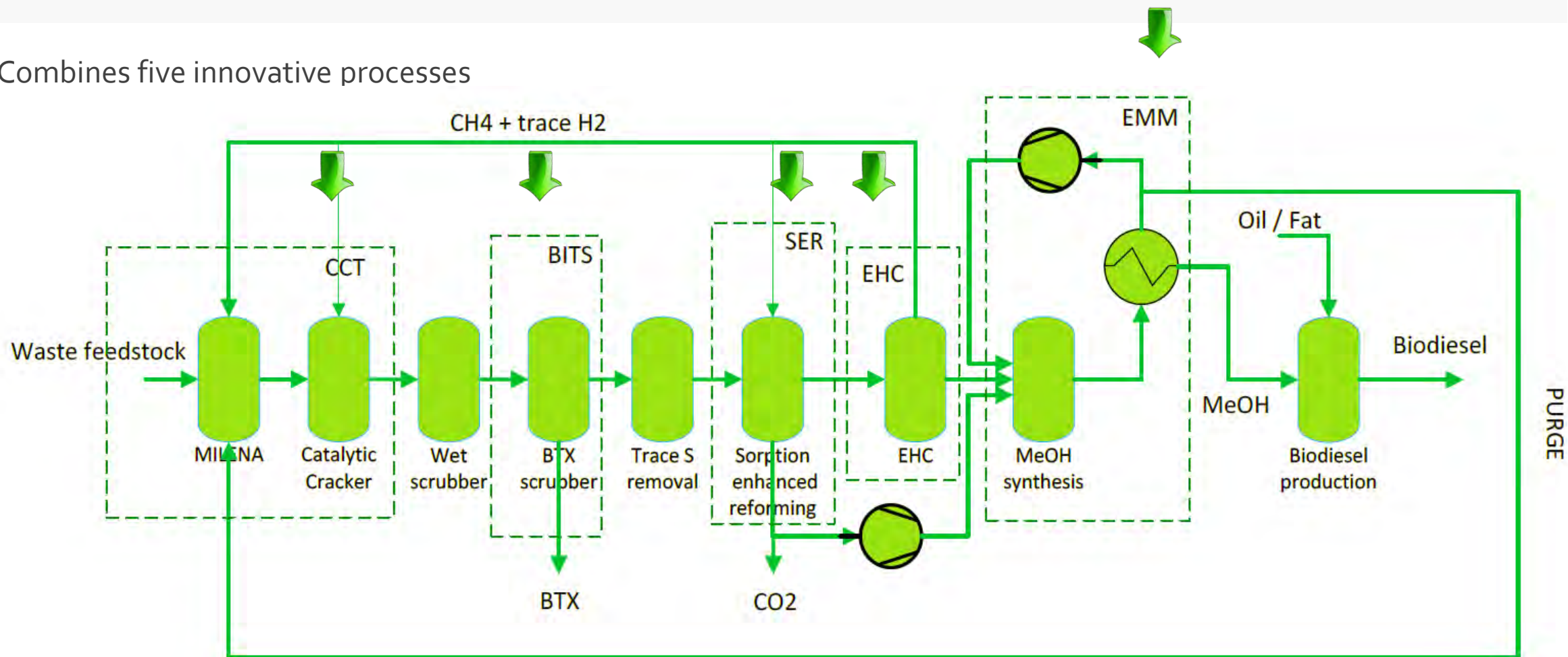


Figure 1. CONVERGE process flowsheet

CONVERGE main units

| CCT | BITS | SER | EHC | EMM |
|---|---|--|---|--|
| <p>» Catalytic cracking of tars from an indirectly heated gasifier to below green C8</p> <p>» Advantage:</p> <ul style="list-style-type: none"> Removes the separation of high molecular weight tars from downstream processes, also allowing other by-product fuels, i.e. CH₄ and methanol purge to fire the gasification and SER units | <p>» Recovery of refinery products including aromatics for green C6-C8 fraction (BTX)</p> <p>» Advantage:</p> <ul style="list-style-type: none"> Avoid the need to pressurize all the producer gas to perform hydrodesulphurization (HDS), and create an extra revenue stream that will also receive positive price pressure in a future carbon-constrained world | <p>» Sorption-Enhanced Reforming of C₁-C₆ for excess-carbon removal, and H₂ production</p> <p>» Advantage:</p> <ul style="list-style-type: none"> Lowers the temperature at which reforming is performed, and produces a CO₂ stream that only partially needs to be compressed for methanol production | <p>» Highly efficient electrochemical compression of green H₂ with by-product fuel</p> <p>» Advantage:</p> <ul style="list-style-type: none"> Elimination of mechanical compression costs for H₂ compression. In combination with SER and EMM compression costs are driven to an absolute minimum | <p>» Enhanced Methanol Membrane to ensure efficient green biodiesel production</p> <p>» Advantage:</p> <ul style="list-style-type: none"> Due to in situ separation of inhibition products the catalyst for methanol production operates more efficiently as the composition remains further away from equilibrium |

CONVERGE - Advantages

Technical

- » \searrow 30% of energy losses related to biodiesel production \rightarrow \nearrow 12% in production;
- » **Syngas treatment:** \nearrow 5% in C/H₂ purity \rightarrow \nearrow 17% overall carbon usage;
- » **SER:** reduce the H₂ production and CO₂ separation from 2 MJ/kgCO₂ down to 1.2 MJ/kgCO₂;
- » **EHC:** reduce the purification and compression work from 16 MJ/kgH₂ down to 12 MJ/kgH₂;
- » **Enhanced Membrane Methanol synthesis:** single pass conversion >33% \rightarrow size reduction of the methanol reactor;

Economic

- » 15% \searrow of CAPEX for the overall process;
- » 10% \searrow of OPEX;

Environmental

- » Reduction of CO₂ emissions by 0.2 kgCO₂/kgMeOH as consequence of higher production efficiency;
- » Reduce the biomass transportation costs as consequence of the process flexibility and supply chain evaluations for 4 distinct geographical regions;

WP5 - Details

WP objectives

- Definition of the Base Case (BC) and CONVERGE Case



Steps to reach the objectives

- Identification of possible raw-materials for BC and CONVERGE Case
- Identification of the main blocks for BC and CONVERGE Case
- Identification of the best operating conditions of various sub-units
- Construction of BC and CONVERGE Case process flow-diagram



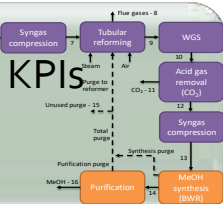
Tools to reach the objective

- Process flow-modelling tools (i.e. Aspen Plus)
- Validation of the models
- Discussions, side-meetings, e-mails, skype calls



Results obtained

- Detailed mass & heat balances for BC and CONVERGE Case
- Plants economics (e.g. levelized cost of fuel)



WP 5 Objectives



Energy efficiency



Costs



Environmental impact



Social Impact

Comparison between state-of-the-art and CONVERGE technologies

Technical analysis

Base case

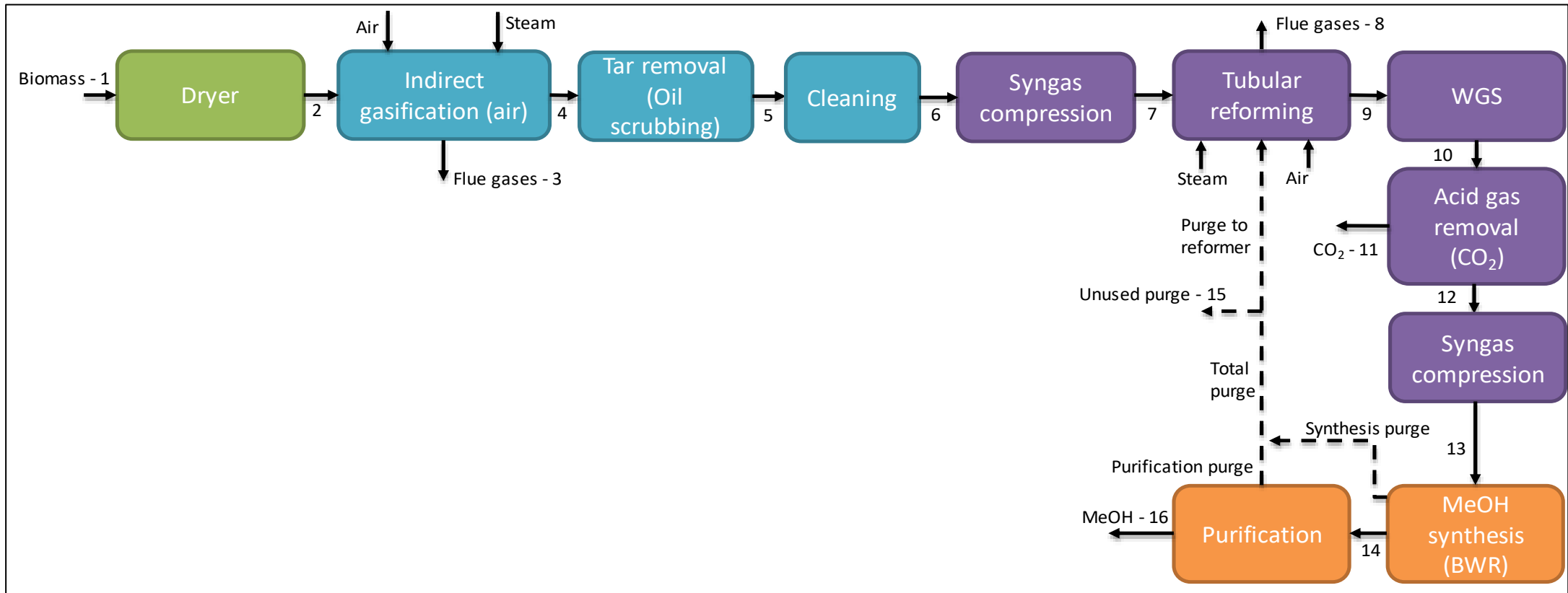


Figure 2. Simplified process flow-sheet of the Base Case

Technical analysis – Case studies

CONVERGE Case

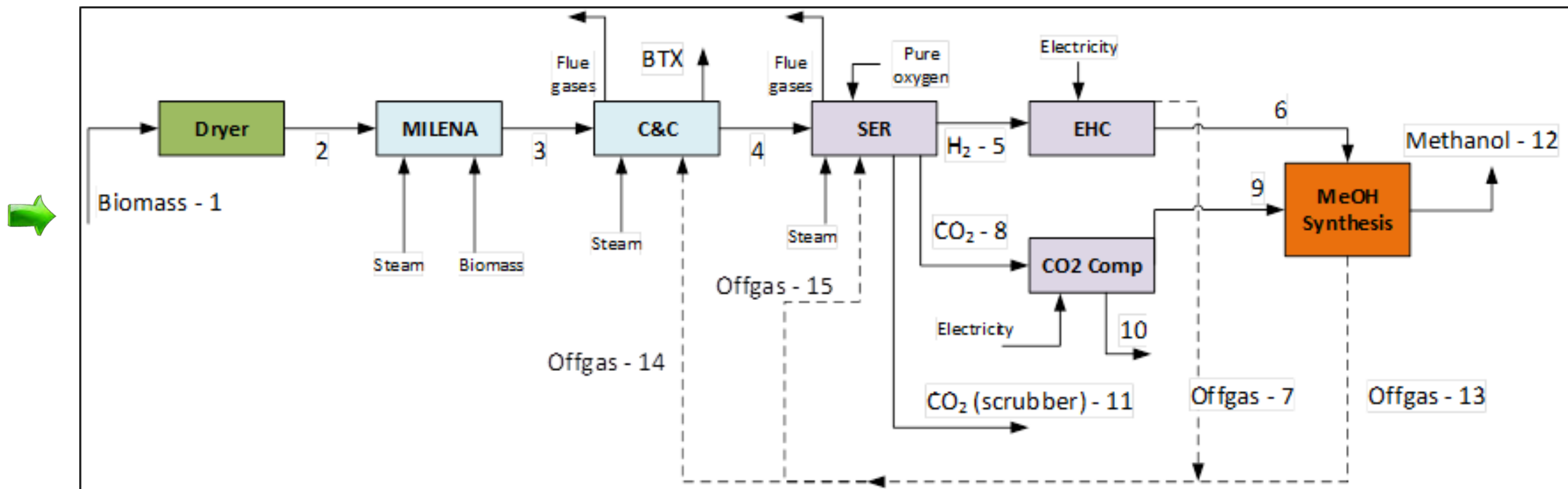


Figure 3. Simplified process flow-sheet of the CONVERGE Case

Technical analysis

Table 1. Case studies comparison

| PROCESS | BASE CASE (BC) | CONVERGE CASE |
|---|---|---|
| Biomass drying | Tube bundle drier | Tube bundle drier |
| Biomass conversion (Syngas production) | Indirect gasification (MILENA) Atmospheric pressure Air and steam | Indirect gasification (MILENA) Atmospheric pressure Air and steam |
| Tar removal | Oil scrubbing (OLGA) | Catalytic Cracking |
| Syngas cleaning and conditioning | Water scrubbing | Water scrubbing |
| | Compression up to 22 bar | - |
| | Tubular reforming | - |
| | WGS bypassed | - |
| | Acid gas removal - MDEA | SER+CO ₂ compression (up to 80 bar) |
| Methanol synthesis | Boiling water reactor | Membrane reactor |
| Methanol purification | Stripping of light gasses and water separation | Stripping of light gasses and water separation |

Technical analysis

Table 2. Examples of possible biomass

| | Forest residues | Cereal straw | Residual lignin |
|-----------------|-----------------|--------------|-----------------|
| C | 50.71 | 48.12 | 57.80 |
| H | 6.08 | 6.57 | 6.20 |
| O | 42.84 | 48.18 | 33.83 |
| N | 0.38 | 0.45 | 0.80 |
| S | 0.06 | 0.07 | 0.13 |
| Cl | 0.09 | 0.30 | 0.00 |
| Fixed C | 17.93 | 21.02 | 27.80 |
| Volatile matter | 82.07 | 78.98 | 72.20 |
| Ash | 1.00 | 6.70 | 0.10 |
| Moisture | 35.00 | 7.80 | 52.00 |
| LHV [MJ/kg] | 11.55 | 15.37 | 11.01 |

Table 3. Global plant performance

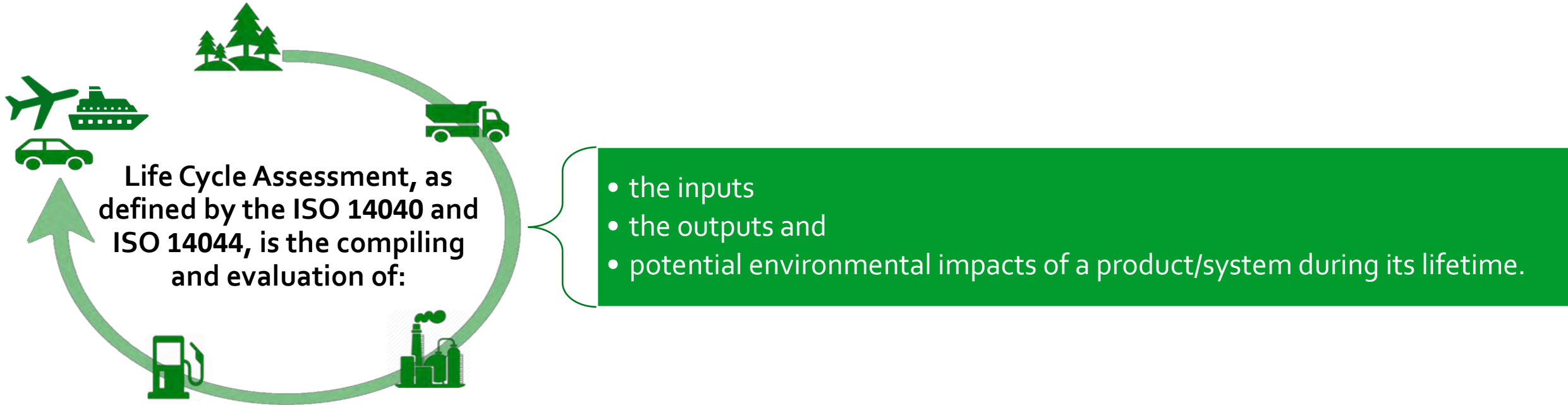
| CGE section | | Base Case | CONVERGE | CONVERGE Optimized |
|--------------------------------|----------|-----------|----------|--------------------|
| Global (methanol) | | 58.59% | 42.55% | 49.43% |
| Global (methanol +BTX) | | - | 51.45% | 58.75% |
| MILENA | Gasifier | 82.73% | 84.41% | 84.43% |
| Cleaning | | 99.79% | 97.89% | 94.96% |
| Reformer | SER | 104.79% | 88.34% | 94.27% |
| WGS+CO ₂ separation | | 99.98% | - | - |
| Methanol synthesis | | 68.36% | 82.64% | 81.72% |
| Methanol purification | | 97.84% | | |

Technical and economic analysis for BC

Table 4. Case studies comparison

| Technical KPI | | BASE CASE (BC) | | |
|---------------------------|-------|----------------------|-----------------------|-----------------------|
| Plant capacity | | 10 MW _{LHV} | 100 MW _{LHV} | 300 MW _{LHV} |
| MeOH production | ton/d | 25.1 | 251 | 753 |
| CO ₂ separated | ton/d | 27.7 | 277 | 831 |
| CGE global | % | | 58.6 | |
| Costs | | BASE CASE (BC) | | |
| Total Capital Investment | M€ | 39.1 | 206 | 424 |
| | M€/y | 7.09 | 43.8 | 101.6 |
| Total yearly cost | €/ton | 1010 | 525 | 406 |
| LCOF | €/MWh | 183 | 95 | 73 |

Environmental analysis



» Life Cycle Assessment Steps



Goal and scope definition



Life cycle inventory



Life cycle impact assessment



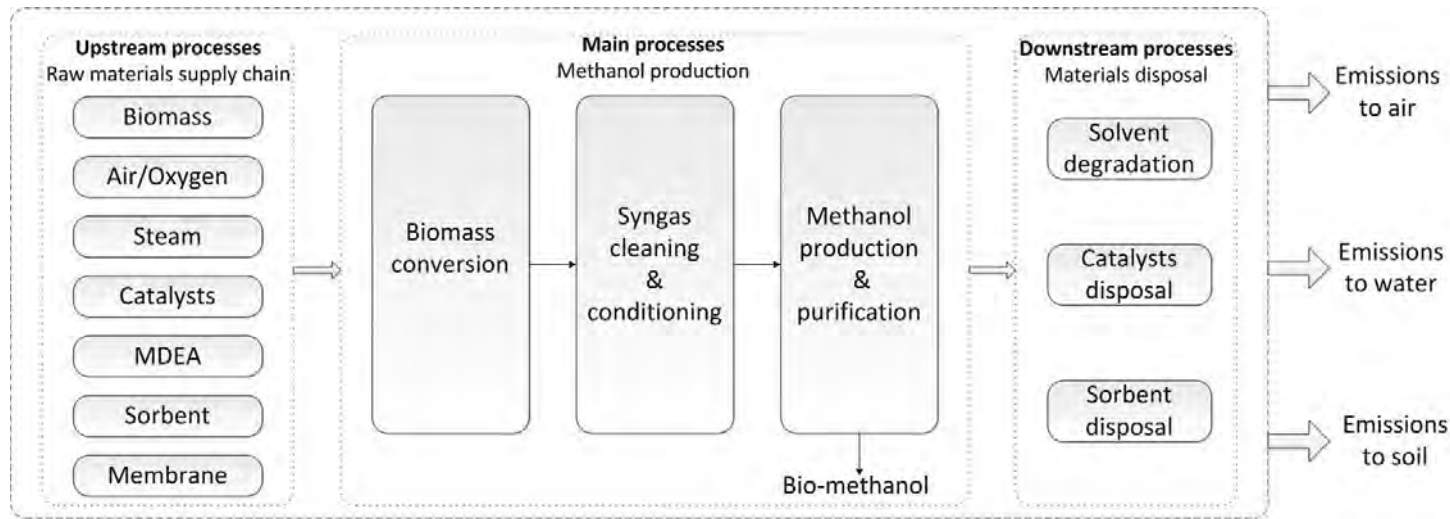
Interpretation

Environmental analysis



Goal and scope definition

- » **Goal:** Evaluate and compare the environmental burden of bio-methanol production proposed in the CONVERGE technology with other technologies for bio-methanol production.
- » **Scope:**
 - boundary conditions

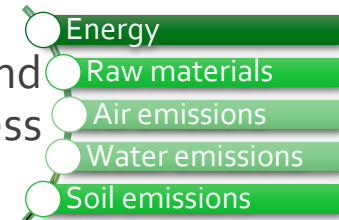


- functional unit - one tone of MeOH
- plant lifetime - 20 years
- plant location - Europe: Sweden

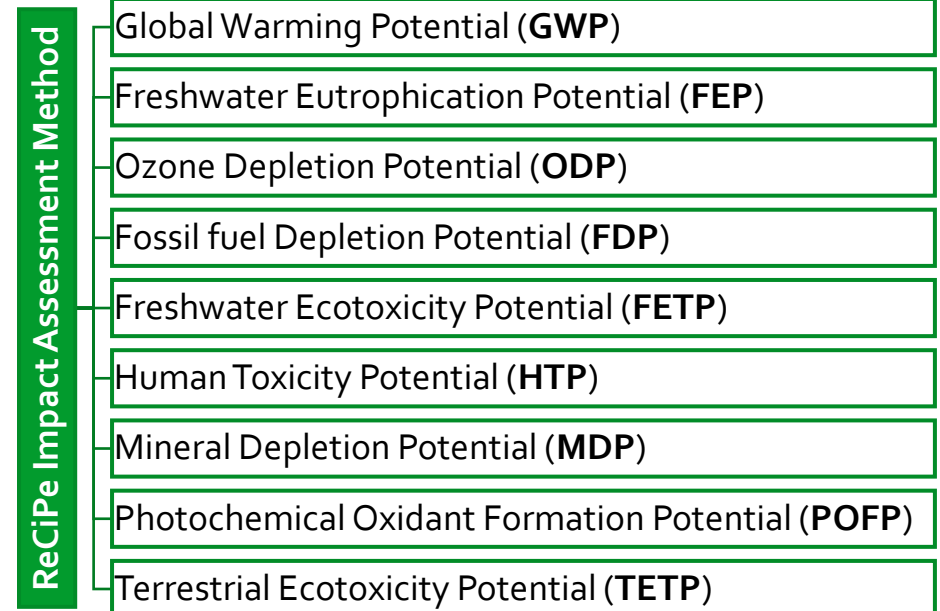


Life cycle inventory

- » Quantification of inputs and outputs for a product/process throughout its life cycle



Life cycle impact assessment



Environmental analysis



Interpretation

Table 5. LCA Results

| | KPI | Units | Base Case | CONVERGE |
|---|-----------------------|-------------------------------|-----------|----------|
| | GWP | kg CO ₂ eq./ tMeOH | 1305.4 | 1470.47 |
| ➡ | ODP*10 ⁹ | kg CFC-11 eq./ tMeOH | 5.85 | 4.89 |
| | FDP | kg oil eq./ tMeOH | 6.15 | 8.35 |
| ➡ | FETP | kg 1,4-DB eq./ tMeOH | 0.51 | 0.19 |
| ➡ | HTP | kg 1,4-DB eq./ tMeOH | 36.69 | 7.06 |
| | MDP | kg Fe eq./ tMeOH | 2.51 | 2.81 |
| ➡ | POFP | kg NMVOC/ tMeOH | 0.15 | 0.149 |
| ➡ | TETP *10 ³ | kg 1,4-DB eq./ tMeOH | 9.18 | 4.61 |

Concluding remarks

- » Different types of biomass are/will be considered in the CONVERGE project for biomass transformation into bio-methanol
- » The attention was focused on forest residues biomass
- » Cereal straw and residual lignin will be considered in future evaluations
- » Calculation of technical KPIs for CONVERGE concept have been performed
- » Economic analysis is an on-going task
- » Environmental impact was evaluated for the main process (base case and CONVERGE concept) but upstream and downstream processes should be included in the analysis (on-going task)

Thank you for your attention!

Acknowledgements



The CONVERGE project has received funding from the European Union's Horizon 2020 research and innovation programme under grant agreement N° 818135



letitia.petrescu@ubbcluj.ro

INTERNATIONAL WORKSHOP ON CO₂ CAPTURE AND UTILIZATION

TU/e - EINDHOVEN - 16-17 FEBRUARY 2021

Opening & Plenary Sessions (chairperson Fernanda Neira D'Angelo)

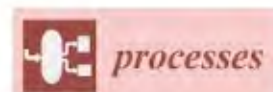
9:30-10:00 All coordinators - Introduction to projects

10:00-11:00 Dr. K. Bakke - Northern Lights – concept, plans and future

ORGANIZED BY



SPONSORED BY



Northern Lights

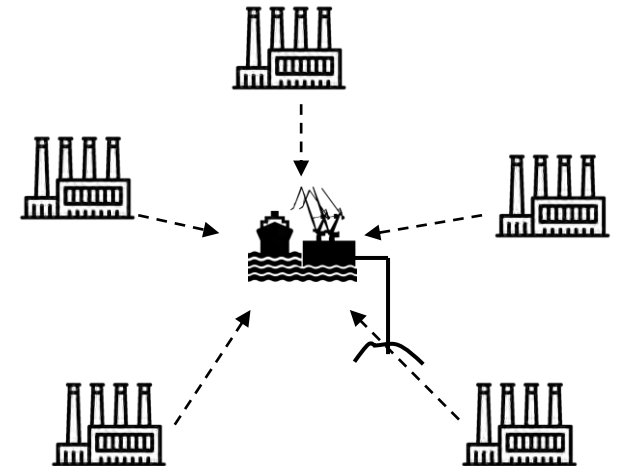
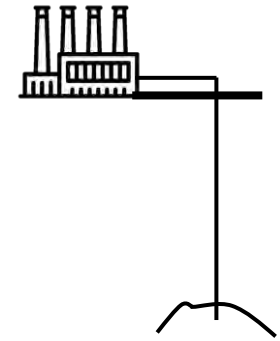
A European CO₂ transport and storage network

<https://northernlightscs.eu/>



Agenda

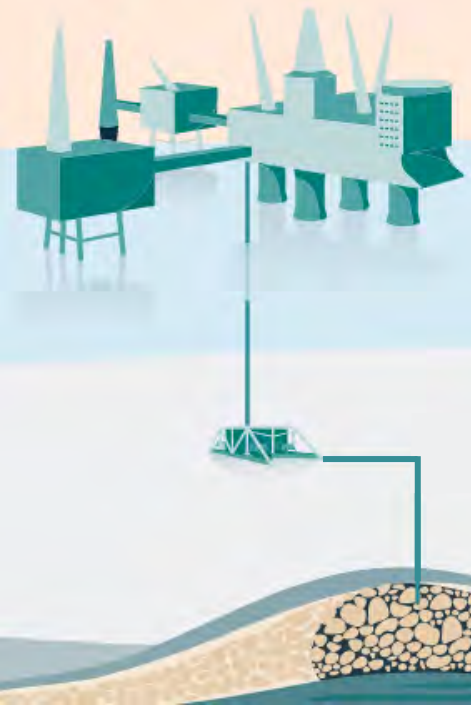
- Introduction
- Separating source and sink
- Longship
- What is Northern Lights?
- Storage experience
- Is there a business opportunity?
- Some challenges
- Summary
- Q&A



Separating source and sink

SEPARATING SOURCE AND SINK

Traditional model



SEPARATING SOURCE AND SINK

Traditional model

Northern Lights





Longship

01.03.2021

NORTHERN LIGHTS

CO₂ Capture

Capture from industrial plants

Compressed and temporarily stored

Liquid CO₂

Transport

Compressed CO₂ transported by ship

Liquid CO₂

Injection and storage

CO₂ received and temporarily stored

Exported via pipeline offshore

Injection in formation from 2300 – 2500 meters below seabed



Longship in summary

- Norcem facilities with start-up in 2024
- Partial funding of Fortum Oslo varme (FOV)
 - A FID must be made by FOV within three months of EU Innovation fund announcing awards in the second round, but no later than 31. December 2024
- Northern Lights
 - Facility scope with 1,5 mtpa capacity
 - 2 ships

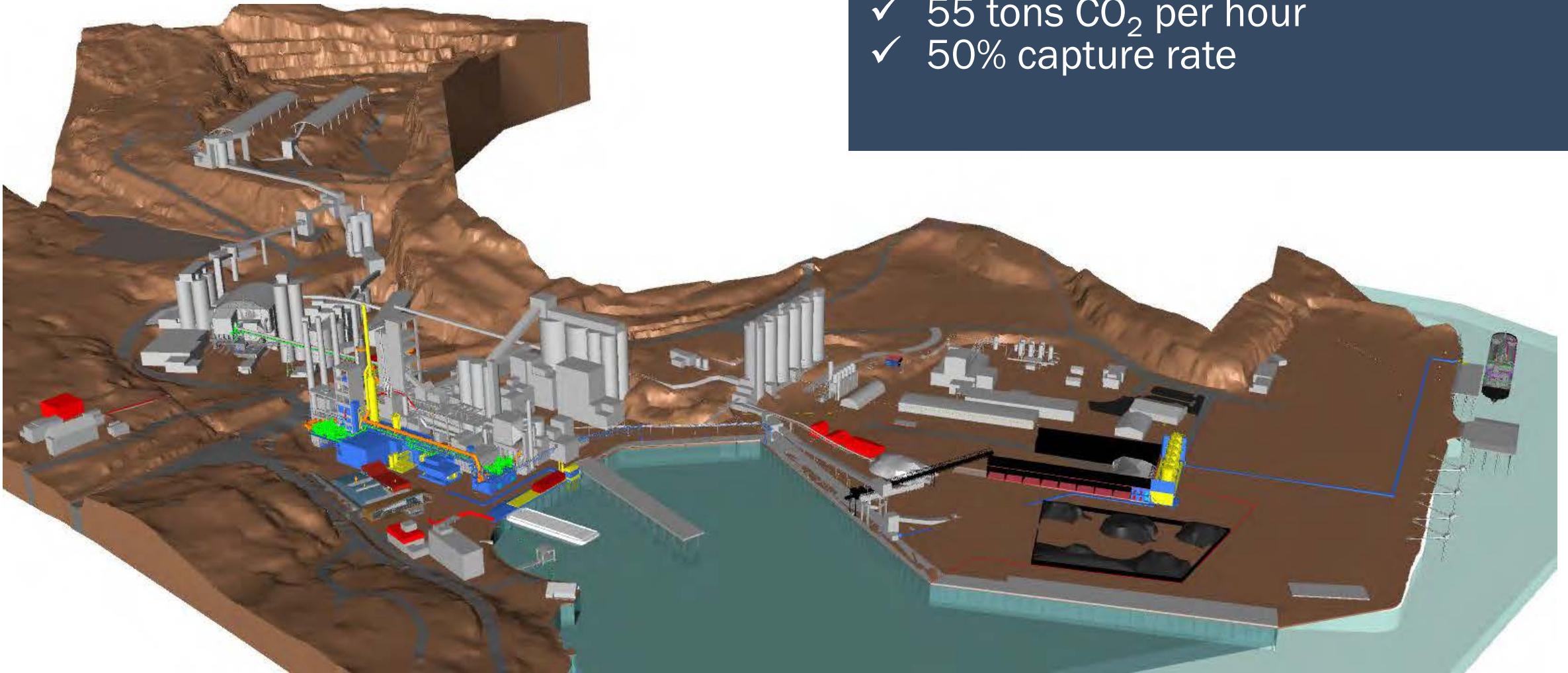


Demonstration plant

400.000 tons per year

- ✓ 55 tons CO₂ per hour
- ✓ 50% capture rate

CO₂ capture Brevik



What is Northern Lights?

01.03.2021

CO₂ TRANSPORT BY SHIP

Cargo Systems for CO₂

‘LPG standard’ design

Proven concept based on food industry model

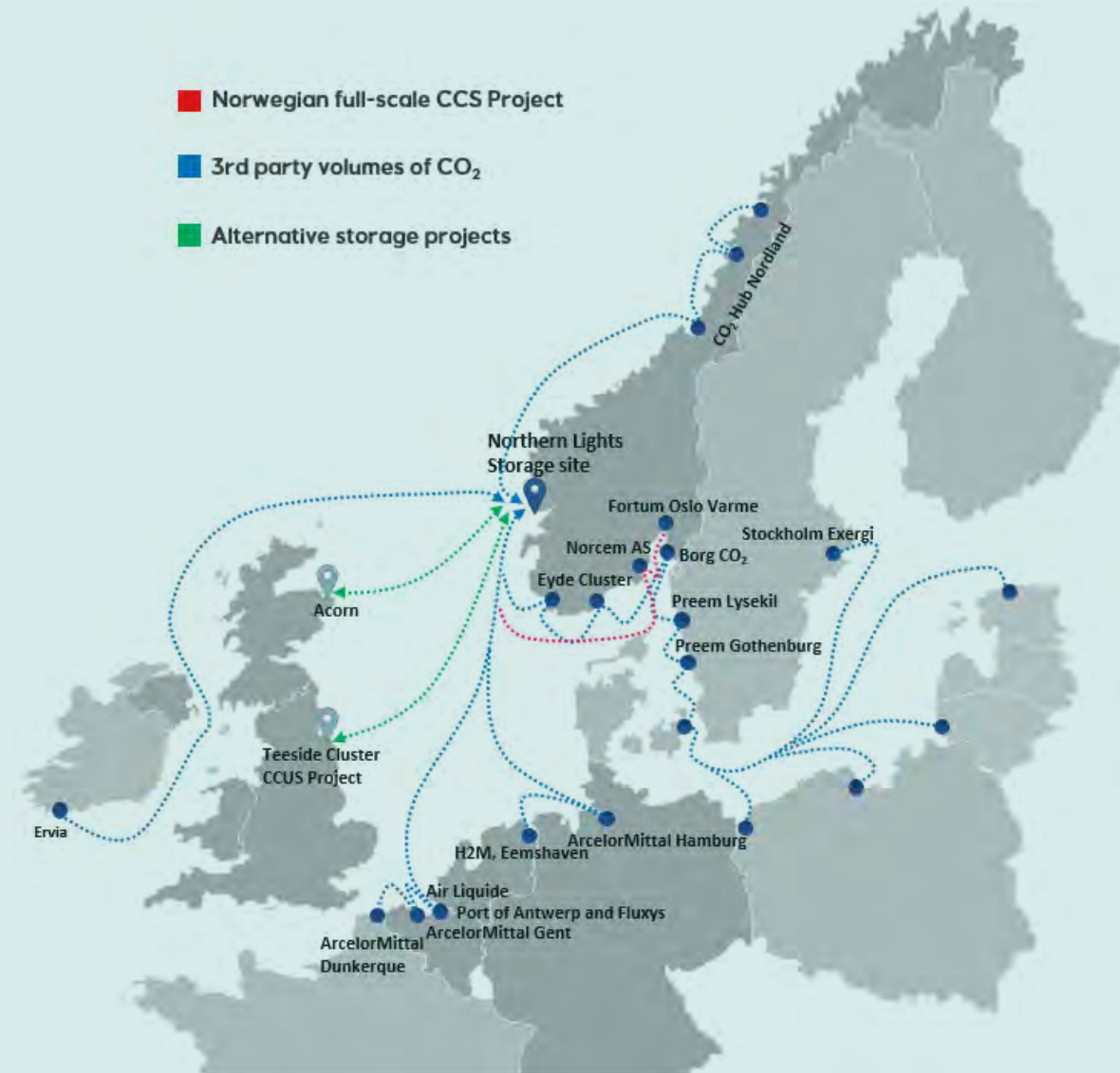
Initially two ships

Transport capacity scalable with number of ships

A fleet is required for the planned scale-up – perfect for driving ship technology and fuels development



Delivery contract starts in Q2 2021



Northern Lights landanlegg i Øygarden



Onshore plant

Civil works started

Preparations for jetty construction

Project office under construction

Detail engineering of plant started

Fabrication of plant starts spring 2022



Pipeline and subsea facilities

Template installed in 2019, well drilled in 2020

Fabrication of umbilical started

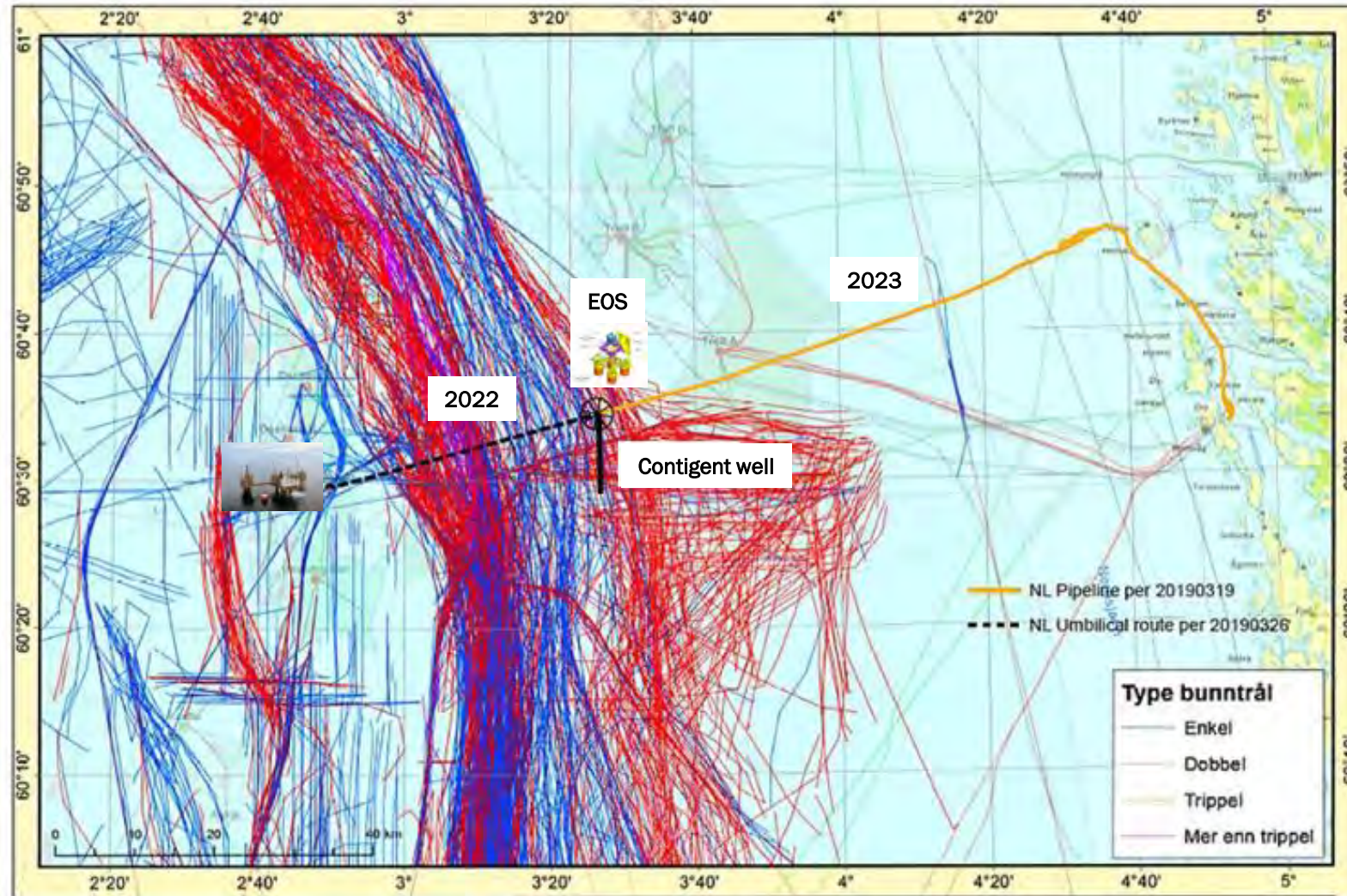
Fabrication of power and fibre optic control cable started

Engineering of topsides modifications at Oseberg started

Engineering of pipelay started

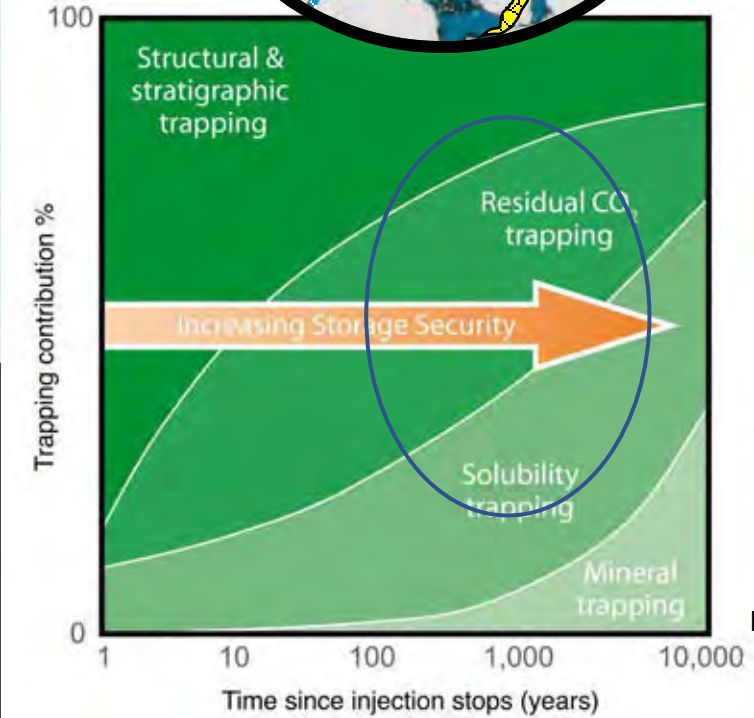
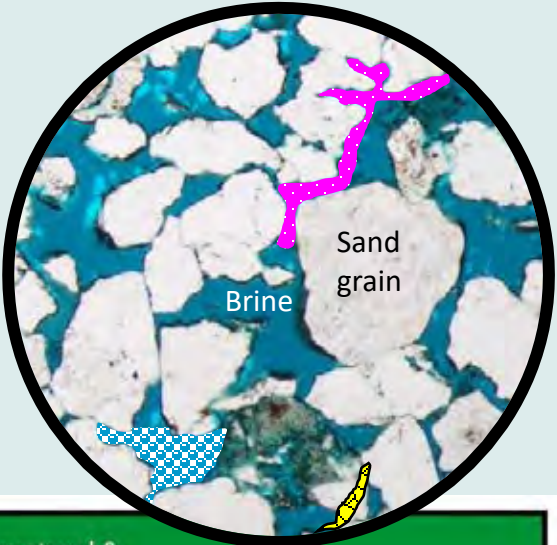
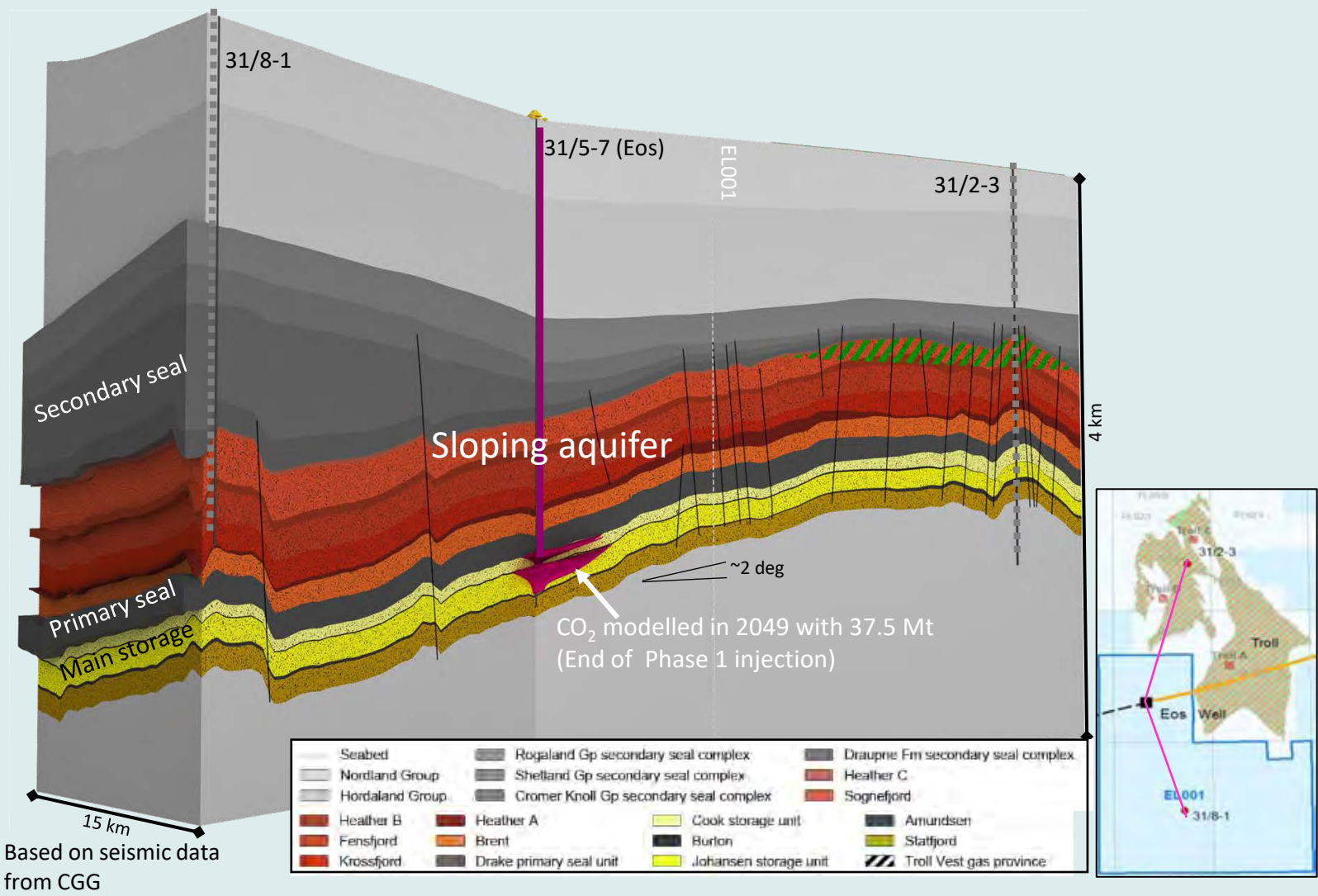


Northern Lights infrastructure versus fisheries



Bottom trawling activity (2018), as illustrated in IA (Phase 1) – based on satellite tracking datas of vessels

Northern Lights storage concept



IPCC, 2005

Containment and large pore volume required

Storage experience

01.03.2021

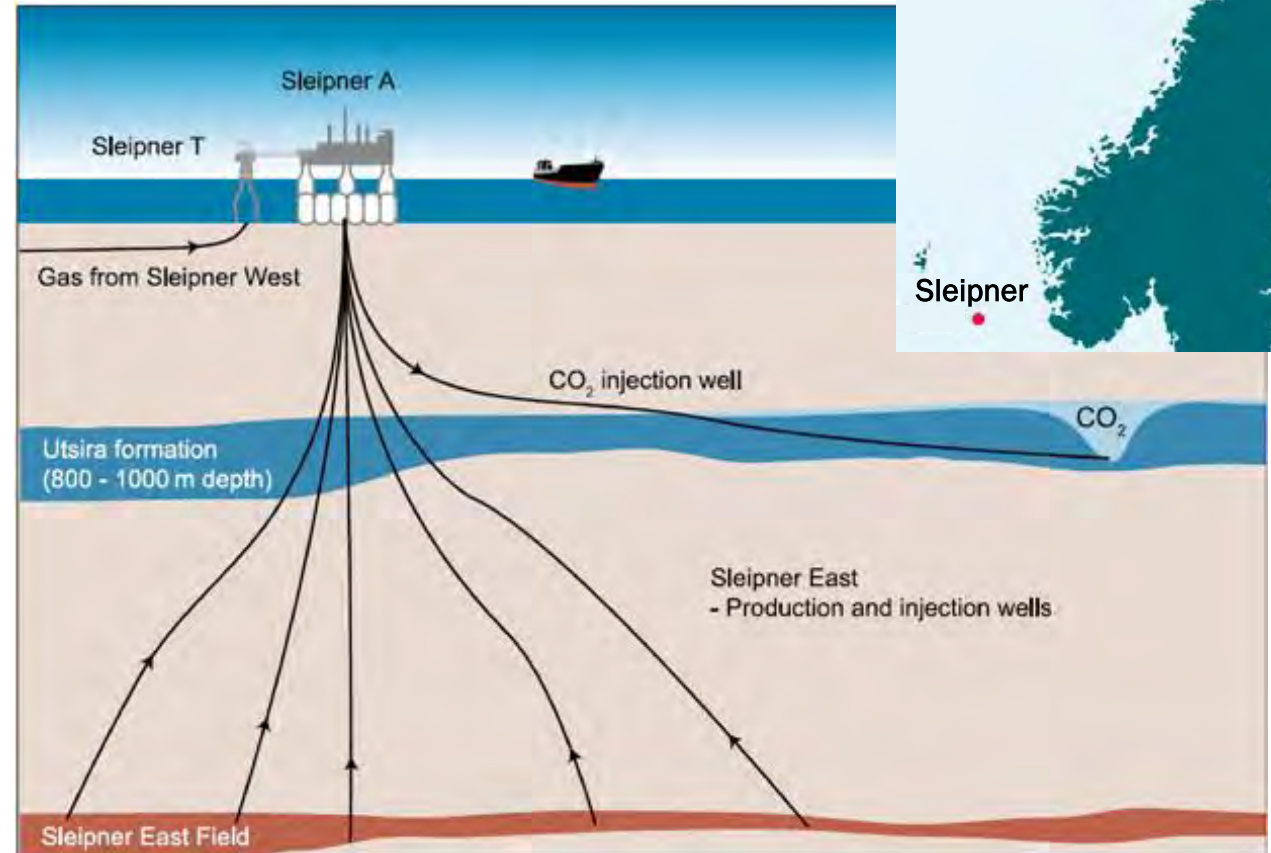
Industrial experience – Norway

Sleipner:

- Injection since 1996
- More than 18 mill t CO₂ stored*
- Frequent monitoring, many academic projects
- Data set publicly available

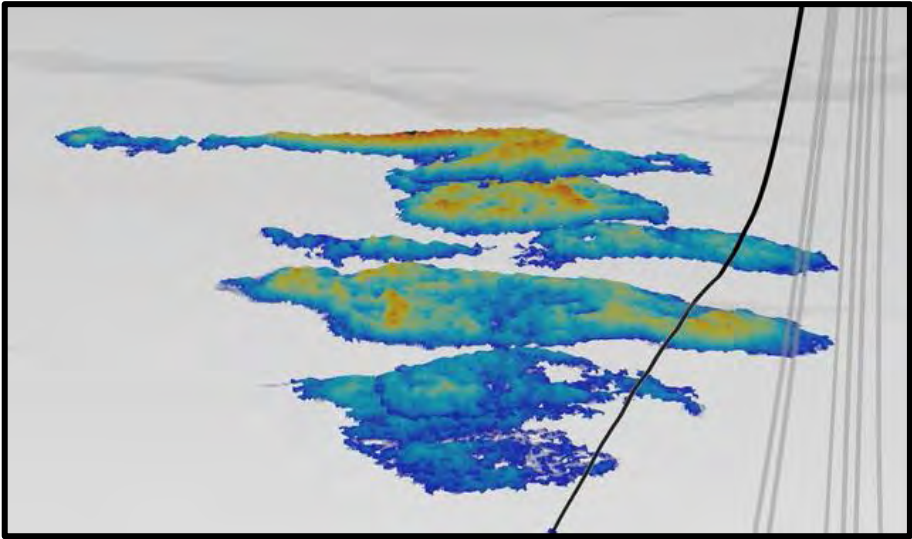
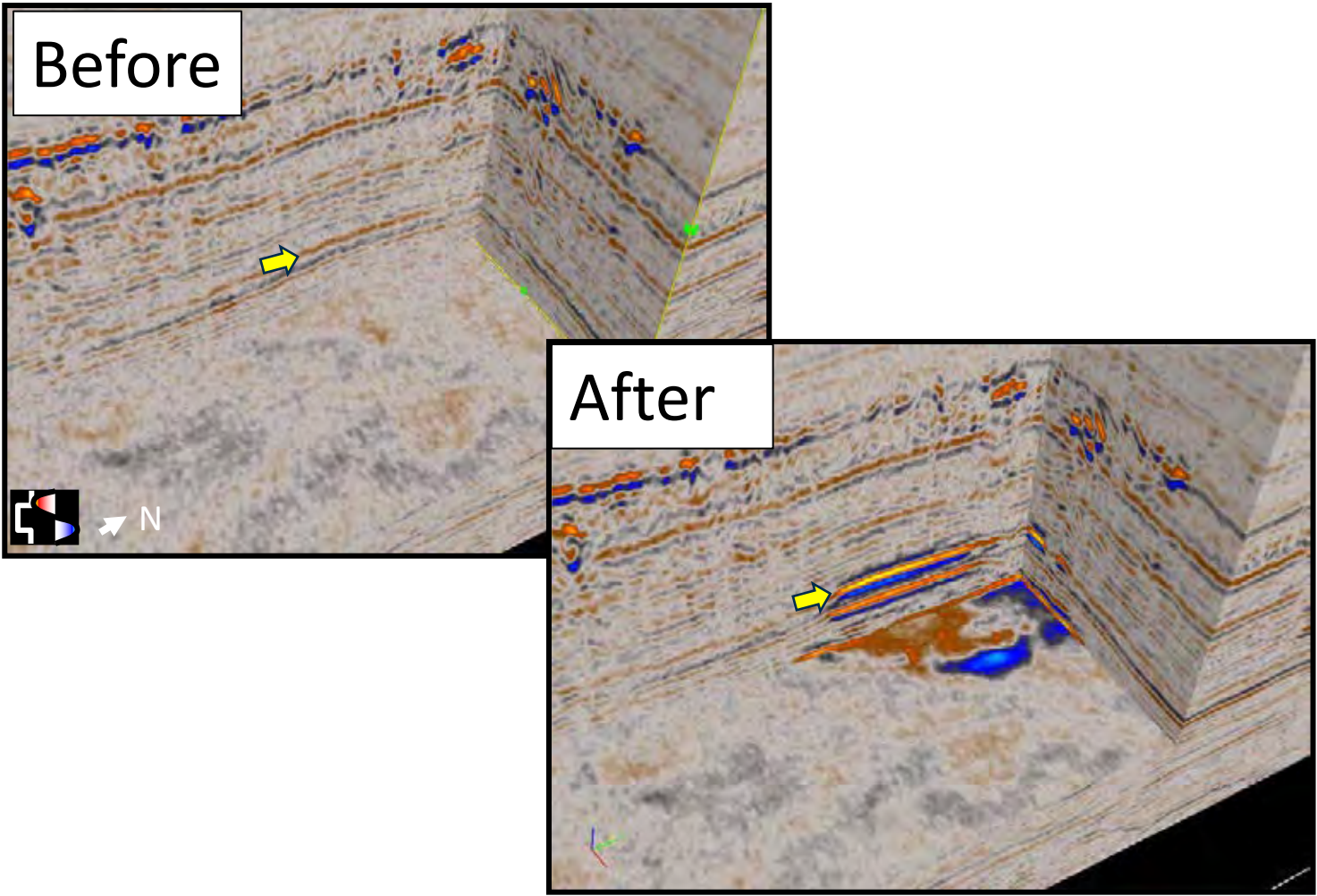
Snøhvit:

- Injection since 2008
- More than 6 mill t CO₂ stored*
- Subsea facilities



*: status end of 2019

Seismic monitoring (Sleipner)



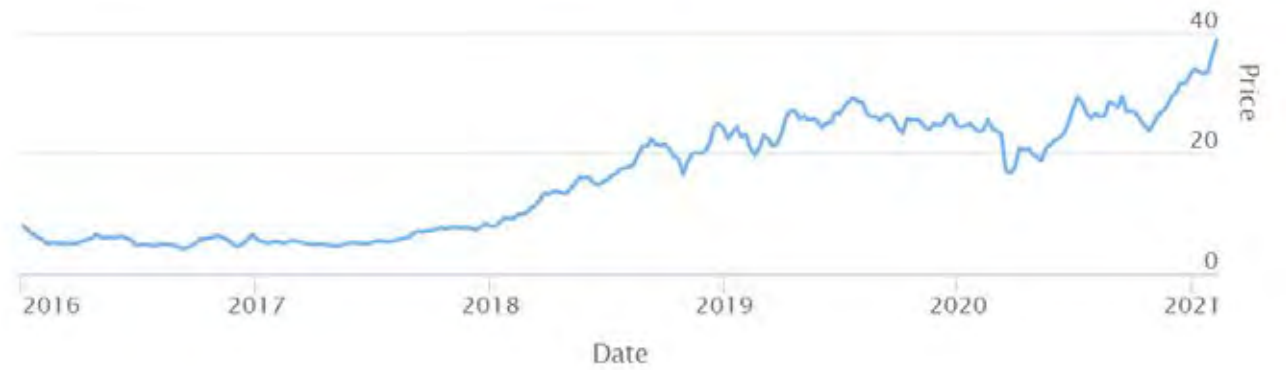


Is there a business opportunity?

01.03.2021



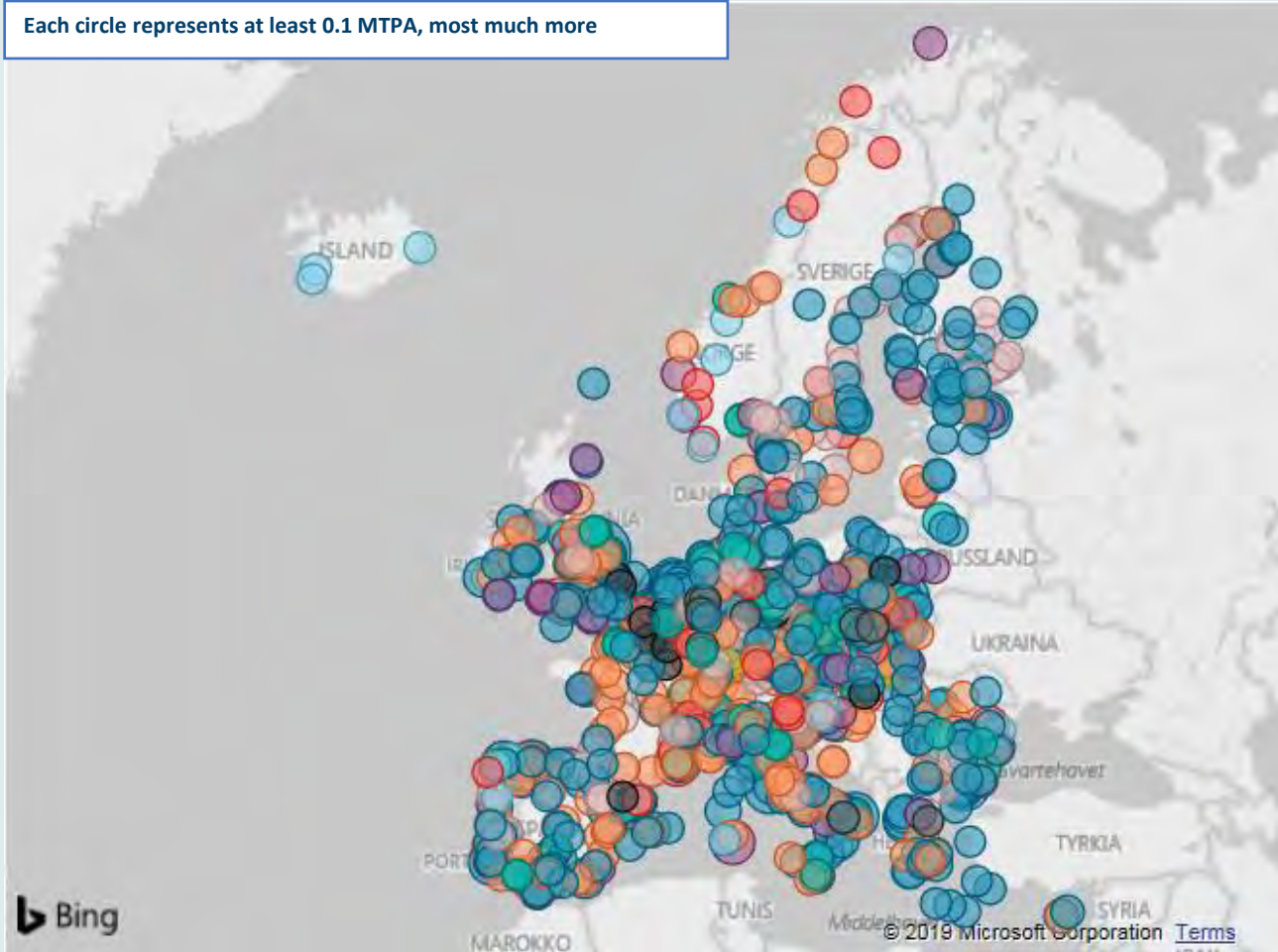
<https://davidappell.blogspot.com/2019/04/EEK-CARBON-TAX.html>



<https://ember-climate.org/data/carbon-price-viewer/>

IS THERE A BUSINESS OPPORTUNITY?

Each circle represents at least 0.1 MTPA, most much more



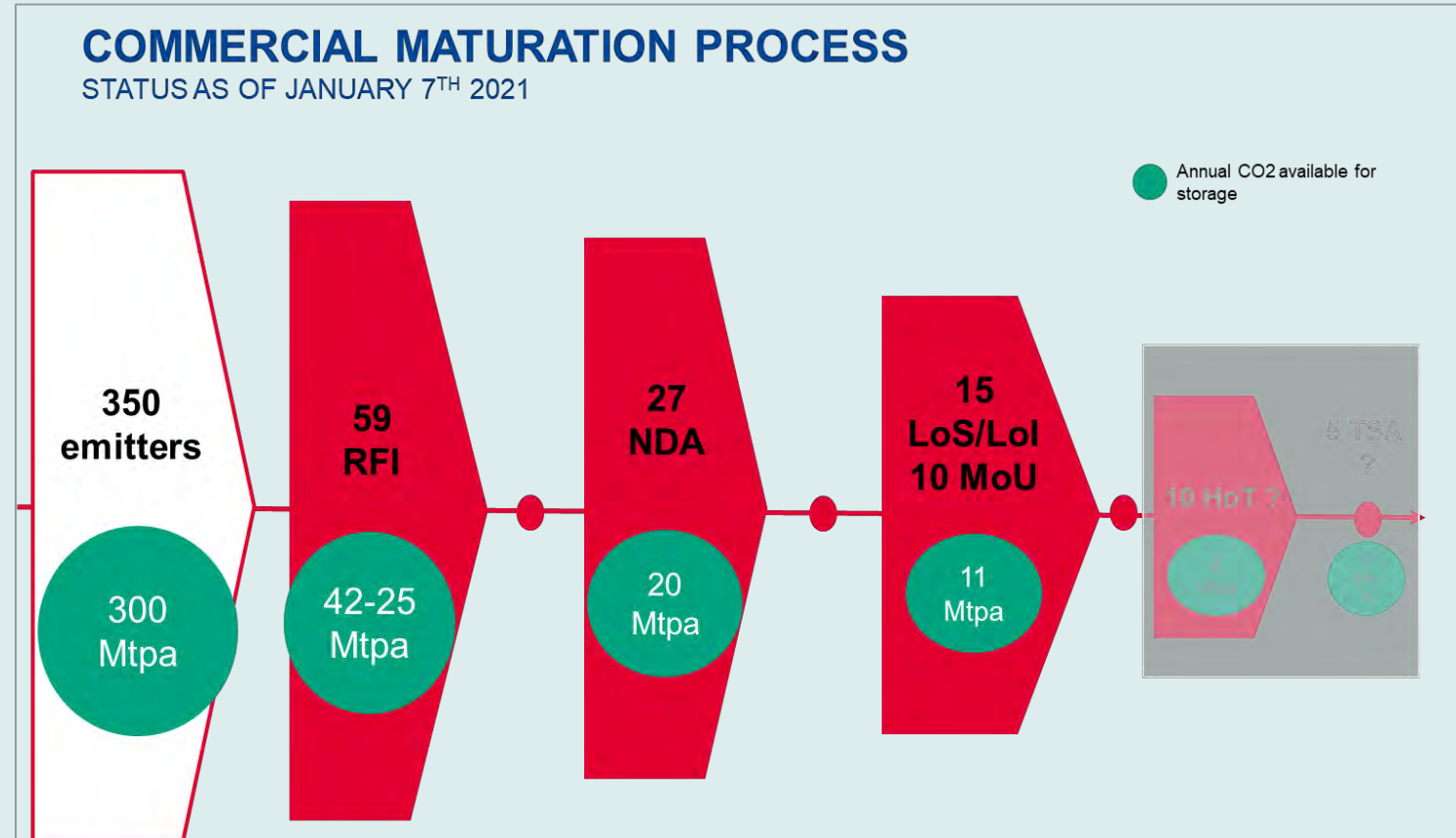
Sectors with the largest potential:

- Waste incineration and waste to energy
- Cement
- Biomass and biofuel
- Refineries
- Steel
- Natural gas
 - Hydrogen
 - Electricity
- Fertilizers
- Data centers
- Direct Air Capture

Business development funnel

MoU

- Heidelberg Group (cement), **Germany**
- Fortum Group (WtE); **Finland**
- Ervia (natural gas supply), **Ireland**
- Air Liquide (chemicals, hydrogen), **Belgium**
- Stockholm Exergi (WtE), **Sweden**
- ArcelorMittal (steel and iron), **Luxemburg**
- Preem (refineries and fuels, hydrogen), **Sweden**
- ETH Zürich, **Switzerland**
- Microsoft, **USA**



Some challenges

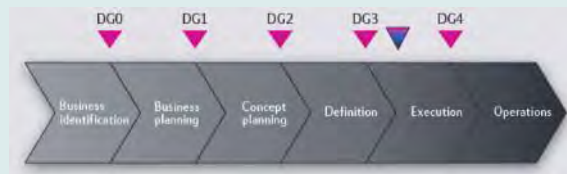
Northern Lights seen from conventional oil & gas project perspective

Normal oil & gas

Regulatory framework exists

Business case

Resource is known, permanent, validated



Markets existing and predictable

Develop project to harvest business case

- Technical maturation with DGs
- Risks identified
- Concept freeze early
- Not schedule driven

Northern Lights

Regulatory framework not in place

No business case

Resource is NOT known, validated:

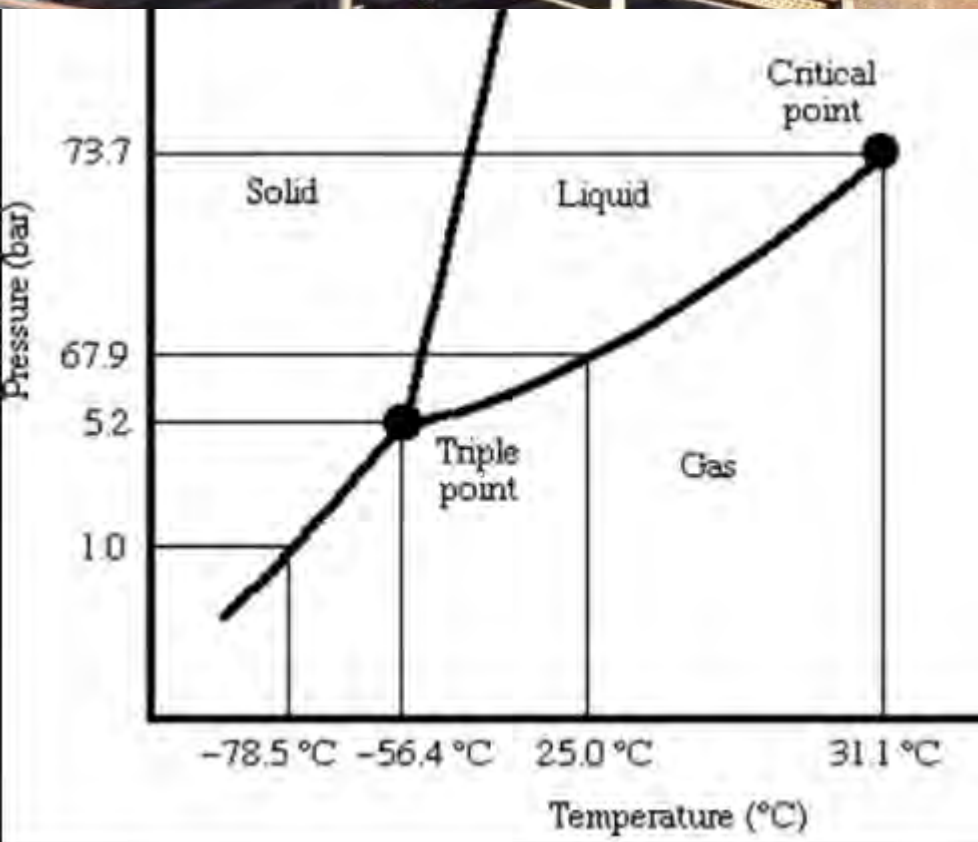
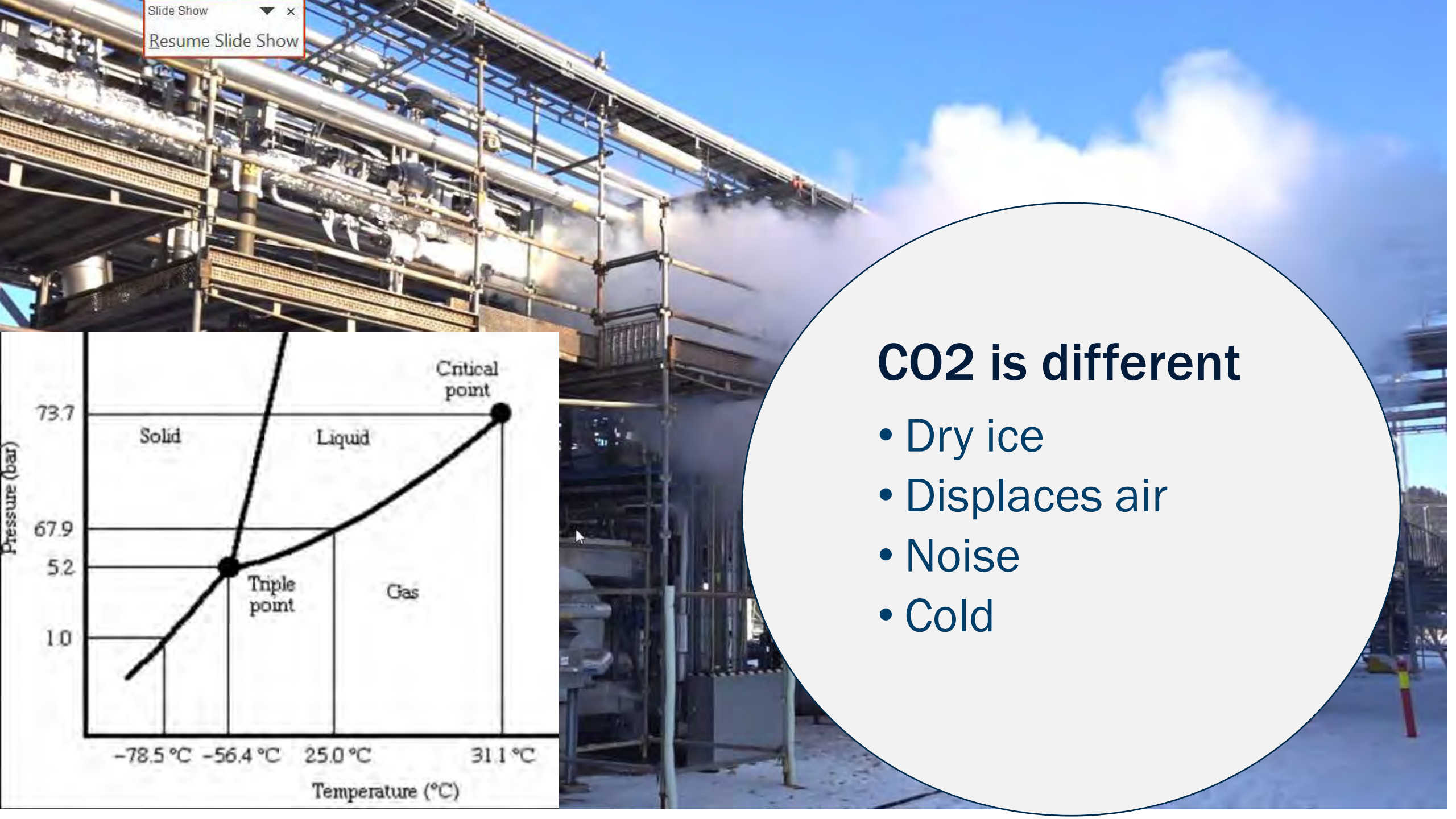
- Not reservoir
- Not CO2



No normal markets

Develop project *to build future markets*

- Technical maturation with DGs
- Identified risks, *and many*
- Concept *partly* frozen early (*not SSV*)
- *Schedule driven*



CO₂ is different

- Dry ice
- Displaces air
- Noise
- Cold

Summary

01.03.2021

The process behind us



Historic investment decision for transport and storage of oil and gas

May 15 2020, 16:04 CEST / Last modified: May 15 2020, 17:26 CEST

Equinor, Shell and Total have decided to invest in the ELOO1 North project in Norway's first exploitation licence for CO2 on the Norwegian Continental Shelf. Plans for development of the project have been handed over to the Ministry of Petroleum and Energy.

ESA EFTA Surveillance Authority

Newsroom

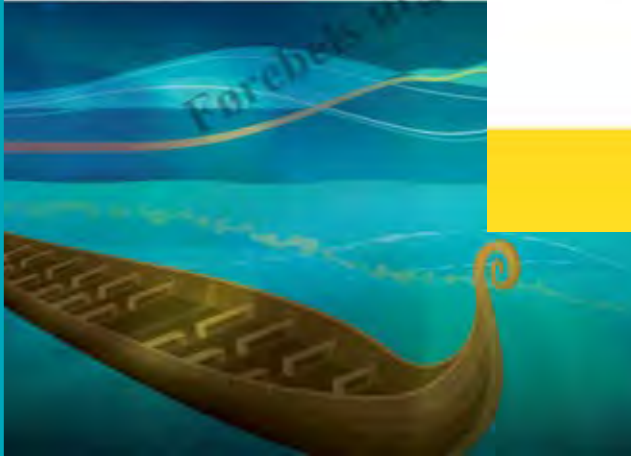
17.08.2020 STATE AG

ESA approves Norwegian Full-Scale CO2 Transport and Storage: up to 1 million tonnes per year

DET KONGELIGE OLJE- OG ENERGIDEPARTEMENT

Meld. St. 33
(2019–2020)
Melding til Stortinget

Langskip – fangst og lagring av CO2



STORTINGET

10:55:33

Tina Bru (H)
Olje- og energiminister

DET KONGELIGE FINANSDEPARTEMENT

Prop. 1 S
(2020–2021)
Proposisjon til Stortinget (forslag til stortingsvedtak)

FOR BUDSJETTÅRET 2021
Statsbudsjettet

Enighet om statsbudsjettet 2021
mellom Høyre, Framskrittspartiet, Venstre og Kristelig Folkeparti

| Beskrivelse | Pålept endring | Bokført endring |
|---|-----------------------|-----------------------|
| Skatte- og avgiftslettelser | 4 514 500 000 | 4 171 500 000 |
| Økte utgifter | 8 752 844 000 | 8 187 844 000 |
| Økte utgifter som følge av avtale om LTP | 303 600 000 | 253 000 000 |
| Sum økte utgifter og skatte- og avgiftslettelser | 13 570 944 000 | 12 612 344 000 |
| Skatte- og avgiftslettelser, tilleggsnummer | 2 816 400 000 | 2 681 400 000 |
| Økte utgifter, tilleggsnummer | 1 891 000 000 | 1 891 000 000 |
| Sum økte utgifter og skatte- og avgiftslettelser, tilleggsnummer | 4 707 400 000 | 4 572 400 000 |
| SUM TOTALT ØKTE UTGIFTER OG SKATTE- OG AVGIFTSLETTEELSE | 18 278 344 000 | 17 184 744 000 |
| Inndekning/reduerte utgifter | -3 842 600 000 | -3 642 600 000 |
| SUM TOTALT (SVEKKET BUDSJETTBALANSE) | 14 635 744 000 | 13 542 144 000 |

STATUS

Project

- Majority of execution contracts awarded
- Execution started
- Site office in Øygarden in operation
- Start up mid-2024 aligned with Norcem's plans

New company - «Northern Lights JV DA»

- Formally established on 5th Feb 21
- Regulatory obstacles passed (competitive clarifications in EU)





Q&A

01.03.2021

Research for a better future



Renewable
energy



Nuclear
technology



Materials
technology



Digitalization



Radiopharmacy
and health



Oil and gas



Industry and
environment



Safety and
security

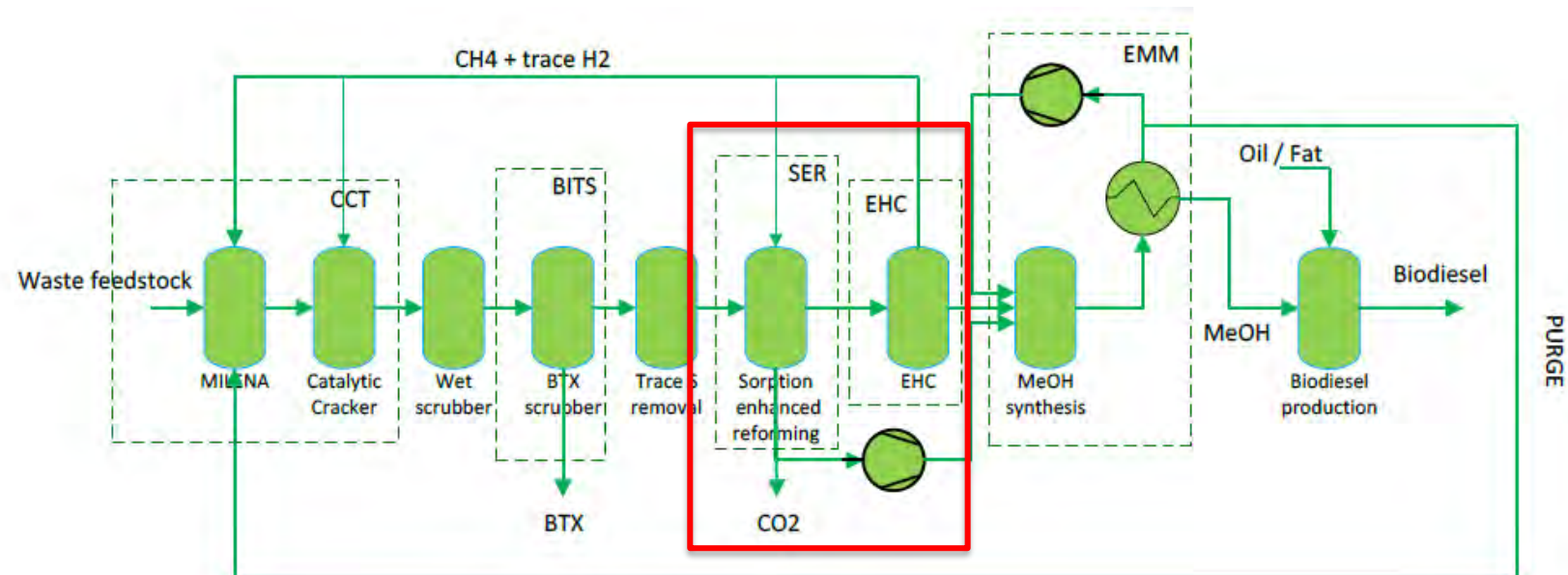
CONVERGE: CarbON Valorisation in Energy-efficient Green fuels

SER and SEWGS for CO₂ capture: preliminary experimental results

CONVERGE WP3: Objectives

The main objective of WP3 is to validate the integration of the SER and EHC technologies at TRL5 in relevant operating conditions adapted to the CONVERGE concept with the following specific targets:

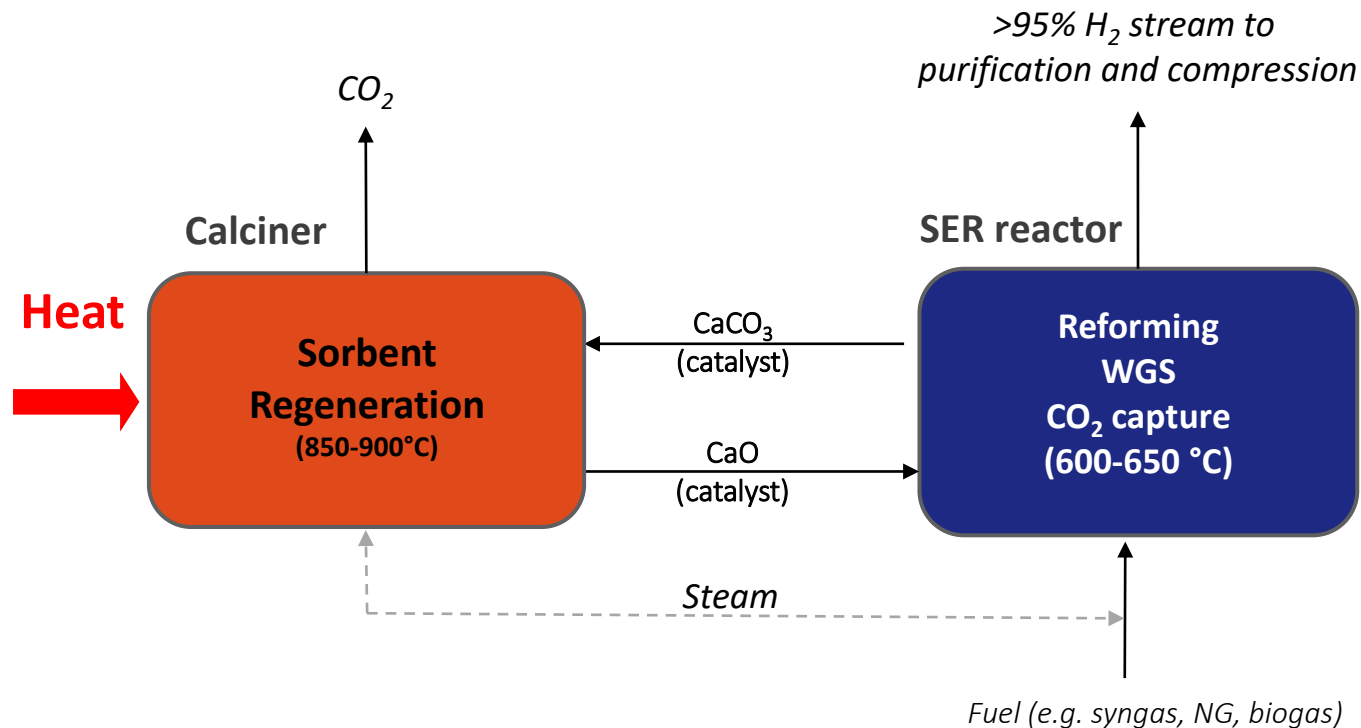
- Reduce the energy consumption for hydrogen production, CO₂ removal and compression to 1.2 MJ/kg CO₂
 - **Optimization of the CO₂ sorbent material used in the SER process**
 - **Development of new improved catalytic materials suited for the CONVERGE syngas**
- Extract and compress H₂ at >99.5% purity, 50 bar and at a primary energy consumption of 12 MJ/kg H₂
- Operate the SER and EHC for 500 hours on C1-C6 containing emulated syngas feed at 10 Nm³/hr H₂ production



Sorption Enhanced reforming (SER)

SER integrates Reforming, Water-Gas Shift (WGS) and CO₂ separation through the addition of a high temperature CaO-based CO₂ solid sorbent

SER Concept scheme



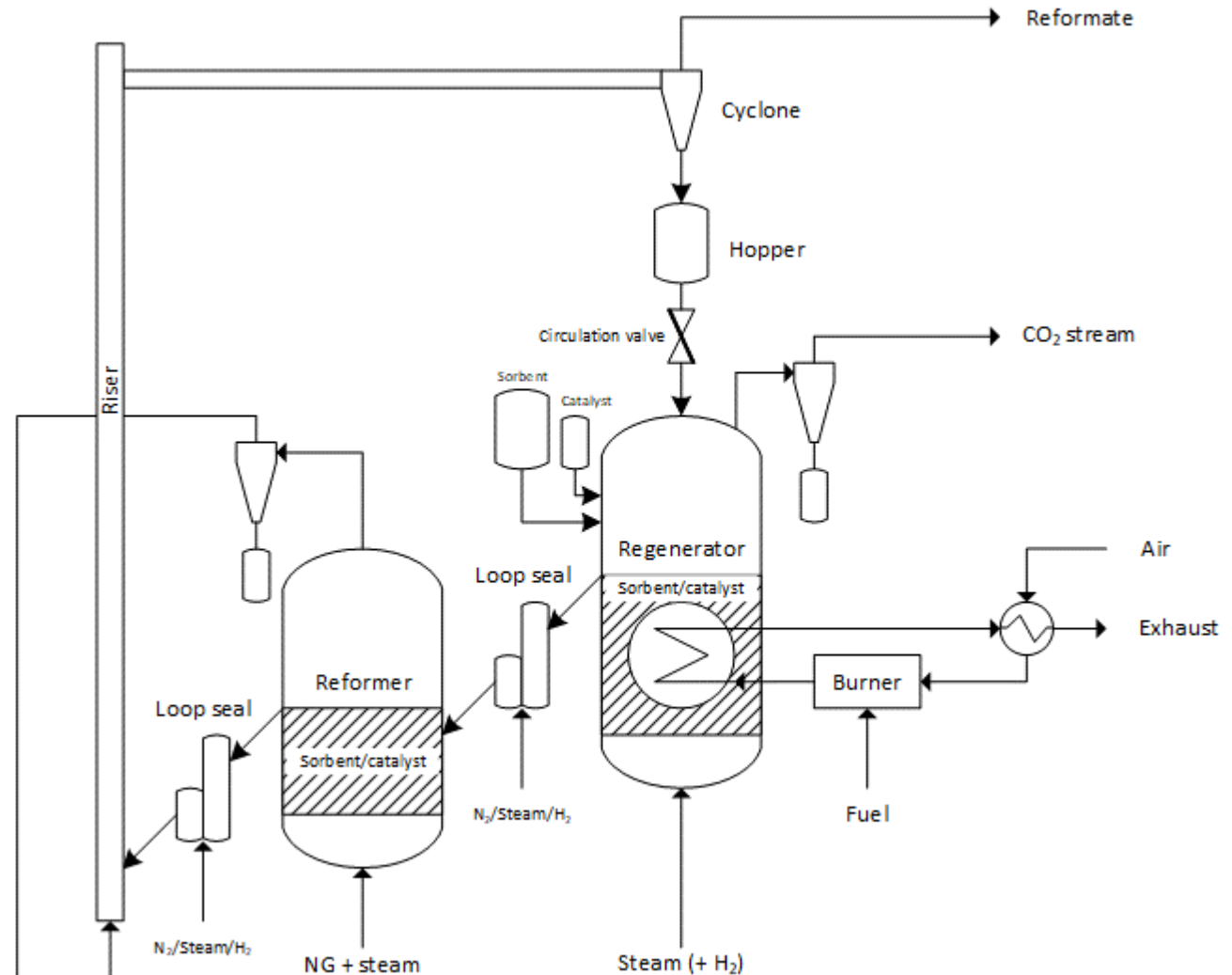
Feed Gas after CCT

H₂ - 41.9%
CO - 10.0%
CO₂ - 32.4%
CH₄ - 10.5%
C₂H₄ - 4.4%
N₂ - 0.9%

SER reactor technology developed at IFE

Dual Bubbling Fluidized Bed (DBFB) reactor system

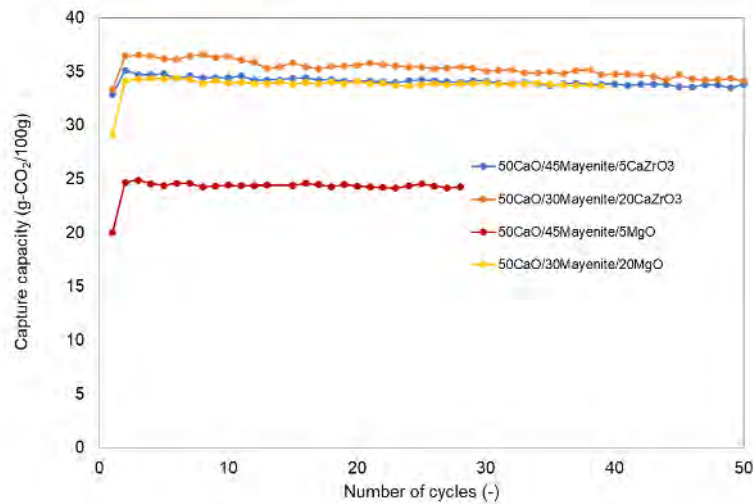
- Dual bubbling fluidized bed reactor (DBFB)
 - 2 FB-reactors coupled with loop-seals and riser
 - Continuous mode
 - Bubbling regime
 - Circulation rate adjusted with slide valve



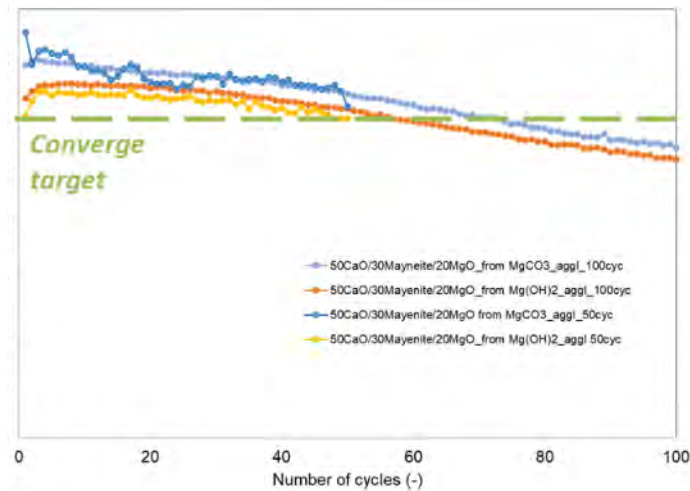
Materials Development and Optimization

CO₂ sorbent material used in the SER process

- added a thermally stable dopant (ZrO₂, MgO and Fe₂O₃) in the CaO/Mayenite sorbent to increase its stability

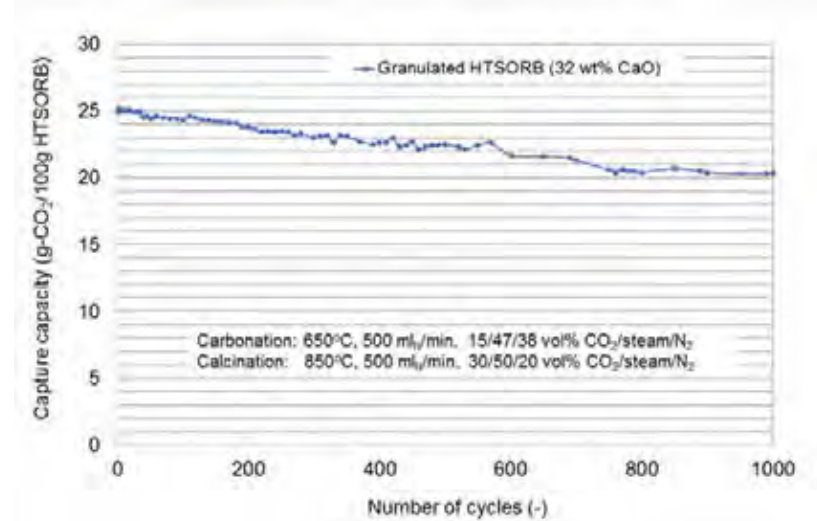


Sorbent powders: stable activity and capacity target achieved in some cases



100 cycles test: capacity decreases more severely. The addition of thermally stable agents does not allow reaching the target

- HTSORB – Chosen for experiments

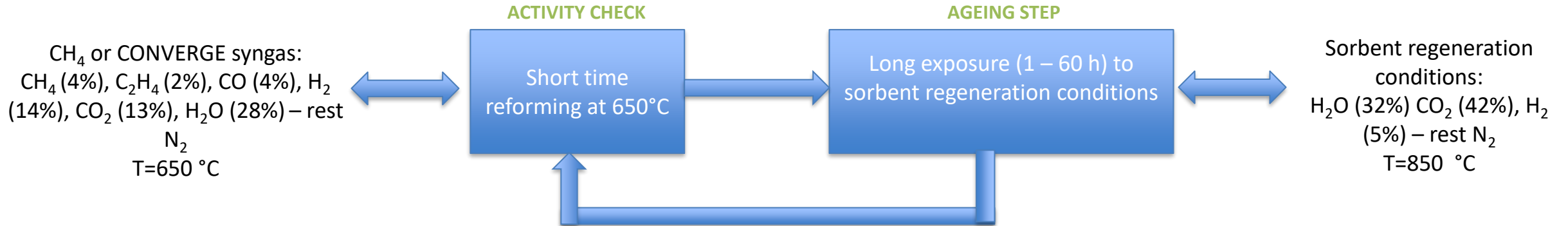


Long-term sorption capacity: stabilized at < 20 g-CO₂/100g sorbent after 1000 carbonation-calcination cycles

Development of catalyst tailored for SER process– Stability test

SER Catalyst testing and aging

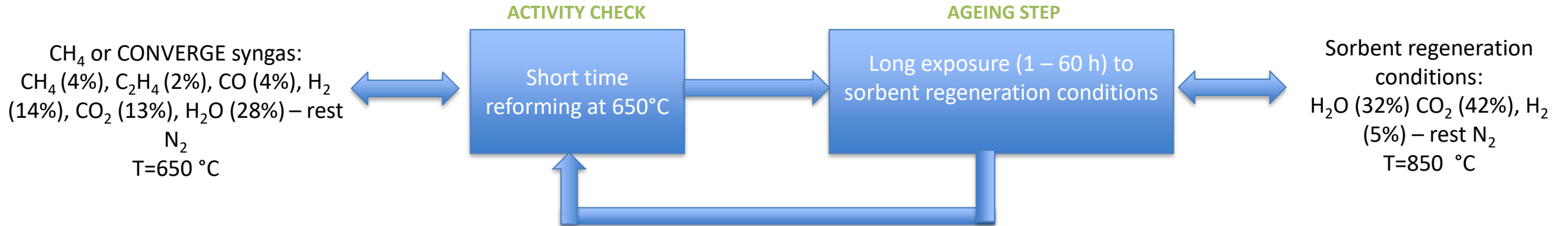
- New catalytic set-up designed and constructed within CONVERGE project for “stability” and “kinetic” tests.



Development of catalyst tailored for SER process– Stability test

SER Catalyst testing and aging

- New catalytic set-up designed and constructed within CONVERGE project for “stability” and “kinetic” tests.



Materials Development and Optimization

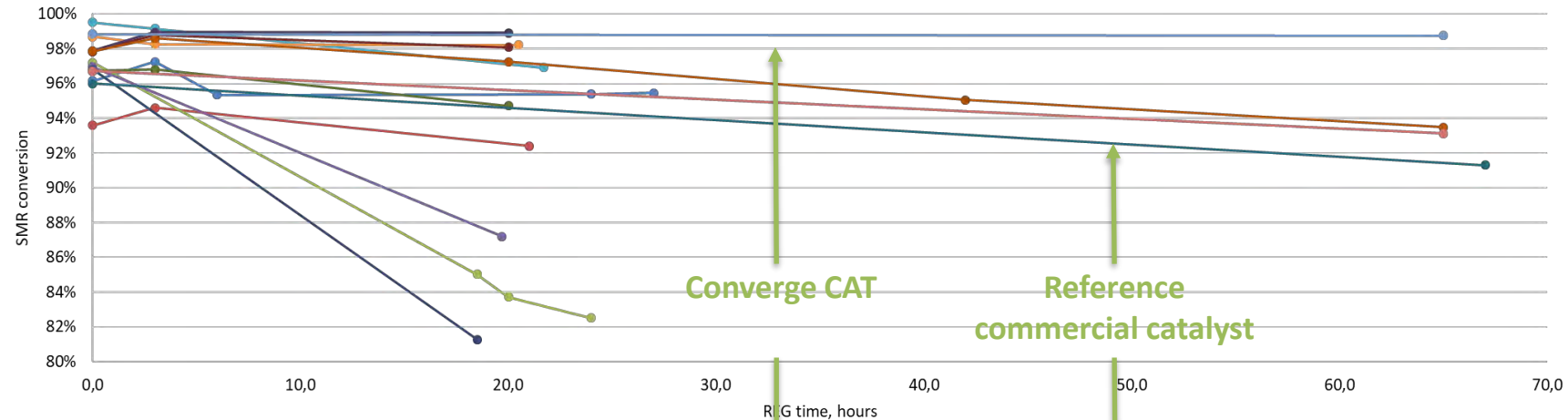
Development of catalyst tailored for SER process – Stability test

Stability tests:

Screening a matrix of 15-20 newly synthesized materials

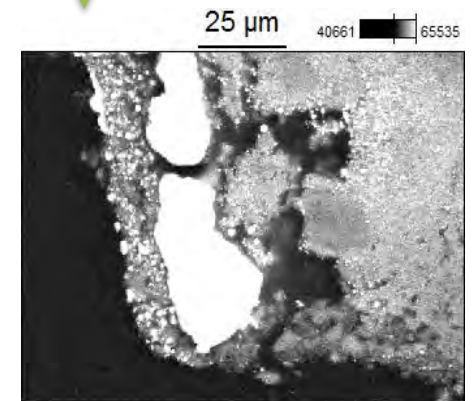
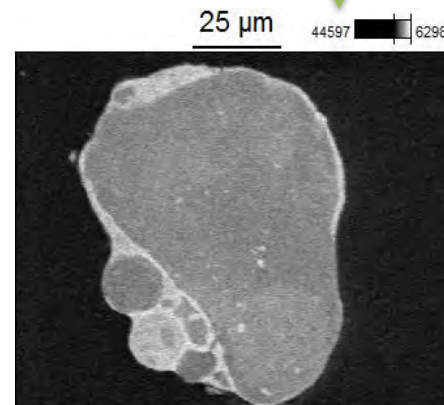
- 5 different supports
- 5-10-15-20 wt % Ni

Satisfactory results, higher activity than commercial reference for some of the prepared catalysts



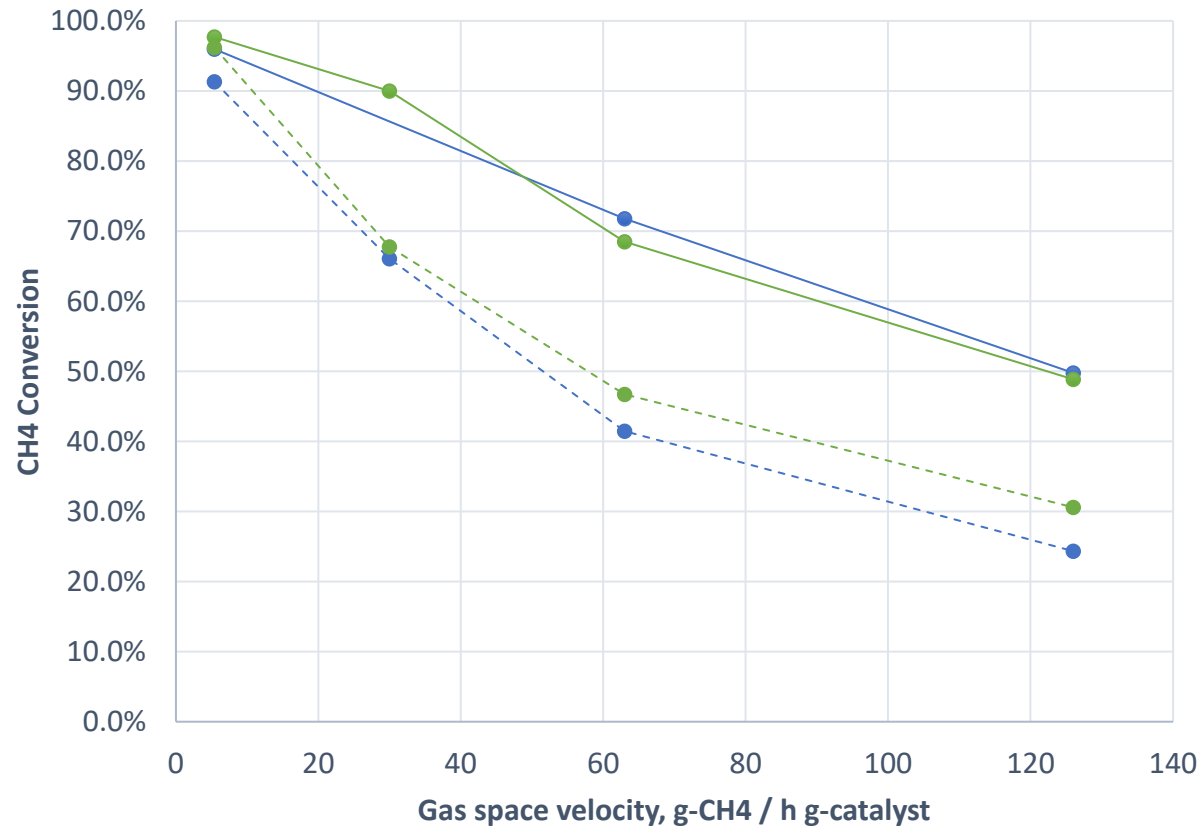
SEM characterization after 60h of test:

- Nickel sintering well evident in the commercial catalyst
- No evidence of nickel sintering but total nickel loading to be decreased to avoid nickel «envelop» effect



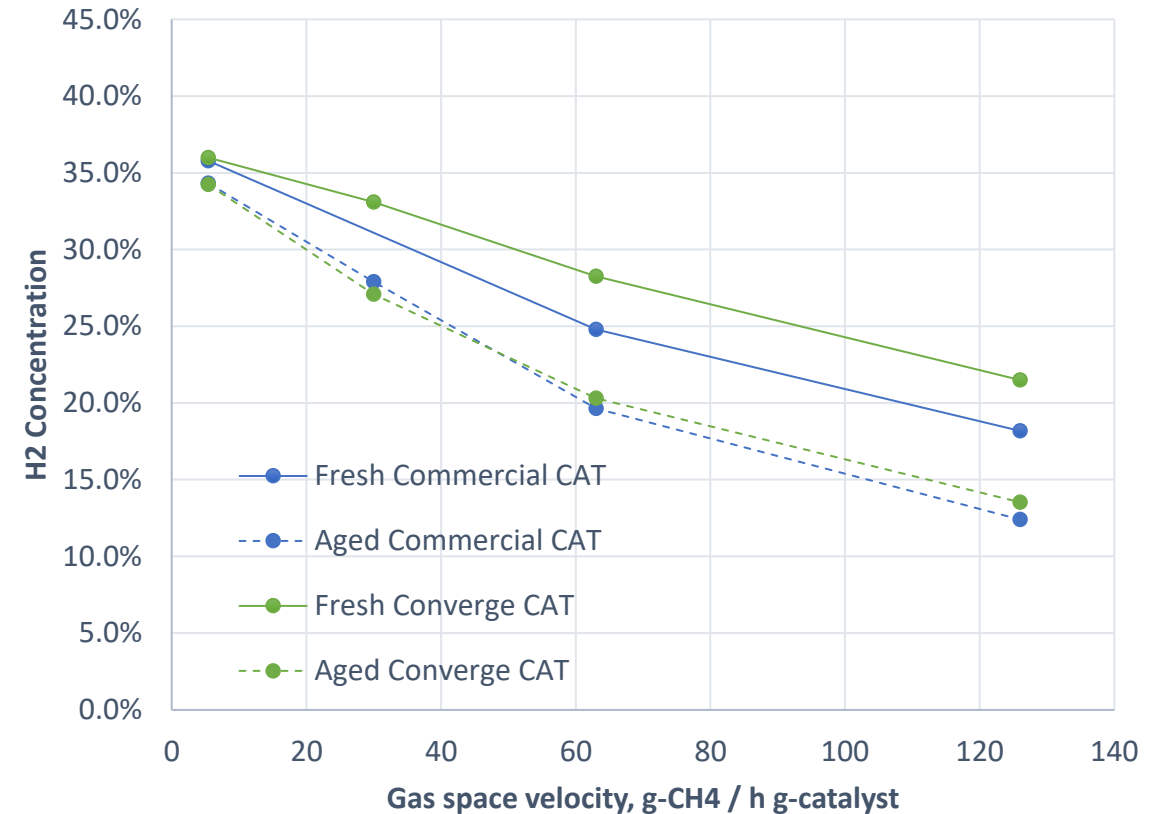
Materials Development and Optimization

Development of catalyst tailored for SER process– Stability test in SMR conditions (Aged 60h)



CH₄ conversion

- Converge CAT presents better CH₄ conversion after aging. Difference more apparent in higher GSV.



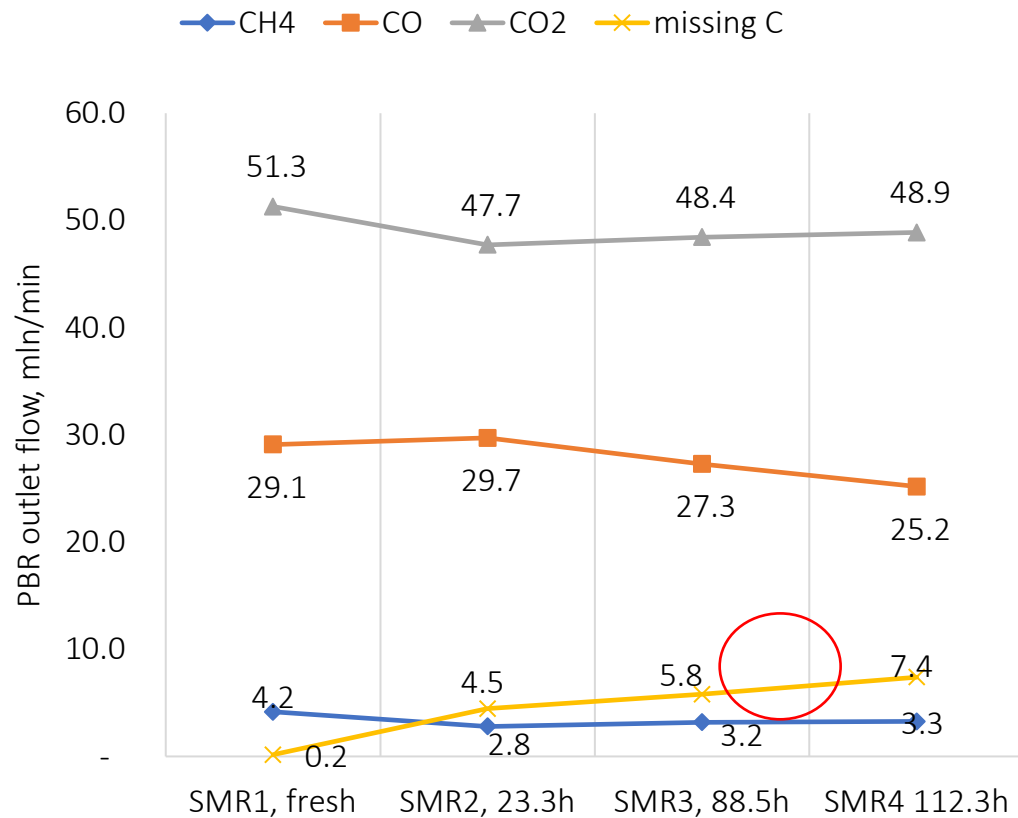
H₂ concentration

- Converge CAT presents better H₂ selectivity fresh and after aging

Materials Development and Optimization

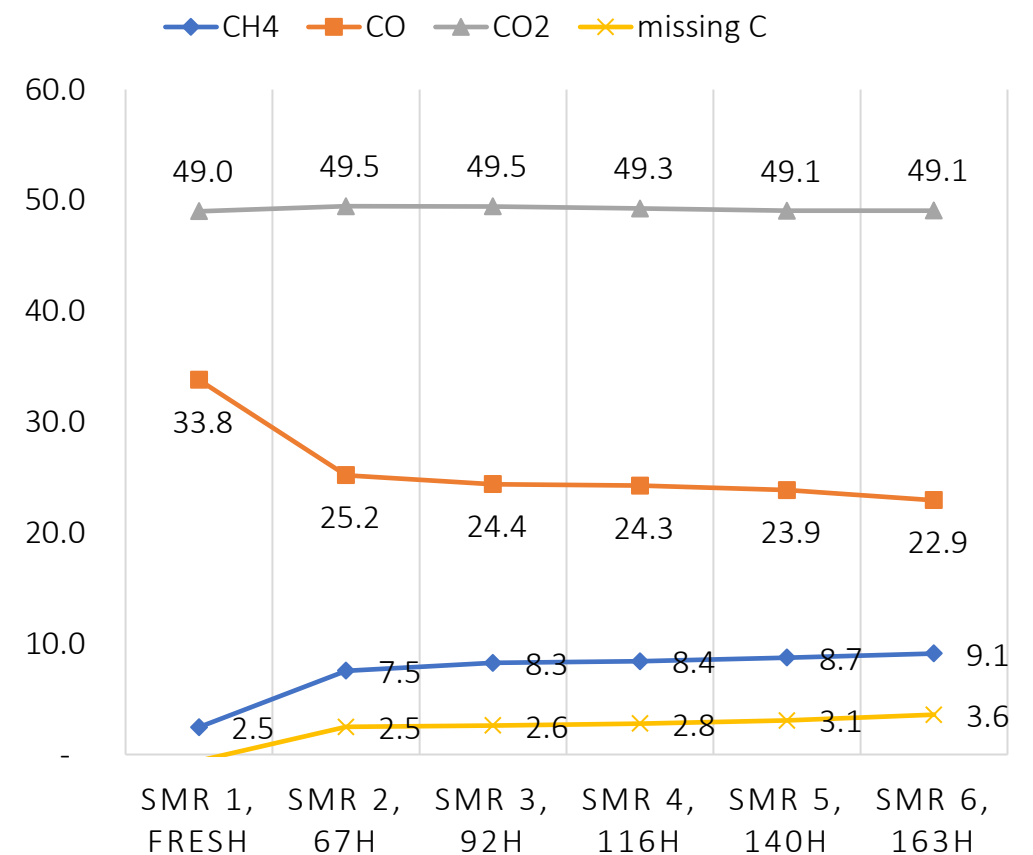
Development of catalyst tailored for SER process– Stability test

Commercial CAT



- Increase in carbon deposition. (TPO confirmed)
- Experiment stop after 120h aging – High pressure drop

Converge CAT



- No carbon deposition
- Experiment stable during 160h aging

FBR Tests

SER/SEWGS – Equilibrium Trade-off

Process Parameters

Temperature: 650°C

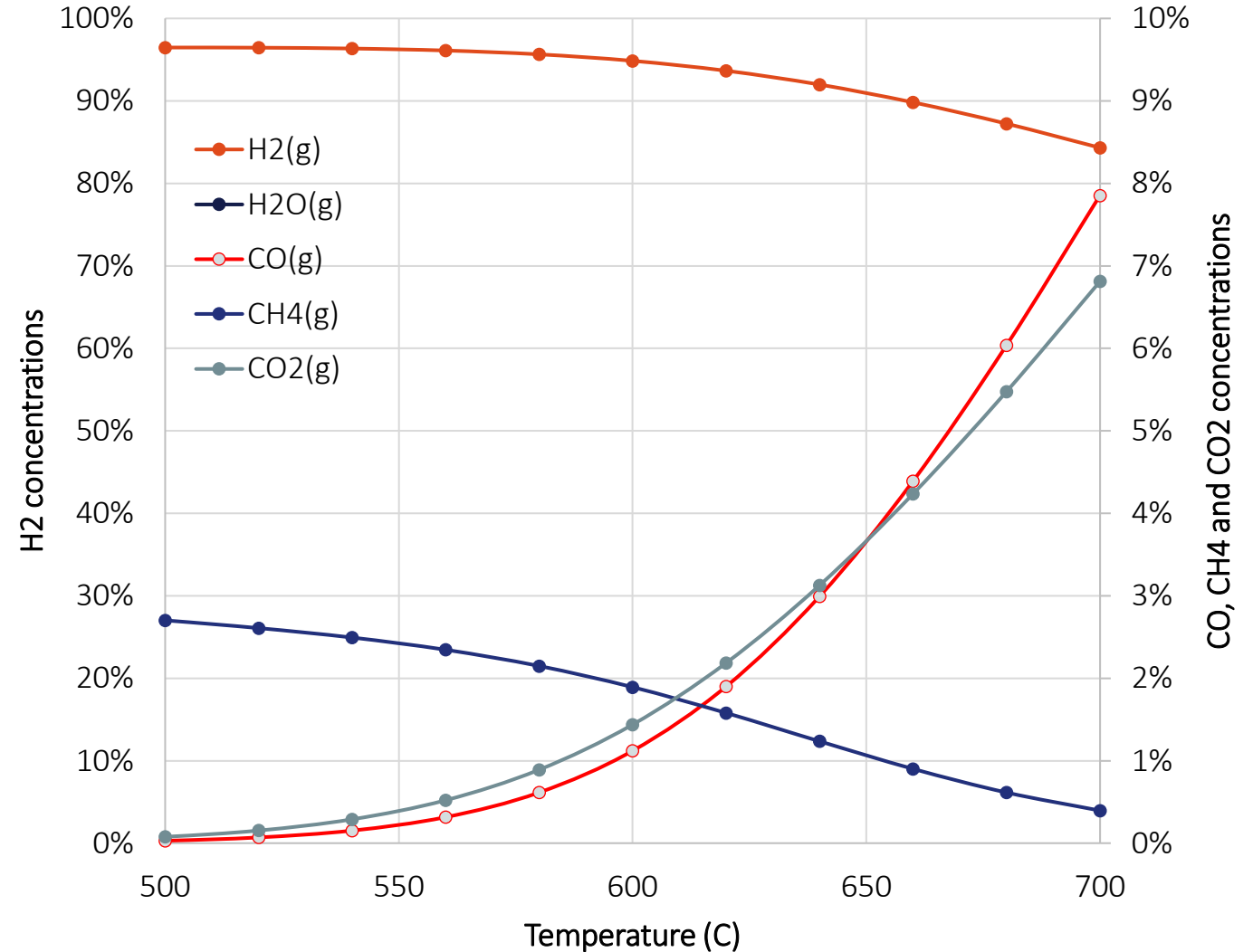
Pressure: 0.5 barg

Fluidization velocity: 0.036 m/s

Feedstock and Materials

Gas Feed: (mol%): 41.9% H₂, 10.0% CO, 32.4% CO₂, 10.5% CH₄, 4.4% C₂H₄, 0.9% N₂

Steam R value: 2.0



SER/SEWGS – With syngas - Converge Cat

Process Parameters

Temperature: 650°C

Pressure: 0.36 barg

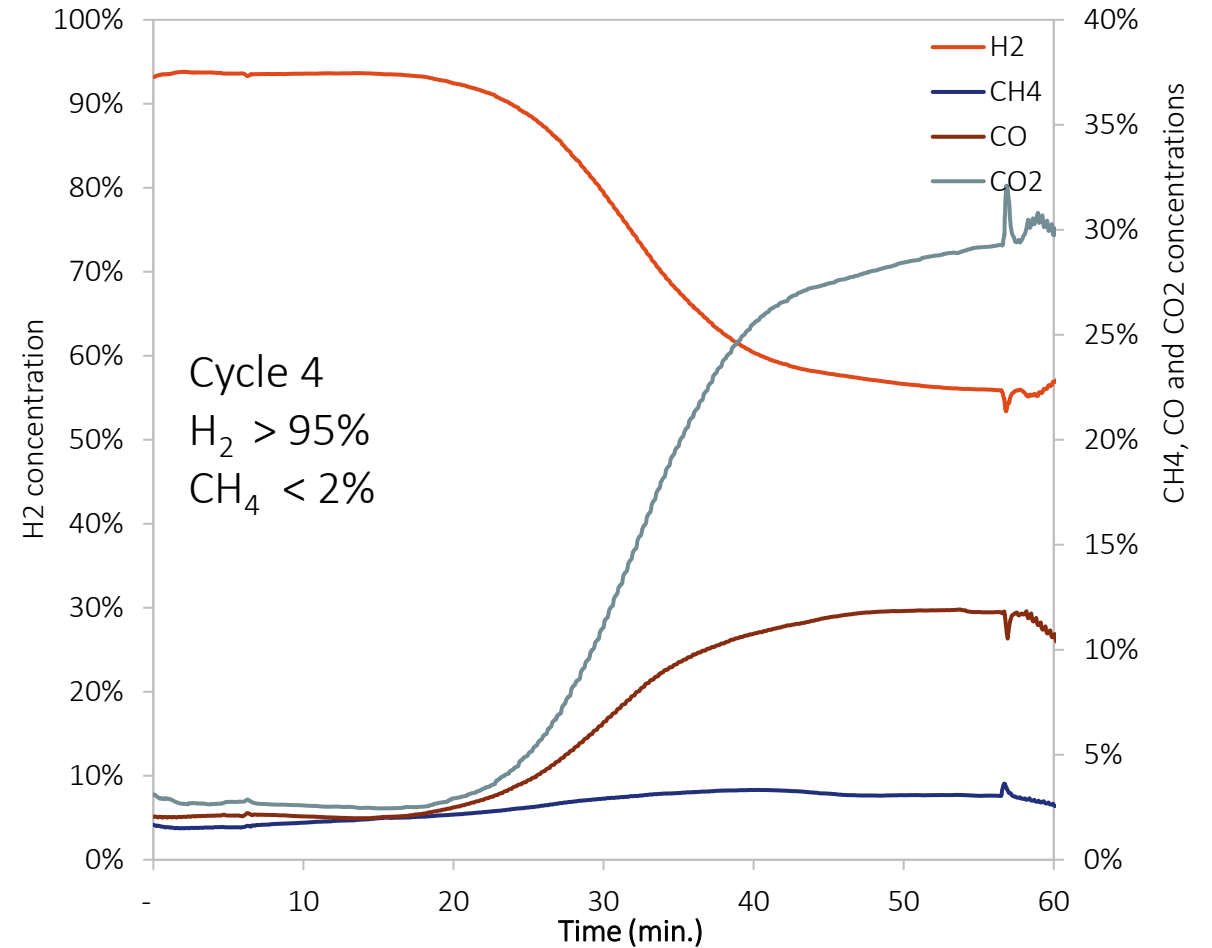
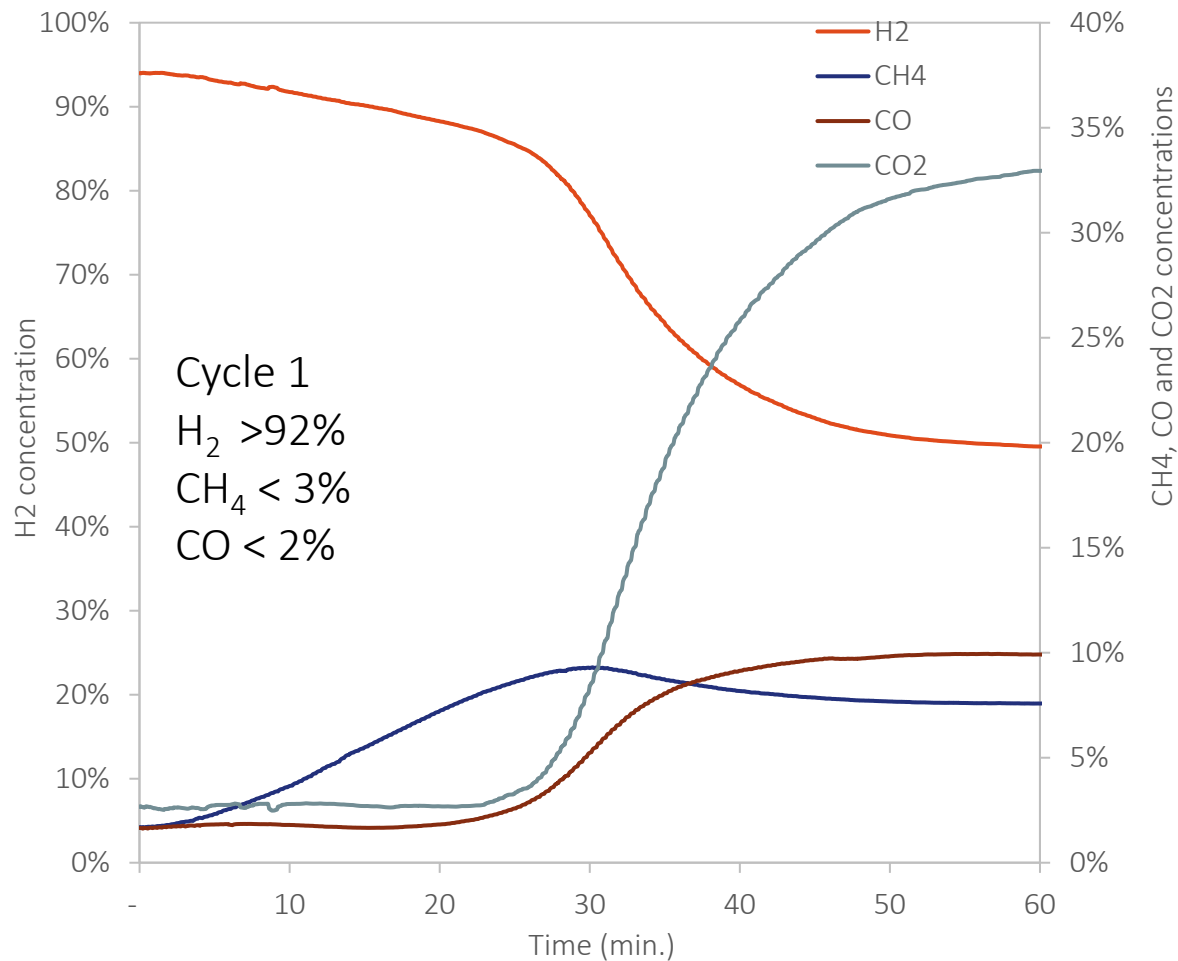
Fluidization velocity: 0.05 m/s

Feedstock and Materials

Gas Feed: (mol%): 41.9% H₂, 10.0% CO, 32.4% CO₂, 10.5% CH₄, 4.4% C₂H₄, 0.9% N₂

Steam R value: 2.0

Materials: 120.7 g CaO sorbent + 12.5 g Converge Cat



SER/SEWGS – With syngas and glycerol - Commercial Catalyst

Process Parameters

Temperature: 600°C

Pressure: 0.23 barg

Fluidization velocity: 0.053 m/s

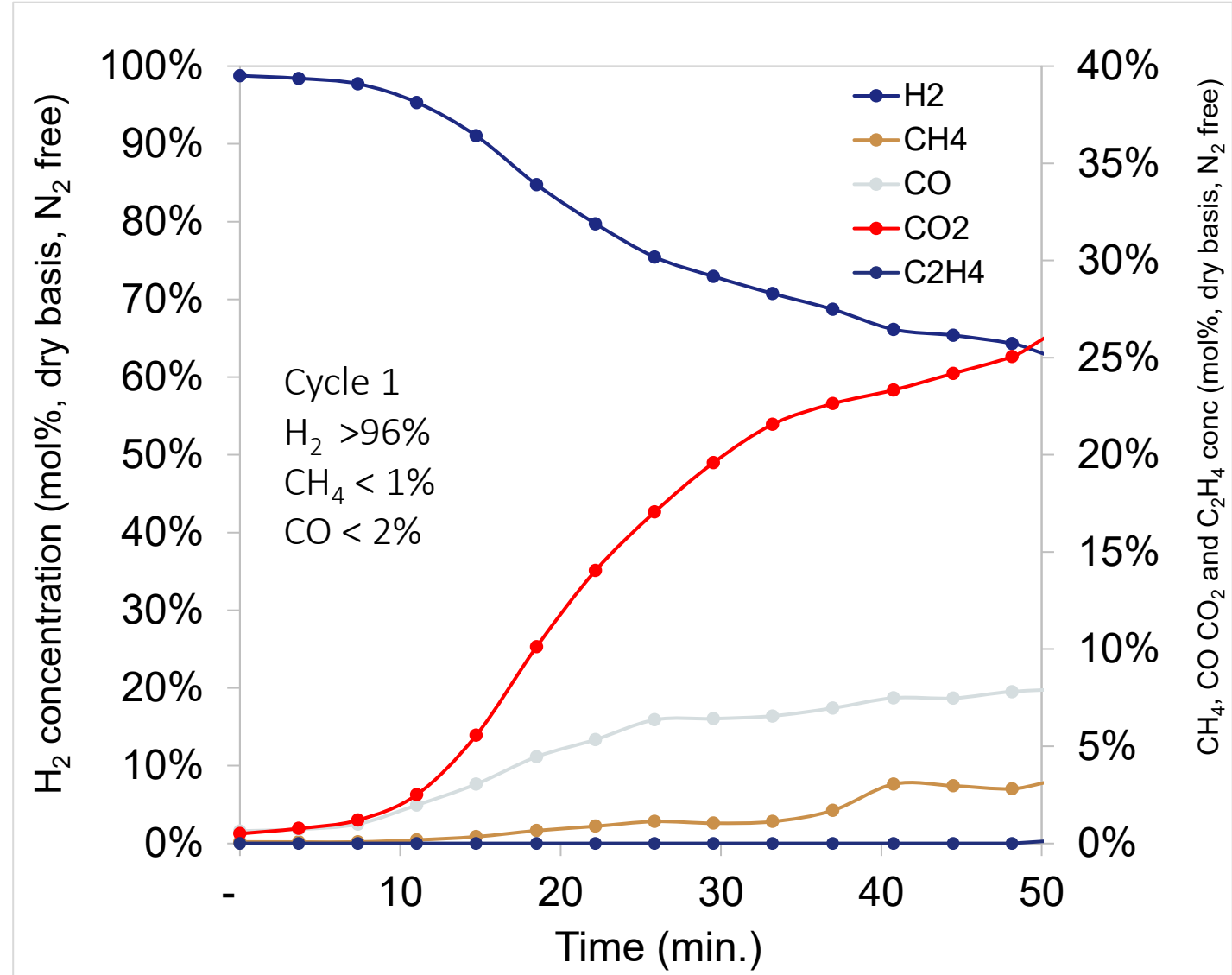
Feedstock and Materials

Gas Feed: (mol%): 41.9% H₂, 10.0% CO, 32.4% CO₂, 10.5% CH₄, 4.4% C₂H₄, 0.9% N₂

Liquid Feed: glycerol 5% of gas feed

Steam R value: 2.0

Materials: 102 g CaO sorbent + 15.4 g Commercial Catalyst



Next Steps

SER – EHC 500h demonstration at the IFE-HyNor Hydrogen Technology Center, Norway

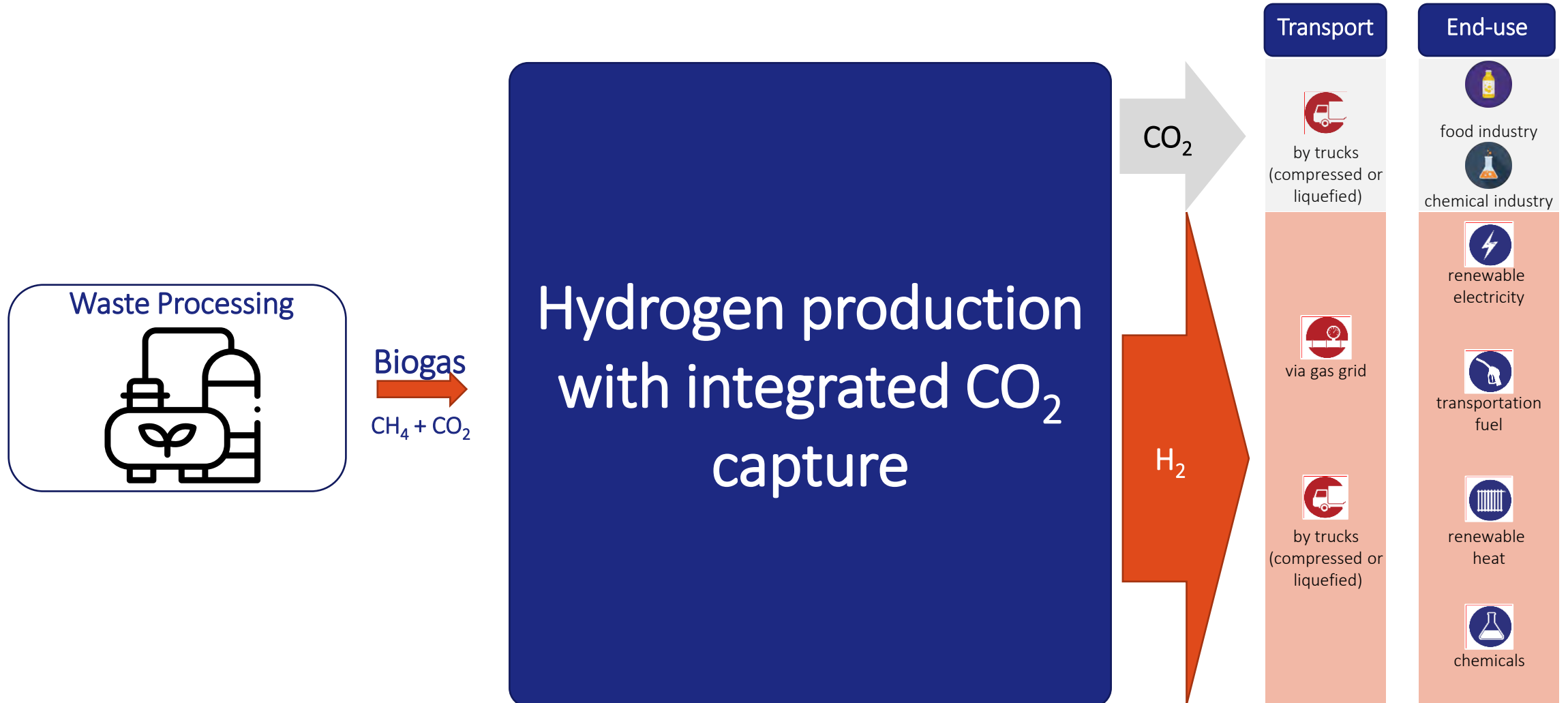




Beyond CONVERGE

Bio4Fuels - Green Hydrogen from Biogas

Sorption Enhanced Reforming - SER

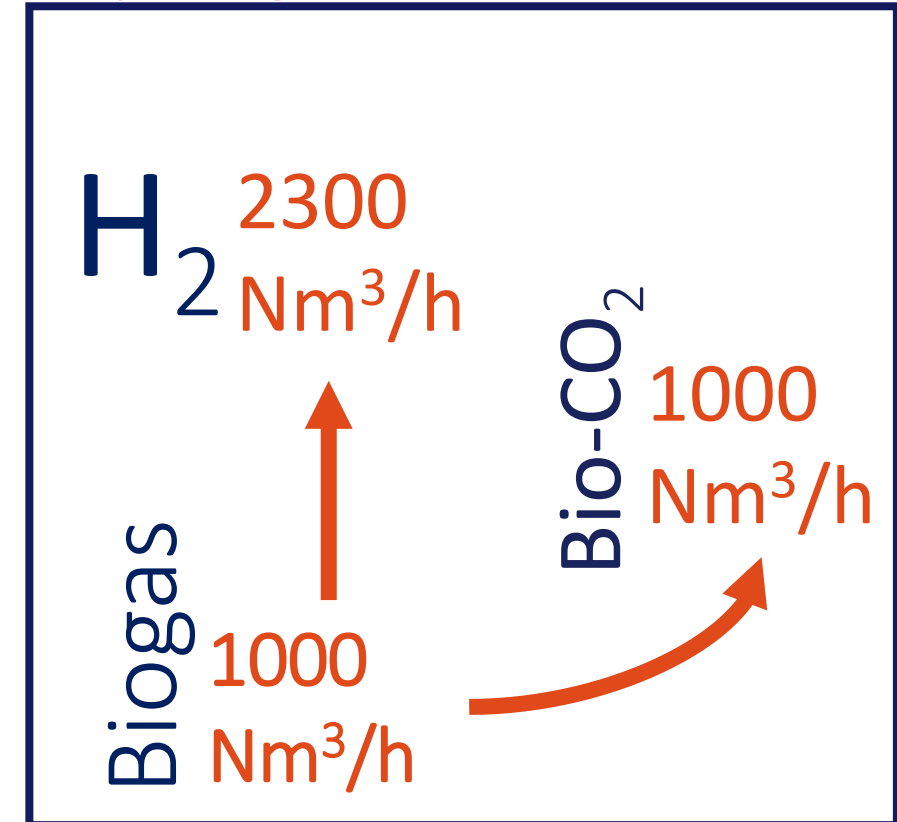


Biogas Upgrading - SER in Numbers

Conversion Efficiency

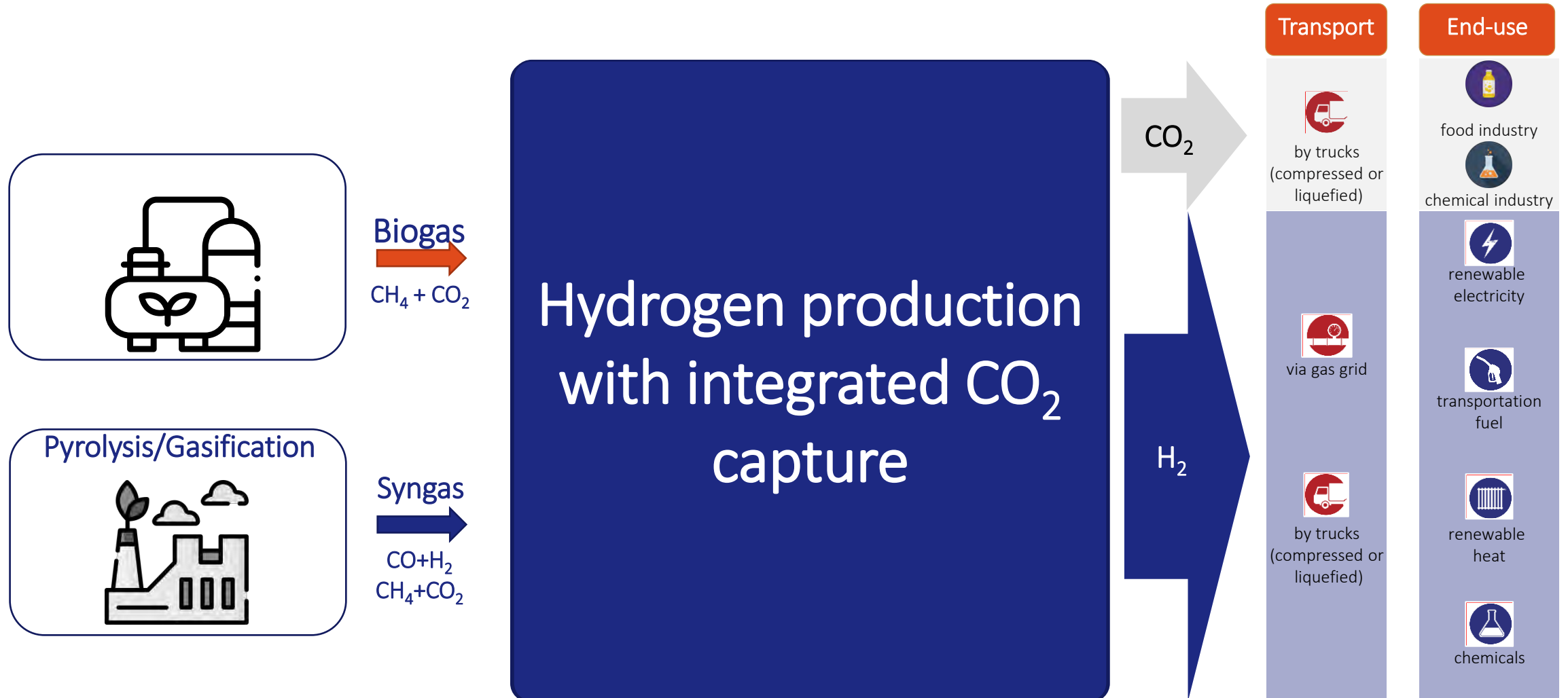
- H_2 yields (>98%) - for CH_4/CO_2 ratios varying between 1 and 2.33.
- CO_2 is over 98% pure.

Hydrogen Production



Green Hydrogen from Syngas and Biogas

Sorption Enhanced Water Gas Shift - SEWGS



The Sorption-Enhanced Reforming/Shift technology (SER/SEWGS) allows to combine the reforming, shift and CO₂ separation in two reactor vessels only providing the following advantages:

- A simpler and intensified process with fewer reactors, leading to a potentially more compact system
- Fewer costly consumables (no shift catalysts, no CO₂ solvent + additives)
- Improved heat integration possibilities due to CO₂ removal at high temperature
- Separated H₂ (>95 vol%) and CO₂ (> 95 vol%) streams that can be recombined for different fuel/chemical synthesis (methanol, DME) or valorised separately for other markets.
- The excess CO₂ can be sequestered (BECCS), used to substitute fossil CO₂ in industrial applications or as chemical, or combined with renewable H₂ to produce electro-fuels in power-to-X concepts for energy storage.
- The produced H₂ can also be used alone, as chemical or as fuel.
- Can reform liquid such as glycerol
- **These advantages result in CAPEX reduction of about 20-30% compared to conventional commercially available technologies.**



The CONVERGE project has received funding from the European Union's Horizon 2020 research and innovation programme under grant agreement N° 818135

Website: www.converge-h2020.eu

Researchgate: **CONVERGE: CarbON Valorisation in Energy-efficient Green fuels**

Linkedin: [showcase/converge-horizon2020](#)

Antonio Oliveira
Researcher

antonio.oliveira@ife.no

CO₂ direct hydrogenation to DME via membrane reactor

S. Poto¹, M. A. Llosa Tanco², D.A. Pacheco Tanaka²,
F. Gallucci¹, M. F. Neira d'Angelo¹

¹Inorganic membranes and membrane reactors, Eindhoven
University of Technology.

²TECNALIA, Basque Research and Technology Alliance (BRTA)

International workshop on CO₂ capture and utilization
16th and 17th February 2021



C2FUEL



EINDHOVEN
UNIVERSITY OF
TECHNOLOGY



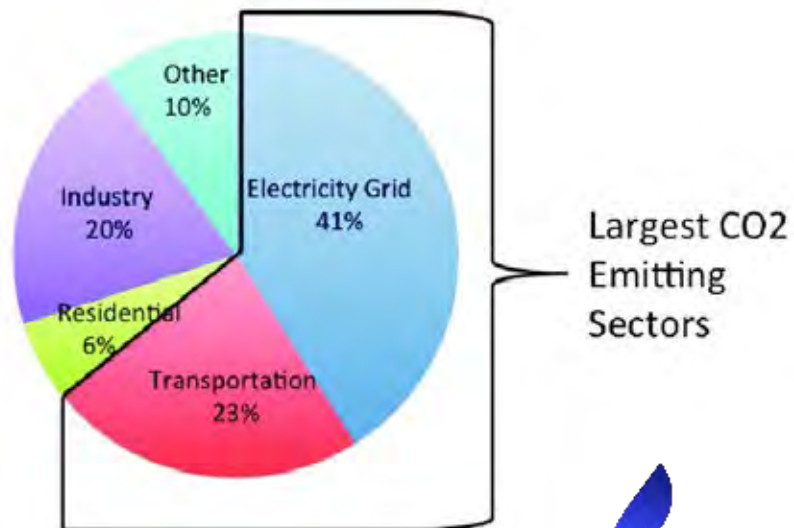
C2FUEL project – Agreement N°83014 - confidential

Introduction

CO₂ emissions and possible solution

CO₂ emission per sector

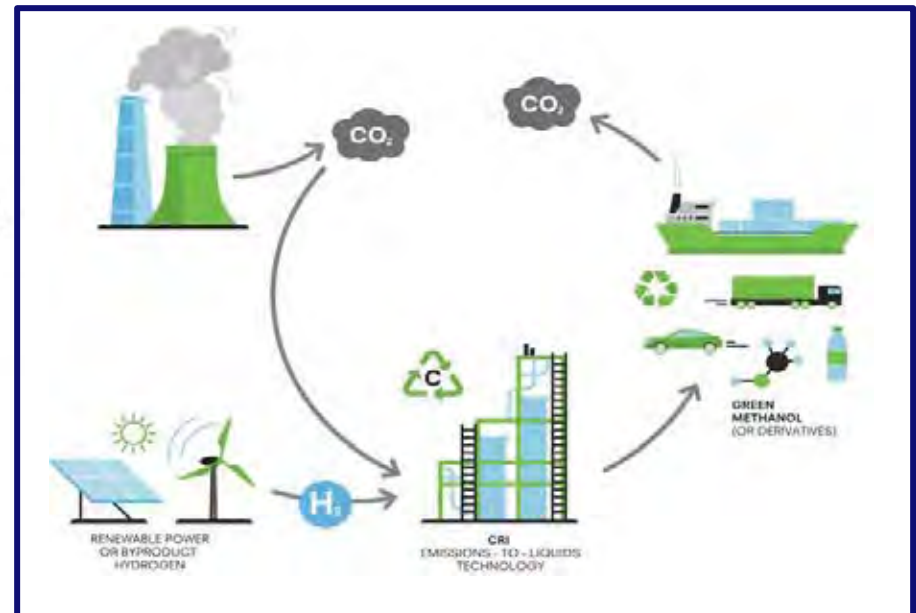
Source: IEA (2017)



Largest CO₂ Emitting Sectors


C2FUEL

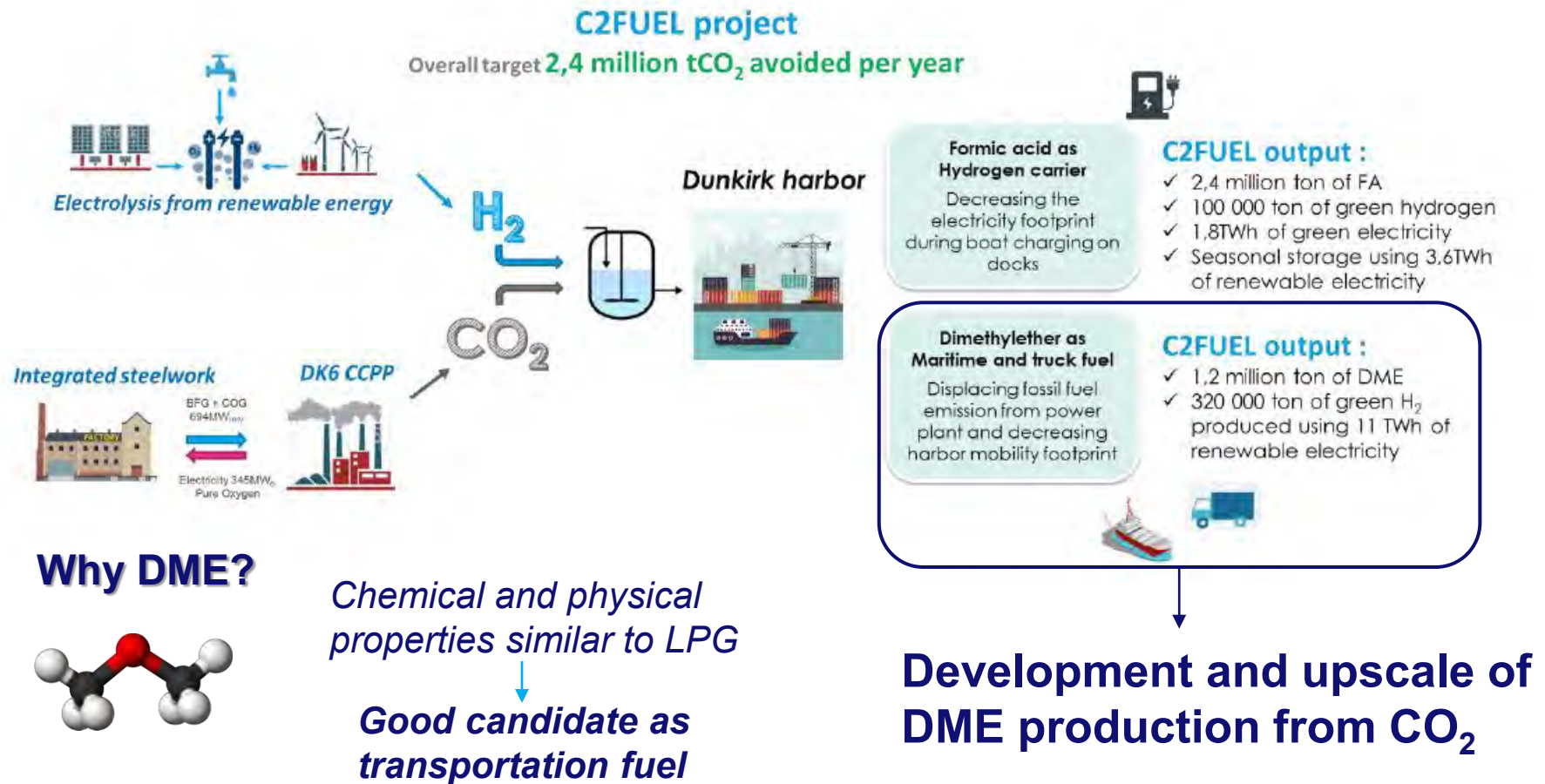
How to reduce emissions? CO₂ capture and reconversion



European Union's Horizon 2020

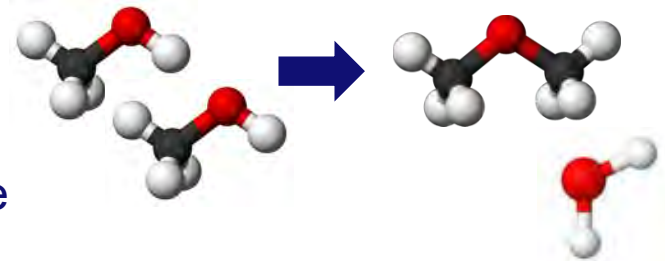
Introduction

CO₂ emissions and possible solution



Introduction

DME production



Indirect route

Methanol synthesis over a Cu-ZnO-Al₂O₃ catalyst



Methanol dehydration to DME over an acid catalyst (HZSM-5)

Direct route

DME synthesis over a Cu-ZnO-Al₂O₃/HZSM-5 bifunctional catalyst

- ✓ One reactor
- ✓ Less limited by thermodynamics
- ✗ More difficult separation

Nowadays the main source is syngas



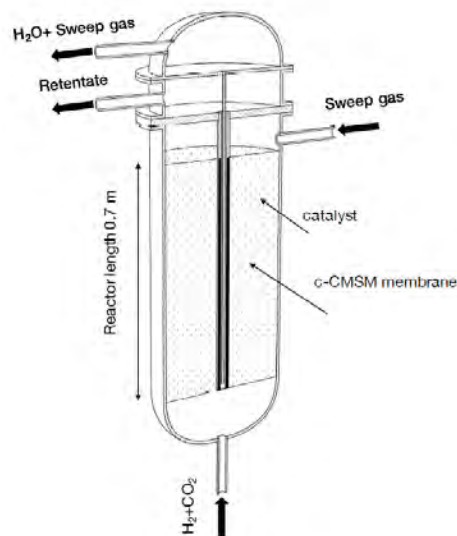
- Syngas production causes CO₂ emissions
- Depending on syngas composition, CO₂ can be produced

Introduction

Direct DME synthesis from CO₂

1. CO₂ hydrogenation: $\text{CO}_2 + 3\text{H}_2 \rightleftharpoons \text{CH}_3\text{OH} + \text{H}_2\text{O}$ $\Delta H_0 = -49.5 \text{ kJ/mol}$
2. Reverse WGS: $\text{CO}_2 + \text{H}_2 \rightleftharpoons \text{CO} + \text{H}_2\text{O}$ $\Delta H_0 = 41.2 \text{ kJ/mol}$
3. Methanol dehydration: $2\text{CH}_3\text{OH} \rightleftharpoons \text{CH}_3\text{OCH}_3 + \text{H}_2\text{O}$ $\Delta H_0 = -23.4 \text{ kJ/mol}$

Process conditions 200-250 °C - 20-50 bar



Membrane reactor

Membrane for selective water removal

- ✓ Reaction and separation in the same unit
- ✓ Overcome thermodynamic limitations
- ✓ Avoid catalyst deactivation due to water adsorption

Introduction

Membrane requirements:

Hydrophilicity

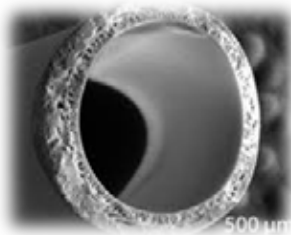


Stability
(thermal, mechanical,
chemical)



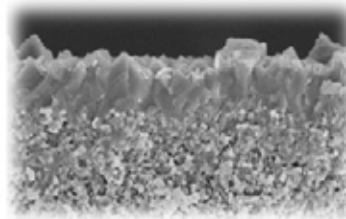
High vapor/gas
selectivity

Polymeric membranes



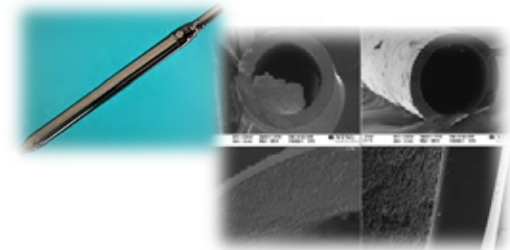
- High permeability
- Low stability
(thermal-mechanical)

Ceramic membranes (zeolite, alumina, etc.)



- High permeability/selectivity
- Low stability
(hot humid environment)

Carbon membranes



- Possible hydrophilicity
- Stability
- Possibility to tune properties

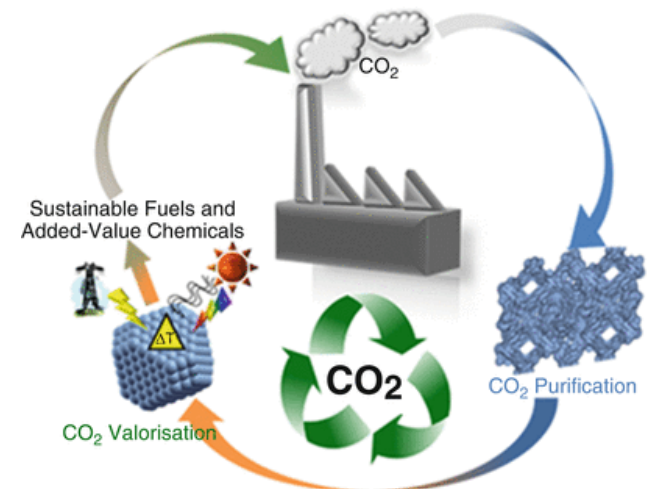
Introduction

Project goals:

1. Development of carbon membranes (TECNALIA & TU/e)
 - Synthesis of Al-CMSM with improved hydrophilicity
 - Characterization of Al-CMSM
2. Development of a 1D-phenomenological membrane reactor model (TU/e)
 - Effect of membrane properties on reactor performance
 - Optimize the operating conditions
 - Propose a cooling strategy

Main objective:

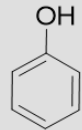
Promote a valid alternative for CO₂ valorization



Development of Al-supported Carbon Molecular Sieve Membranes

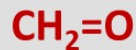
Carbon molecular sieve membranes

Development and manufacturing Al-CMSM



Phenol

+



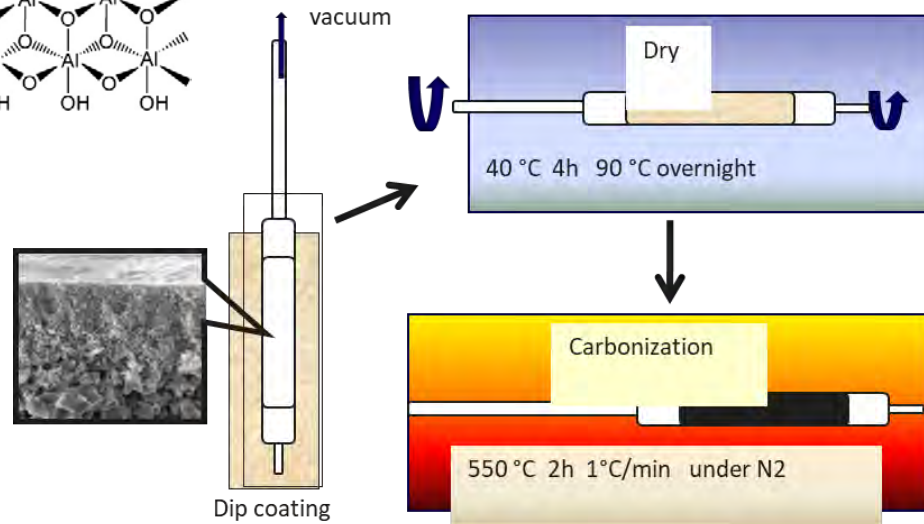
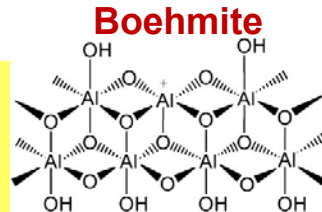
Formaldehyde

Phenolic resins

Novolac : acidic media and Formaldehyde /Phenol ≈ 0.75 -0.85

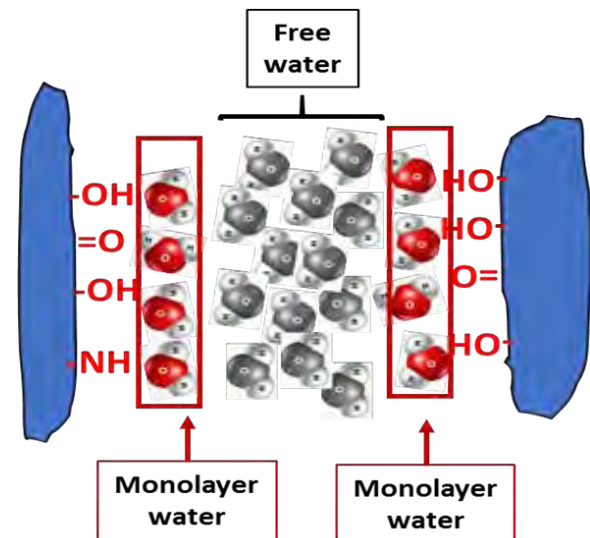
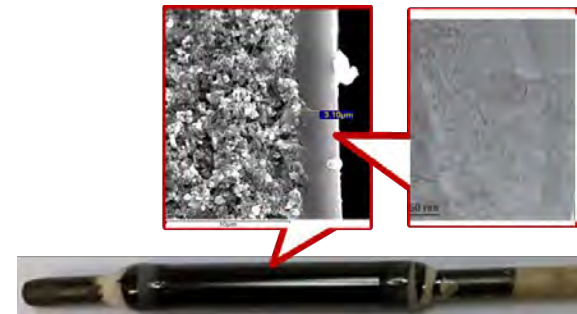
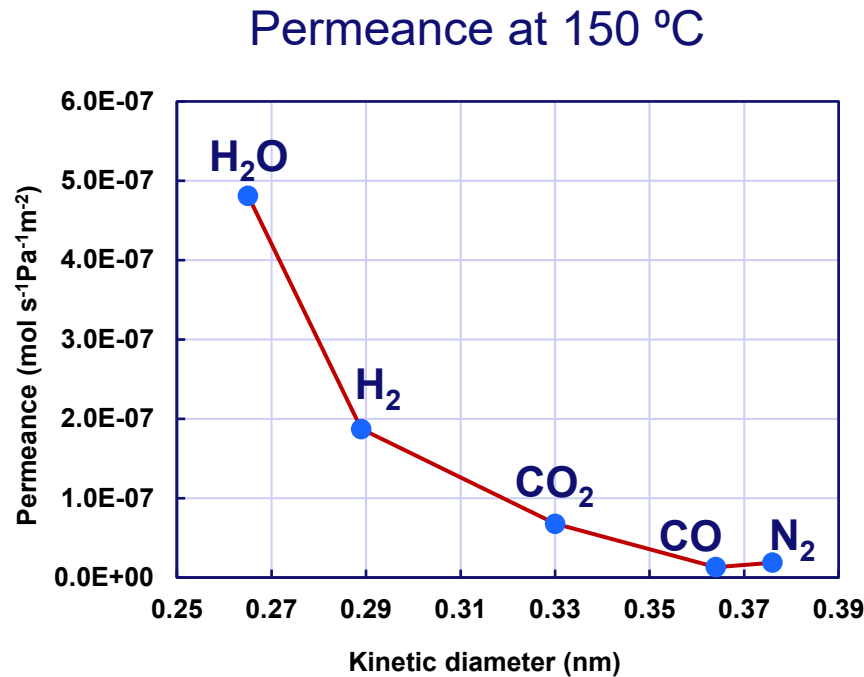
Dipping solution

| | |
|-------------------------------|--------------|
| Boehmite nanoparticles | 0,8 % |
| Novolac resin | 13,0 % |
| Formaldehyde | 2,0 % |
| Ethylenediamine | 0,6 % |
| Solvent | NMP |



Carbon molecular sieve membranes

Development and manufacturing AI-CMSM

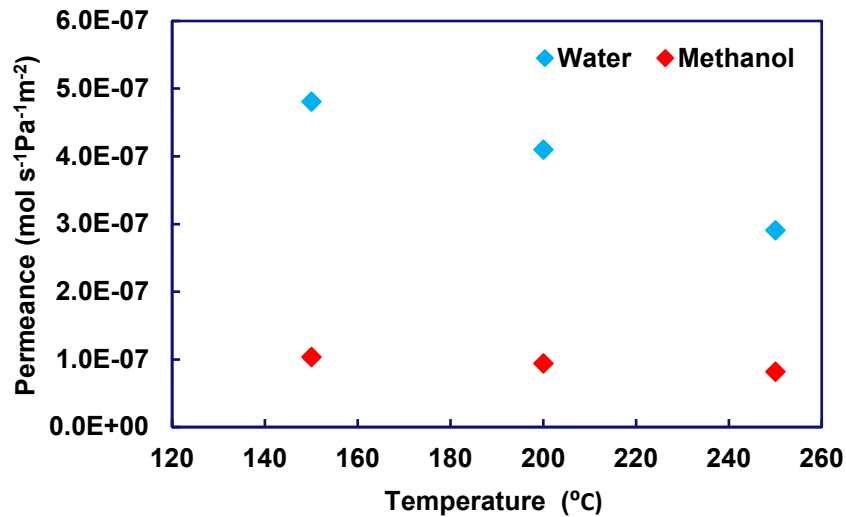


Carbon molecular sieve membranes

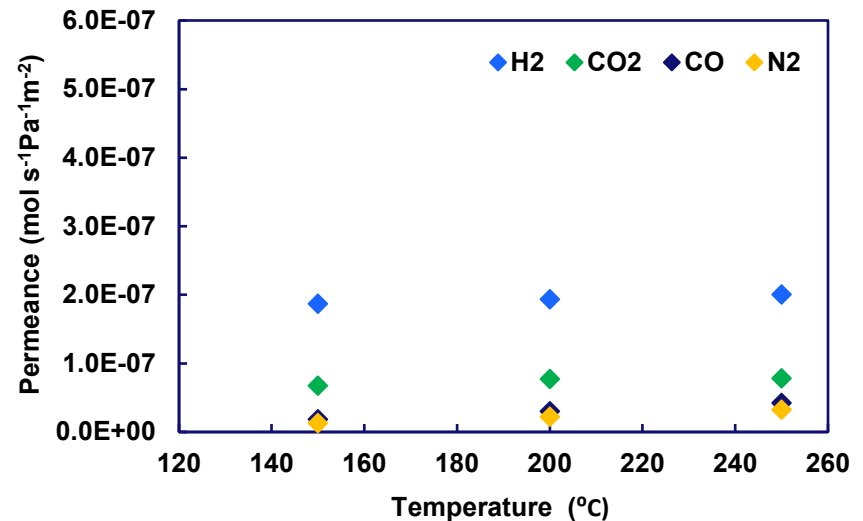
Development and manufacturing AI-CMSM

Single gas-vapor permeation experiment at $\Delta P = 3$ bar

Vapor permeation



Gas permeation



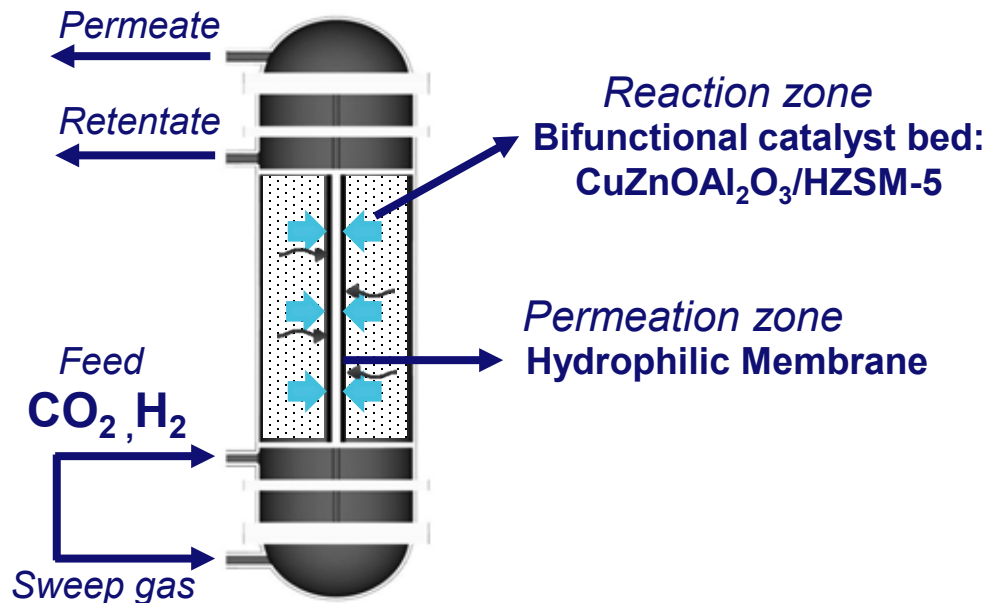
Water has the highest permeance at each condition

Membrane reactor model for the CO₂ hydrogenation to DME

Membrane reactor model

Reactor features and model hypotheses:

Fixed bed membrane reactor



Trans-membrane flux :

$$J_i = \rho_i \cdot (P_i^R - P_i^P)$$

Sweep gas ($\text{CO}_2 + \text{H}_2$)

Water removal Heat removal
Co-current configuration

Model equations



Mass
balances



Energy
balances



Momentum
balance

- Reaction
- Permeation

- Reaction (Ergun)
- Permeation (No P drops)

Membrane reactor model

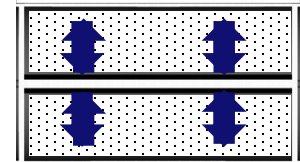
Model equations and approach:

Reactor performances

$$X_{CO_2} = \frac{F_{CO_2,0}^R - F_{CO_2}^R + F_{CO_2,tmb}}{F_{CO_2,0}^R + F_{CO_2,tmb}^*}$$

CO₂ transmembrane flow

$$F_{CO_2,tmb} = F_{CO_2,0}^P - F_{CO_2}^P$$



$$Y_i = \frac{N_{c,i}(F_i^R + F_i^P)}{F_{CO_2,0}^R + F_{CO_2,tmb}^*}$$

$$F_{CO_2,tmb}^* = 0 \quad \text{if } F_{CO_2,tmb} \leq 0 \quad \text{Reactant loss}$$

$$F_{CO_2,tmb}^* = F_{CO_2,tmb} \quad \text{if } F_{CO_2,tmb} > 0 \quad \text{Reactant cofeeding}$$

$$WR = \frac{F_{H_2O}^P}{F_{H_2O}^P + F_{H_2O}^R} \longrightarrow \text{Amount of water removal}$$

1. Assessment of the membrane optimal properties (permeability and selectivity)



Isothermal conditions

2. Optimization of the operating conditions



Sweep gas for heat management

$T_{in}^R \quad T_{in}^P$

$$\Delta P = P^R - P^P$$

$$SW = F_{in}^P / F_{in}^R$$

H₂:CO₂

Influencing the driving force for permeation

$P_{in}^R = 40 \text{ bar}$

$T_{avg}^R = 200^\circ\text{C}$

Fixed conditions

Membrane reactor model

Assessment of the membrane optimal properties:

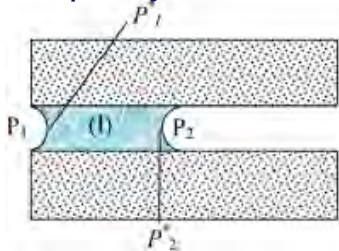
Definitions:

Permeance \wp_i [$\text{mol}/(\text{Pa} \cdot \text{m}^2 \cdot \text{s})$]

Selectivity $S_{H_2O,i} = \wp_{H_2O} / \wp_i$

Main mechanism of water and methanol permeation:

Capillary condensation



Main mechanism of gases permeation:

Molecular sieving

Kinetic diameters

$H_2 < CO_2 \approx CO < DME$

Procedure:

Ideal membrane



Real membrane

H_2O and H_2 permeating

All the species permeating

Hypotheses:

1. CO_2 and CO same permeance
2. H_2O / CH_3OH selectivity ≥ 1 (slightly)
3. DME is not permeating (largest size and $T_c = 128^\circ\text{C}$)

| Operating conditions | | | |
|----------------------|---------------------|------------------|---------------------------|
| T^R and T^P | 200°C | SW | 3 |
| P^R | 40 bar | $H_2:CO_2$ | 3 |
| ΔP | 0 bar | $\Phi_{H_2,0}^R$ | $1 \text{ Nm}^3/\text{h}$ |

Membrane reactor model

Assessment of the membrane optimal properties:

According to the assumption made **+** Criteria used

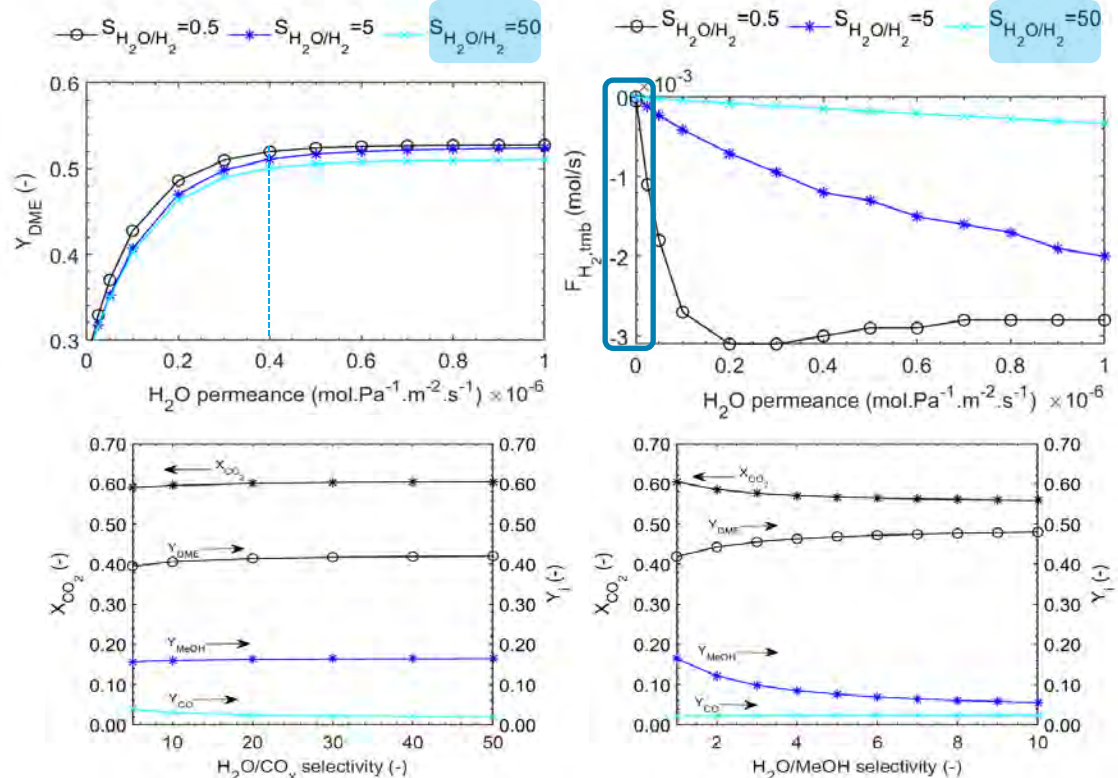
1. Maximize water permeation flow
2. Minimize loss and co-feeding of reactants
3. Minimize methanol and CO permeation

| Membrane optimal properties | |
|---|-------------------|
| ρ_{H_2O} (mol/(Pa · m ² · s)) | $4 \cdot 10^{-7}$ |
| S_{H_2O/H_2} | 50 |
| S_{H_2O/CO_2} | 30 |
| $S_{H_2O/CO}$ | 30 |
| S_{H_2O/CH_3OH} | 10 |
| $S_{H_2O/DME}$ | ∞ |

Good agreement with:

- ceramic membranes
- polymeric membranes

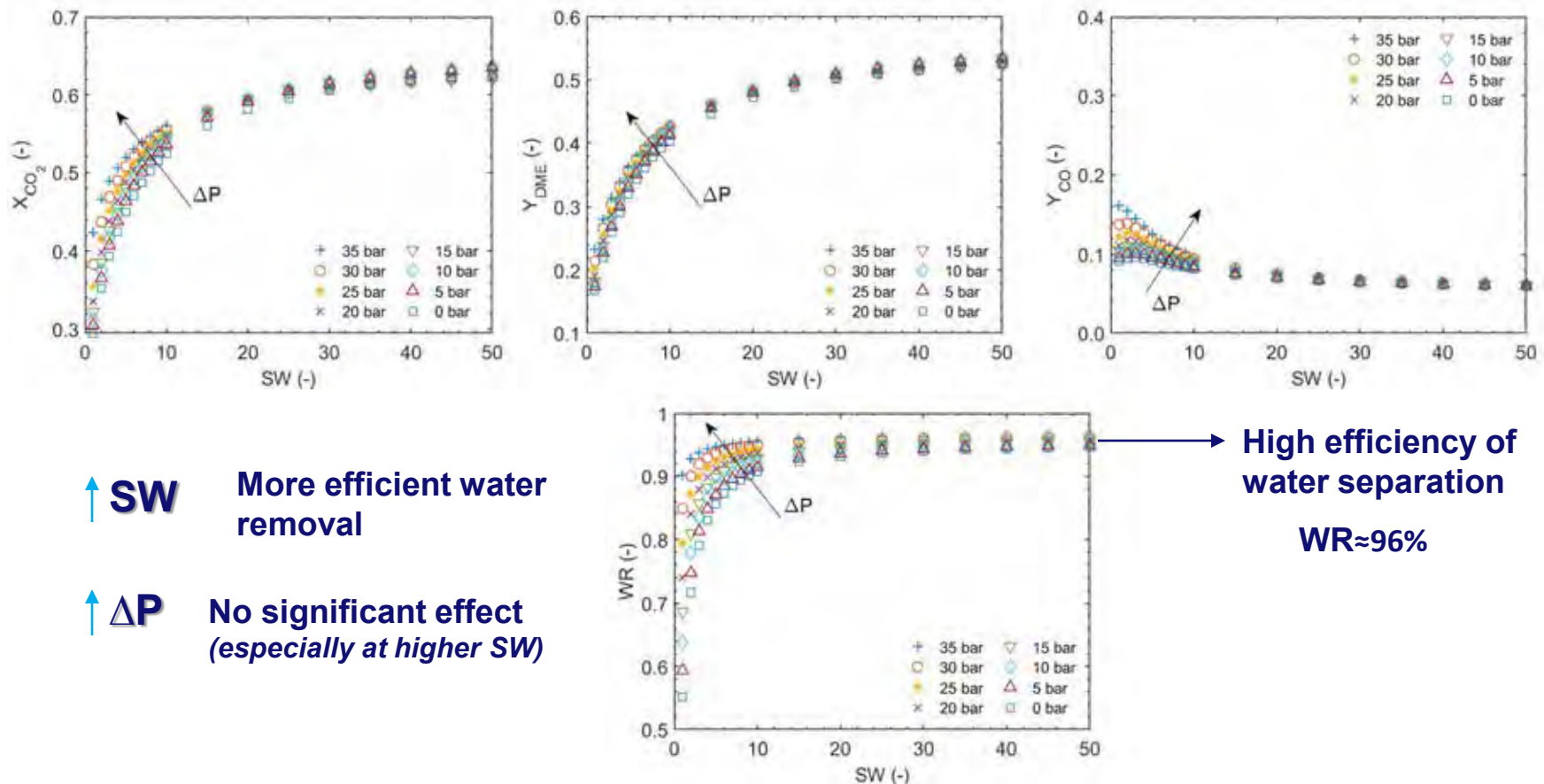
Not enough data available
for carbon membranes



Membrane reactor model

Optimization of the operating conditions:

Effect of SW and ΔP on reaction performance



↑ **SW**

More efficient water removal

↑ **ΔP**

No significant effect (especially at higher SW)

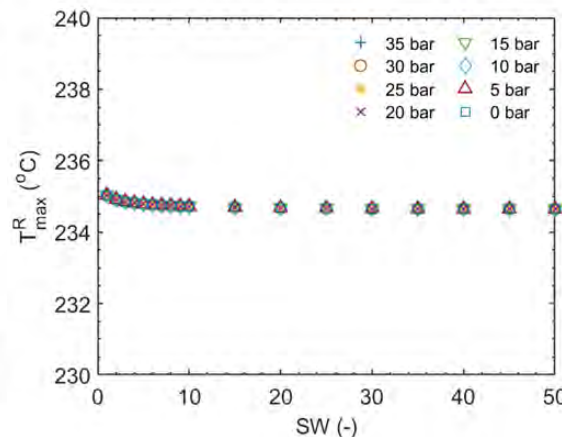
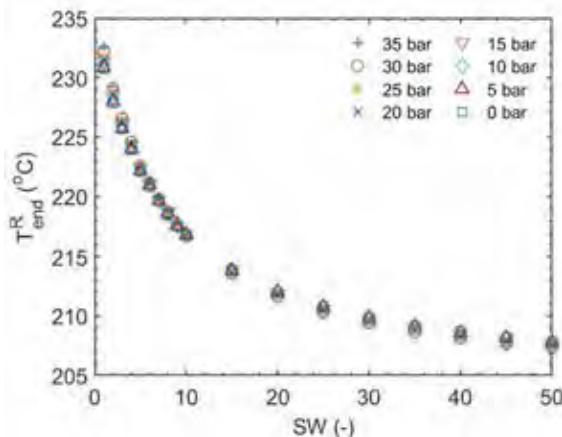
High efficiency of water separation

WR≈96%

Membrane reactor model

Optimization of the operating conditions:

Effect of SW and ΔP on heat management



↑ **SW** More heat removal
↑ **ΔP** No significant effect
(especially at higher SW)

T-profile optimization criteria:

- T lower than 270-300°C (catalyst deactivation due to sintering)
- As low as possible (desired reactions: exothermic, undesired reactions: endothermic)
- Lower T guarantees higher water permeation and lower gas permeation
- Higher than 190-200 °C (catalyst activation temperature)

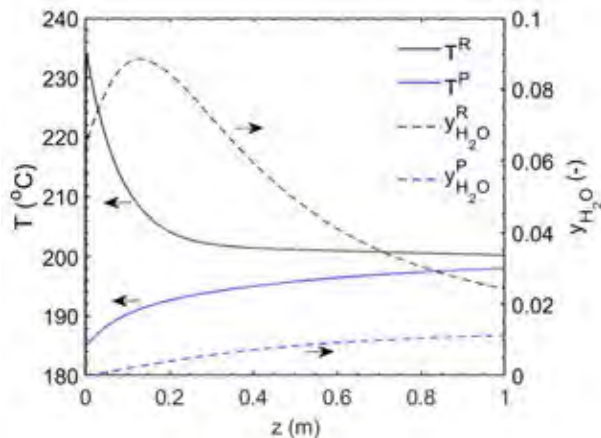
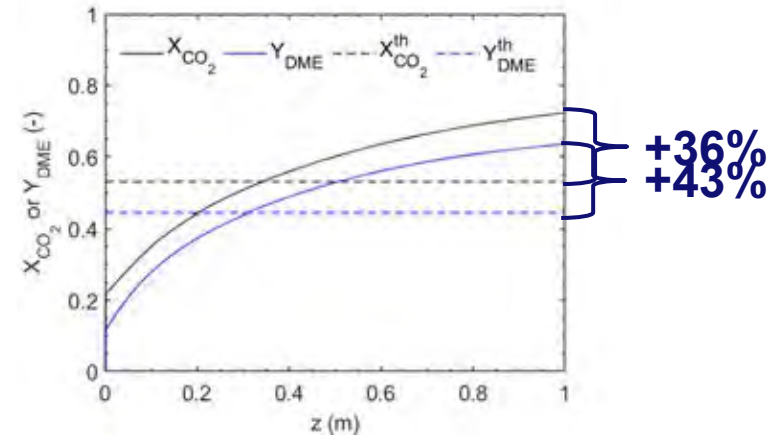
$$T_{in}^P = 185 \text{ }^{\circ}\text{C} \quad T_{in}^R = 200 \text{ }^{\circ}\text{C} \quad SW = 20 \quad \Delta P = 5 \text{ bar}$$

Optimize heat & water removal

Membrane reactor model

Membrane reactor optimal performance:

| Optimal conditions | | Fixed conditions | |
|--------------------|--------|------------------|---------------------------|
| SW | 20 | $\Phi_{H_2,0}^R$ | $1 \text{ Nm}^3/\text{h}$ |
| ΔP | 5 bar | P_{in}^R | 40 bar |
| $H_2:CO_2$ | 3.5 | T_{in}^R | 200 °C |
| T_{in}^P | 185 °C | | |



- Temperature and water concentration show similar profiles
- The efficiency of water removal is 96%

Conclusions

1. The **AI-CMSM** showed high water permeance and vapor/gas selectivity
2. There is no need to have the highest **membrane performance**.
An optimum has been found for water permeance and selectivity.
3. The **sweep gas** promotes both **heat** and **water removal**.
The temperature profile can be optimized thanks to the sweep gas inlet temperature
4. The **cocurrent configuration** has several positive effects:
 - Highest driving force for heat and water removal is at the entrance
 - Water back permeation is avoided
5. The operating conditions have been optimized. Considerations are:
 - There is no need to have a high ΔP
 - A sweep gas is used instead, with a higher flow rate. The sweep gas can be recirculated.
6. The **thermodynamic limitations** have been overcome
(with a 96% efficiency of water removal)



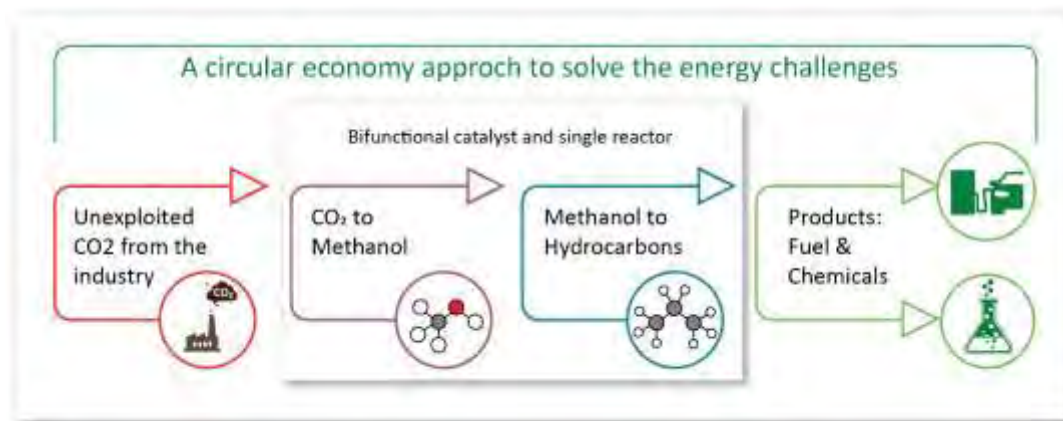
Any question?



This project has received funding from the European Union's Horizon 2020 research and innovation programme under grant agreement No 838014 (C2Fuel project).

COZMOS

Efficient CO₂ conversion over multisite Zeolite-Metal nanocatalysts to fuels and Olefins



Catalyst development within the COZMOS project

Unni Olsbye, University of Oslo

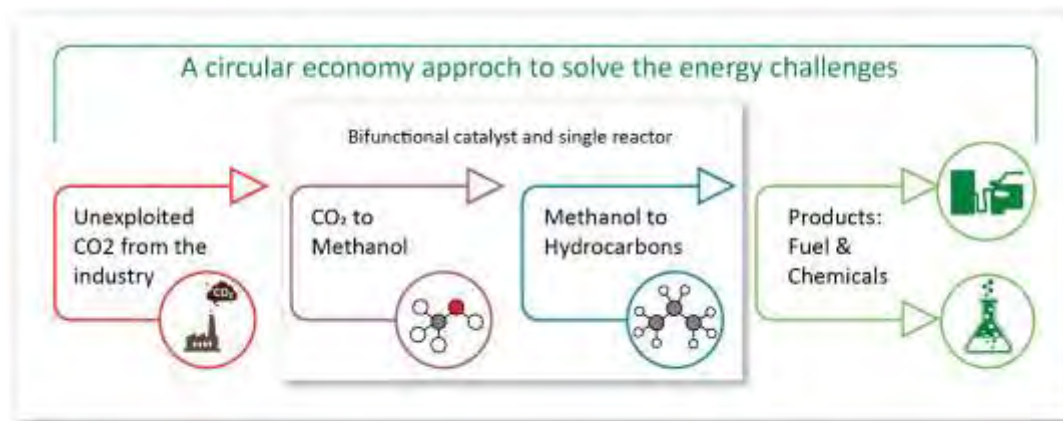


COZMOS: Efficient CO₂ conversion over multisite Zeolite-Metal nanocatalysts to fuels and Olefins.

This project has received funding from the European Union's Horizon 2020 research and innovation programme under Grant Agreement No. 837733.

COZMOS

Efficient CO₂ conversion over multisite Zeolite-Metal nanocatalysts to fuels and Olefins



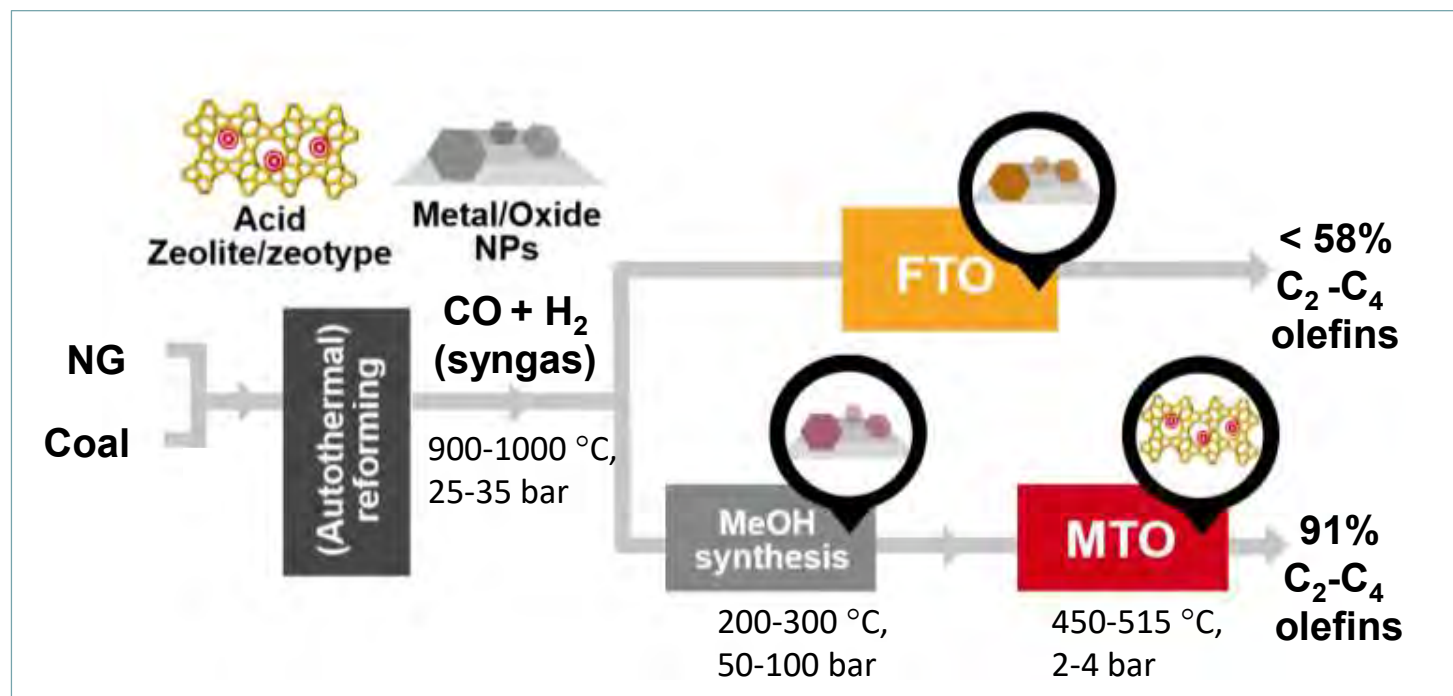
Catalyst development within the COZMOS project

Unni Olsbye, University of Oslo



COZMOS: Efficient CO₂ conversion over multisite Zeolite-Metal nanocatalysts to fuels and Olefins.

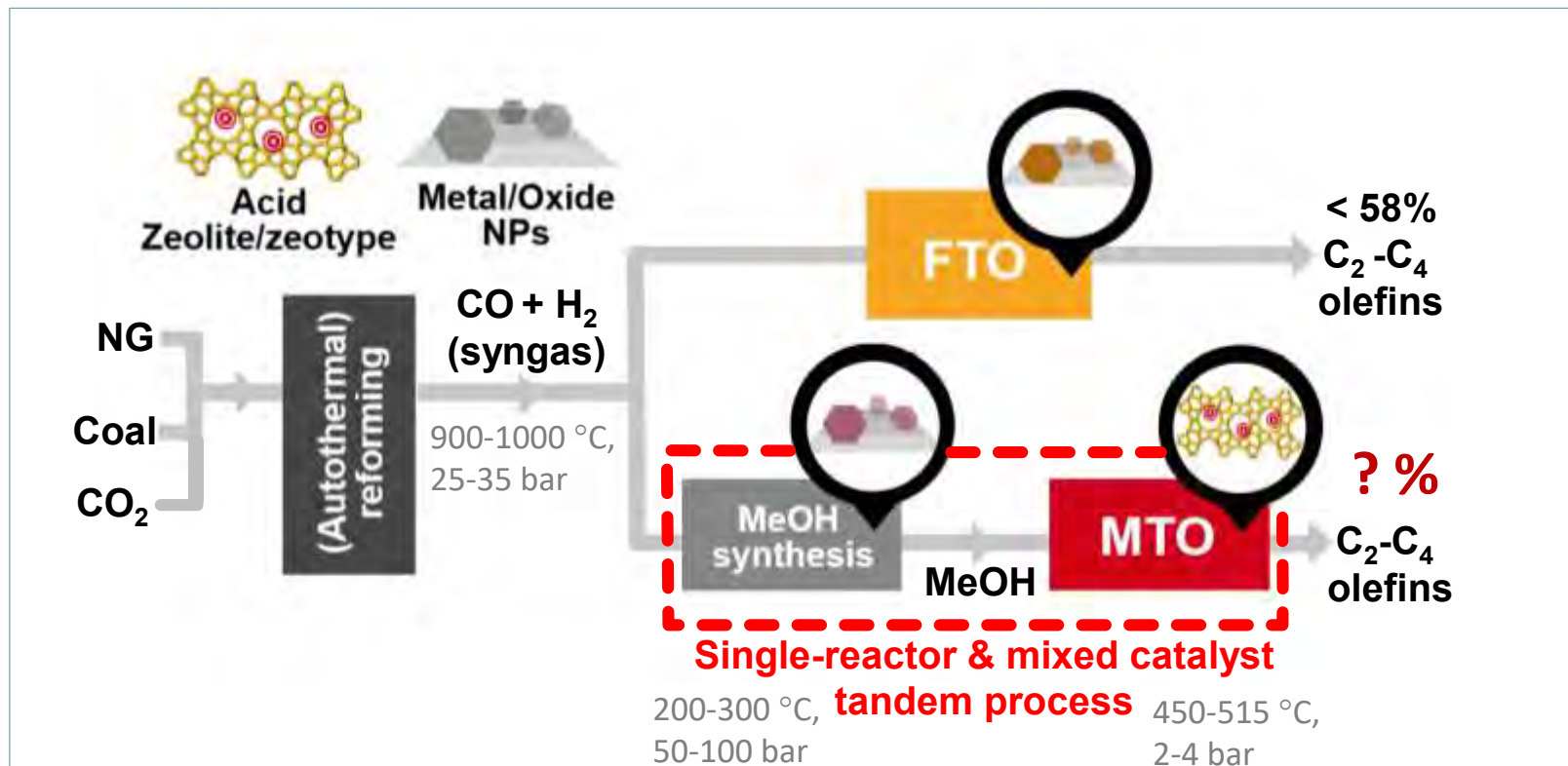
This project has received funding from the European Union's Horizon 2020 research and innovation programme under Grant Agreement No. 837733.



H.M. Torres Galvis, K.P. de Jong *ACS Catalysis* **2013**, 3, 2130-2149.

J.Q. Chen, A. Bozzano, B. Glover, T. Fuglerud, S. Kvisle *Cat. Today* **2005**, 106, 103-107.

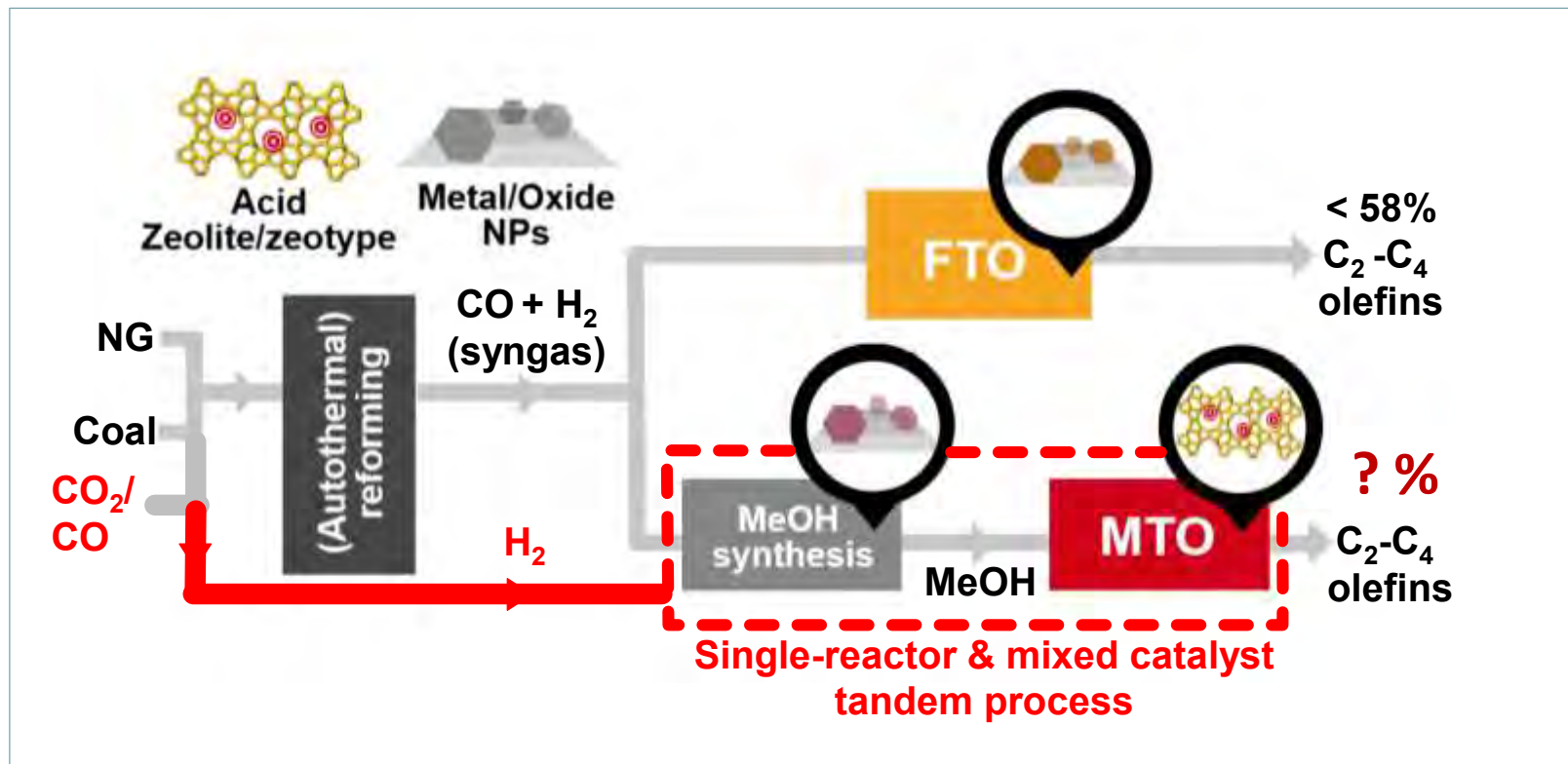




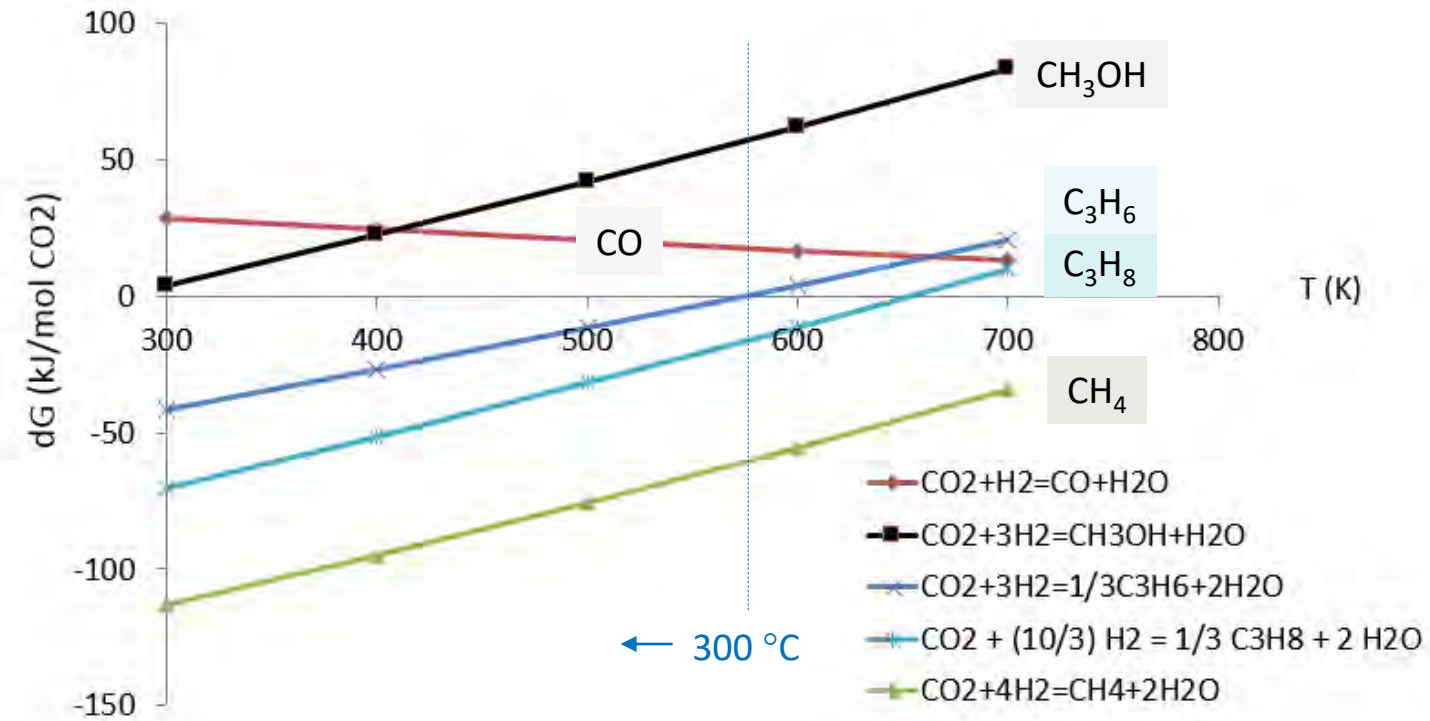
F. Jiao, X. Bao et al. *Science* **2016**, 351, 1065-1068.

K. Cheng, Y. Wang et al. *Angew. Chemie Int. Ed.* **2016**, 55, 4725-4728.





Thermodynamic considerations

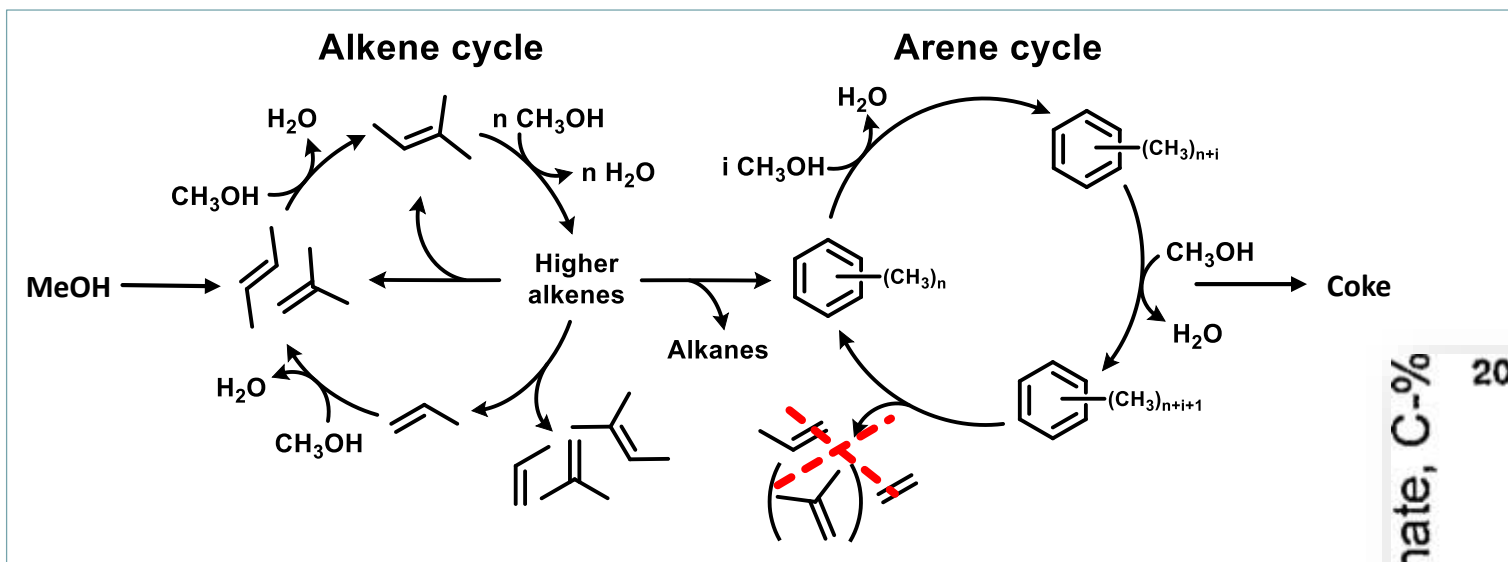


Thermodynamic data from TRC Table

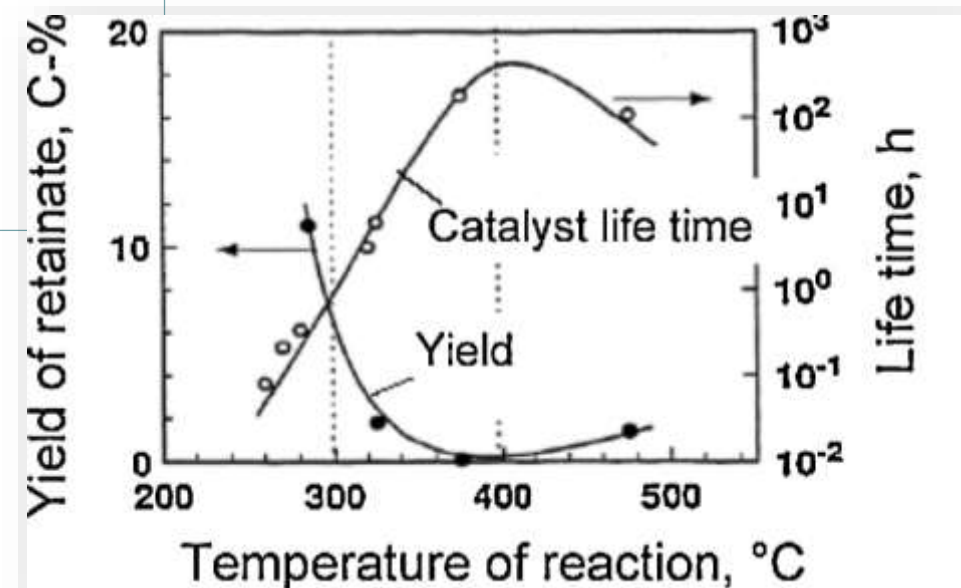


Tandem catalysis challenges

- The temperature gap -



Olsbye, U. et al. *Angew. Chemie Int. Ed.* **2012**, 51 (24), 5810-5831.



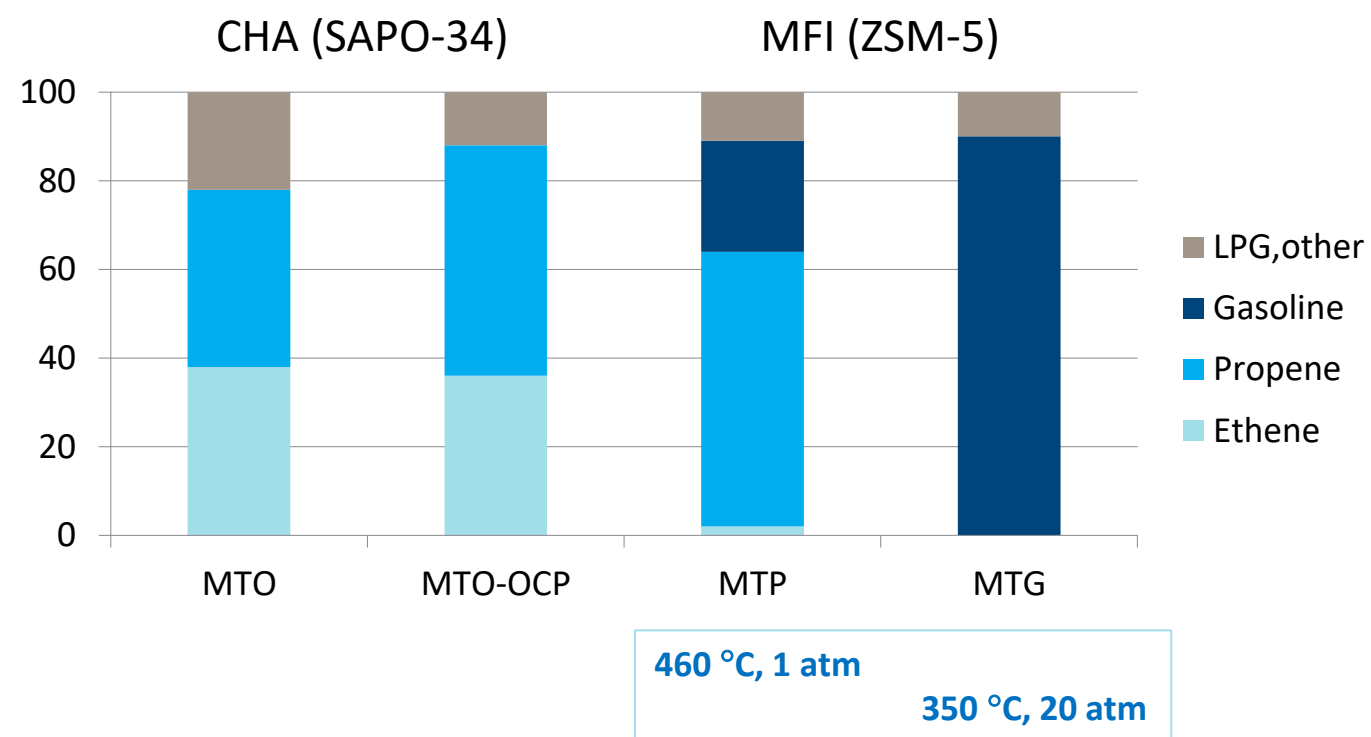
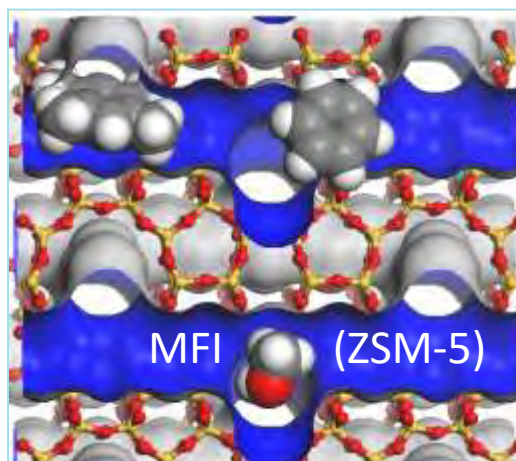
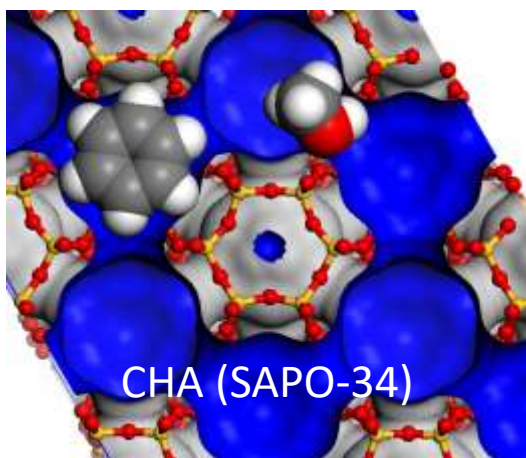
Schulz, H., *Cat. Today*, **2010**, 154, 183-194



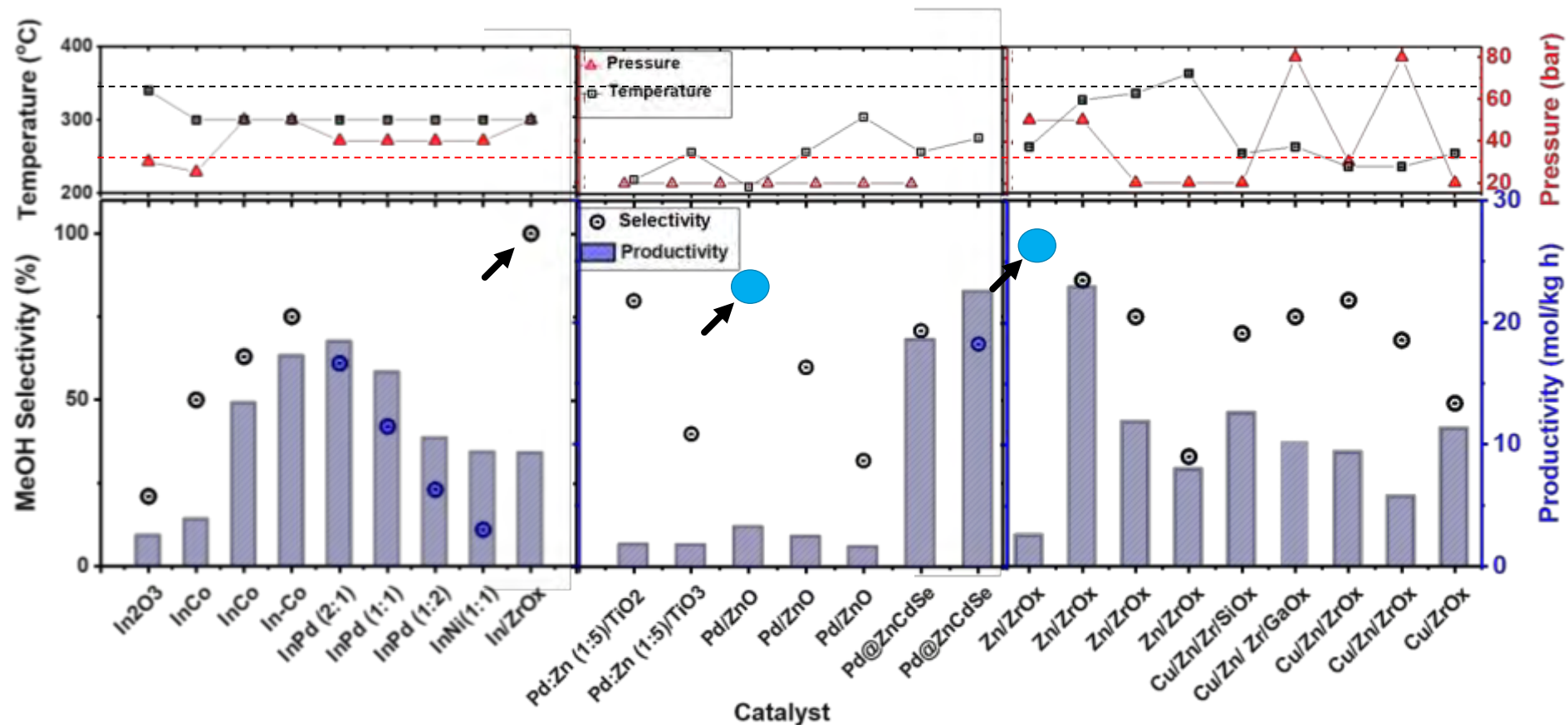
COZMOS: Efficient CO₂ conversion over multisite Zeolite-Metal nanocatalysts to fuels and OlefinS.

This project has received funding from the European Union's Horizon 2020 research and innovation programme under Grant Agreement No. 837733.

Tandem catalysis: Methanol to propane/propene candidates



Tandem catalysis: CO₂ hydrogenation candidates



P. Gao et al., Nature Chem. 2017, 9, 1019
 US Patent application nb 62/599,978, KAUST
 B. Anastasiya et al. ChemRxiv., 2018
 J. L. Snider et al., ACS Catal., 2019, 9, 3400
 O. Martin et al., Angew. Chem. Int. Ed. 2016, 55, 6261

H. Bahruji et al., Faraday discuss. 2017, 197, 309
 H. Bahruji et al., J. Catal. 2016, 343, 133-146
 SCE Tsang et al, Green Chem., 2017, 270

J. Wang et al., Science Advances 2017, 3, e1701290
 T. Phongamwong et al., Engineering Journal, 2017, 316, 692
 J. Sloczynski et al., Appl. Catal. A, 2006, 310, 127 & 2004, 278, 11
 Y Wang et. al. Nature Comm., 2019, 10, 1166
 J. Liu et al., Appl. Catal. A, 2001, 218, 113



COZMOS: Efficient CO₂ conversion over multisite Zeolite-Metal nanocatalysts to fuels and OlefinS.

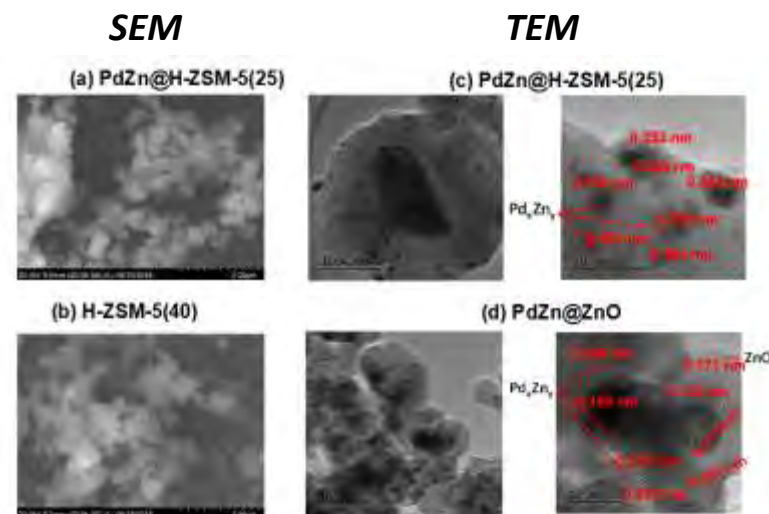
This project has received funding from the European Union's Horizon 2020 research and innovation programme under Grant Agreement No. 837733.

Case 1: PdZn/ZnO + ZSM-5

PdZn@ZnO: Pd salt was impregnated onto ZnO, mixed with H-ZSM-5 and pretreated in H₂ flow at 400 °C for 1 h.

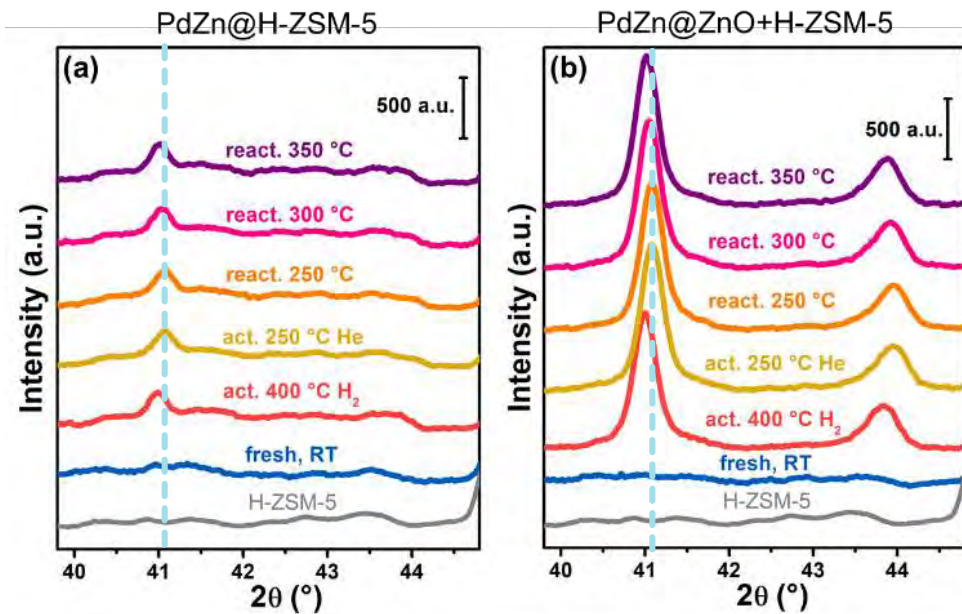
PdZn@H-ZSM-5: Pd complex was grafted onto mesoporous H-ZSM-5, followed by reduction and Zn grafting, and reduction in H₂ at 500 °C for 4 h.

| Sample | Elemental composition | | Textural properties | |
|-------------------|-----------------------|-------|------------------------------|---------------------------------------|
| | Si/Al | Zn/Pd | BET area (m ² /g) | Micropore volume (cm ³ /g) |
| H-ZSM-5 (25) | 25 | | 420 | 0.176 |
| PdZn@H-ZSM-5 (25) | 25 | 5 | 348 | 0.121 |
| H-ZSM-5 (40) | 40 | | 444 | 0.196 |
| PdZn@ZnO | | 16 | | |



PdZn/ZnO + ZSM5

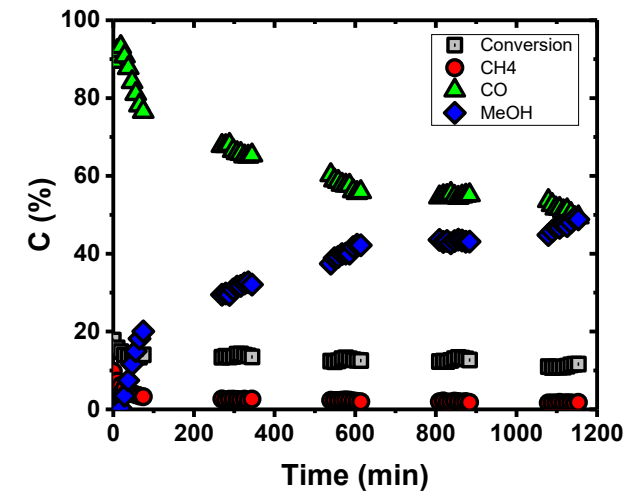
PXRD – PdZn alloy formation



Catalyst testing

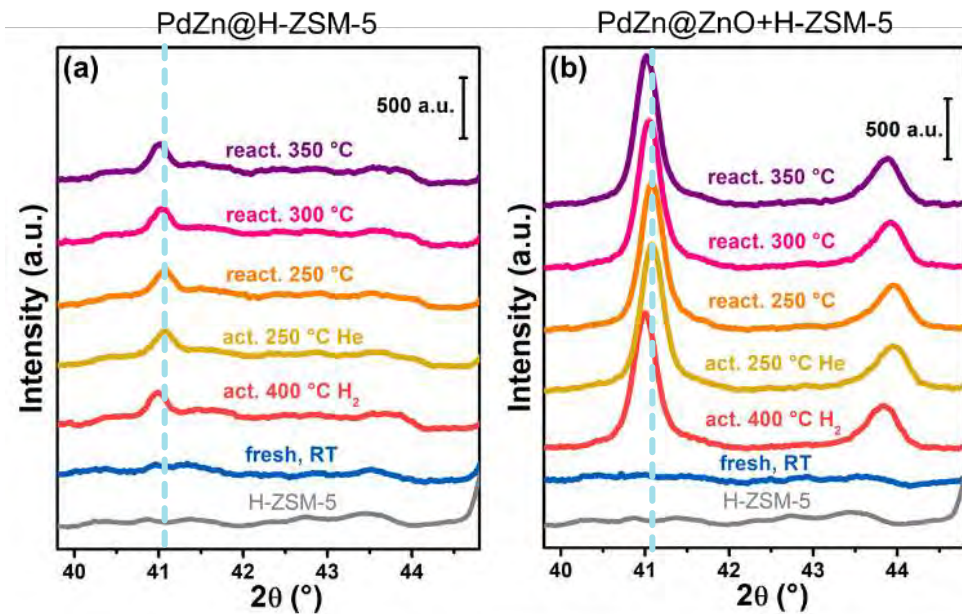
300 °C, 20 bar

PdZn@ZnO



PdZn/ZnO + H-ZSM-5

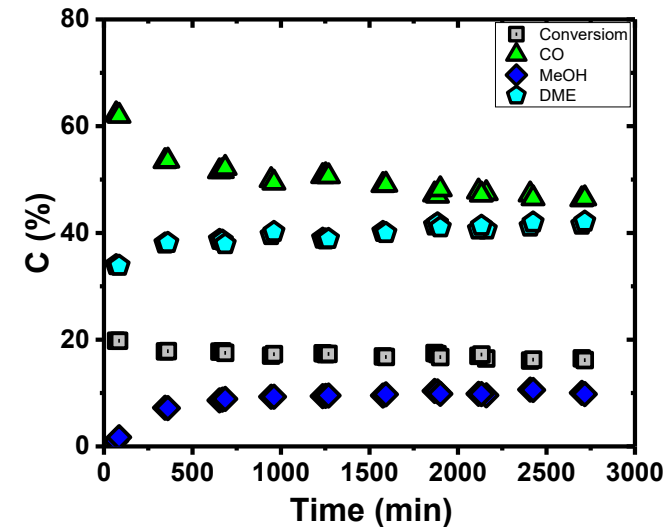
PXRD – PdZn alloy formation



Catalyst testing

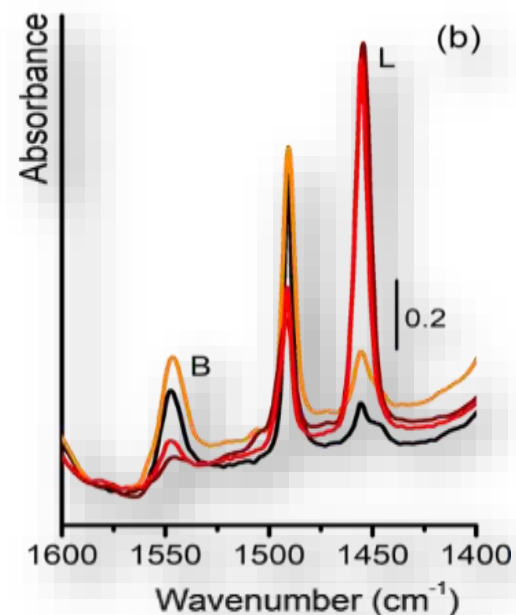
300 °C, 20 bar

PdZn@ZnO + H-ZSM-5



PdZn/ZnO + H-ZSM-5

Acid sites quantification using pyridine FT-IR spectroscopy



Black curve: Parent H-ZSM-5(40),

Orange curve: PdZn@ZnO+H-ZSM-5(40) as-prepared sample,

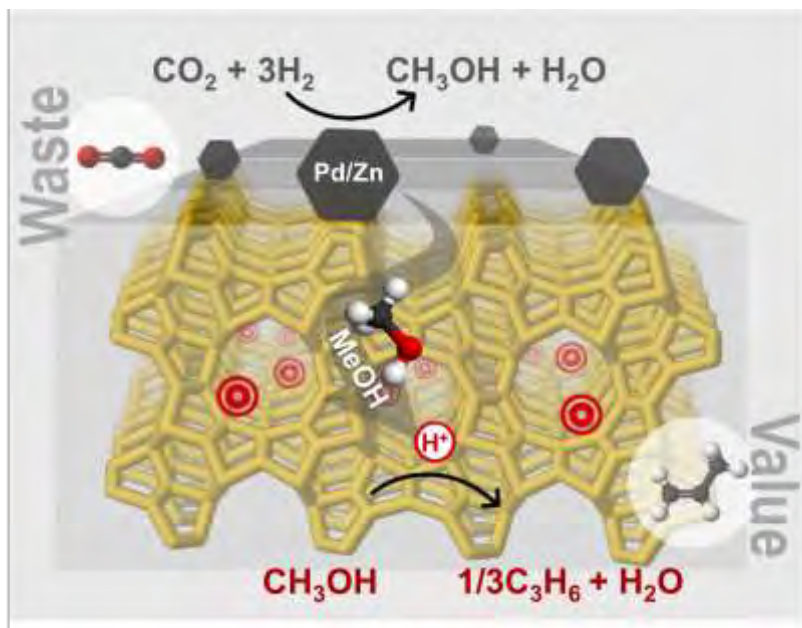
Red curve: PdZn@ZnO+H-ZSM-5(40) sample treated with H₂ at 400 °C for 1 h,

Brown curve: PdZn@ZnO+H-ZSM-5(40) tested sample.

| Sample | Step | Brønsted sites (mmol/g) | Lewis sites (mmol/g) |
|-------------------------|-------------|-------------------------|----------------------|
| Fresh H-ZSM-5 | Si/Al = 25 | 0.21 | 0.07 |
| | Si/Al = 40 | 0.15 | 0.07 |
| PdZn@H-ZSM-5 (25) | As prepared | 0.02 | 0.57 |
| | Tested | 0.02 | 0.46 |
| PdZn@ZnO + H-ZSM-5 (40) | As prepared | 0.11 | 0.05 |
| | Activated | 0.04 | 0.25 |
| | Tested | 0.03 | 0.32 |



Summary and outlook – Case 1



- **PdZn alloy** maintains high methanol selectivity at 300 °C, and may be suited for the tandem process
- However, excess Zn migrates to the H-ZSM-5 zeolite, where it ion exchanges onto the Brønsted acid sites (confirmed by Zn K edge EXAFS measurements), thereby hindering hydrocarbons formation

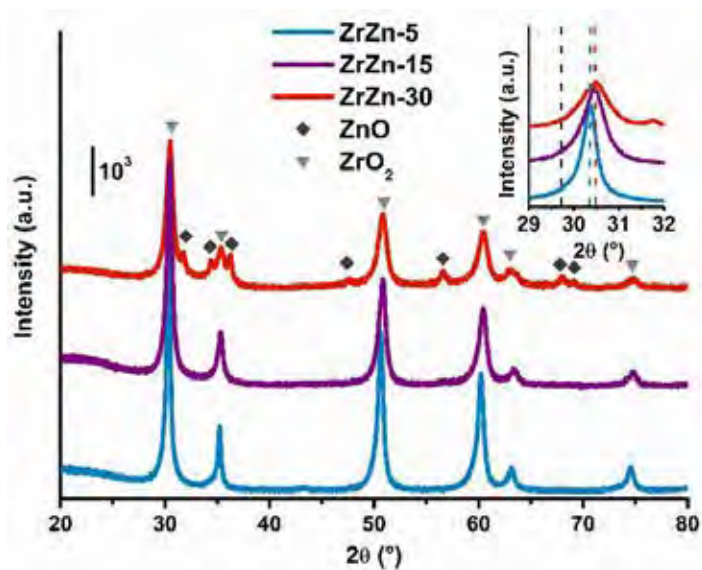
Paper 1. Ahoba-Sam, C.; Borfecchia, E.; Lazzarini, A.; Bugaev, A.; Isah, A.A.; Taoufik, M.; Bordiga, S.; Olsbye, U.; On the conversion of CO_2 to value added products over composite PdZn and H-ZSM-5 catalysts: excess Zn over Pd, a compromise or a penalty? *Catalysis Science & Technology*, **2020**, 10, 4373–4385.



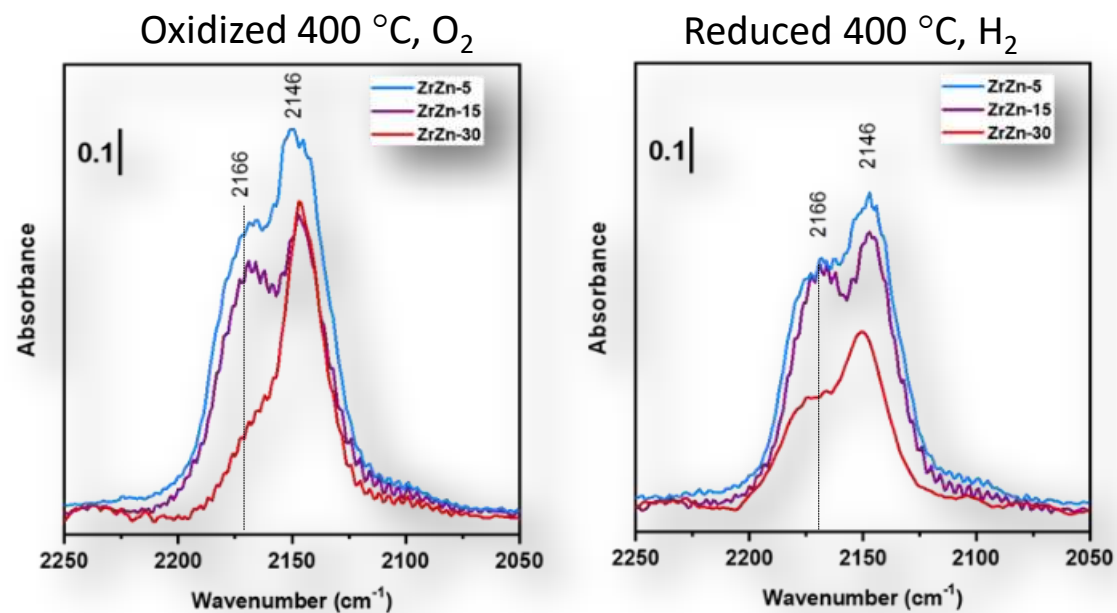
Case 2: $\text{Zr}_{1-x}\text{Zn}_x\text{O}_2$ + H-ZSM-5 (or H-SAPO-34)

$\text{Zr}_{1-x}\text{Zn}_x\text{O}_2$ (X = 0.05, 0.15 or 0.30) was prepared by co-precipitation and eventually mixed with H-ZSM-5 (or SAPO-34) before testing.

PXRD

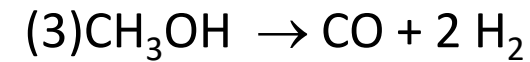
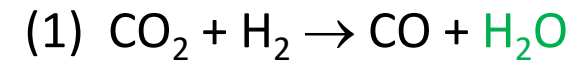
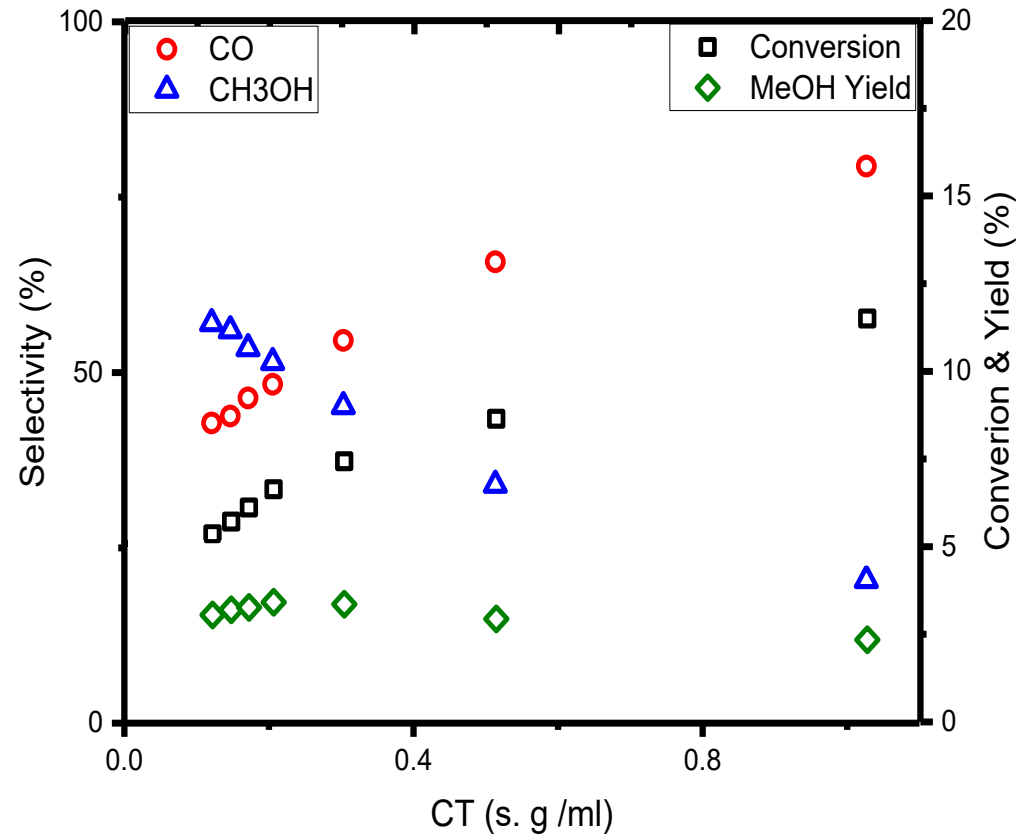


FT-IR with CO



$\text{Zr}_{1-x}\text{Zn}_x\text{O}_2$ alone

Catalytic testing in $\text{H}_2/\text{CO}_2 = 3$ at 350 °C, 30 bar

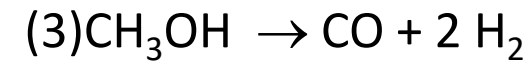
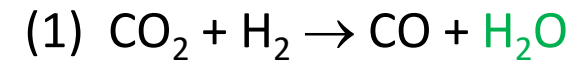
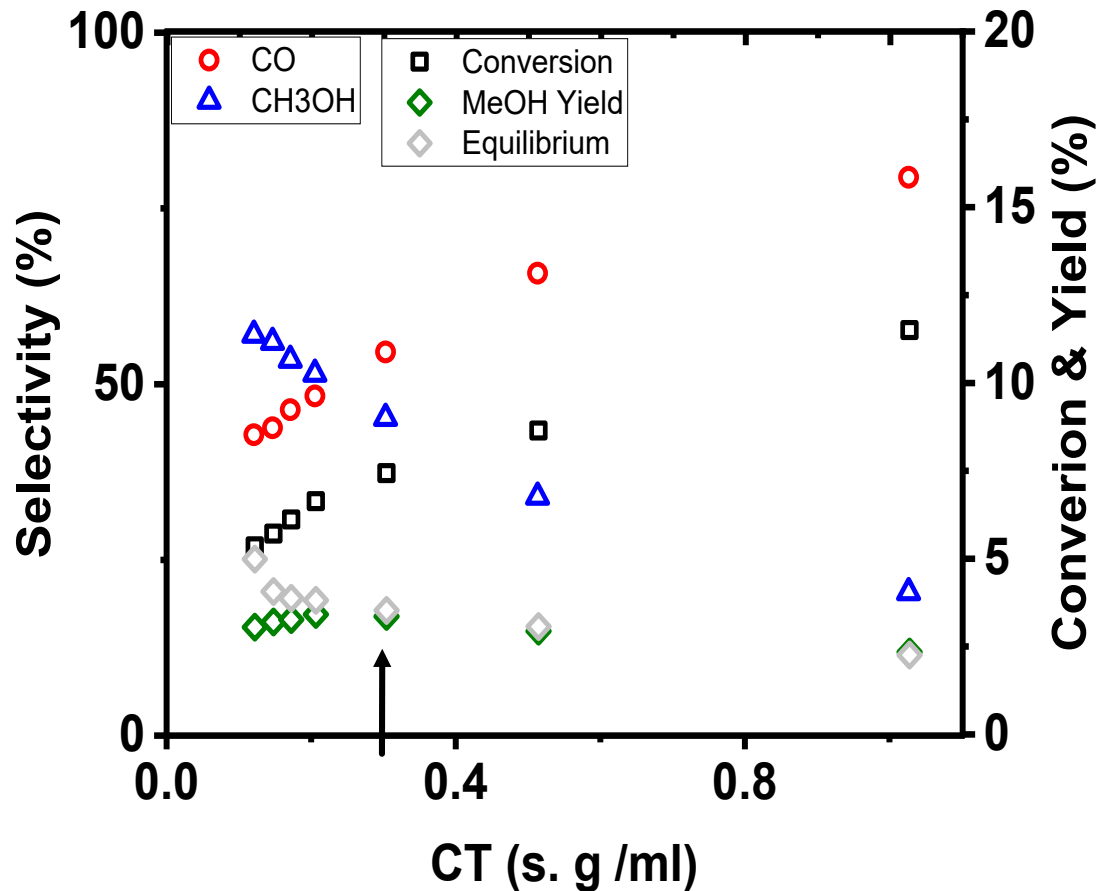


$$K_{eq,2} = \frac{P(\text{CH}_3\text{OH}) * P(\text{H}_2\text{O})}{P(\text{CO}_2) * P(\text{H}_2)^3}$$



$\text{Zr}_{1-x}\text{Zn}_x\text{O}_2$ alone

Catalytic testing in $\text{H}_2/\text{CO}_2 = 3$ at 350 °C, 30 bar



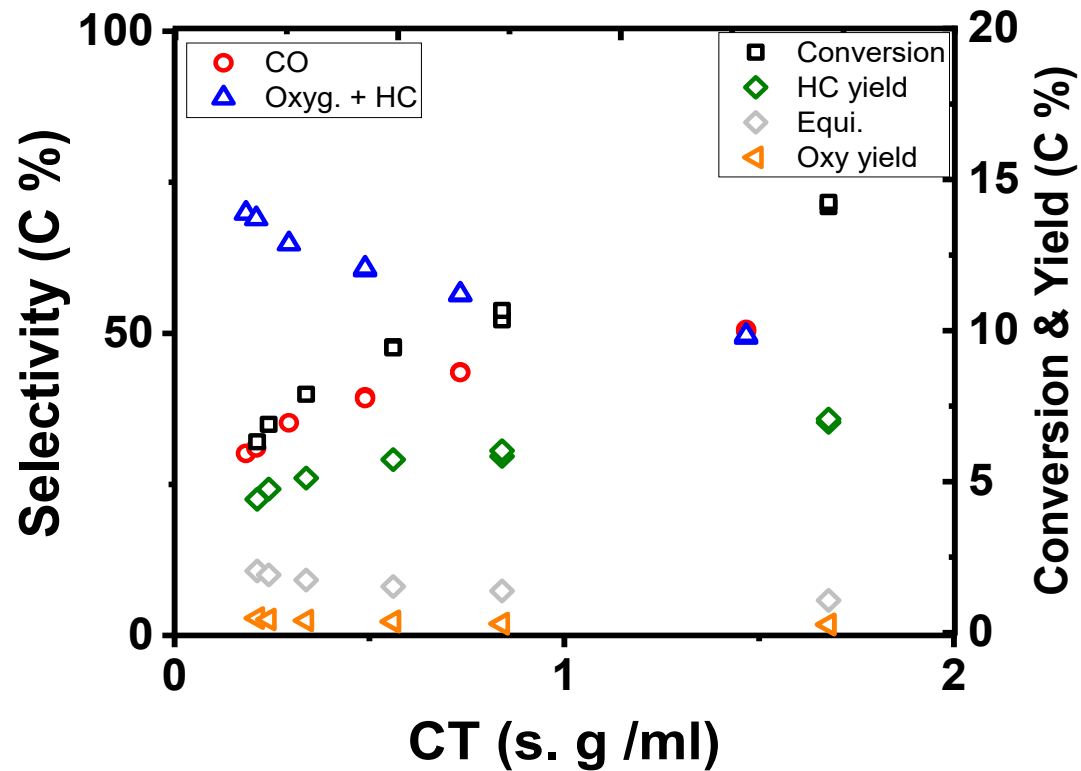
$$K_{eq,2} = \frac{P(\text{CH}_3\text{OH}) * P(\text{H}_2\text{O})}{P(\text{CO}_2) * P(\text{H}_2)^3}$$



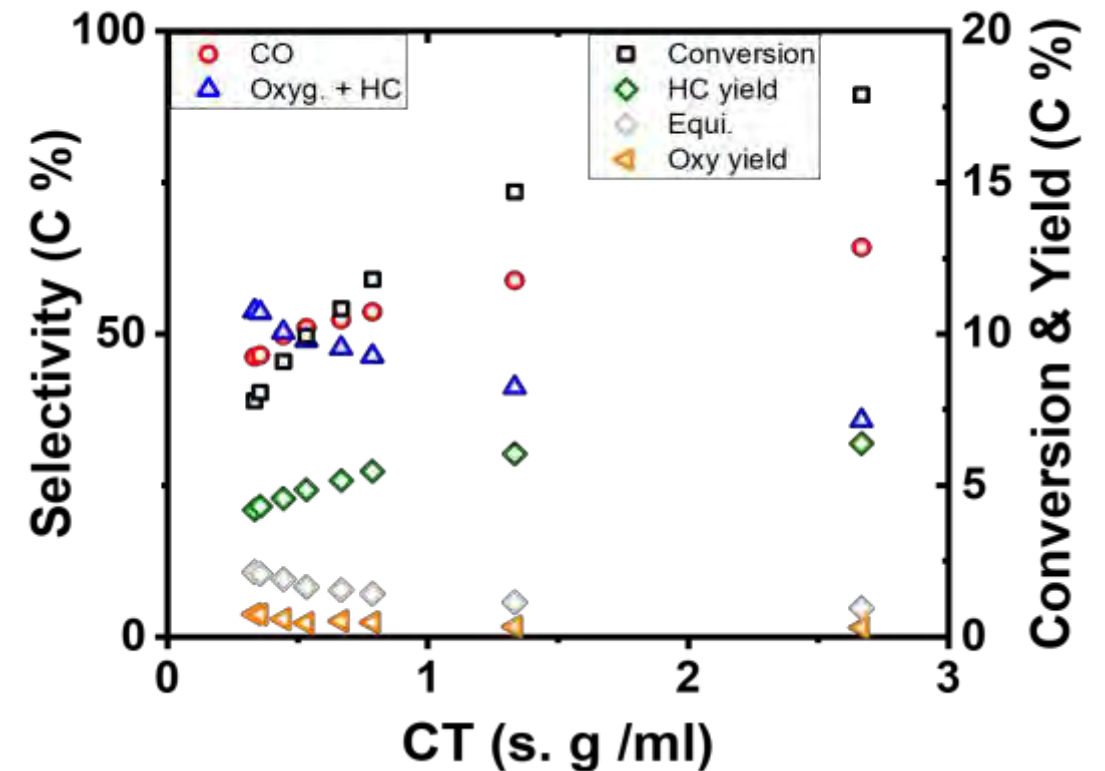
$\text{Zr}_{1-x}\text{Zn}_x\text{O}_2 + \text{H-ZSM-5}$

Catalytic testing in $\text{H}_2/\text{CO}_2 = 3$ at 350 °C, 30 bar

Si/Al = 25

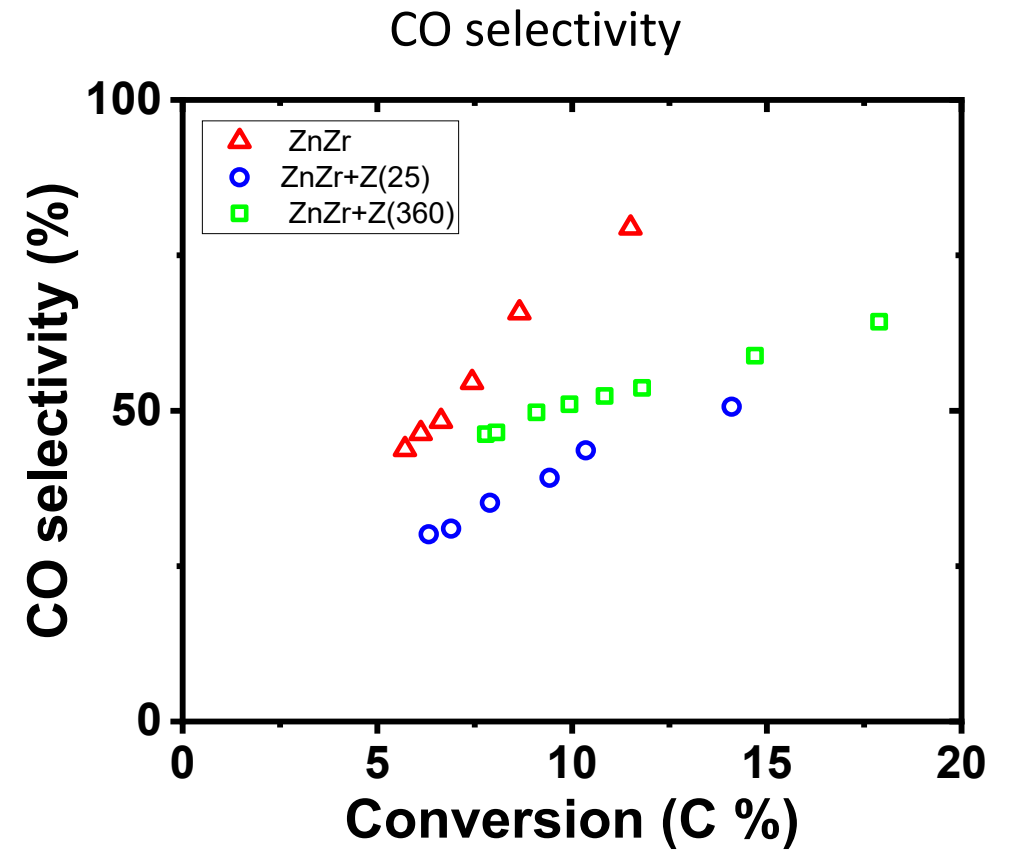
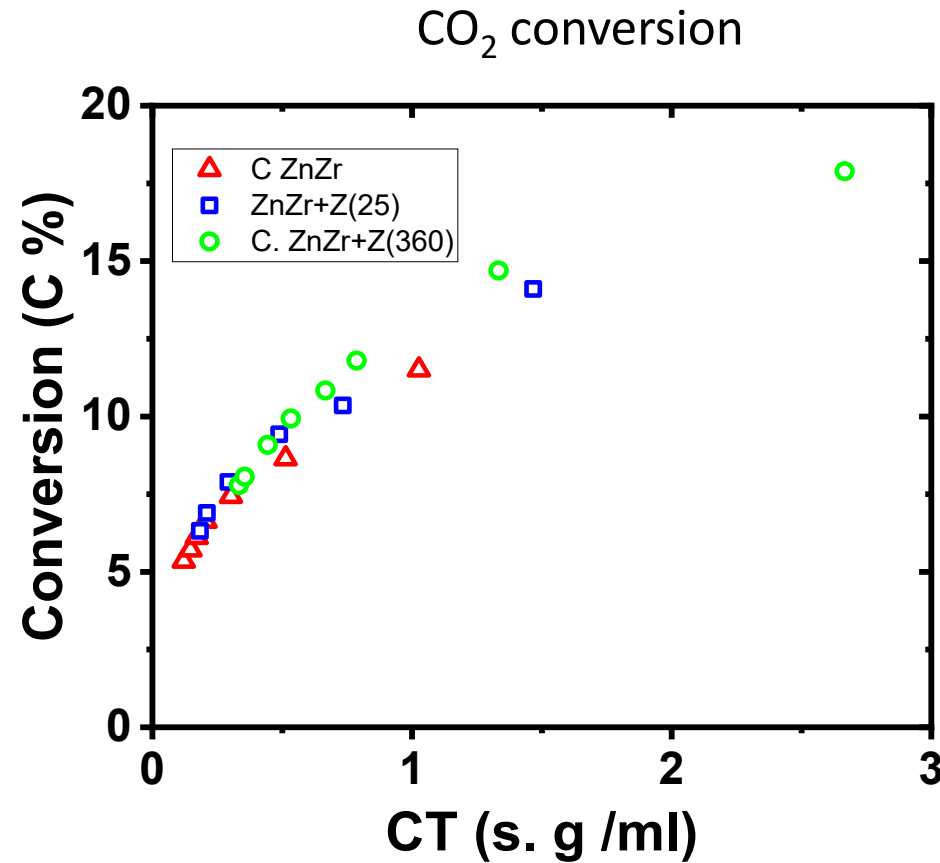


Si/Al = 360

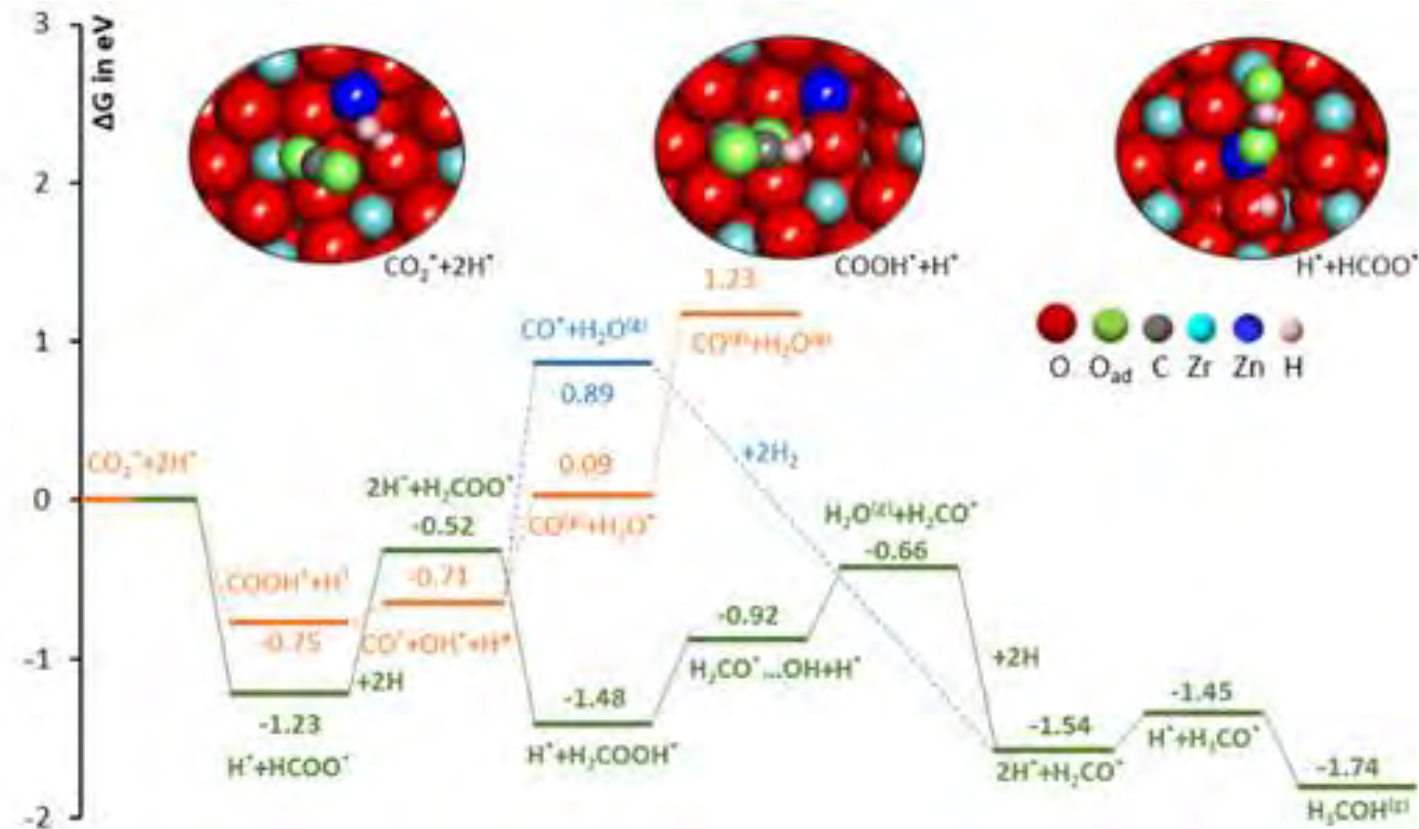


$\text{Zr}_{1-x}\text{Zn}_x\text{O}_2 + \text{H-ZSM-5}$

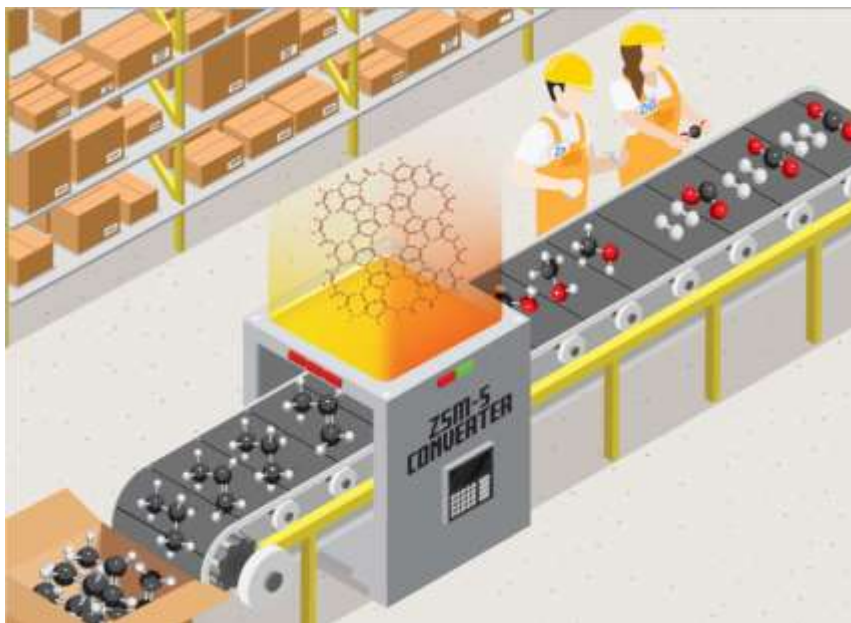
Catalytic testing in $\text{H}_2/\text{CO}_2 = 3$ at 350 °C, 30 bar



ZnZrO – computational studies



Summary and outlook – Case 2



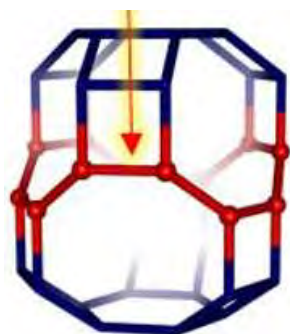
- Studies of the **ZnZrO+H-ZSM-5** system shows that methanol is a primary product from CO₂, and both CO and hydrocarbons are formed from methanol, over the tandem catalyst
- Methanol is formed via the formate route over ZnZrO
- CO₂ hydrogenation is the rate-limiting step of the tandem reaction

Paper 2. Ticali, P.; Salusso, D.; Ahmad, R.; Ahoba-Sam, C.; Ramirez, A.; Shterk, G.; Lomachenko, K.A.; Borfecchia, E.; Morandi, S.; Cavallo, L.; Gascon, J.; Bordiga, S.; Olsbye, U. **CO₂ hydrogenation to methanol and hydrocarbons over bifunctional Zn-doped ZrO₂/Zeolite catalysts.** *Catalysis Science & Technology*, **2020**, <https://doi.org/10.1039/D0CY01550D>.



Case 3: ZnCeZrO + H-RUB-13

SAPO-34



RUB-13

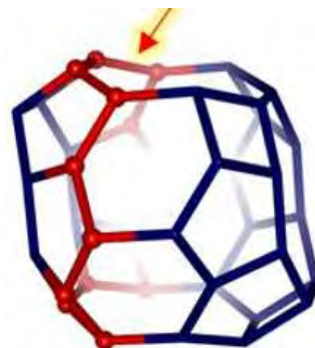
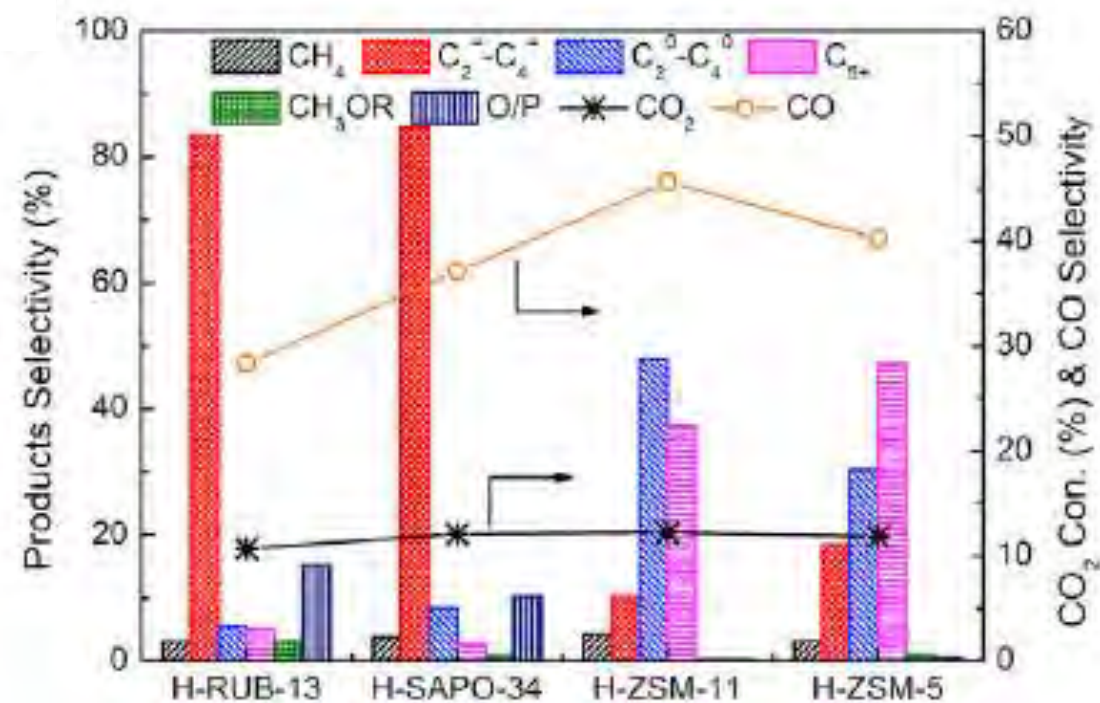


Illustration from: J. H. Kang, J.H et al.,
ACS Catal. **2019**, 9, 6012.

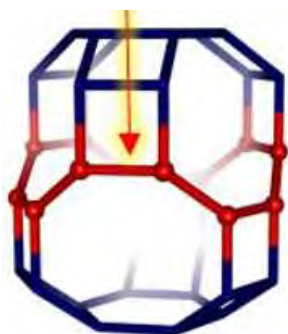


Zn_{0.5}Ce_{0.2}Zr_{1.8}O₄ + zeolite, 350 °C, 10 bar, H₂/CO₂ = 3:1,
GHSV = 4,800 mL/g_h



ZnCeZrO + H-RUB-13

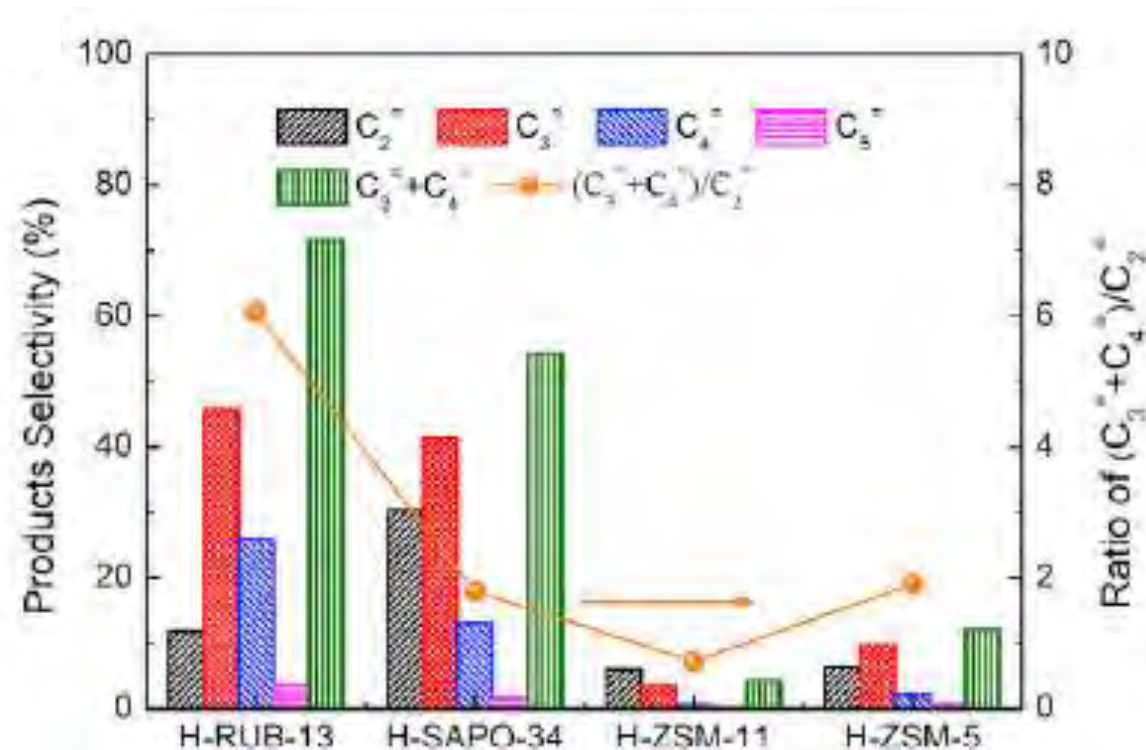
SAPO-34



RUB-13



Illustration from: J. H. Kang, J.H et al.,
ACS Catal. **2019**, 9, 6012.

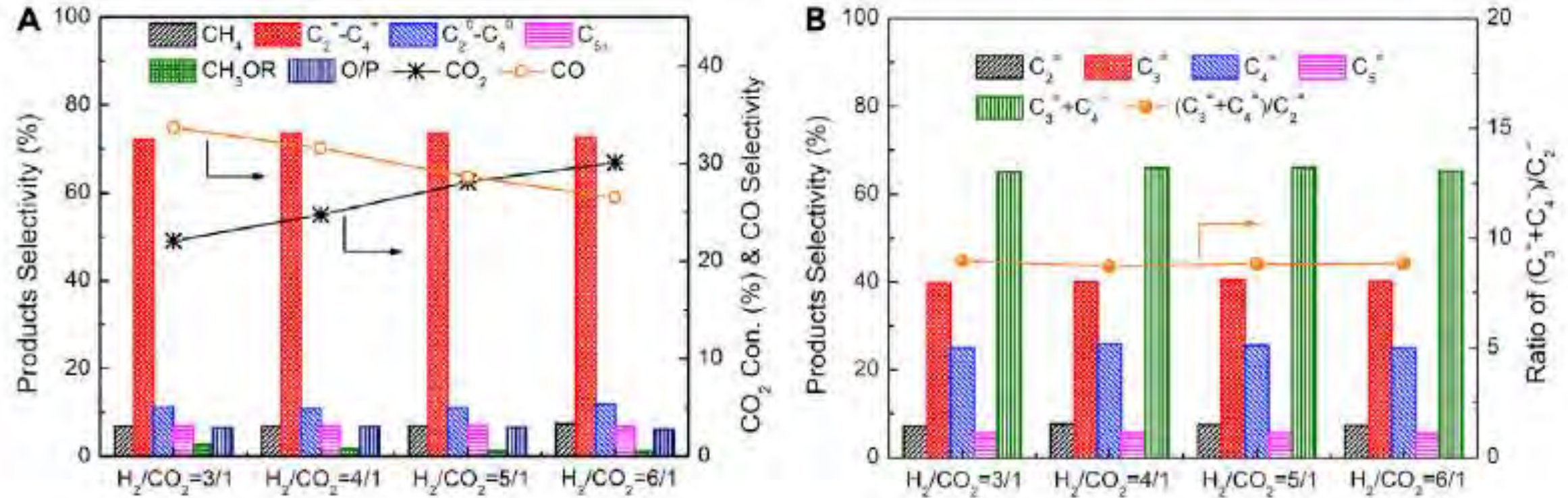


$\text{Zn}_{0.5}\text{Ce}_{0.2}\text{Zr}_{1.8}\text{O}_4$ + zeolite, 350 °C, 10 bar, $\text{H}_2/\text{CO}_2 = 3:1$,
GHSV = 4,800 mL/g_h



ZnCeZrO + H-RUB-13

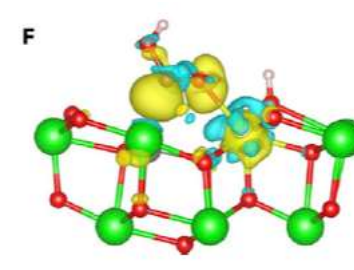
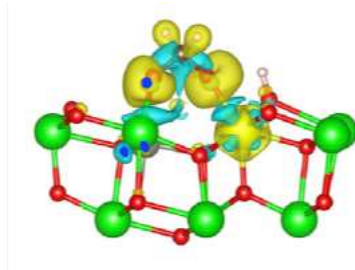
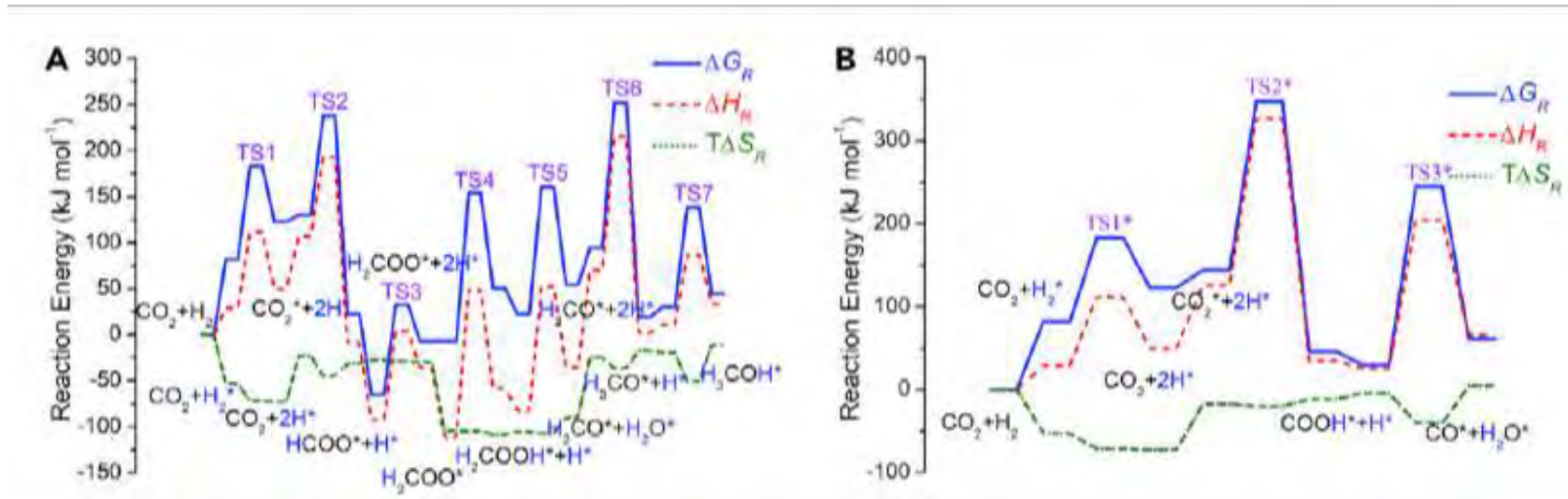
Influence of test conditions



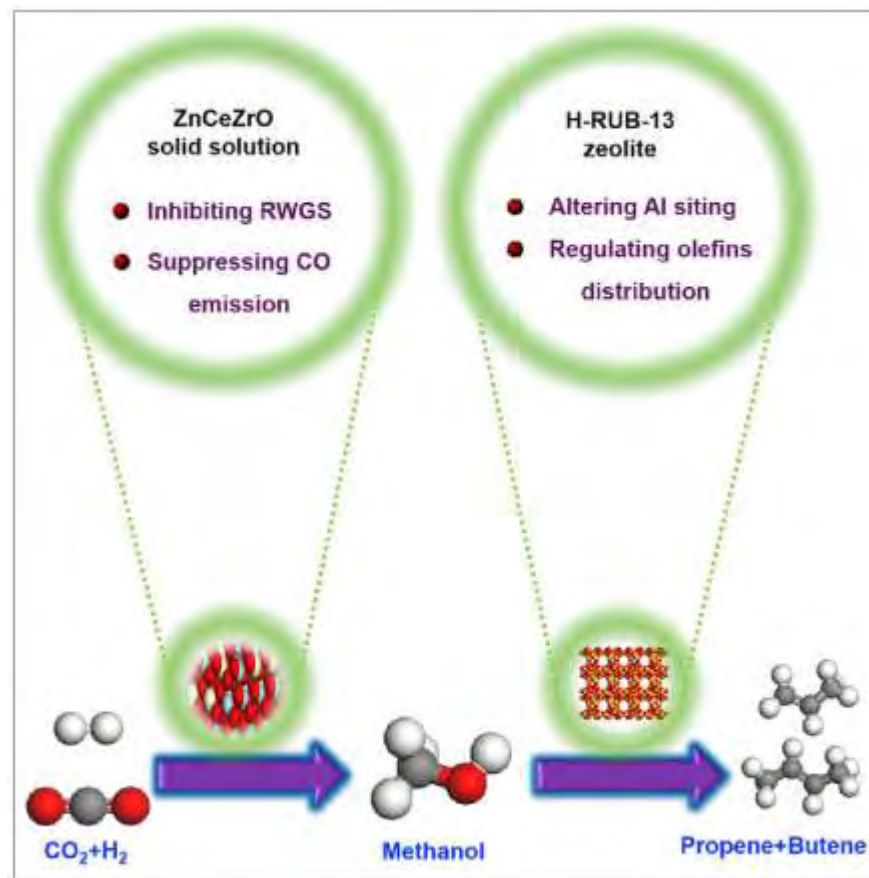
Zn_{0.5}Ce_{0.2}Zr_{1.8}O₄ : RUB-13 = 1:2, 350 °C, 35 bar, H₂/CO₂ = 3:1 – 6:1



ZnCeZrO + RUB-13



Summary and outlook – Case 3



- Studies of the **ZnCeZrO+H-RUB-13** system shows that small changes in the cavity-window size of the zeotype has substantial impact on hydrocarbon product distribution.
- C₃= and C₄= account for 90% of light olefins due to the promotion of the alkene-based cycle
- CH₃OH is formed on Zn_{0.5}Ce_{0.2}Zr_{1.8}O₄ via the formate - methoxyl intermediates mechanism.

Paper 3. Wang, S.; Zhang, L.; Zhang, W.; Wang, P.; Qin, Z.; Yan, W.; Dong, M.; Li, J.; Wang, J.; Lin He, L.; Olsbye, U.; Fan, W., **Selective conversion of CO₂ into Propene and Butene.** *Chem* **2020**, *6*, 1-20.



Conclusions and Outlook

Case 1. Studies of the **PdZn+H-ZSM-5** system shows that methanol selectivity of PdZn/ZnO may be maintained under MTO-relevant conditions, but leaching of Zn into the zeolite, thereby poisoning the Brønsted acid sites, is a challenge.

Case 2. Studies of the **ZnZrO+H-ZSM-5** system shows that methanol is a primary product from CO₂, and both CO and hydrocarbons are formed from methanol, over the tandem catalyst. CO₂ hydrogenation is the rate-limiting step of the tandem reaction.

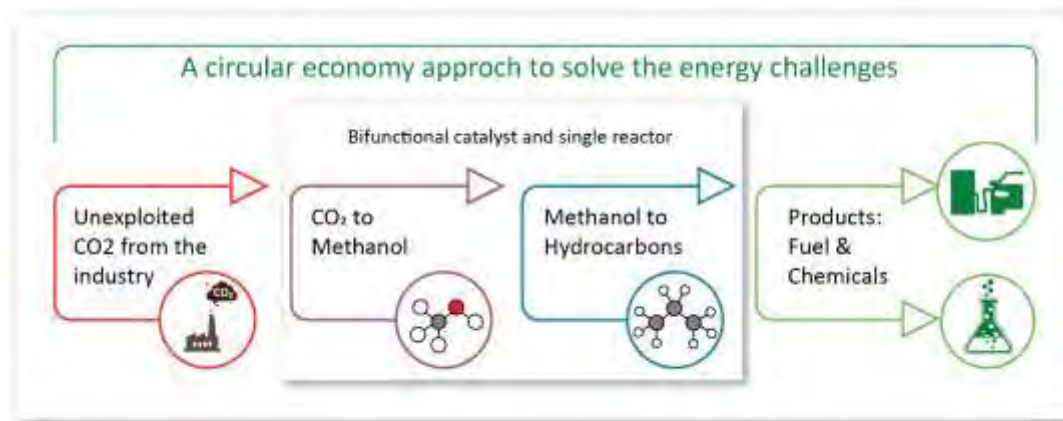
Case 3. Studies of the **ZnCeZrO+H-RUB-13** system shows that small changes in the cavity-window size of the zeotype has substantial impact on hydrocarbon product distribution. CH₃OH is formed selectively on Zn_{0.5}Ce_{0.2}Zr_{1.8}O₄ via the formate - methoxyl intermediates mechanism

Overall, the three case studies yield important insight in function – performance correlations for the methanol-mediated conversion of CO₂ and H₂ to propane and propene



COZMOS

Efficient CO₂ conversion over multisite Zeolite-Metal nanocatalysts to fuels and Olefins



Thanks to all COZMOS WP1 partners for their contributions, and

Thank you for your attention!



COZMOS: Efficient CO₂ conversion over multisite Zeolite-Metal nanocatalysts to fuels and Olefins.

This project has received funding from the European Union's Horizon 2020 research and innovation programme under Grant Agreement No. 837733.



CO₂ Capture Using 3D Printed PEI Adsorbents Supported By Carbon Nanostructures

Shreenath Krishnamurthy¹, Richard Blom¹, Carlos Adolfo Grande¹,
Kari Anne Andreassen¹, Vesna Middelkoop², Marleen Rombouts²
and Adolfo Bendito Borrás³

1. SINTEF Industry, Oslo, Norway 2. VITO, Mol, Belgium 3. AIMPLAS, Valencia, Spain

Shreenath.Krishnamurthy@sintef.no



Introduction



High pressure drop



Low pressure drop and better mass transfer

- CO₂ capture from power plants is associated with large capture footprint
- Fast cycling and higher flowrates can lower footprint
- Structured sorbents are advantageous over pellets for lowering the footprint
- 3D printing offers good control over shape of the sorbent and channel geometry
- Aim of this work : Evaluate a 3D printed monolith for post-combustion carbon capture: From equilibrium data to process simulations



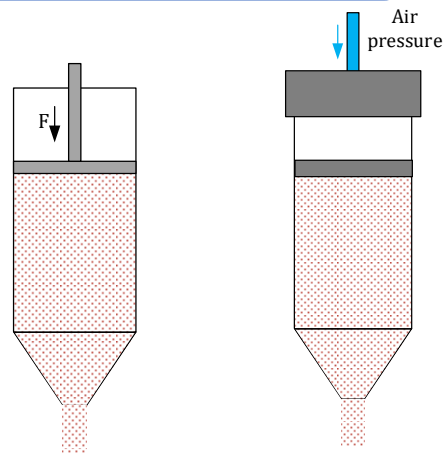
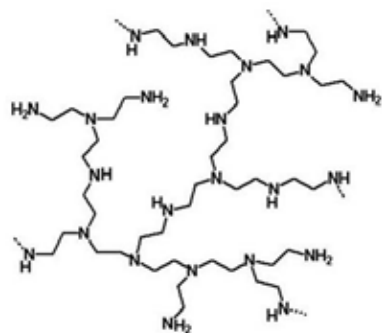
Extrusion through
nozzle at room
temperature



Computer controlled deposition of fibres



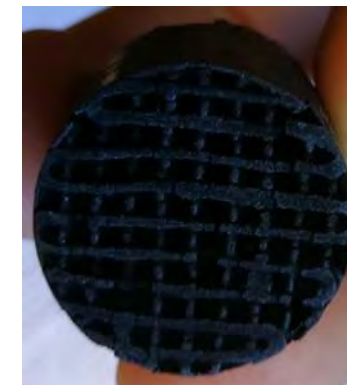
Drying



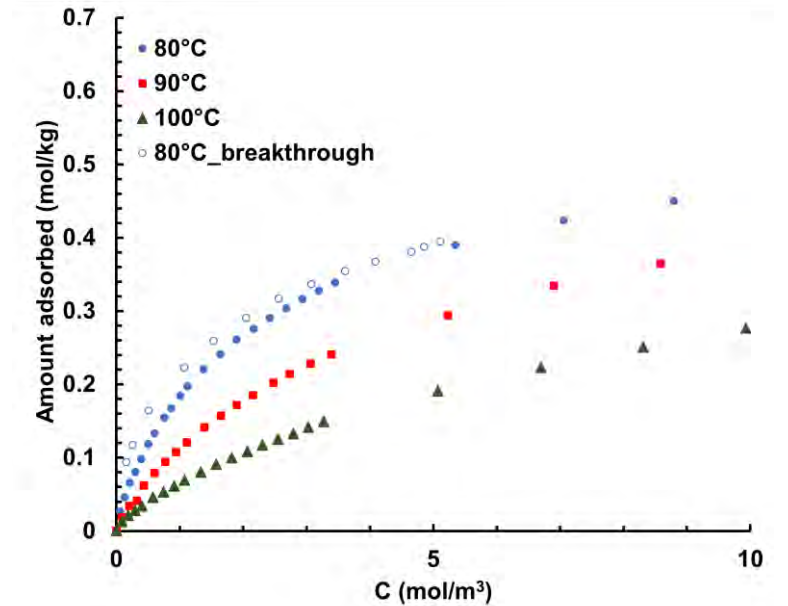
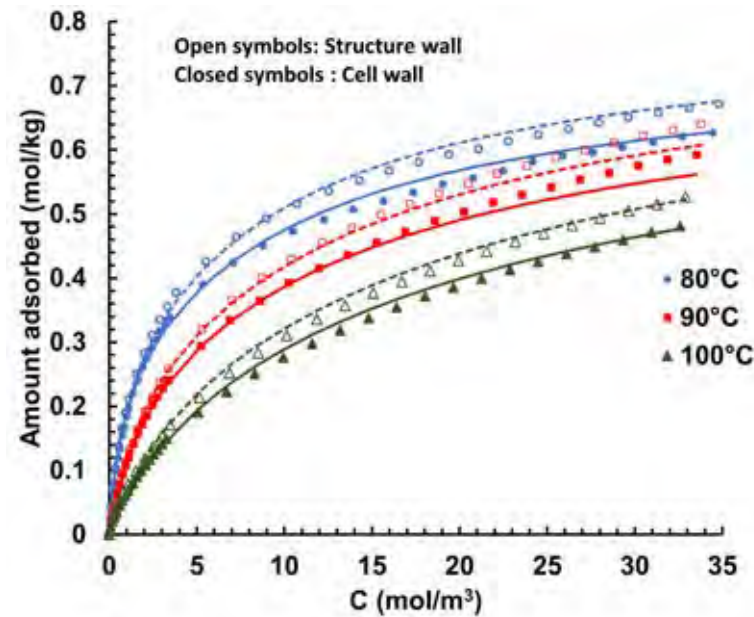
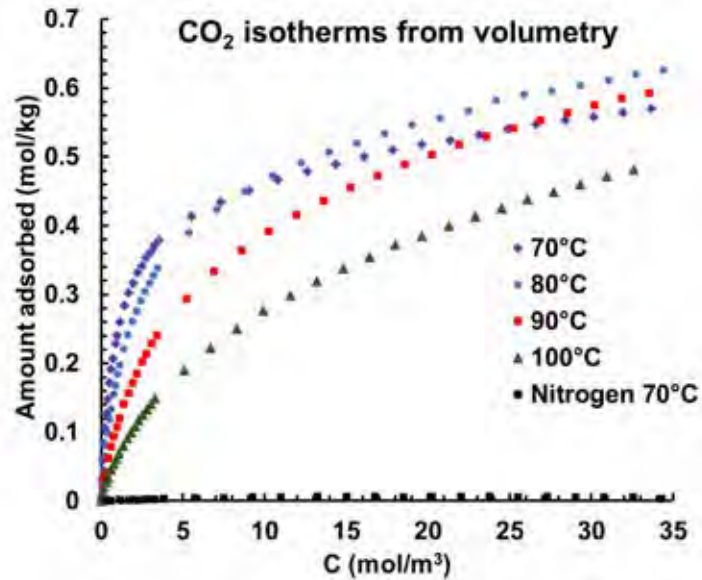
Piston-based and pneumatic dispensing



Channel diameter 1.4 mm
Wall thickness 0.6 mm

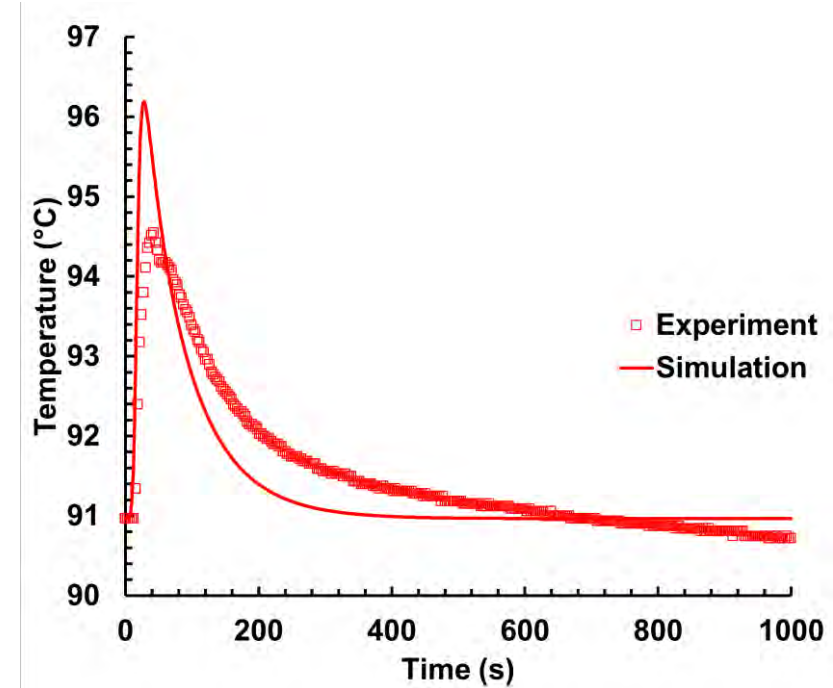
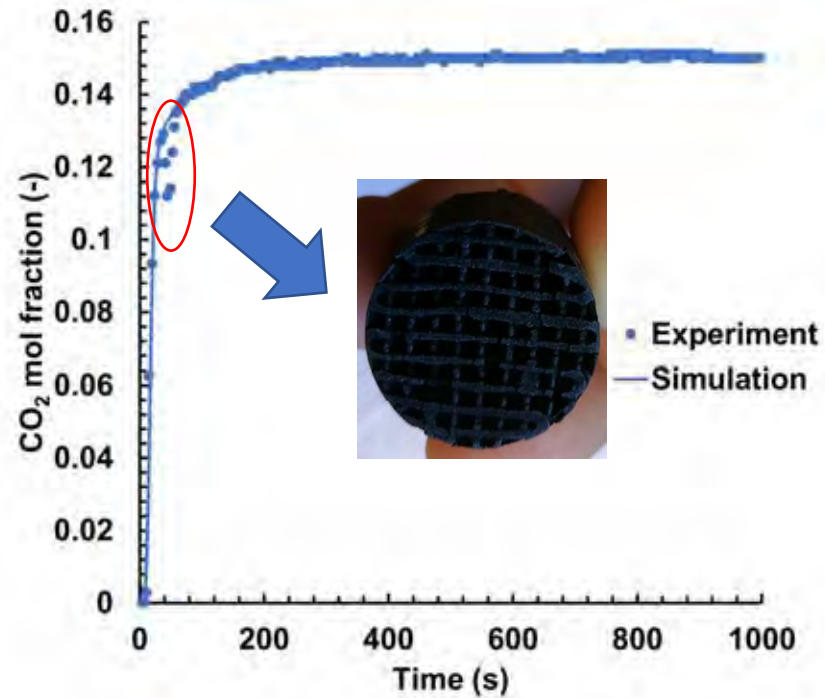
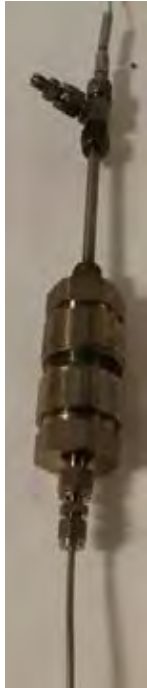


CO₂ adsorption equilibrium



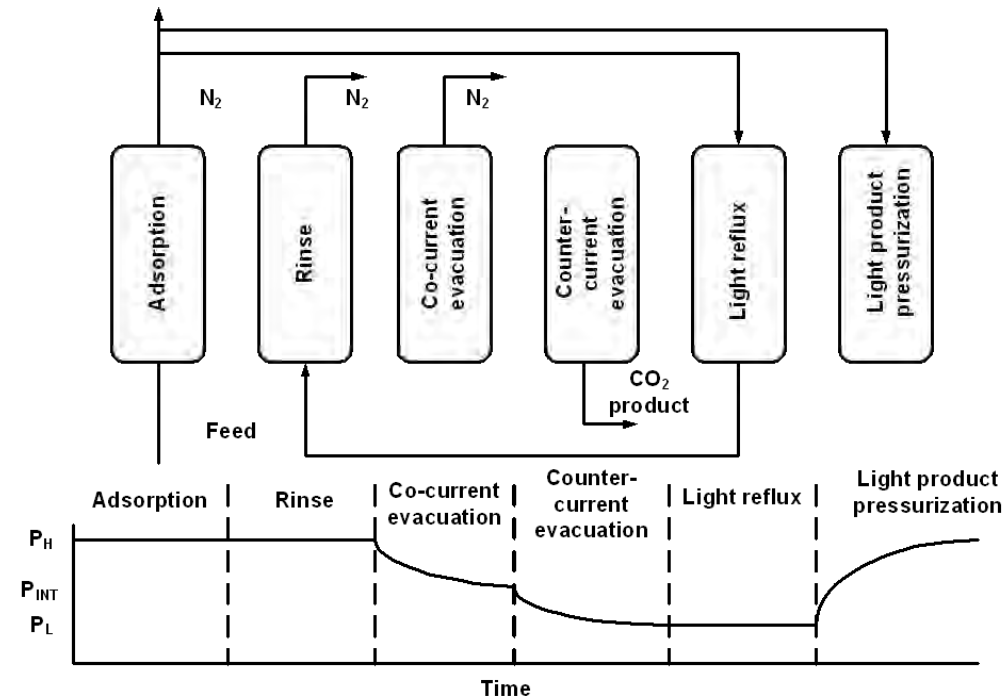
- Volumetric experiments to measure adsorption isotherms
- One structure was crushed and isotherms on cell wall material and monolith wall material measured for different temperatures
- Breakthrough experiments carried out with 15% CO₂ in N₂ feed, desorption with pure N₂
- Heat of adsorption for CO₂ = -100 kJ/mol, CO₂ adsorption capacity at 0.15 bar and 90°C = 0.3 mol/kg
- Minor variations observed in CO₂ adsorption capacity within the 3D printed adsorbent

CO₂ adsorption kinetics



- Dynamic column breakthrough experiments (2 structures stacked one on top of the other, 15% CO₂, 85% N₂)
- Adsorption part of the breakthrough experiments analysed with a 1D process model
- Fitting the LDF and heat transfer co-efficient values for 3 temperatures.

Process simulation and optimization



6-step VSA cycle³

The system : 15% CO₂ , 85% N₂ , 90°C

Length of column 1 m : diameter 0.29 m

Isotherms and LDF coefficient values obtained from volumetry and breakthrough

1D non-isothermal, non-isobaric model

Pressure drop¹

$$\frac{-dP}{dZ} = \frac{28.4u\mu}{d_{ch}^2}$$

Axial dispersion²

$$D_L = D_m + \frac{(2ud_{ch})^2}{192D_m}$$

$$\text{CO}_2 \text{ purity} = \frac{\text{mass CO}_2 \text{ in evac}}{\text{total mass evac}}$$

$$\text{Productivity} = \frac{\text{mass CO}_2 \text{ in evacuation}}{\text{volume of adsorbent X cycle time}}$$

$$\text{CO}_2 \text{ recovery} = \frac{\text{mass CO}_2 \text{ in evac}}{\text{mass CO}_2 \text{ in feed}}$$

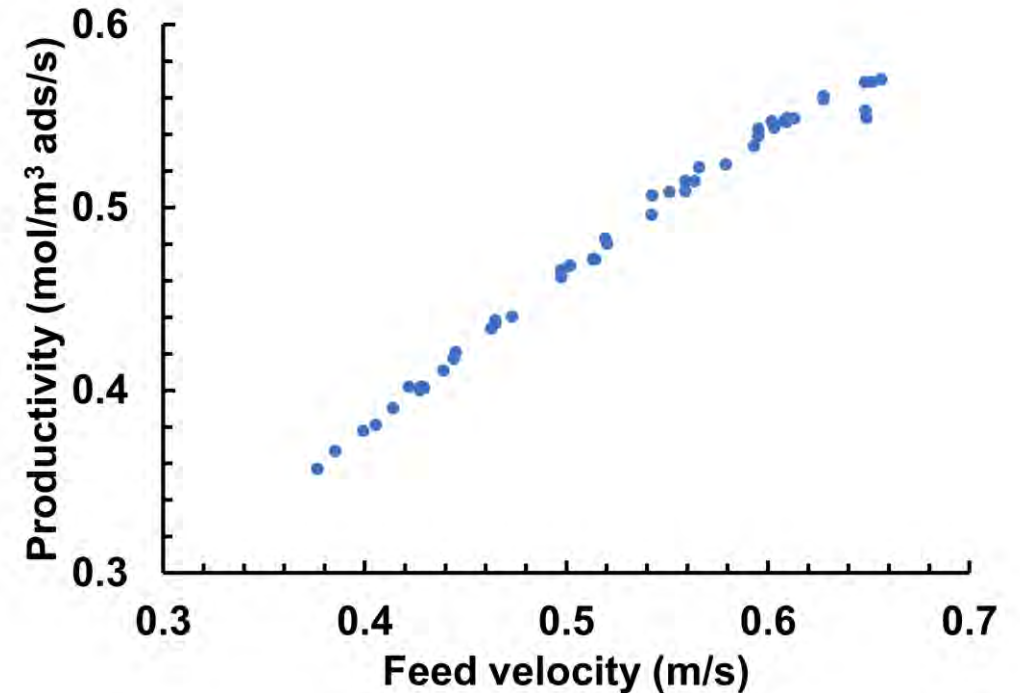
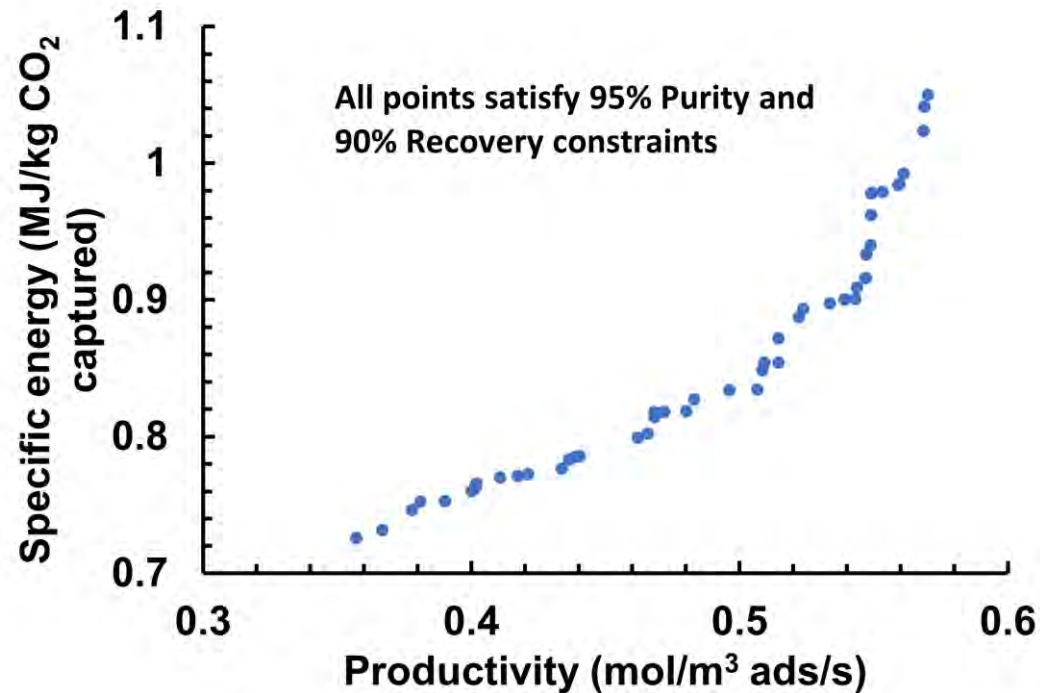
$$\text{Specific energy} = \frac{\text{Compression+Evacuation energy}}{\text{mass CO}_2 \text{ in evacuation}}$$

Aim of process study

- Identify minimum specific energy and maximum productivity
- Target CO₂ purity ≥ 95%, Target recovery ≥ 90%

- Patton et al., **2004**, Chem Eng Res Des, 82, 199-209
- Rezaei and Webley **2009**, Chem Eng Sci, 64,5182-5191
- Khurana and Farooq, 2016, Chem Eng Sci, 152, 507-515

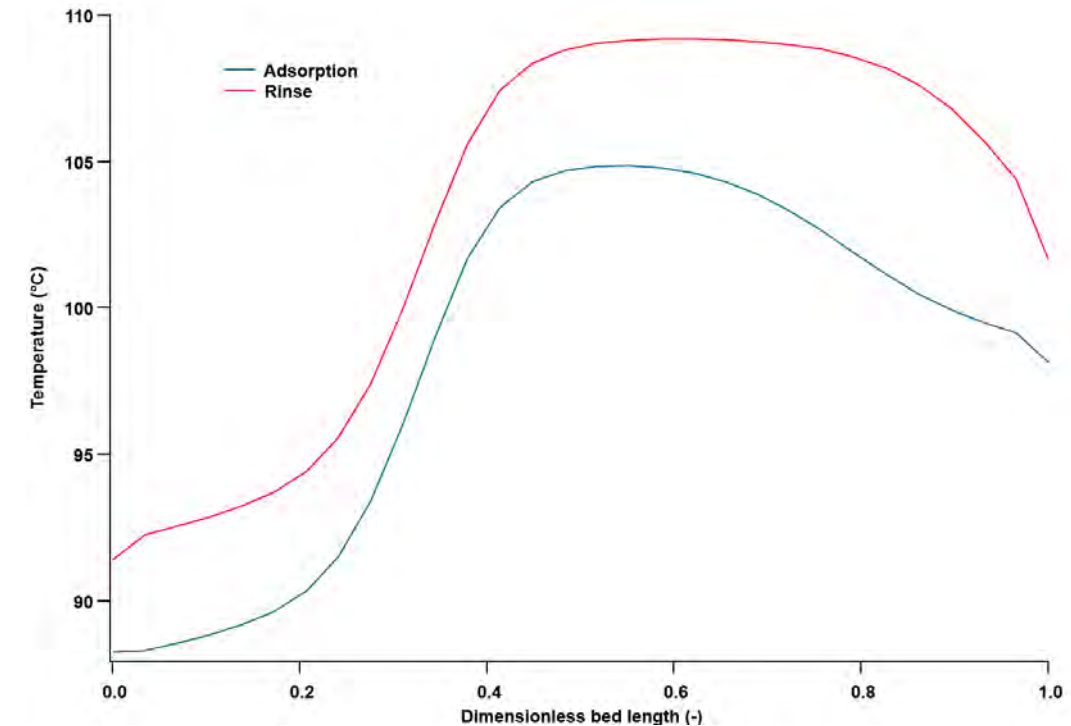
Results from process optimization



- Minimum specific energy = 0.72 MJ_{Electric}/kg CO₂ captured, Maximum productivity 0.57 mol/m³ ads/s
- Cycle time = 2.5 – 3 minutes (adsorption step duration = 30-40 s)

Conclusions & future work

- **95-90 purity-recovery targets achieved**
- Minimum specific energy = $0.72 \text{ MJ}_{\text{Electric}}/\text{kg CO}_2$ captured
- Maximum productivity = $0.57 \text{ mol/m}^3 \text{ ads/s}$
- Adsorbent to be "married" to its best cycle to understand true potential : Need for alternative cycle configuration
- Effect of moisture on CO_2 adsorption to be studied
- High temperatures in a cyclic process can affect sorbent stability



Temperature profiles in the column

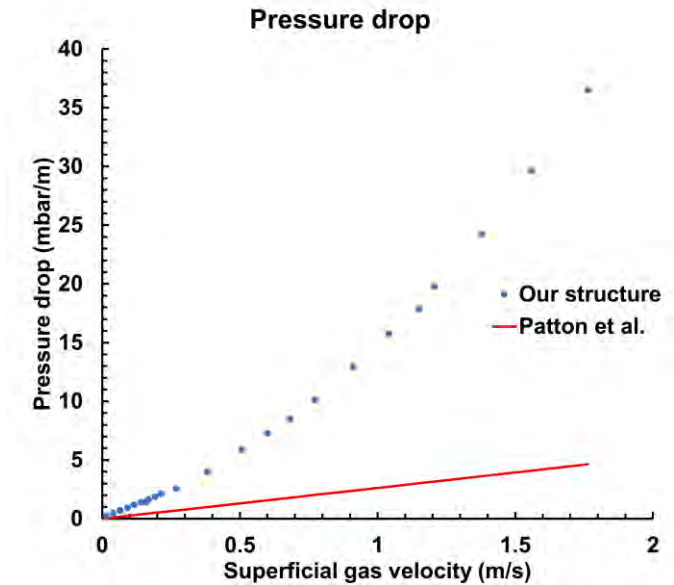
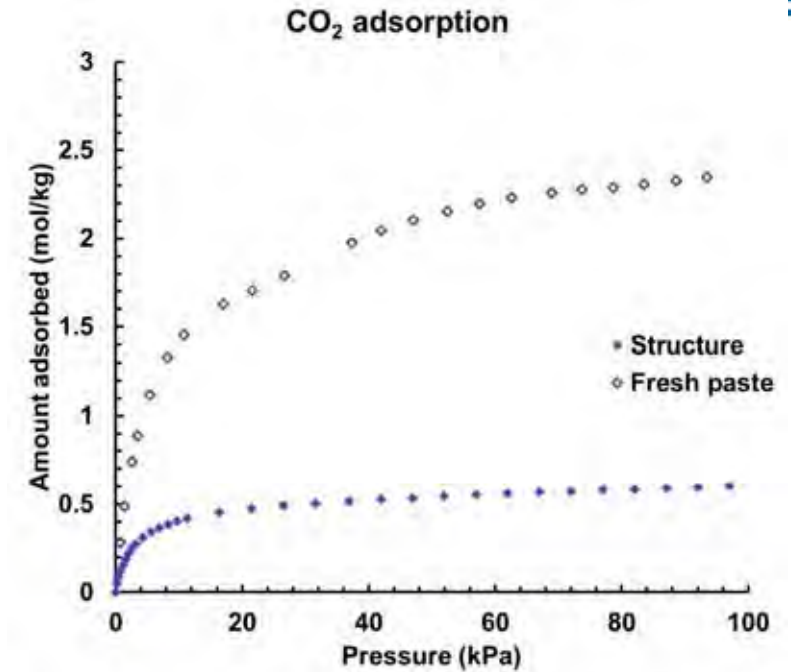
Conclusions & future work

Challenges with 3D printing

- Instability in printing due to phase separation necessitated the use of additives
- Reduction in capacity in comparison with pristine paste
- High shrinkage due to the presence of water

Challenges in the process

- High temperature swings and presence of O_2 can reduce stability of sorbent
- Measured pressure drop higher than predicted pressure drop



Acknowledgement



This project has received funding from the European Union's Horizon 2020 research and innovation programme under grant agreement No 760884 (CARMOF).

For more information on this project visit the project web page

<https://carmof.eu/>



Questions ?

Process intensification in the conversion of CO₂ with a milli-structured reactor

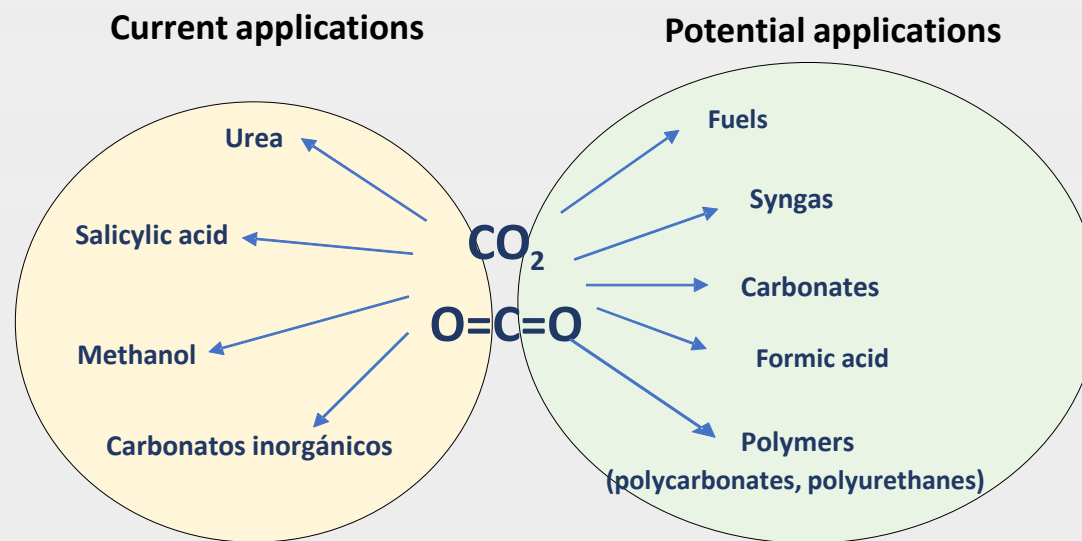


S. Perez, S. Prieto

Outline

1. Process Intensification: microreactors
2. Tecnalia's millichannel reactor
3. Catalytic tests in Sabatier reaction
4. Millichannel reactor scaling-up
5. Conclusions

1. Process Intensification: microreactors



**Current processes:
Poor energy and mass transfer**

Process intensification

Microstructured reactor

1. Process Intensification: microreactors

What is a micro or a millireactor?

Denomination according to Kiwi-Minsker & Renken (2005):

- 10 - 1000 microns of ID: microchannel reactors
- 1 - 10 millimeters of ID: millichannel reactors

It's a system to obtain processes:

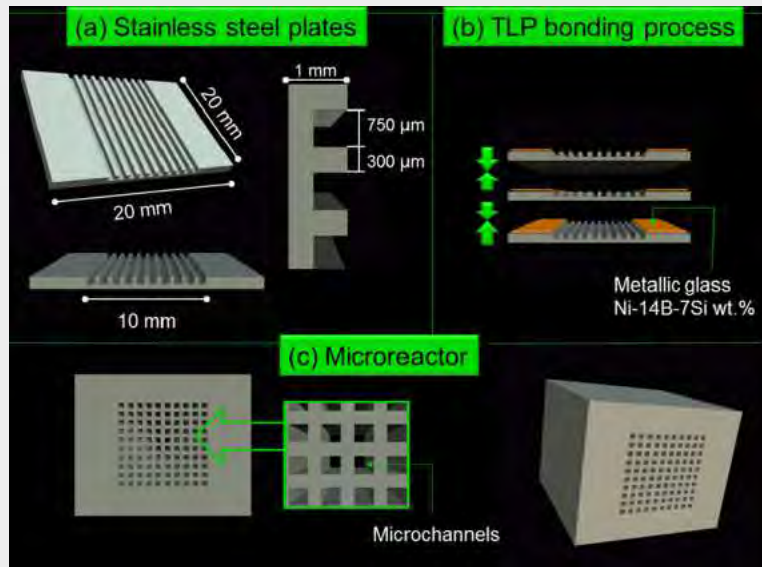
- more efficient,
- with lower operation costs,
- that generates low amount of waste,
- safer,
- smaller
- and with higher productivity.

In chemical synthesis, the use of millireactors improves the mass and energy transfer between the products and the catalyst.



Conventional fixed bed reactor vs 40 times intensified reactor. (Source: Dow Chemical, proceso HOCl)

1. Process Intensification: microreactors



O.H. Laguna et al. / Chemical Engineering Journal 275 (2015) 45–52

Disadvantages:

- Manufacturing method with several phases
- Catalyst deposition
- Scale-up



Micromining



Stacking



Welding

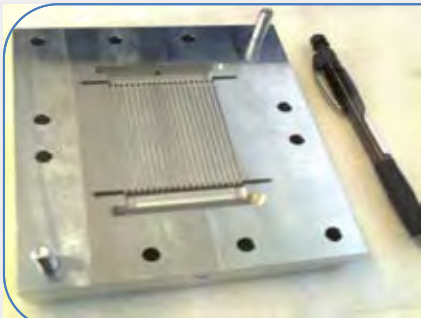


Peripherals

Stages needed for the manufacture of microreactors.

Adapted from S. Cruz et al. (2011). Chemical Engineering Journal 167. 634-642

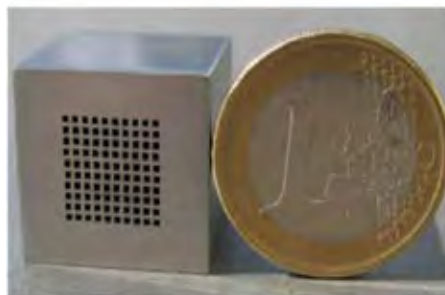
1. Process Intensification: microreactors



Methanol reforming to H₂

<http://dx.doi.org/10.1016/j.ijhydene.2015.11.047>

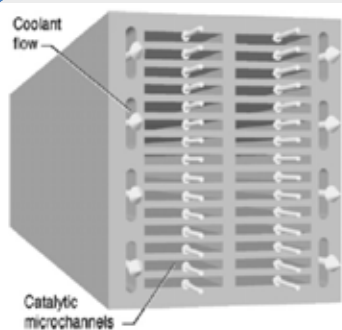
PROX reaction



O.H. Laguna et al. 2011 doi:10.1016/j.cej.2010.08.088

CO₂ hydrogenation to methane

Pacific Northwest National Laboratory USA. K.P. Brooks et al. *Chemical Engineering Science* 62 (2007) 1161 – 1170



Nitrobenzene hydrogenation to aniline

www.hzdr.de/db/Cms?pOid=42528&pNid=3367

Fischer-Tropsch reaction

Velocys, Inc. 2013



2. Tecnalia's millichannel reactor

Based on new additive technologies, Tecnalia R&I has developed a **microstructured reactor** consisting of several tubes with internal diameter in the range of millimeters (1-4) **enhancing both the mass and energy transfer.**



The reactor can be designed and integrated in a pilot plant for a specific process

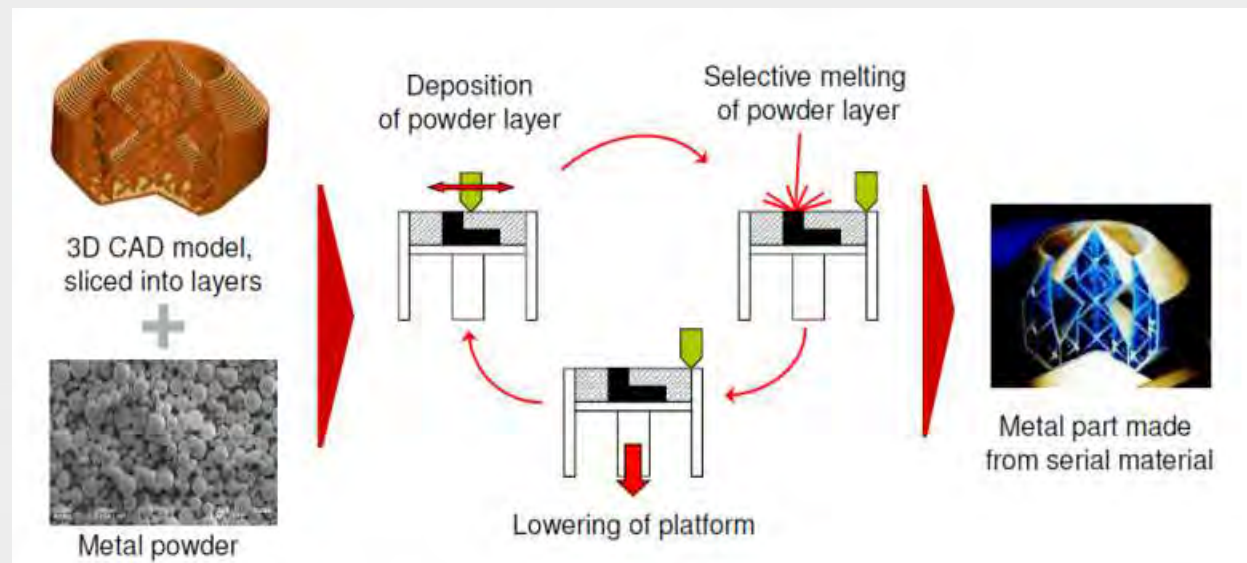
2. Tecnalia's millichannel reactor

Design features of the reactor

- a high length / diameter ratio
- a good heat transmission / evacuation
- a dimensional uniformity of tubes
- a good thermal and mechanical stability
- a simple manufacture method in one piece, "without layers"
- catalyst filling the tubes

Reactor manufacture

Selective
Laser
Melting



2. Tecnalia's millichannel reactor

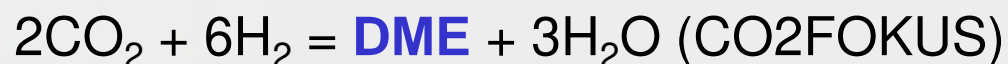
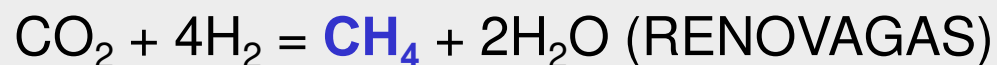
| Features | Advantages |
|--|---|
| Intimate contact between substrates/catalysts | <ul style="list-style-type: none"> • High mass transfer • Decreases the residence time • Increases 10-20% performance vs conventional reactors |
| High area/volume ratio | <ul style="list-style-type: none"> • High heat transfer: stainless steel AISI 316L • Minimizes hot spot formation • Limits the propagation of an eventual flame |
| Low volume | <ul style="list-style-type: none"> • Savings in production materials, space and energy • Reduced pressure drop |
| Reduced diffusion distances | <ul style="list-style-type: none"> • Minimizes hot spot formation • High heat transfer |
| Scaling-up (not by increasing reactor size) | <ul style="list-style-type: none"> • Faster implementation of the process on an industrial level • Flexibility to be adapted to the production needs |
| Thermic fluid introduced through reactor gaps | <ul style="list-style-type: none"> • Removes heat continuously through the entire reactor • Manages heat in an efficient and flexible way |

2. Tecnia's millichannel reactor

The millichannel reactor technology is appropriate for **exothermic reactions** and allows to overcome **mass transference** limitations

Our applications

- Hydrogenation
- Butanediol from acetoin (Patented)
- Fischer-Tropsch synthesis
- **CO₂ transformation**



3. Catalytic tests in Sabatier reaction

Comparison traditional fixed-bed vs. millichannel reactor

Fixed-bed:

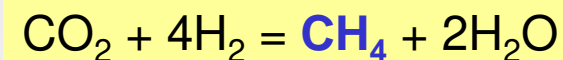
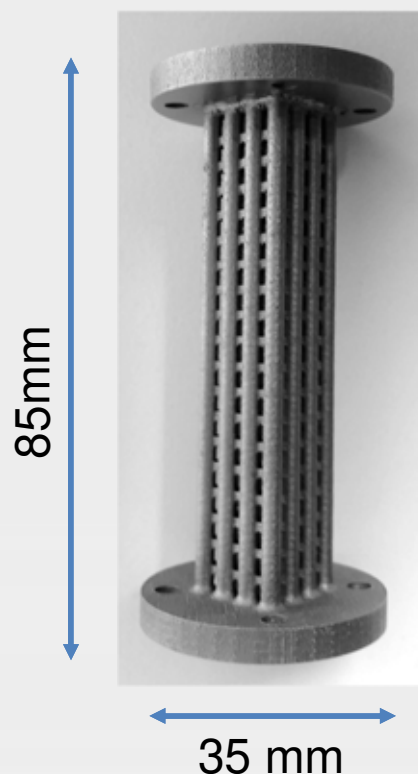
9 mm inner diameter



Millichannel reactor:

16 channels

1.75 mm inner diameter



CATALYST Ni/ γ -Al₂O₃

Metal content (Ni) 25.2 %

Particle size < 220 μm

Bulk density 0.85 gr/cm^3

REACTION CONDITIONS

GHSV 80 $\text{NL. g}_{\text{cat}}^{-1}.\text{h}^{-1}$

H₂/CO₂ 4

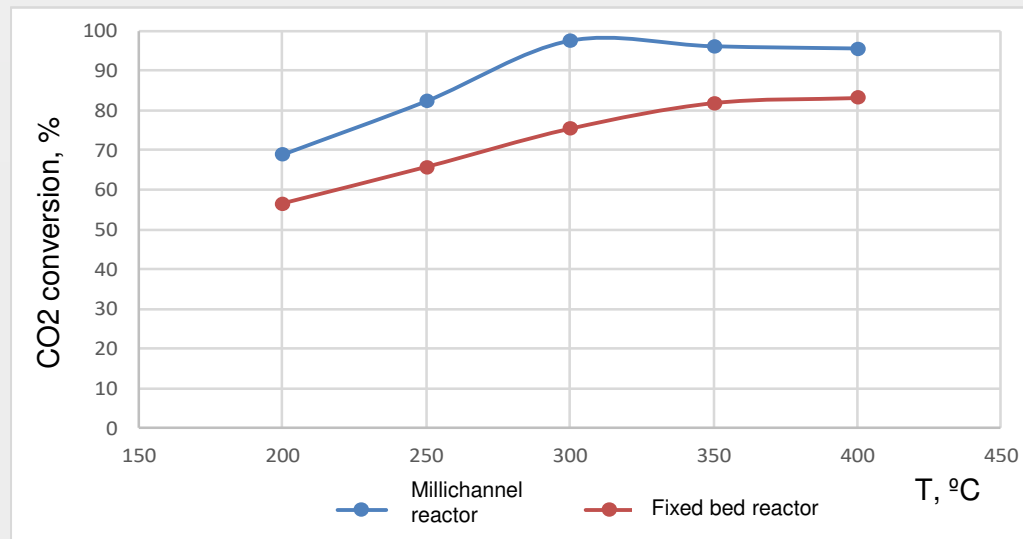
Catalyst mass 2.56 g.

3. Catalytic tests in Sabatier reaction

Comparison traditional fixed-bed vs. millichannel reactor

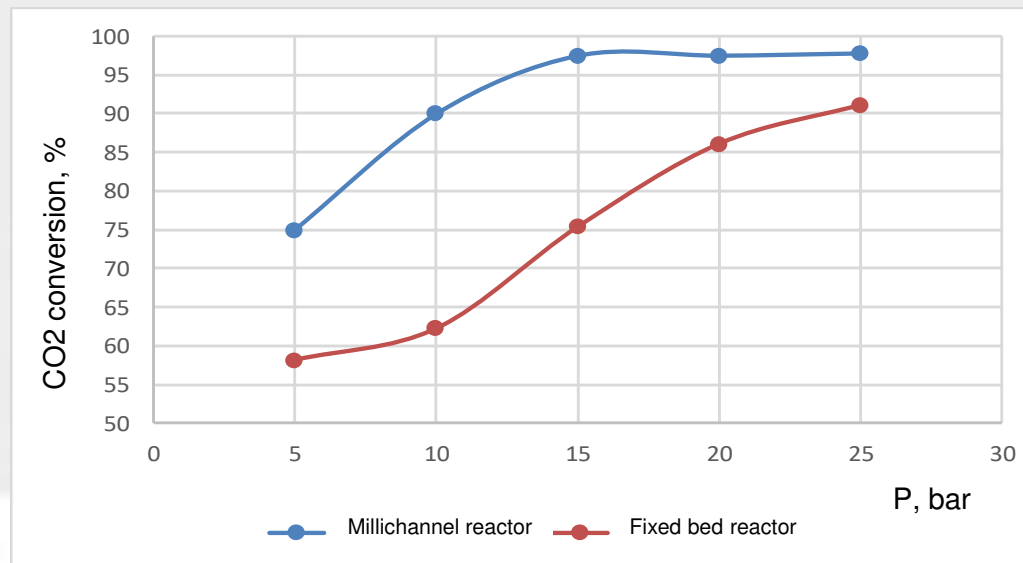
Temperature effect

- At 15 bar



Pressure effect

- At 300°C



CO₂ conversion
increase up to
27,7%



Better mass
transfer

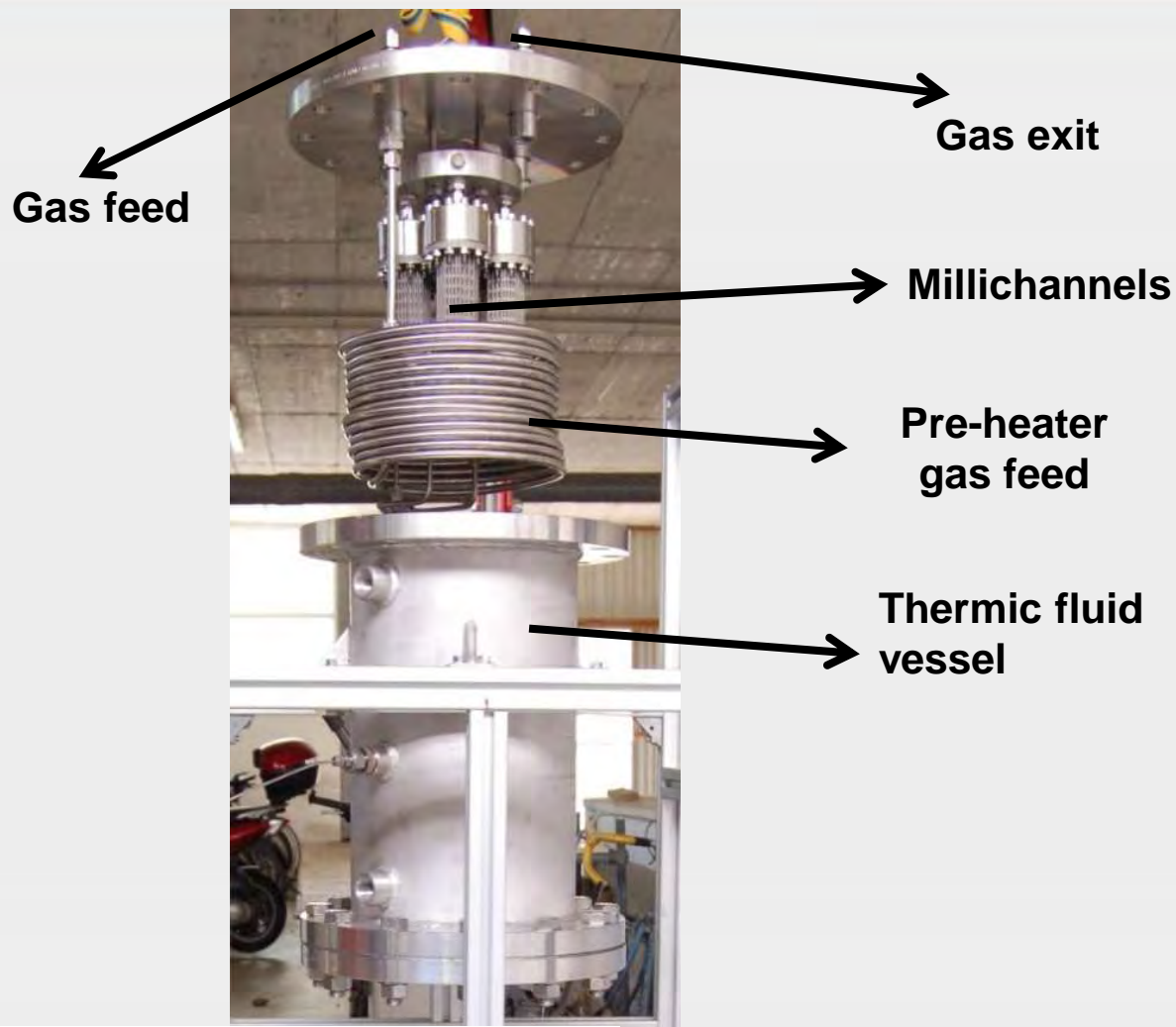
4. Millichannel reactor scaling-up



15kW pilot plant

CO₂ methanation

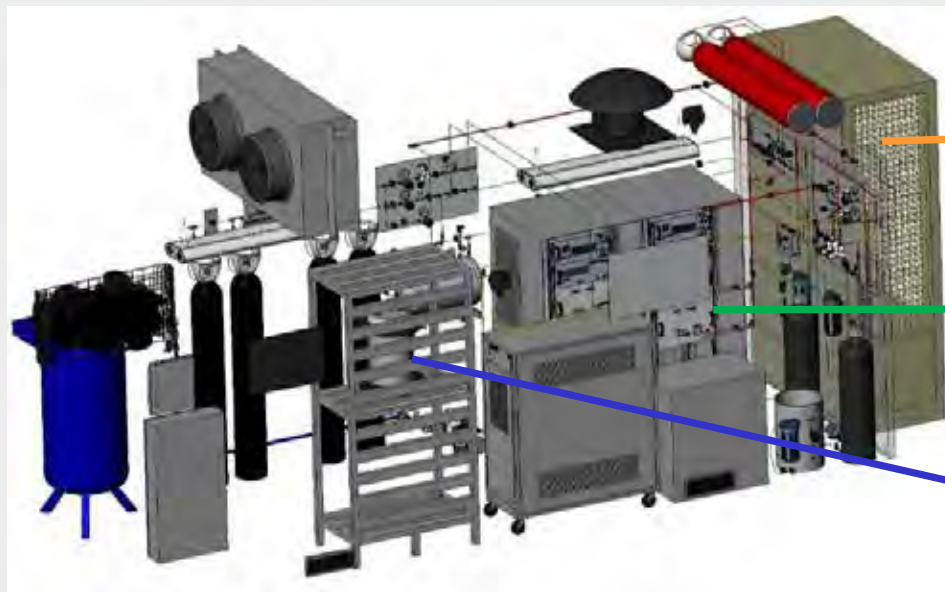
- Feeding: cleaned biogas
- TRL 5
- Number of channels: 388
- ICP-CSIC catalyst (Ru/CeO₂)



| Input | | | Output | | |
|-----------------------|------------------------|------------------------|-----------------------|------------------------|------------------------|
| H ₂ , %Vol | CO ₂ , %Vol | CH ₄ , %Vol | H ₂ , %Vol | CO ₂ , %Vol | CH ₄ , %Vol |
| 53,5 | 13,4 | 33,1 | 2,7 | 1,7 | 95,6 |

RENOVAGAS project, funded by the Spanish Ministry of Economy and Competitiveness (MINECO) within the call Retos-Colaboración 2014 (RTC-2014-2975-3).

4. Millichannel reactor scaling-up



→ Distribution panel

→ Electrolyser/H₂ supplier

→ Millichannels (388) reactor



5. Conclusions

- TecNALIA has developed a microchannel reactor for exothermic reactions.
- The reactor:
 - allows a good mass and energy transfer
 - is easy to scale-up by adding channels
 - has a flexible design
 - has a huge number of potential applications
 - has been validated for Sabatier reaction: better results than fixed-bed reactor.

www.tecnalia.com

Thank you for your attention





Production of Sustainable aircraft grade Kerosene from water and air powered by Renewable Electricity, through the splitting of CO₂, syngas formation and Fischer-Tropsch synthesis

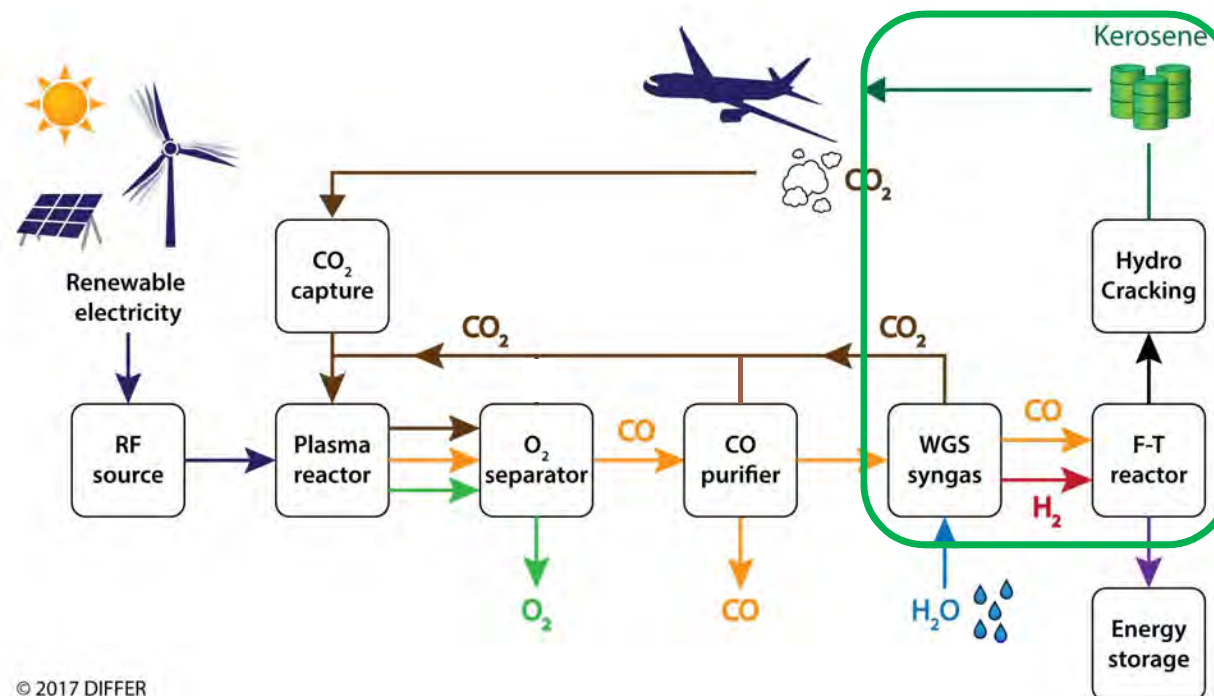
The KEROGREEN syngas route to alternative fuels and chemicals

Francisco Vidal Vázquez (Dr. Sc.)

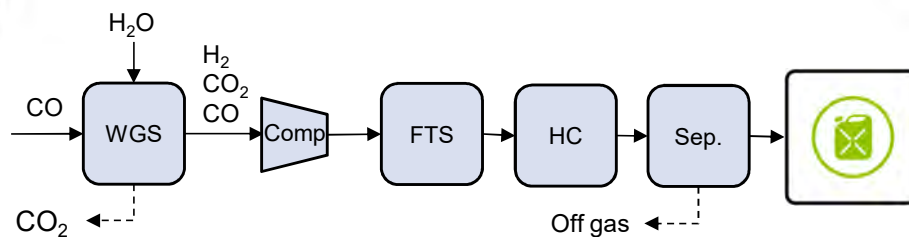
Institute for Micro Process Engineering (IMVT), Karlsruhe Institute of Technology (KIT)

International Workshop on CO₂ Capture and Utilization, 16-17 February 2021, Online Workshop

KEROGREEN: CO route to kerosene



© 2017 DIFFER



Dr. Francisco Vidal Vázquez – Int. Workshop on CO₂ Capture and Utilization, 16-17 February 2021, Online Workshop

This project has received funding from the European Union's Horizon 2020 Research and Innovation Programme under GA-Nr. 763909



Syngas Production via Water-Gas Shift (WGS) reaction

- WGS reaction:

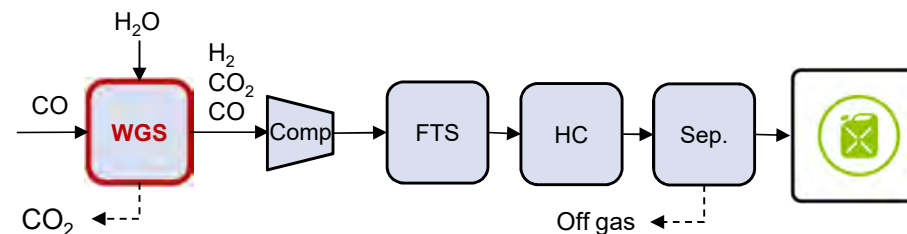


- Chemical equilibrium:

- Independent with pressure
- Favourable at low temperature

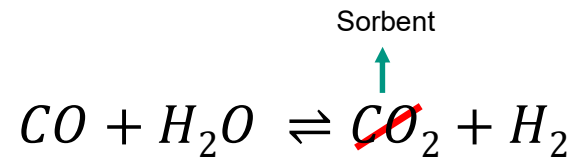
- Different catalysts for different temperatures

- 300 – 400 °C: Fe/Cr-cat (HT-WGS)
- 200 – 300 °C: Cu/Zn-cat (LT-WGS)



Sorption-Enhanced Water-Gas Shift (SE-WGS)

■ SE-WGS:



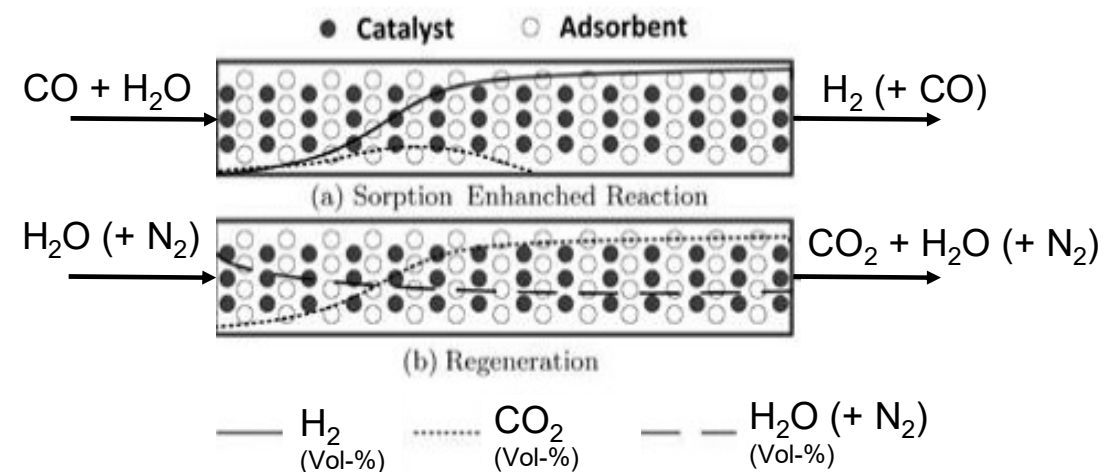
■ Solid sorbent is used for *insitu* CO₂ removal

- Dynamic operation of reactor

■ The sorbent is mixed with the catalyst and placed in the reactor

■ Other advantages:

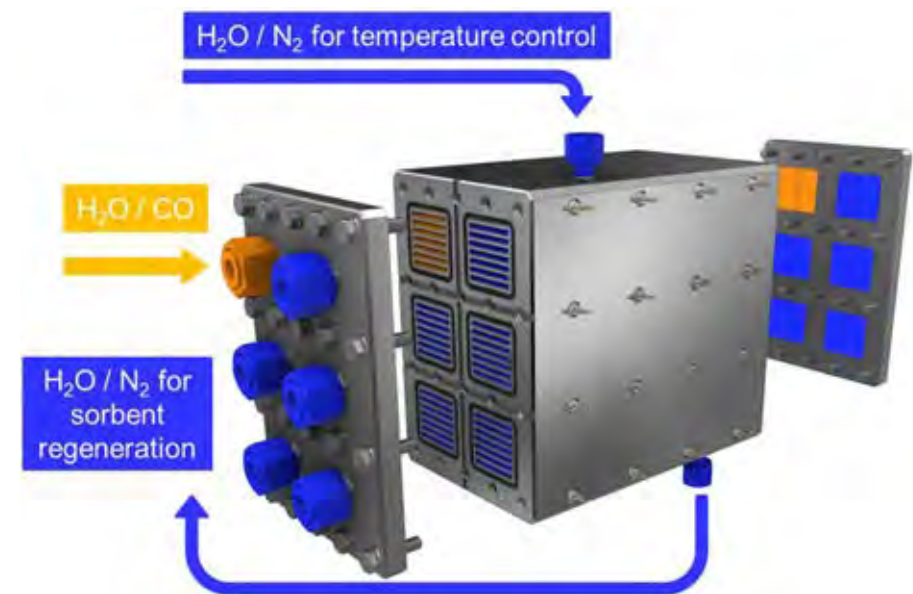
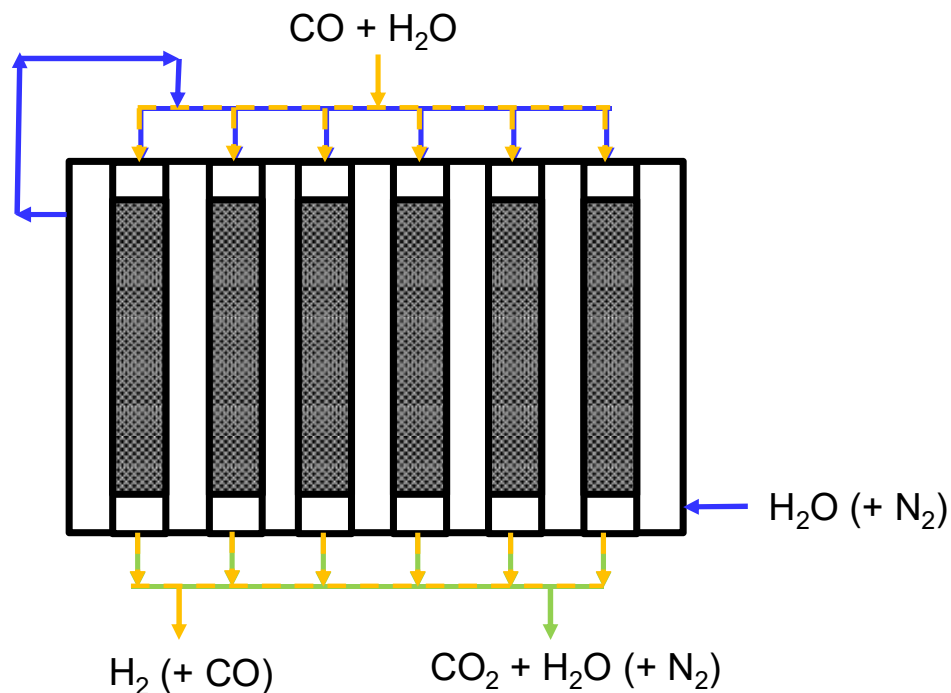
- Higher conversion
- Reduction of required steam for the WGS
- Overall-simplification of the process (WGS + CO₂ removal)
- CO₂ recycle up-stream of the process



Modified figure from Rodrigues et al. 2017

SE-WGS reactor for KEROGREEN

- SE-WGS reactor has 6 different beds which are operated dynamically in order to keep constant outlet flow of syngas
 - Cycle of Reaction/Depressurization/Regeneration/Pressurization

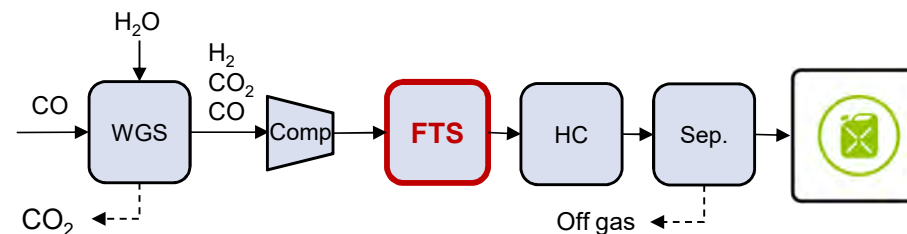
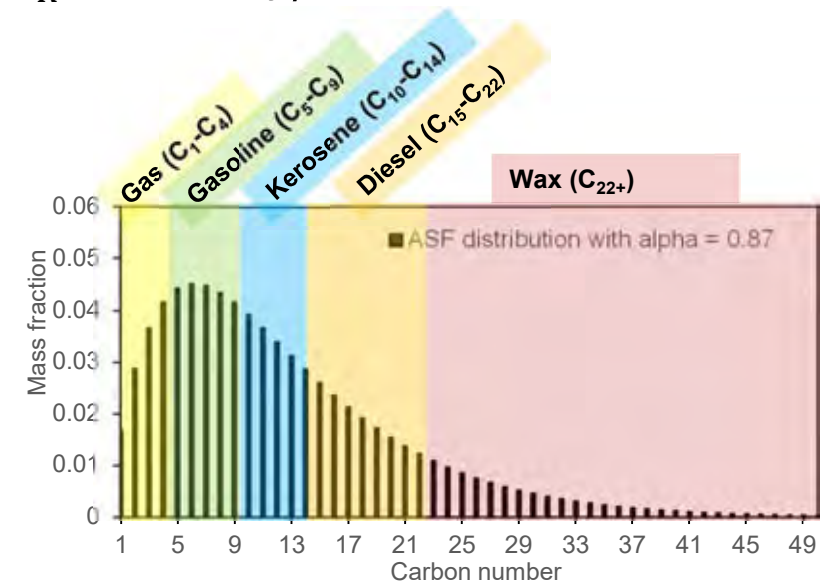


Fischer-Tropsch Synthesis

- Highly exothermic heterogeneously catalysed polymerization reaction



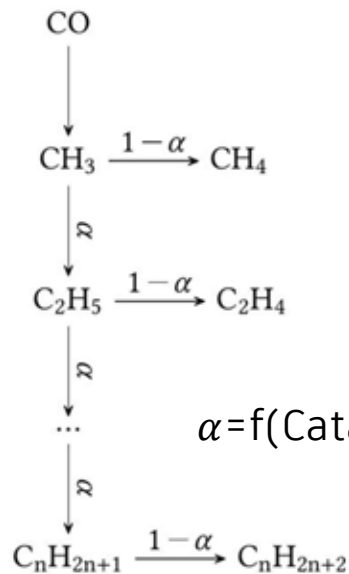
- Chemical equilibrium:
 - Favourable at high pressure and low temperature
- Different catalysts for different application:
 - 300 – 400 °C: Fe-based cat.
 - Shorter chain hydrocarbons, mainly olefins
 - 200 – 250 °C: Co-based cat.
 - Long chain hydrocarbons, mainly parafins



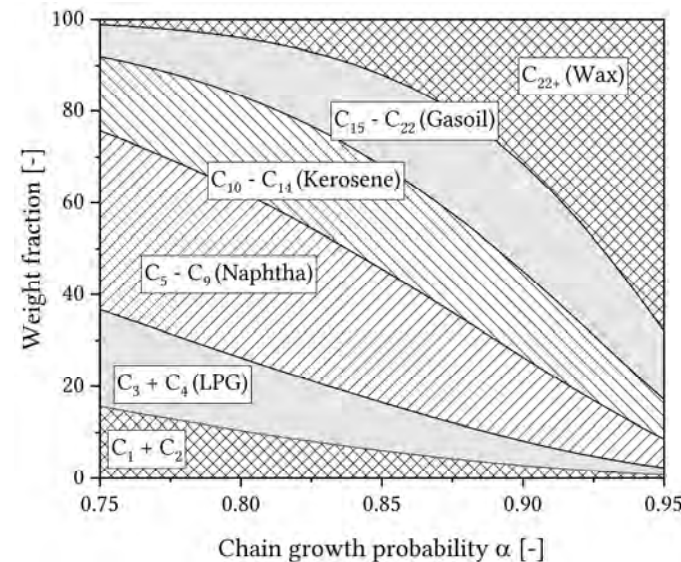
Fischer-Tropsch Synthesis: ASF distribution

- Product distribution can be approximately represented via Anderson-Schulz-Flory (ASF) model – **Chain growth probability**

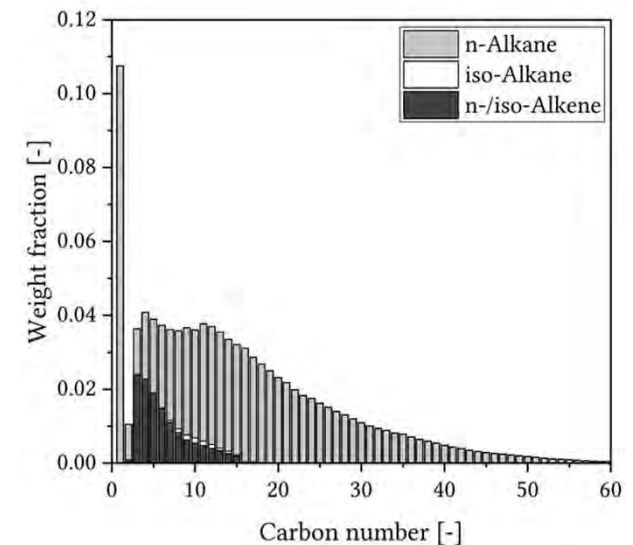
$$W_n = n \cdot (1 - \alpha) \cdot \alpha^{n-1}$$



$$\alpha = f(\text{Catalyst, } T, p, \dots)$$



Real FTS product composition using Co-based catalyst



- Higher CH₄ selectivity
- Lower C₂ selectivity
- Olefin formation
- Formation of alcohols (low)



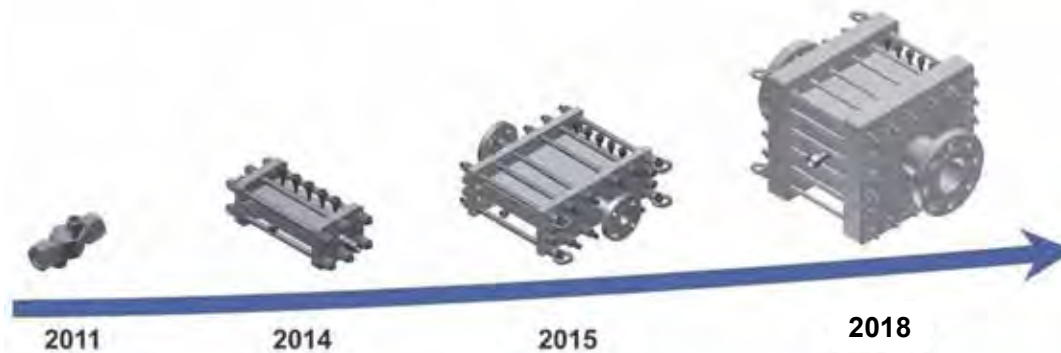
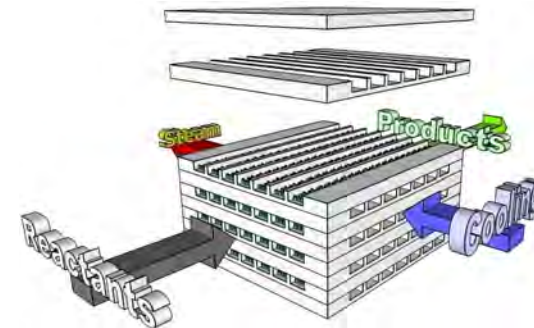
Dr. Francisco Vidal Vázquez – Int. Workshop on CO₂ Capture and Utilization, 16-17 February 2021, Online Workshop

This project has received funding from the European Union's Horizon 2020 Research and Innovation Programme under GA-Nr. 763909



Fischer-Tropsch Synthesis reactor for KEROGREEN

- Microstructured reactor cooled by water evaporation
 - Compact reactor
 - Excellent control of reaction temperature
 - Good performance at wide range of reaction conditions
 - Good performance under dynamic operation
- Developed at KIT-IMVT → Commercialized and upscaled by INERATEC



Hydrocracking of heavier FTS products

- Hydrocracking (HC) basic example reaction:

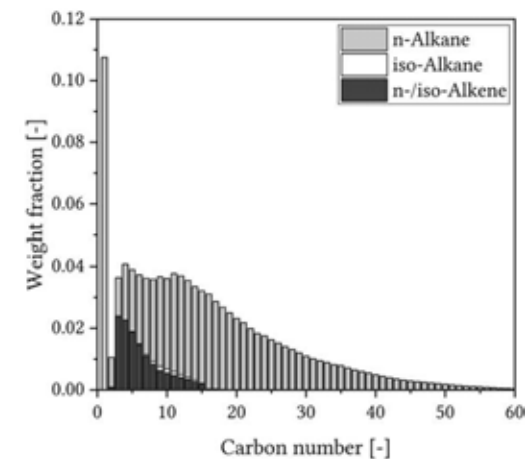
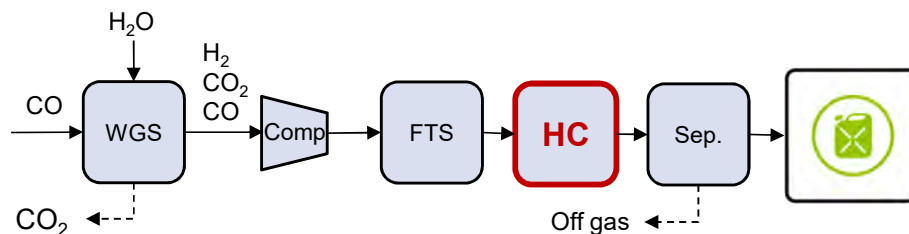


- Typical operating conditions:

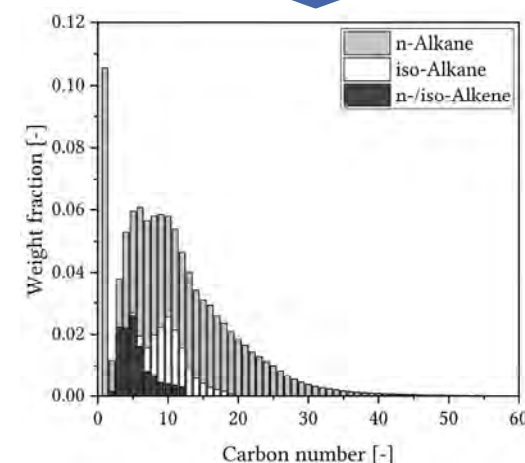
- 250-350 °C
- 20-50 bar
- Bifunctional catalyst (Metal/Zeolite)

- Purpose of HC:

- Increase liquid fuel fraction (remove waxes)
- Decrease alkene (olefins) content → not applicable to kerosene
- Increase isomer content → improve cold flow properties

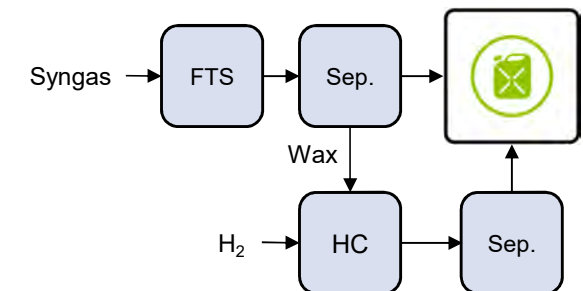
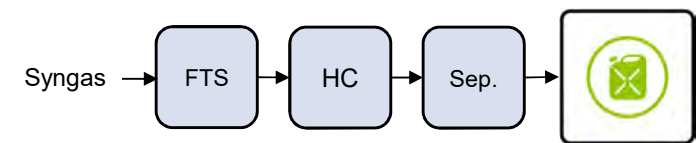


HC



Hydrocracking of FTS products

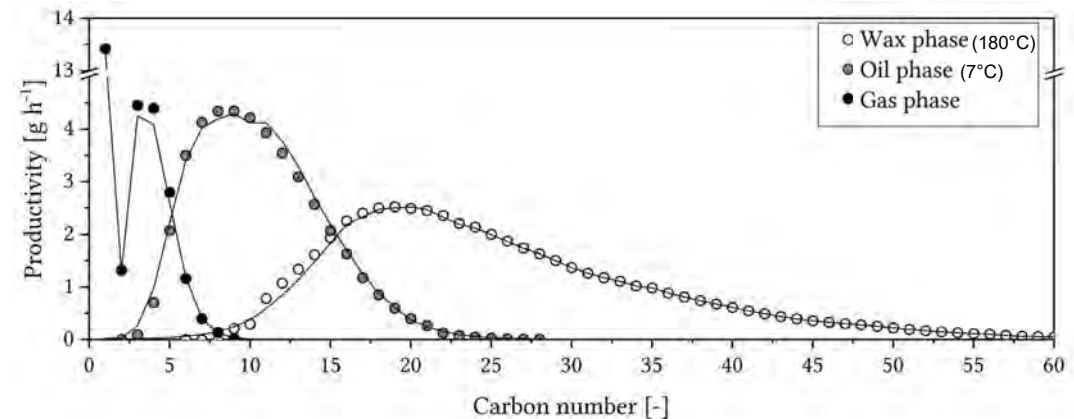
- HC general considerations:
 - Partial conversion of waxes (C_{22+}) in order to avoid overcracking
 - Process design considerations:
 - HC of the full FTS outlet:
 - Simpler process configuration
 - Risk of secondary cracking (overcracking) due to CO in the gas phase
 - Cracking of non-wax fraction can happen
 - HC only of the wax phase:
 - More complex process configuration
 - Pure H_2 to the hydrocracker
 - Better product distribution



Product separation

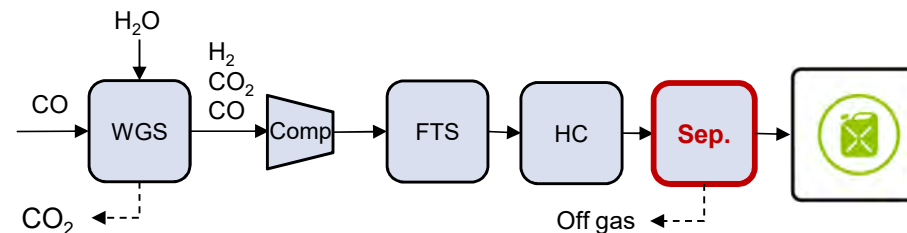
■ Flash separation

- Hot flash (180-220 °C) → Wax product
- Cold flash (5-10 °C) → Liquid product
- Rest → Gas phase (Off-gas)



■ Distillation is required for sharp separation of product

- Kerosene grade only achievable by distillation

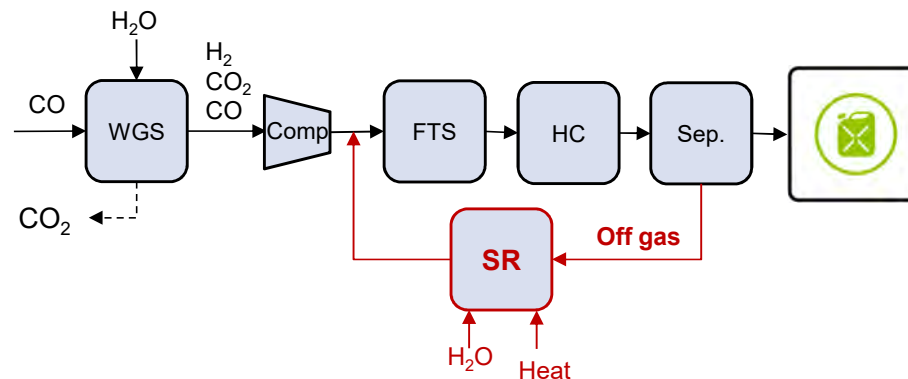


Off-gas recirculation

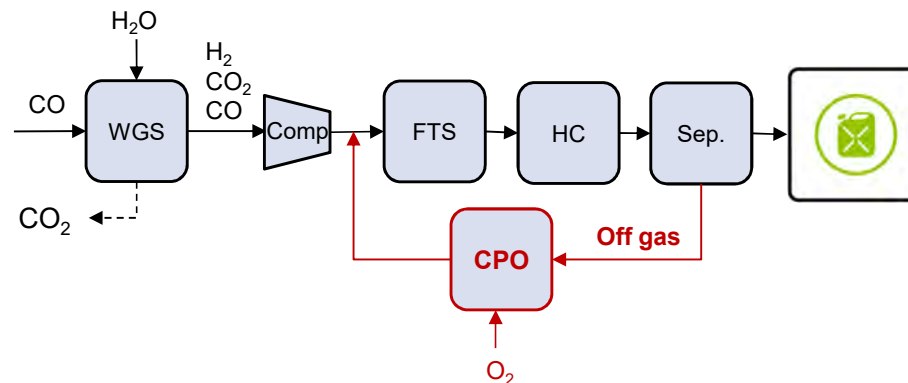
- Off-gas composition → H_2 , CO, methane, C_2 , C_3 , C_4 , C_5 (traces of C_{6+}), maybe CO_2 too

- Options for off-gas recirculation:

- Steam reforming (SR)



- Catalytic partial oxidation (CPO).



Summary and conclusions

- Conclusions
 - Not full selectivity to kerosene can be achieved ($< 50\%$)
 - However, other valuable products such as gasoline, diesel and waxes are obtained.
 - Isomerization stage still might be required to achieve fuel grade
- Other general considerations for process integration
 - Heat and material integration between the different components of the KEROGREEN plant is crucial for maximizing energy and carbon efficiencies
 - Maximize energy and carbon efficiency
 - Difference when using fossil fuels as raw material. Cost structure changes (more OPEX) and plant size changes
 - Techno-economic and LCA analyses are the ultimate test to decide what could be the best option



Francisco Vidal Vázquez

Institute for Micro-Process Engineering, Karlsruhe Institute of Technology

Francisco.vidal-vazquez@kit.edu✉

www.imvt.kit.edu



Acknowledgements:

Tabea Stadler

Peter Pfeifer

Robin Dürrschnabel

Georg Rabsch

Lucas Brübach

Hannah Kirsch

**THANK YOU FOR YOUR
ATTENTION**

RELATED PUBLICATIONS

T. J. Stadler, P. Barbig, J. Kiehl, R. Schulz, T. Klövekorn, and P. Pfeifer, "Sorption-Enhanced Water-Gas Shift Reaction for Synthesis Gas Production from Pure CO: Investigation of Sorption Parameters and Reactor Configurations," *Energies*, vol. 14, no. 2, p. 355, 2021

H. Kirsch *et al.*, "CO₂-Neutral Fischer-Tropsch Fuels from Decentralized Modular Plants: Status and Perspectives," *Chemie-Ingenieur-Technik*, vol. 92, no. 1–2, pp. 91–99, 2020

This project has received funding
from the European Union's Horizon
2020 Research and Innovation
Programme under GA-Nr. 763909



INTERNATIONAL WORKSHOP ON CO₂ CAPTURE AND UTILIZATION

TU/e - EINDHOVEN - 16-17 FEBRUARY 2021

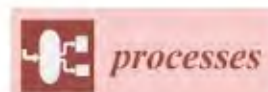
Session 3B (chairperson Oana David)

- 11:45-12:05 Msc. A. Sliousaregko - Industrial membrane requirements for CO₂ removal from different gas mixtures - Current practices and developments
- 12:05-12:25 Dr. I. Kim - Technologies demonstration in REALISE
- 12:25-12:45 Mr. Paul Cobden and Prof. C. Abanades - Pilot preparation for demonstration in the C4U project
- 12:45-13:05 Mr. T. Swinkels - Decentralized FA based power generators
- 13:05-13:25 Dr. L. Roses - Design and development of a membranebased post-combustion CO₂ capture system

ORGANIZED BY



SPONSORED BY



Industrial membrane requirements

for CO₂ removal from different gas mixtures -

Current practices and developments

Anastasia Sliousaregko, R&D Process Engineer, asliousaregko@dm-t-et.nl

Yndustrywei 3, 8501 SN Joure, Netherlands



Who are we?

**Our mission:
to create a clear
and prosperous
future**

- Engineering firm specializing in biogas upgrading and gas desulfurization
- Over 150 references and more than 30 years of experience
- Global provider of solutions that help build a sustainable future
- Award-winning portfolio

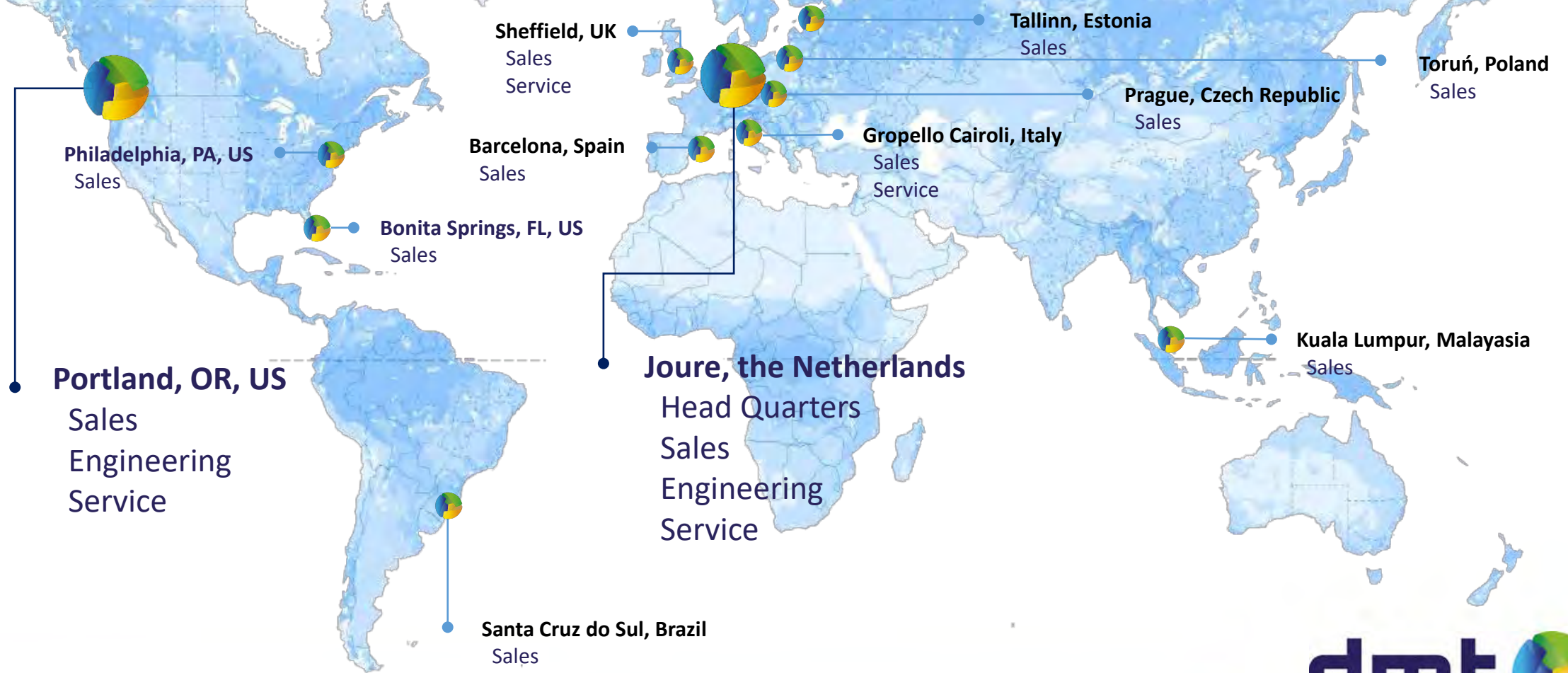
Biogas Upgrading



Gas Desulfurization



Offices, Sales & Service



Your local, global solutions provider

Membrane industrial requirements

Post-combustion flue gas capture

Natural gas sweetening

Biogas upgrading

For the full state-of-the-art report



BioCo
Mem

dmto
International



Post-combustion flue gas capture

Membrane industrial requirements

Mitigation of CO₂ emissions with (CCS)

- Insufficient incentive for the industrial parties
 - Costly overall process (capture, transport and storage)
 - DAC at low TRL. Delocalized emitters are more expensive
 - CO₂ capture range of 35-60 €/ton higher than EUA of 25-40 €/ton
- CO₂ separation techniques
 - Chemical/Physical absorption (Amines as ref.)
 - Membrane separation
 - Adsorption-absorption by solid materials
 - Calcium Looping
 - Cryogenic distillation



[Petra Nova](#), Texas US (2016-2019), Amine absorption commercial plant

Industrial requirements

- 4-20% CO₂ ingas from power generator
 - Low/Atmospheric pressure
 - Vapour, O₂, SO_x, NO_x, NH₃, ...
 - High flows 40,000 Nm³/h
- To be competitive with amines or 90% CO₂ capture for installed prices not less than 50 €/m²

| Specifications | Value | Unit |
|---|--------|------------------|
| P _{CO2} | >2,250 | GPU |
| CO ₂ /N ₂ selectivity | >30 | --- |
| Temperature | 100 | °C |
| Design pressure | 7 | bar |
| Costs | < 100* | €/m ² |

*Target set by the BioCoMem project

[Haibo Zhai \(2019\)](#)

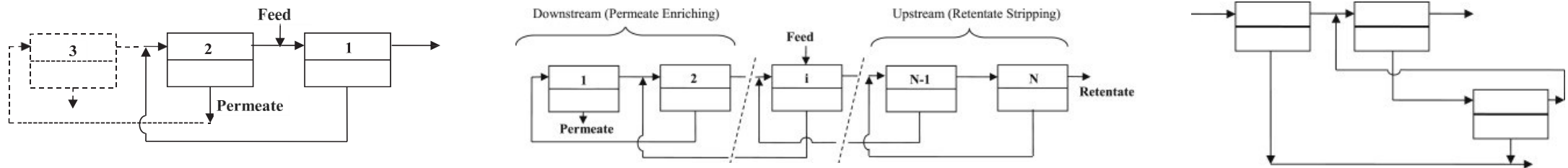
Other requirements

- Compatibility and stability
- Lifetime
- Fabrication and packaging
- Fouling

Membrane-based PCC

- PIM, PEO, TR, PI – high performance polymeric-based membranes
- FSC pilot testings
 - promising under humidified conditions ($5 \text{ m}^3(\text{STP})/(\text{m}^2 \cdot \text{h} \cdot \text{bar})$ and $\text{CO}_2/\text{N}_2 > 500$), NTNU

Configurations



[Kalipour et al \(2015\)](#)

Natural gas sweetening

Membrane industrial requirements

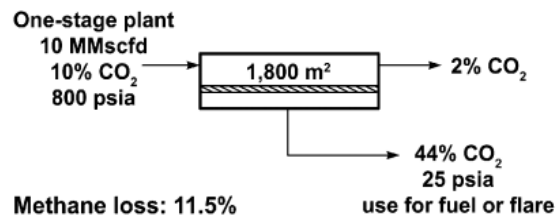


Current practices

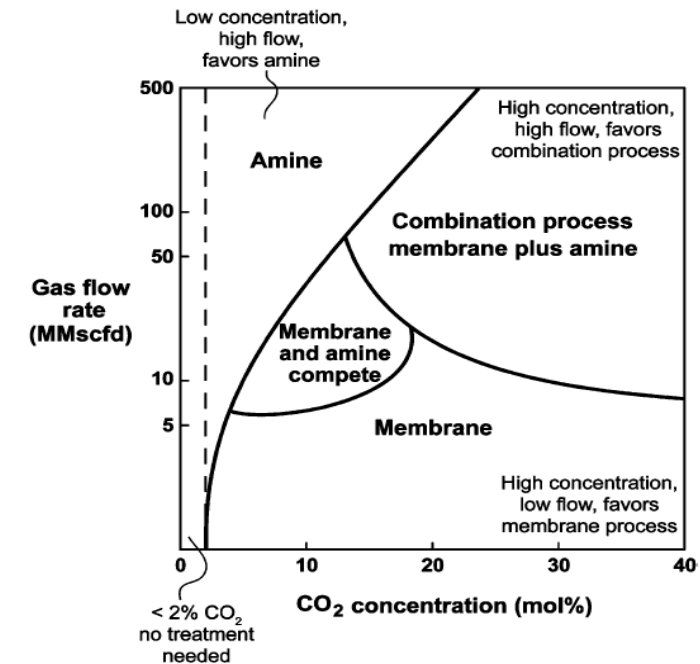
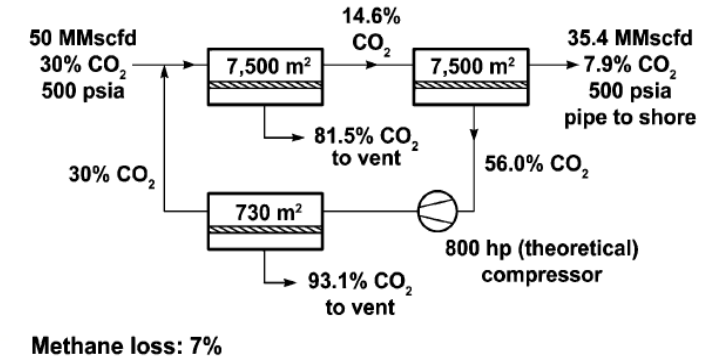
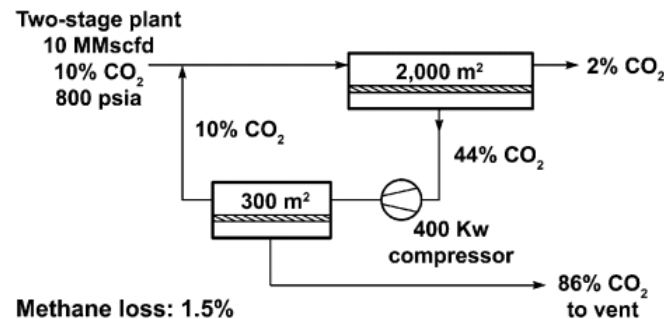
- Amine scrubbing (higher flows, lower CO₂ concentrations)
- Membrane separation (5-10% market share)
 - Polymeric: CA, PA, PI, perfluoro-polymers
 - Silicone composite
 - Hybrid amine membranes

Configurations

- Pretreatment (plasticization)
 - (aromatics, heavy hydrocarbons, oil mist and particulates)
- 1-stage (gas-wells), 2-stage (higher stream) and 3-stage (off-shore)



[Baker, Lokhandwala \(2008\)](#)



Industrial requirements

- From ~8% CO₂/ 80% CH₄
 - H₂O, N₂, H₂S
 - 20,000 - 200,000 Nm³/h
 - Atmospheric pressure
- Grid quality
 - H-gas: > 96 vol% CH₄
 - L-gas: 88-92 vol% CH₄
 - Other parameters
 - WI, calorific value, total sulfur, etc
- Permeance and module size
- Asymmetric hollow fibers
- 4 – 12'' module diameter

State-of-the-art materials

- Polymeric (PEBA, PEO-based)
- Facilitated transport
- Composites (Mixed-matrix membranes)
- Carbon molecular sieve

| Network | Gas | Pressure | Pressure (Netherlands) |
|---------|-----------------|------------------|------------------------|
| HTL | G-gas and H-gas | usually > 16 bar | > 45 bar(a) |
| RTL | Mostly G-gas | about 4-16 bar | 11 – 40,5 bar(a) |
| RNB | Mostly G-gas | < 4 bar | 9 / 4 / < 4 bar(a) |

| Sweet natural gas | Value | Unit |
|--|---------|------|
| P _{CO2} | > 100* | GPU |
| CO ₂ /CH ₄ selectivity | 50* | |
| CO ₂ | <2,5 | % |
| Temperature | 5-30 | °C |
| Design pressure | Depends | bar |

*Target set by the BioCoMem project

For H-gas grid 80% removal efficiency

Biogas upgrading

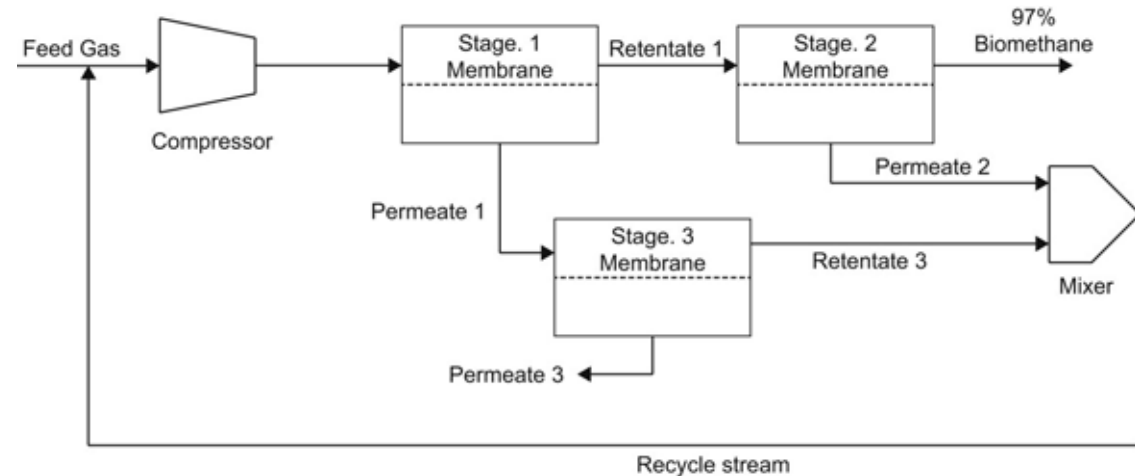
Membrane industrial requirements

Current practices

- Water scrubbing
- Membrane separation (36% market share by 2025)
 - Industrially dominant polymeric membranes: CA, Psf, PI
- Chemical scrubbing
- PSA

Configurations

- CH₄ recovery
- Specific energy
- Specific area
- Cost
- Pressure
- Pretreatment



✓2-stage – 2-4% CH₄ slip*

✓3-stage – 0,5-1% CH₄ slip*

*Depending on the membrane supplier

Industrial requirements

- From ~**45% CO₂/ 55% CH₄**
 - H₂S, siloxanes/VOC, NH₃, H₂O
 - 50 - 5,000 Nm³/h
- Selectivity
- Grid quality
- Hollow fiber and spiral-wound
- 4 – 8'' module diameter

State-of-the-art materials

- Composites
- MOF
- FSC

| Biogas upgrading specifications | Value | Unit |
|--|--------|------|
| P _{CO2} | 50-100 | GPU |
| CO ₂ /CH ₄ selectivity | 50 | |
| CH ₄ slip | <0.5 | % |
| Temperature | 55 | °C |
| Design pressure | 14-20 | bar |

For H-gas grid 90% removal efficiency – depending the supplier

Thank you for your attention!

Any questions?

Follow us on social media



and find more about our products and activities



INTERNATIONAL WORKSHOP ON CO₂ CAPTURE AND UTILIZATION
TU/e - EINDHOVEN - 16-17 FEBRUARY 2021



Technologies demonstration in REALISE project

Inna Kim (SINTEF) and Juliana Monteiro (TNO)



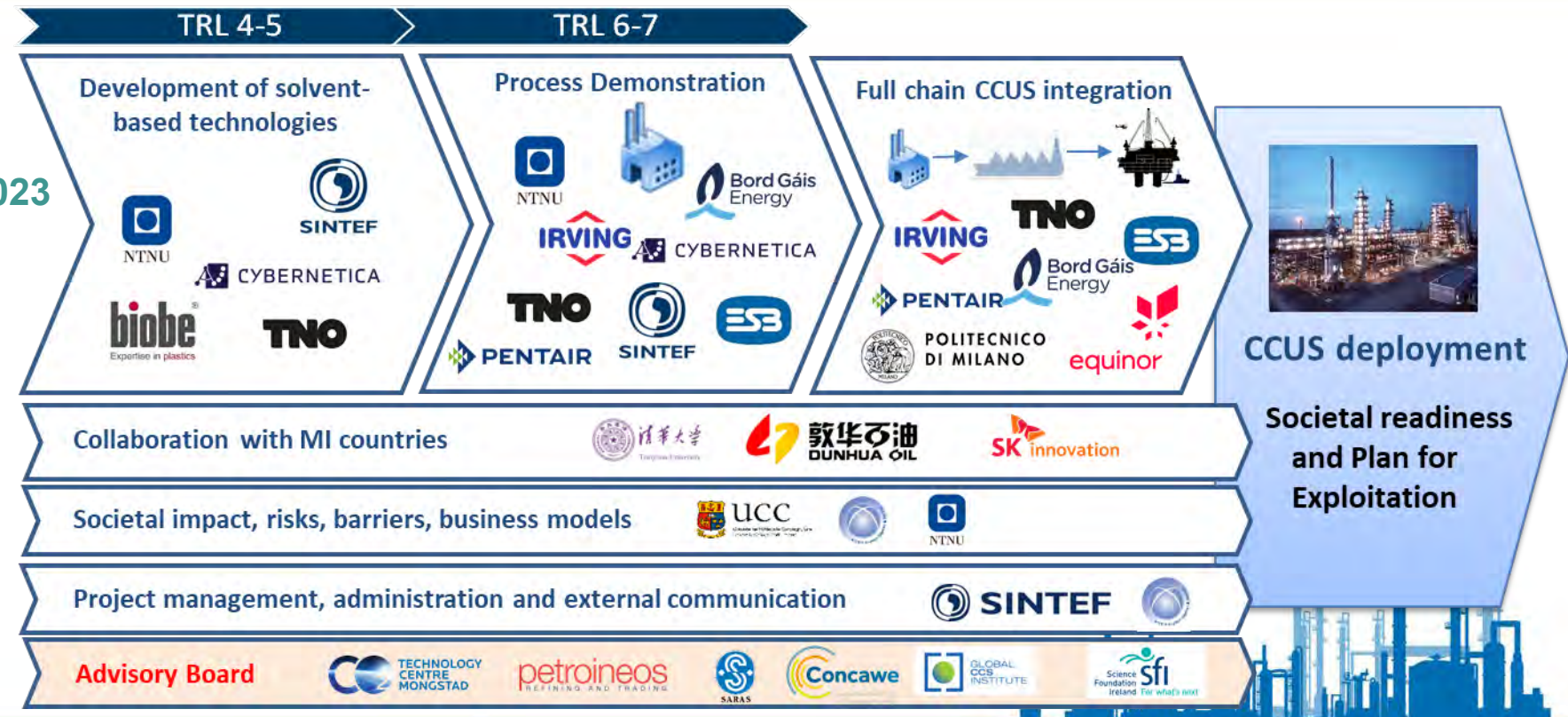
Demonstrating a refinery-adapted cluster-integrated strategy to enable full-chain CCUS implementation - **REALISE**

❑ Project period: 05.2020 - 04.2023

❑ Project partners:

- 14 EU partners
- 2 partners in China
- 1 partner in S. Korea

❑ Project budget: 7 MEuro



REALISE objectives

Reduction of GHG emissions

Increase of cost- and implementation- effectiveness

Using low-energy
HS-3 solvent →
decrease of the
energy demand of
CO₂ capture by 30%

Maximization of
performance thanks
to efficient solvent
management →
active component
losses decreased by
>80%

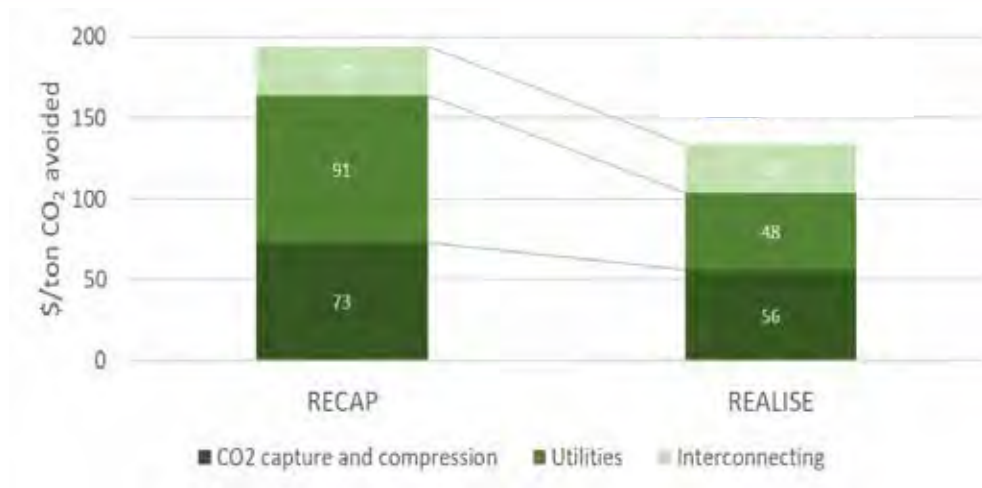
Use of plastic
equipment → lower
CO₂ capital costs by
15%

Coupling of available
facilities with the
power sector →
lower the capture
costs by at least 30%

Safe, flexible and
guided-choice
regarding CO₂
capture scenarios
thanks to an open-
access simulation
tool



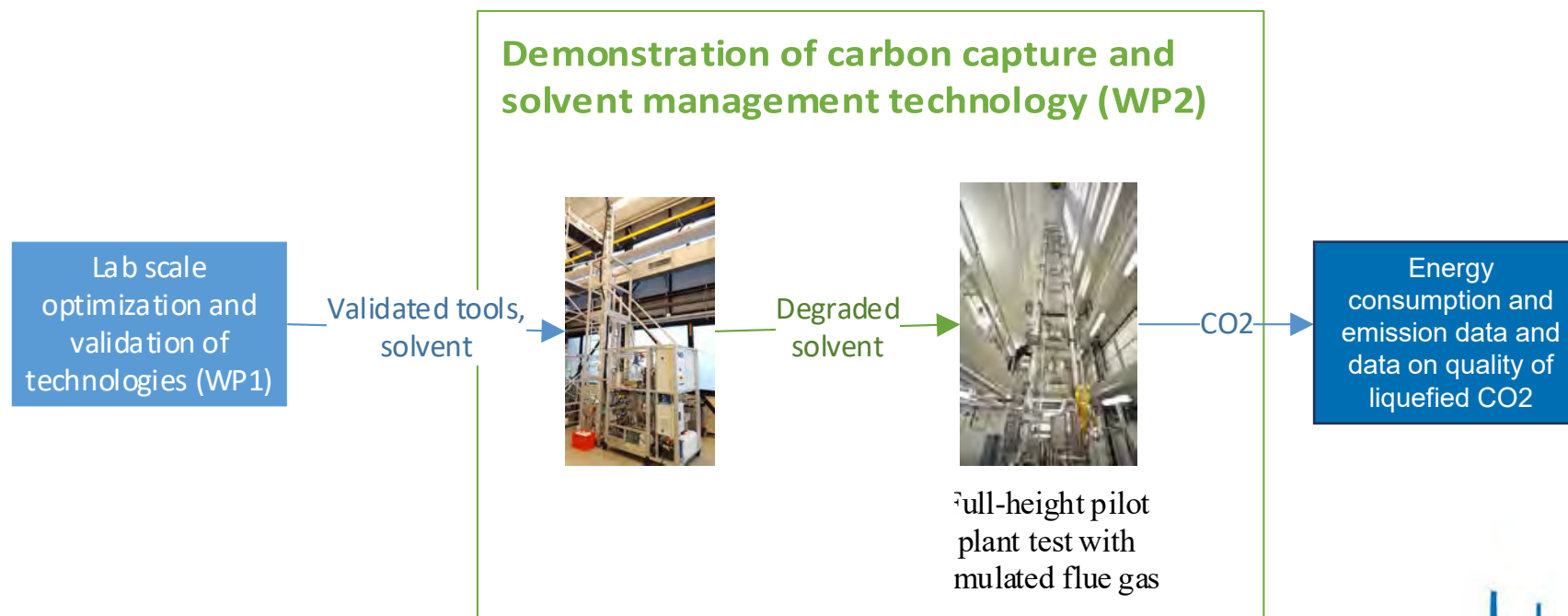
Projection of cost reduction for retrofitting CO₂ capture to refineries



"Utilities" include steam demand in the capture plant;
 "Interconnecting" means integration of capture plant with both refinery and power plant

| REALISE Innovation | Type of reduction | Reduction in capture costs | |
|--|-------------------|---------------------------------|----|
| | | \$ / ton _{CO2} avoided | % |
| Use of plastic as packing material in the absorber Reduced degradation by using DORA and IRIS Sector coupling and optimal integration and operation Novel free-to-operate solvent with low energy requirement | CAPEX | 8 | 4 |
| | OPEX | 8 | 4 |
| | CAPEX and OPEX | 24 | 12 |
| | OPEX | 20 | 10 |
| TOTAL | | 60 | 30 |

REALISE methodology for scaling up and demonstration of carbon capture and solvent management technologies from TRL 4-5 to TRL 6-7



REALISE innovations

❑ Novel low energy solvent for CO₂ capture from different flue gases

- Free-to-operate CO₂ capture solvent developed by NTNU and SINTEF (FP7 HiPerCap)

❑ Solvent management (to reduce solvent degradation and emissions):

- Oxygen removal, DORA (patented by TNO)
- Iron removal, IRIS (patented by TNO)
- Plastics as material of construction, packing, etc.

❑ Process integration

- Nonlinear model predictive control (NMPC developed by SINTEF and Cybernetica)
- Open-access simulation tool for assessing CO₂ capture strategy at refineries

❑ Social studies

- Education and Public Engagement program (Univ. Colledge Cork, see presentation by Dr. Niall Dunphy)



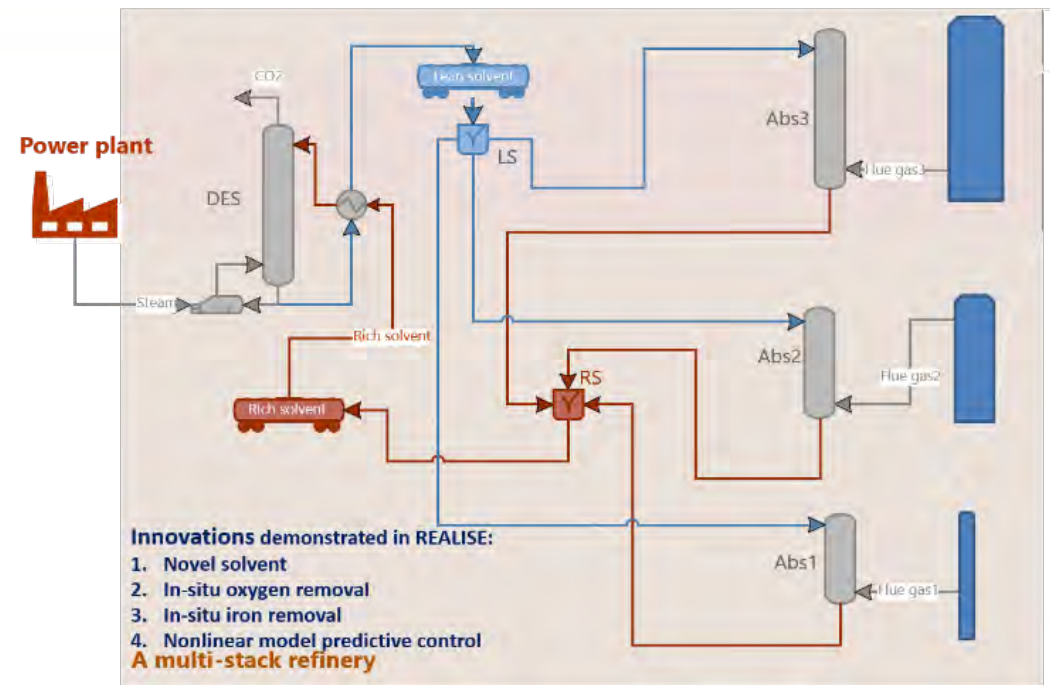
DORA prototype
(TNO)



Multi-absorber concept in REALISE



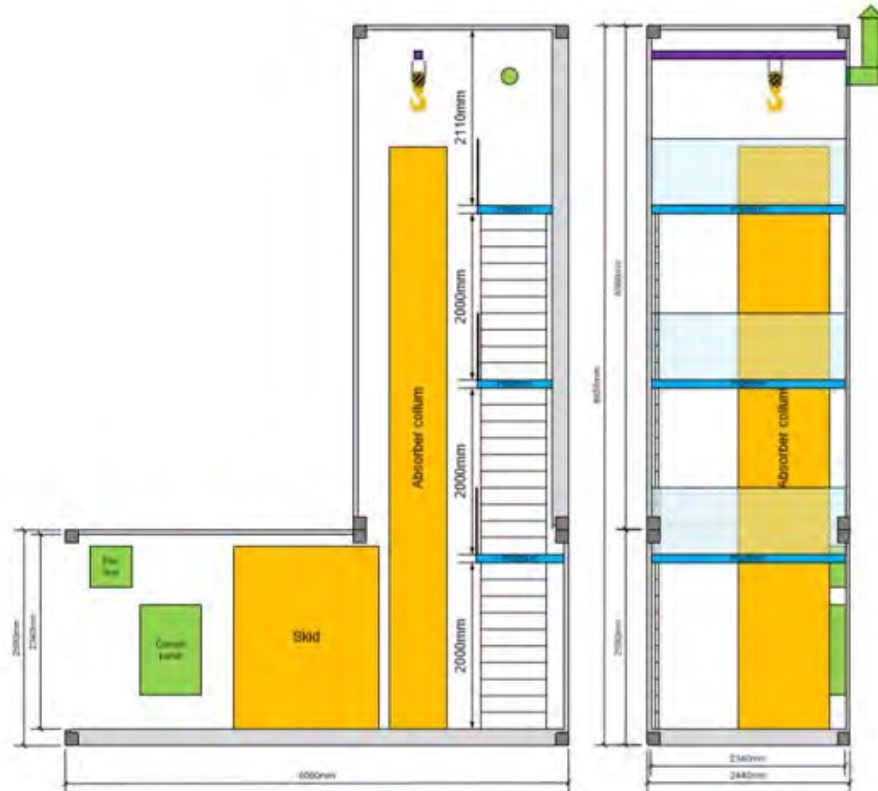
REALISE sector-coupling concept for Irving Oil Whitegate refinery and power stations in Cork, Ireland



Multi-absorber concept example



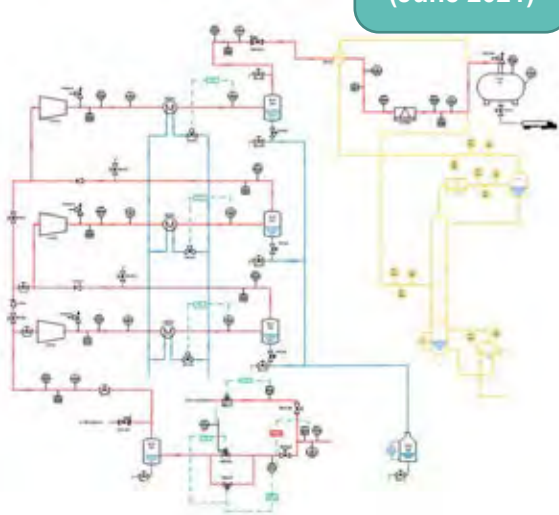
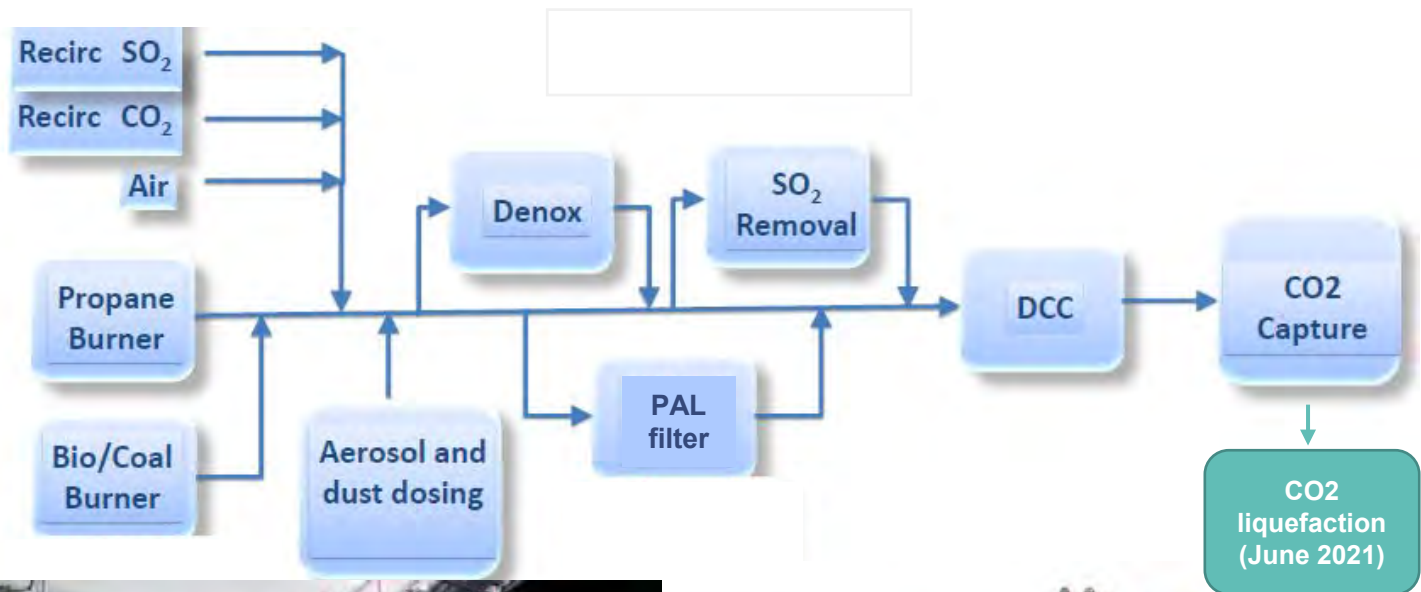
ATEX-proof mobile pilot for testing onsite operating refinery



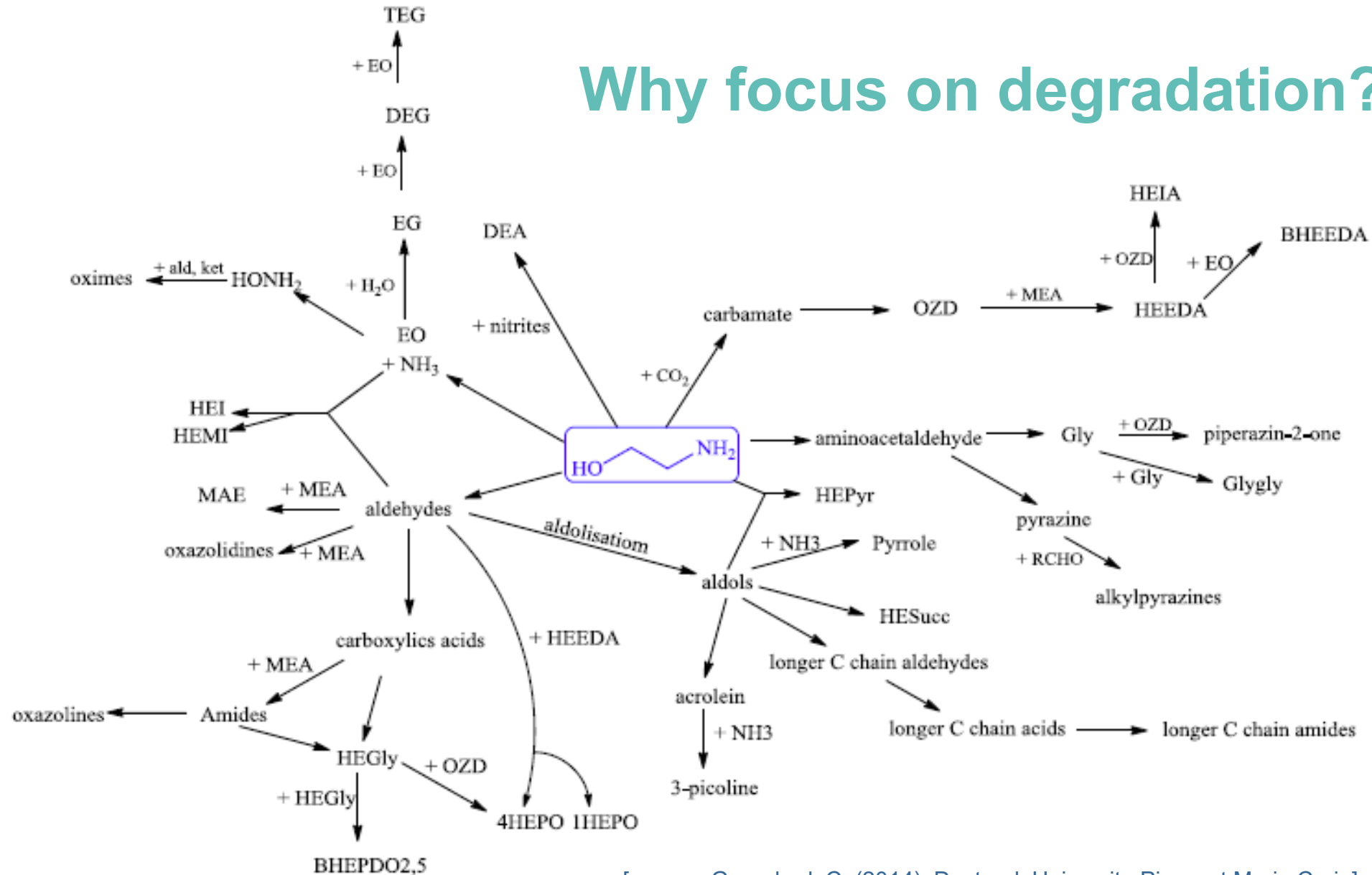
International workshop on CO2 capture and utilization, TU Eindhoven, 16-17 Feb 2020



Full-height CO₂ capture pilot plant

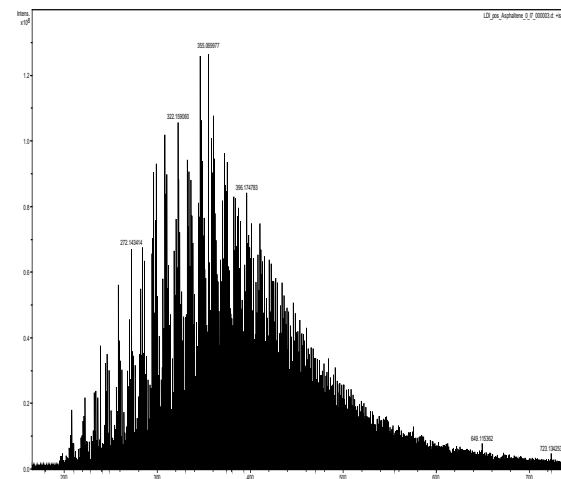


Why focus on degradation?



[source: Gouedard, C. (2014). Doctoral, Universite Pierre et Marie Curie]

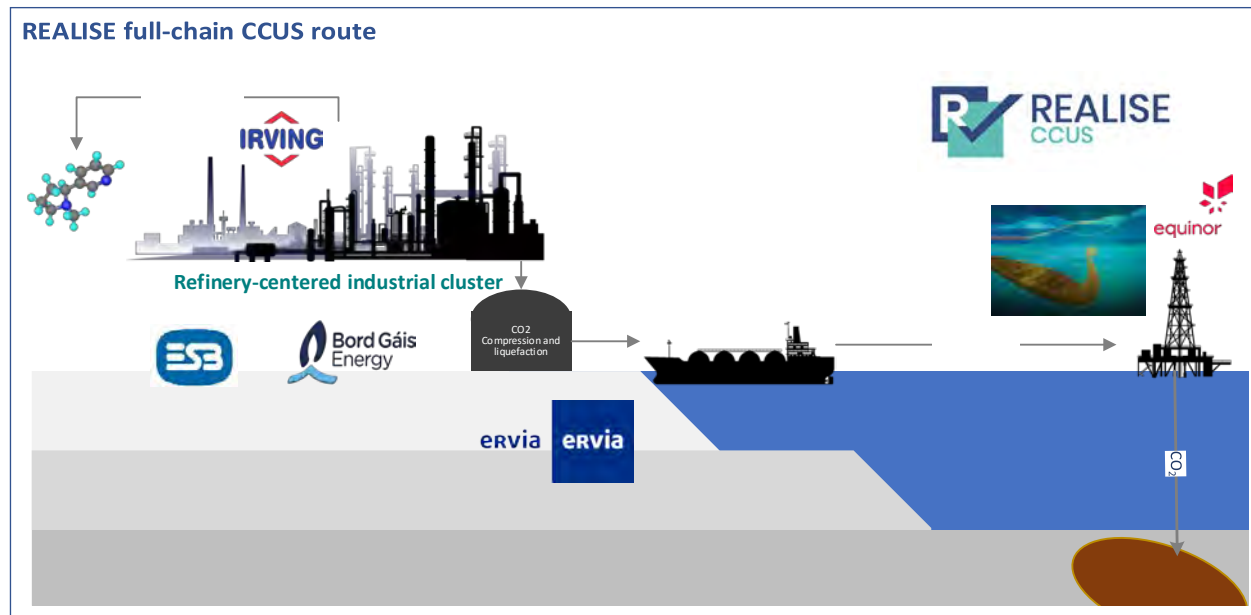
Advanced chemical analysis



Sampling of the cleaned gas from absorber (earlier project)



REALISE business cases: Ireland

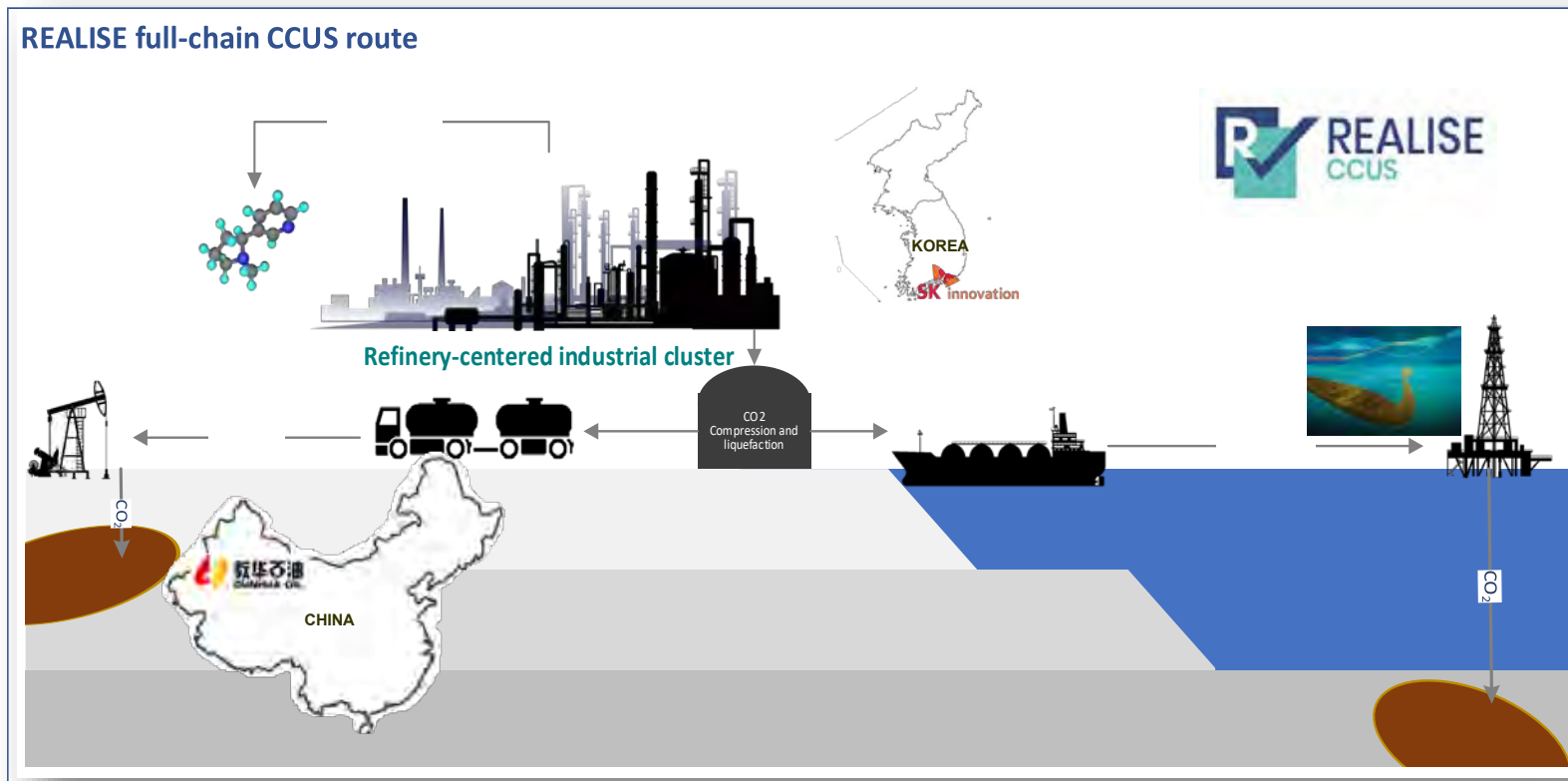


Phase 1 of Northern Lights

(<https://ccsnorway.com/wp-content/uploads/sites/6/2020/07/Plan-for-long-term-use-of-the-Northern-Lights-infrastructure-1.pdf>)



Business cases in REALISE: China and South Korea



Stakeholders' engagement in REALISE

Industry Club



External experts Advisory Board



Acknowledgements



This project has received funding from the European Union's Horizon 2020 research and innovation programme under grant agreement No 884266

Thank you for listening



Presenter

Presenter Name Inna Kim

Presenter Email inna.kim@sintef.no

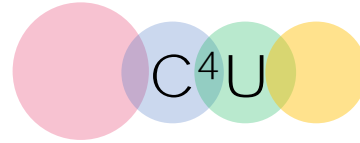
Project

@realise-ccus

www.realiseccus.eu

info@realiseccus.eu





International Workshop on CO₂ Capture and Utilization

Pilot preparation for demonstration in the C4U project



POLITECNICO
MILANO 1863



17 February 2021

Paul Cobden & Carlos Abanades

The contents of this presentation are the sole responsibility of *Swerim and partners* and do not necessarily reflect the opinion of the European Union.

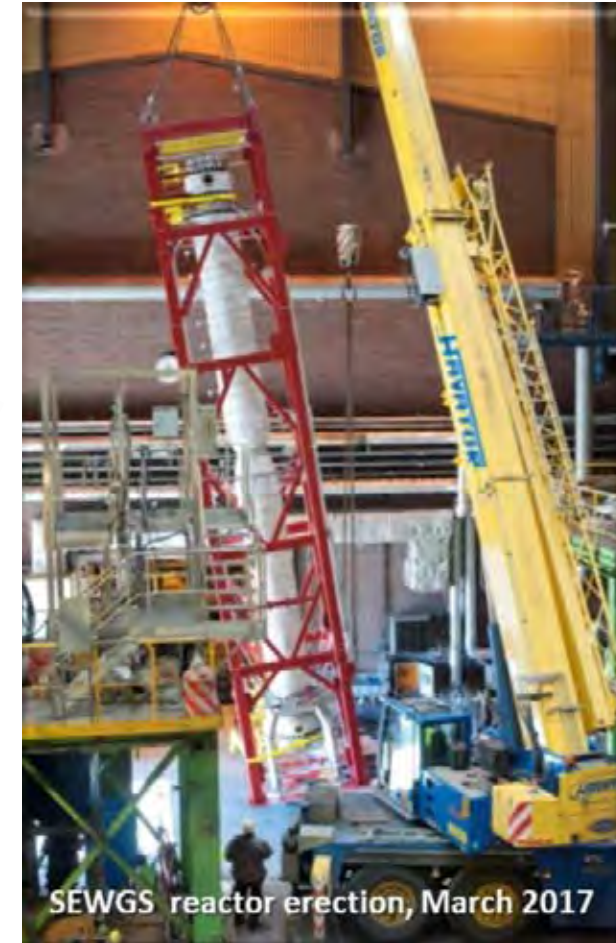


This project has received funding from the European Union's Horizon 2020 research and innovation programme under grant agreement No 884418

C4U IS TYPICAL GOES ATYPICAL

C4U IS GOOD ATYPICAL

CaL
Calcium
Looping



SEWGS
Sorption-
Enhanced
Water
Gas Shift



Post-combustion Capture

Pre-combustion Capture

HIGH TRL MEANS UTILISING INDUSTRIAL SITES/GASES FOR DEMONSTRATION

Asturias

+17°C

CASOH

Ca-Cu

1°C/mm



Pre-combustion testing

4000 km

1°C/100km



Post-combustion testing

Luleå

-24°C

DISPLACE
Hydrotalcite

1°C/cm

C4U

STATUS OF PILOT PREPARATIONS

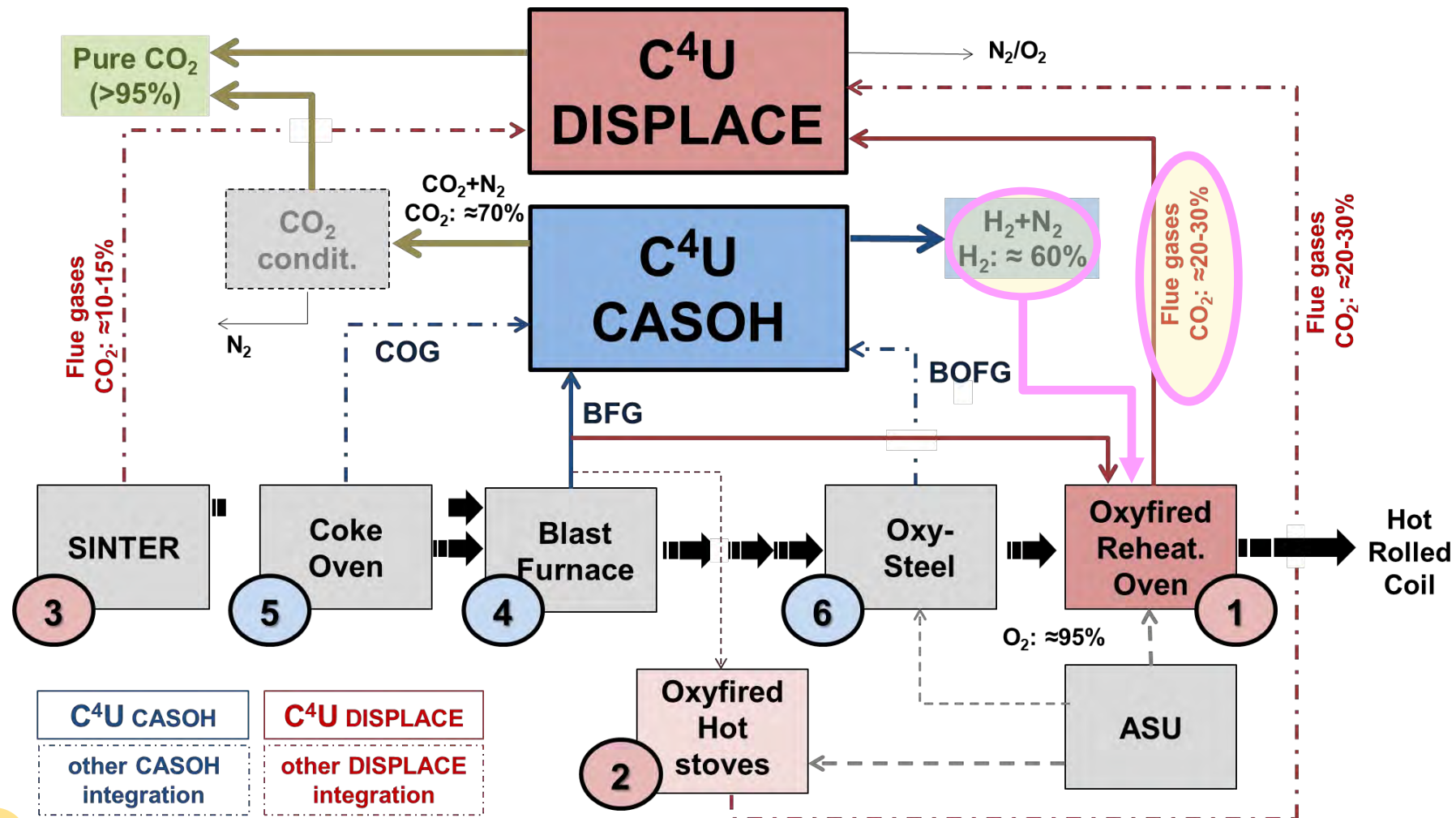
Similar Activities

- Both CASOH and DISPLACE will have 2000 hrs of demonstration at high TRL
- Most activities in 2020 and 2021 are engineering, procurement, construction
- DISPLACE has much of the equipment in place, and the linking of the unit is the main task
- CASOH requires a new pilot installation and building

Status

- Both CASOH and DISPLACE have achieved their respective deliverables on the basis of design
 - Special attention has been paid to the equipment delivery timeline
- Mass balances and operational philosophy of pilot
- All of the responsibilities of all of the involved partners in the different stages
 - Including delivery of the materials for testing, hydrotalcites, WGS catalysts, Ca-based sorbent and Cu-based materials
- Both CASOH and DISPLACE have delivered basic engineering and have started detailed engineering

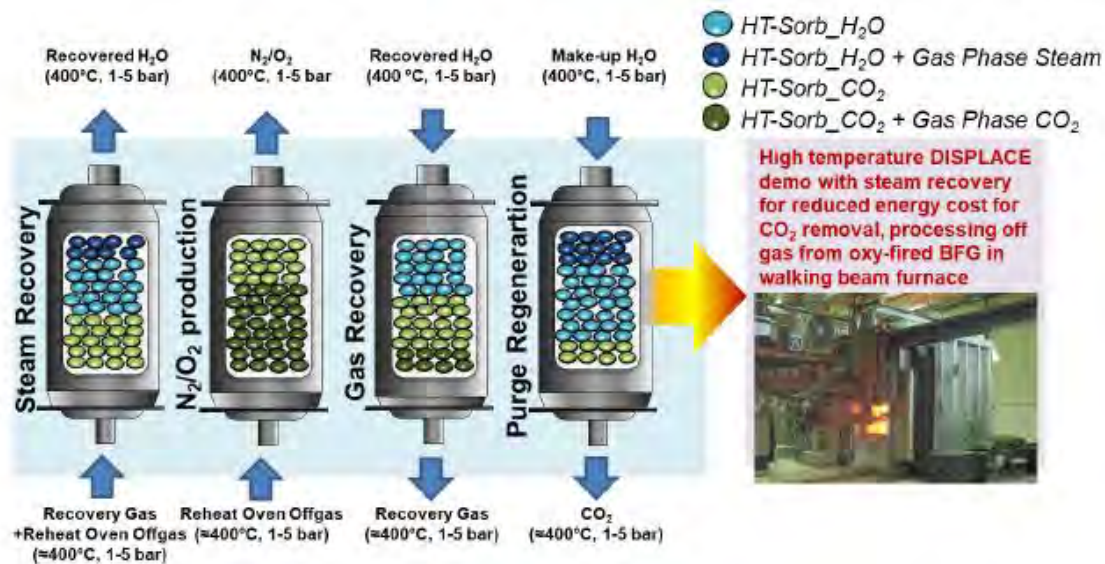
HOW DO TECHNOLOGIES FIT WITHIN C4U?



DEMONSTRATION OF CO₂ CAPTURE PROCESSES IN STEEL MILLS

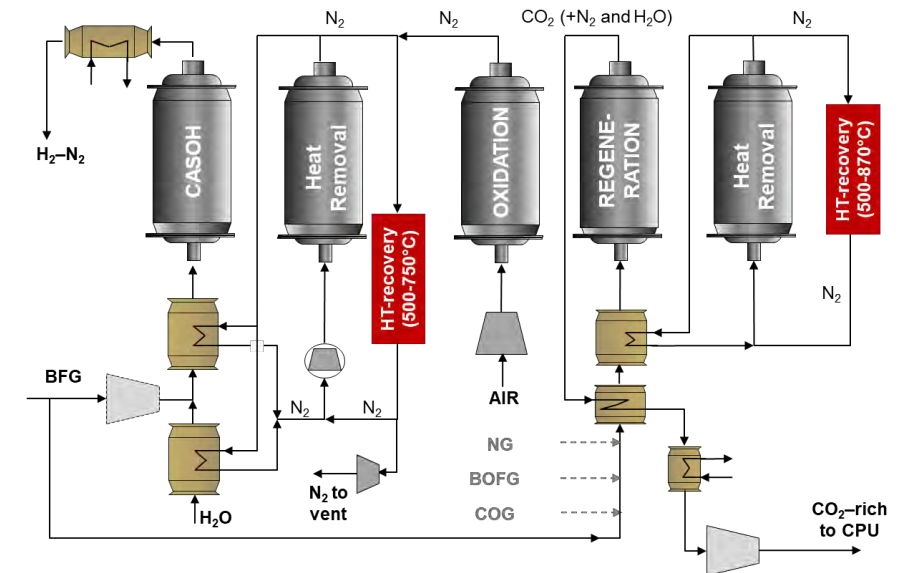
DISPLACE design:

Define the optimal sizing, number and configurations of the DISPLACE process, so to reduce the capture costs and to minimize the steam use while attaining the CO₂ purity target in the real scale plant.



CASOH design:

Provide overall M&H balance, Provide the large scale reactor size, and dynamic operation modelling, Calculate the performance of the single process, Provide the final design based on the experimental campaign at TRL7



DISPLACE TECHNOLOGY OBJECTIVES

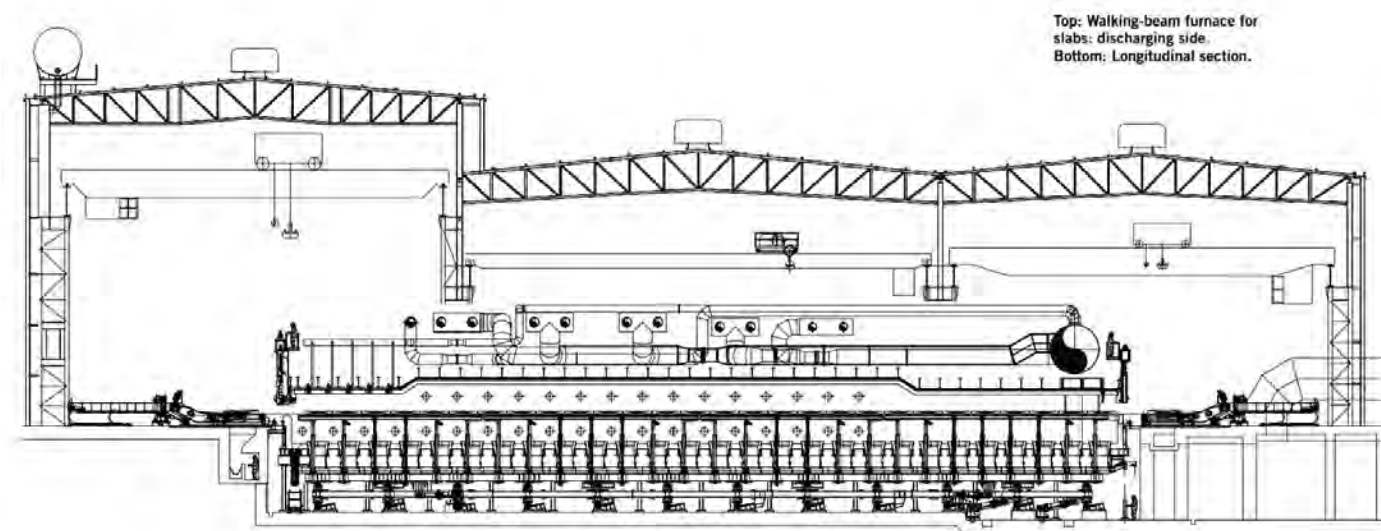


2 x 1000 hr campaigns

- N₂-H₂ Campaign, separation of H₂ from BFG, and subsequent H₂ use in chamber furnace
- DISPLACE Campaign, oxy-combustion of BFG in walking beam furnace, and CO₂ capture of oxy-combusted BFG

WHAT ARE REHEATING OVENS?

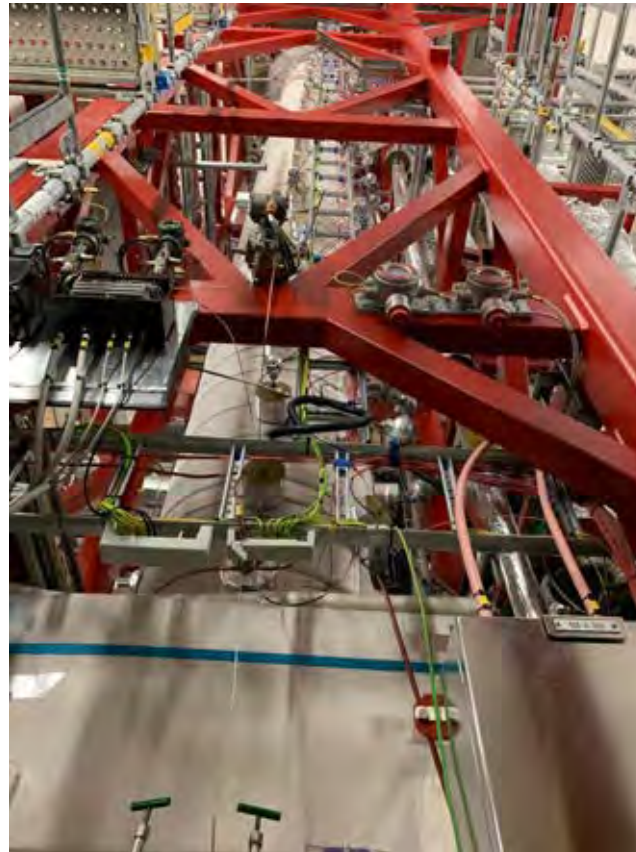
2.4 MT/y WBF



DISPLACE: CO₂ CAPTURE EQUIPMENT



WGS (for N₂/H₂ campaign)

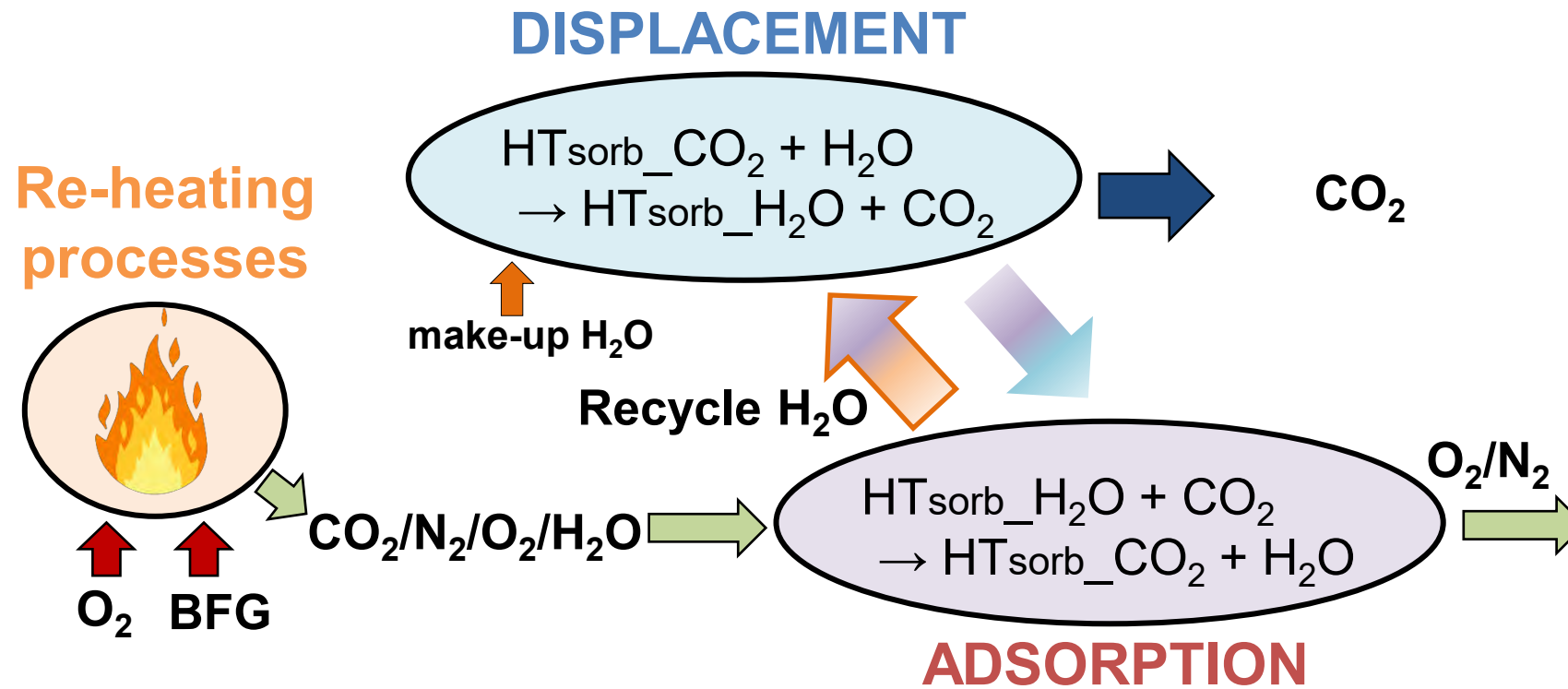


Single Column for N₂/H₂
Single Column DISPLACE



Syngas Cooler

DISPLACE PROCESS



CASOH: Future location of the pilot at the AMA GasLab

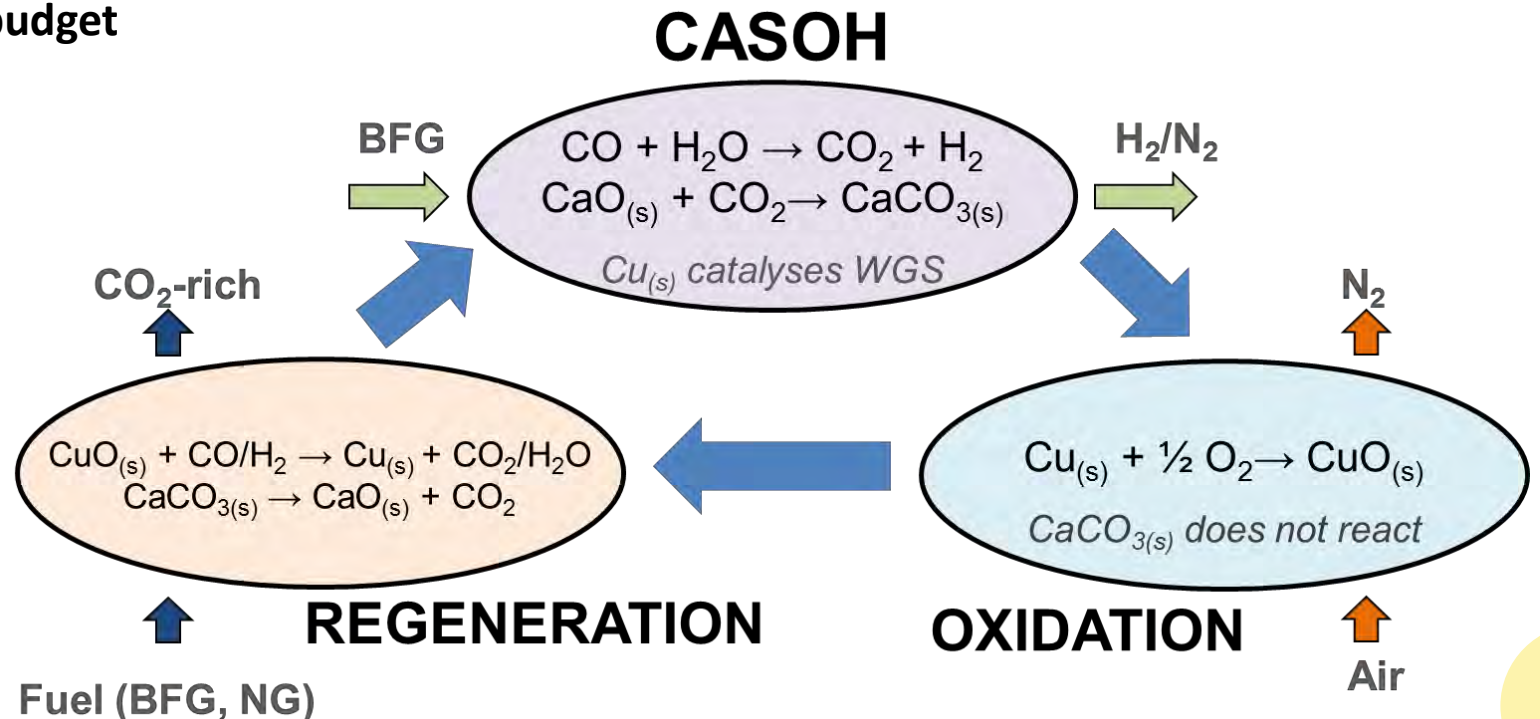
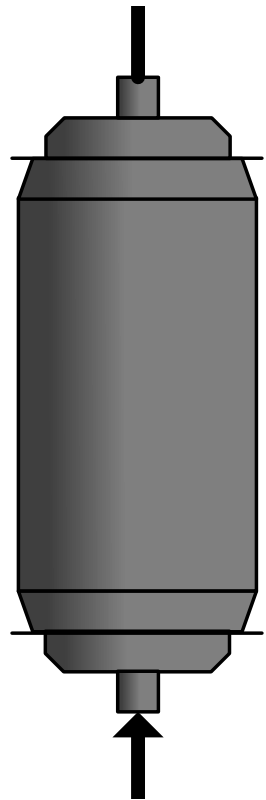


FIGURE 21. Pilot plant location next to Gaslab ArcelorMittal area.

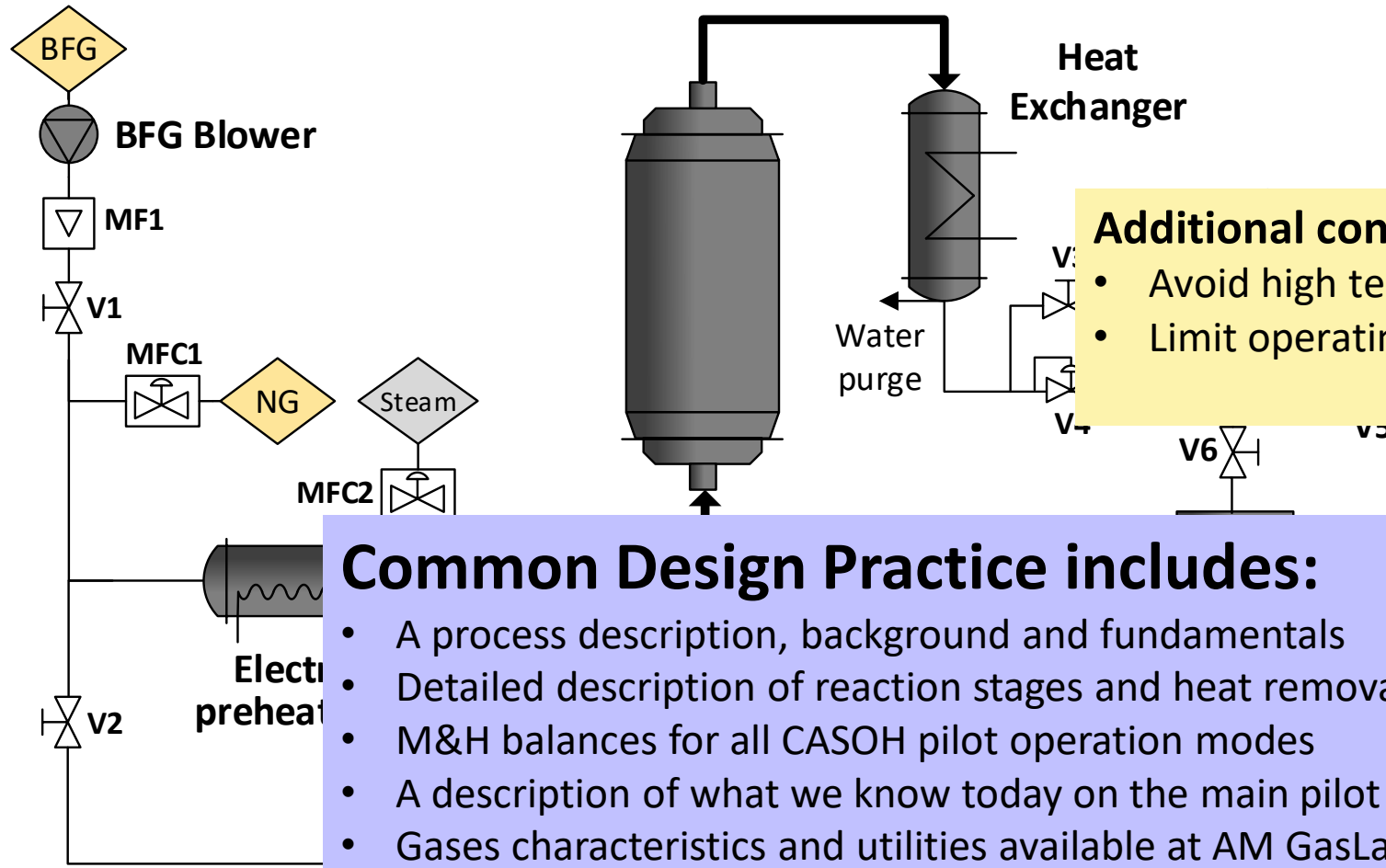
CASOH REACTIONS FOR BLAST FURNACE GAS

Main drivers for pilot design

- A single packed bed reactor is the core of the pilot
- Demonstration of reaction stages is a priority (i.e.: vs the heat removal stages)
- High TRL scale (defined as $0.3 \text{ MW}_{\text{LHV of H}_2} + 0.7 \text{ MW}_{\text{th}}$ as HT heat from regeneration)
- Indicative dimensions: 5 m height, 0.5 m I.D.
- **Keep within budget**



Process Flow Diagram of CASOH pilot



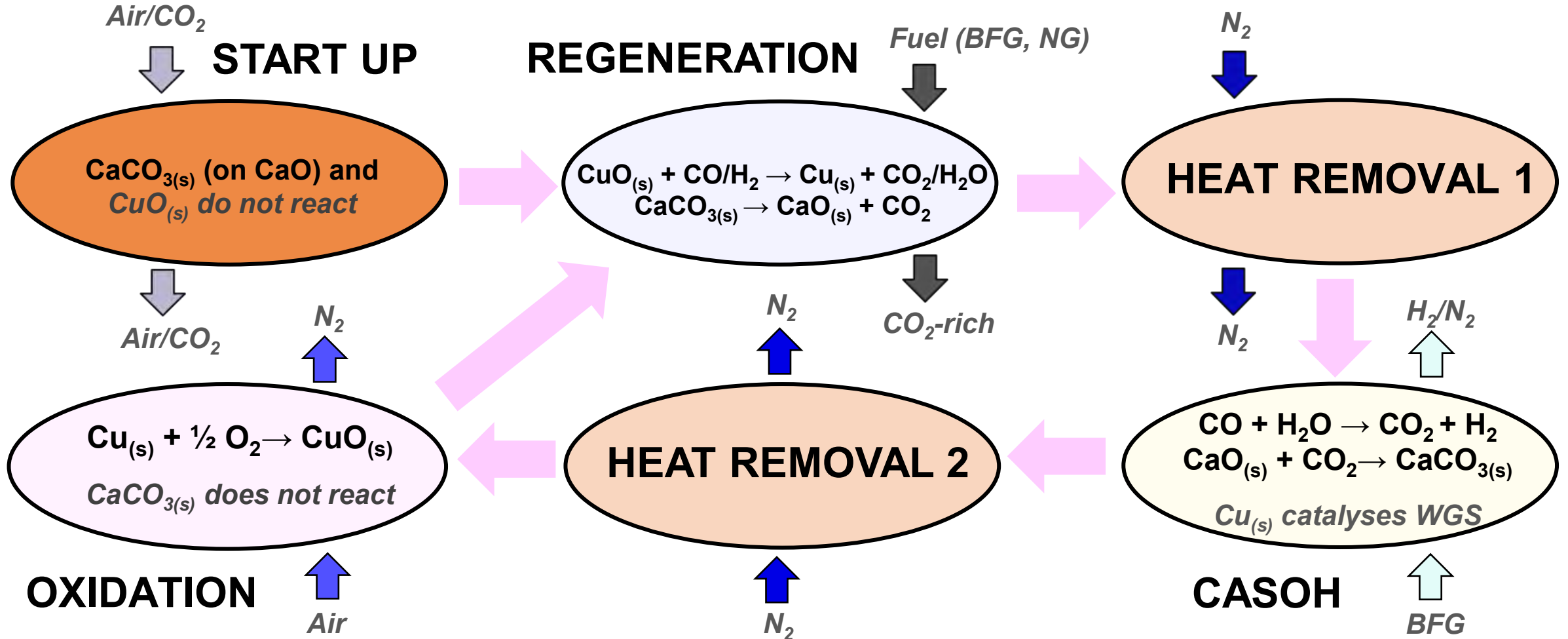
Additional constraints for pilot design

- Avoid high temperature valves
- Limit operating pressure to air at ~10atm

Common Design Practice includes:

- A process description, background and fundamentals
- Detailed description of reaction stages and heat removal stages
- M&H balances for all CASOH pilot operation modes
- A description of what we know today on the main pilot components
- Gases characteristics and utilities available at AM GasLab for the pilot
- Role of each CASOH participant towards WP2 objectives

FULL OPERATION SEQUENCE IN THE PILOT



DESIGN STATUS OF MAIN PILOT COMPONENTS

Bed characteristics

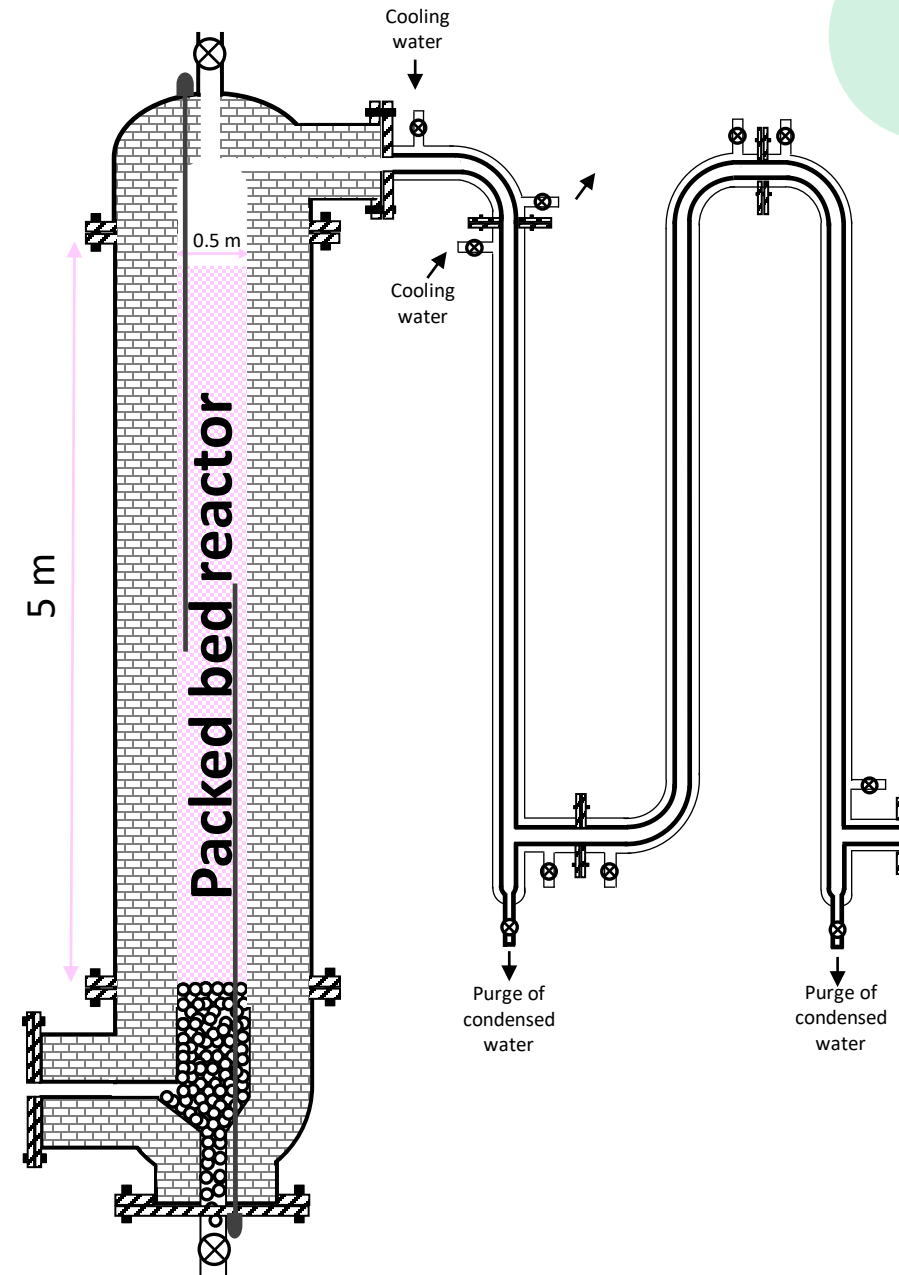
| | |
|-------------------|----|
| CaO active, %w | 10 |
| Cu active, %w | 30 |
| Particle size, mm | 3 |

Reactor characteristics

| | |
|--------------------|------|
| Height, m | 5 |
| Diameter, m | 0.5 |
| Cu/Ca molar | 1.8 |
| Mass Ca-, kg | 900 |
| Mass Cu-, kg | 600 |
| Total bed mass, kg | 1500 |



Samples of candidate materials from Carmeuse and Johnson Matthey received for lab. testing



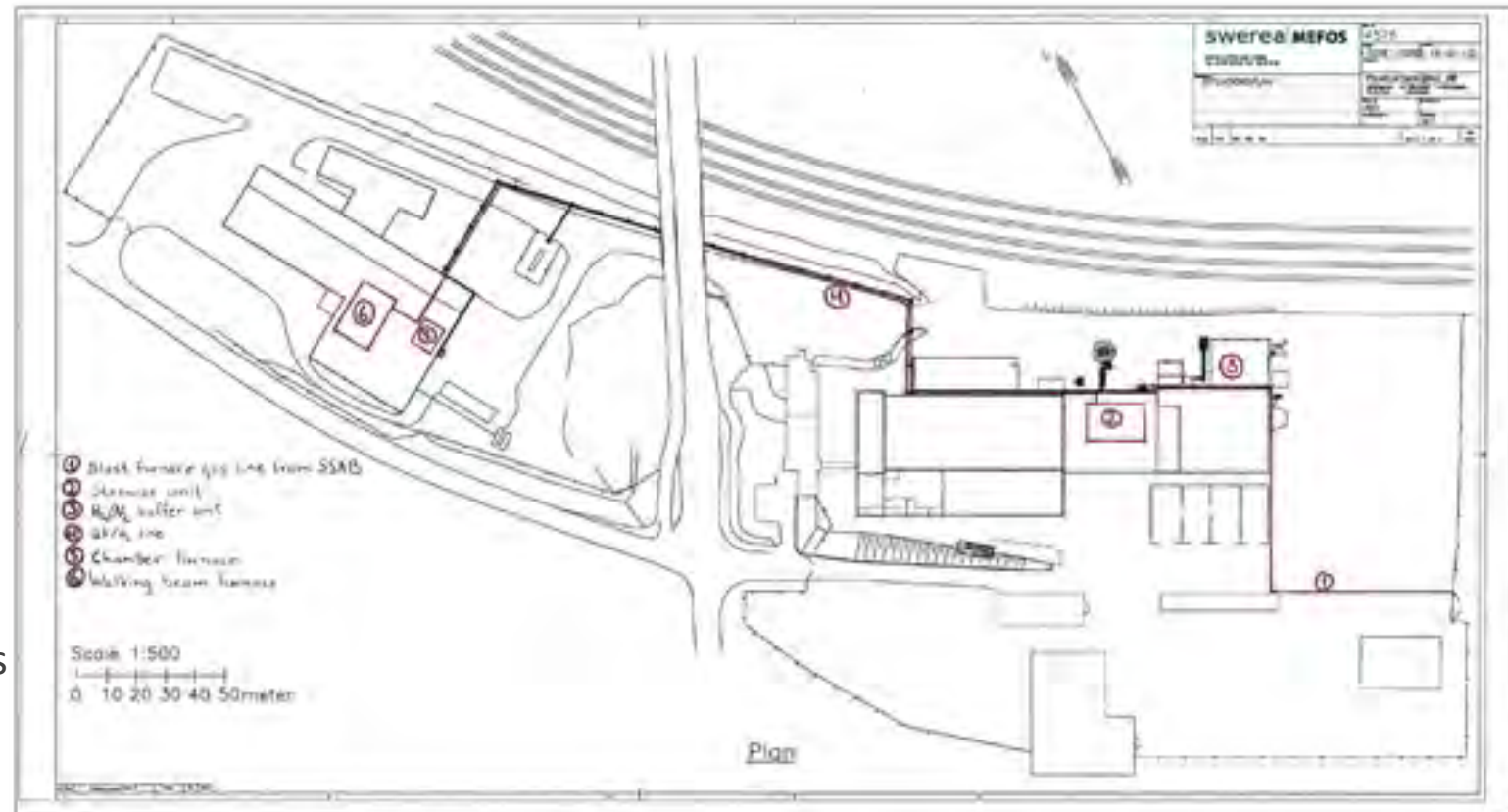
DISPLACE CDP & BOD : COMMON DESIGN PRACTICE AND BASIS OF DESIGN

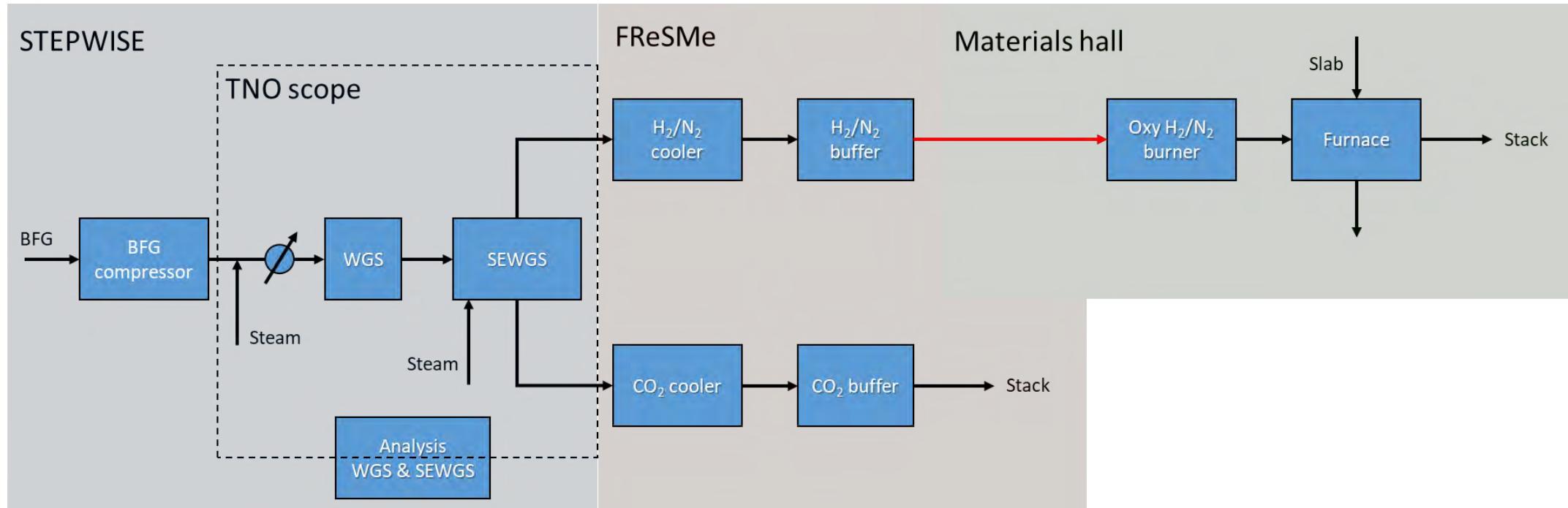
CDP

- Describes all partners activities and responsibilities for all partners involved in building and operating the pilot plant
- i.e. a more detailed description of scope compared to the DoA

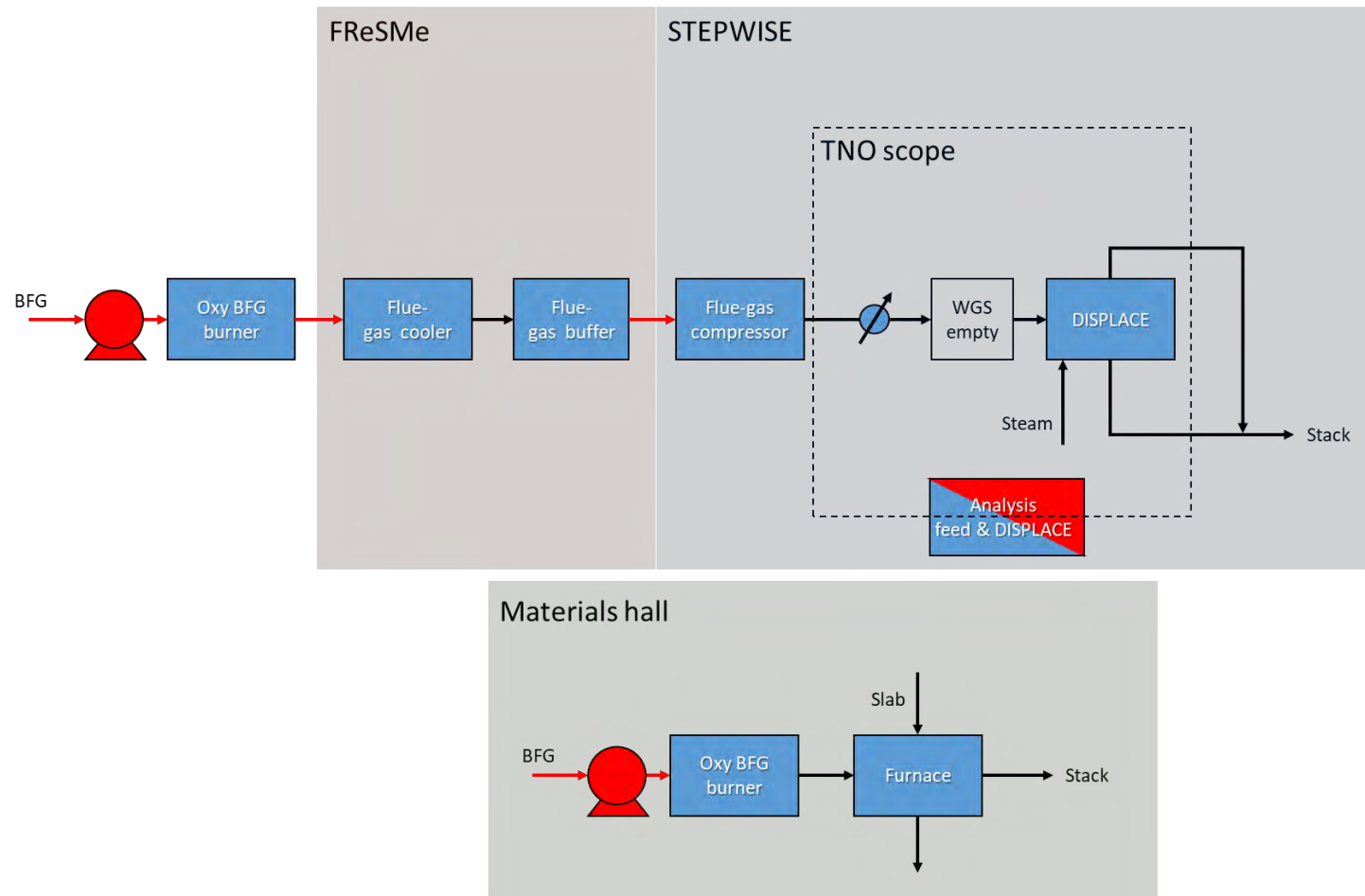
BOD

- Initial layout of equipment (see right)
- Mass and Energy flows and balances to drive basic engineering phase



CPD & BOD N₂/H₂-CAMPAIGNCampaign 1 : N₂/H₂ – SEWGS Campaign

CPD & BOD – DISPLACE CAMPAIGN



Campaign 2 : Oxy-BFG – DISPLACE Campaign

STATUS OF PILOT PREPARATIONS

Similar Activities

- Both CASOH and DISPLACE will have 2000 hrs of demonstration at high TRL
- Most activities in 2020 and 2021 are engineering, procurement, construction
- DISPLACE has much of the equipment in place, and the linking of the unit is the main task
- CASOH requires a new pilot installation and building

Status

- Both CASOH and DISPLACE have delivered their respective deliverables on the basis of design
 - Special attention has been paid to the equipment delivery timeline
- Mass balances and operational philosophy of pilot
- All of the responsibilities of all of the involved partners in the different stages
 - Including delivery of the materials for testing, hydrotalcites, WGS catalysts, Ca-based sorbent and Cu-based materials
- Both CASOH and DISPLACE have delivered basic engineering and have started detailed engineering

SYNERGIES BETWEEN CASOH AND DISPLACE

CASOH

Coke Oven Gas

Basic Oxygen Furnace Gas

Blast Furnace Gas

N₂-H₂ product as fuel

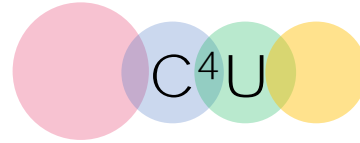
DISPLACE

Sinter Plant Exhaust

Hot stoves

Reheating Furnaces

Blast Furnace Gas
processed by CASOH



International Workshop on CO₂ Capture and Utilization

Pilot preparation for demonstration in the C4U project



POLITECNICO
MILANO 1863



17 February 2021

The contents of this presentation are the sole responsibility of *Swerim and partners* and do not necessarily reflect the opinion of the European Union.



This project has received funding from the European Union's Horizon 2020 research and innovation programme under grant agreement No 884418

DENS CCS

Formic acid as a liquid
organic hydrogen carrier



About DENS



invented in
2015



Founded in
2018



Employees
24



Homebase
HELMOND



'Pico' the first
proof of principle
2.5W



The first 25W
prototype



Hydrozine range
extender concept
for a bus



First practical
test with system
construction site



DENS' X1 2kW
power equipment



DENS' X2 20kW
Stroom generator
First field pilots



Start of serie
production

2015

2016

2017

2018

2019

2020

2021

TU/e
Eindhoven
University of
Technology

TEAM FAST

TEAM FAST

TEAM FAST

DENS
Power Generation



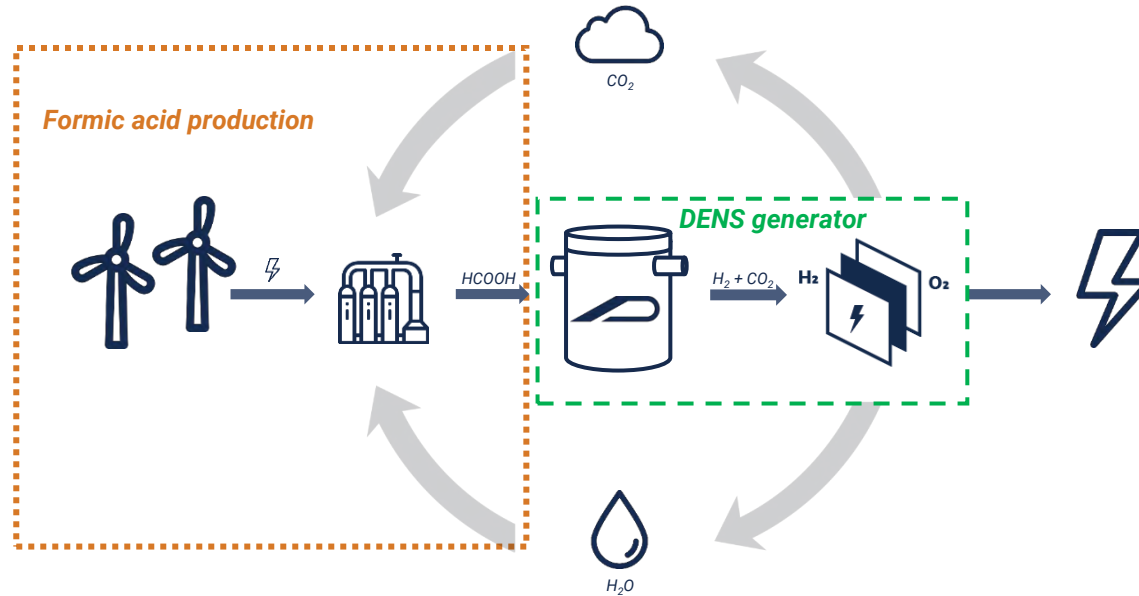
DENS

heijmans

TBI infra

F&L
POWERRENTAL

CO₂ neutral energy carrier



~~NO_x~~

~~SO_x~~

~~PM~~

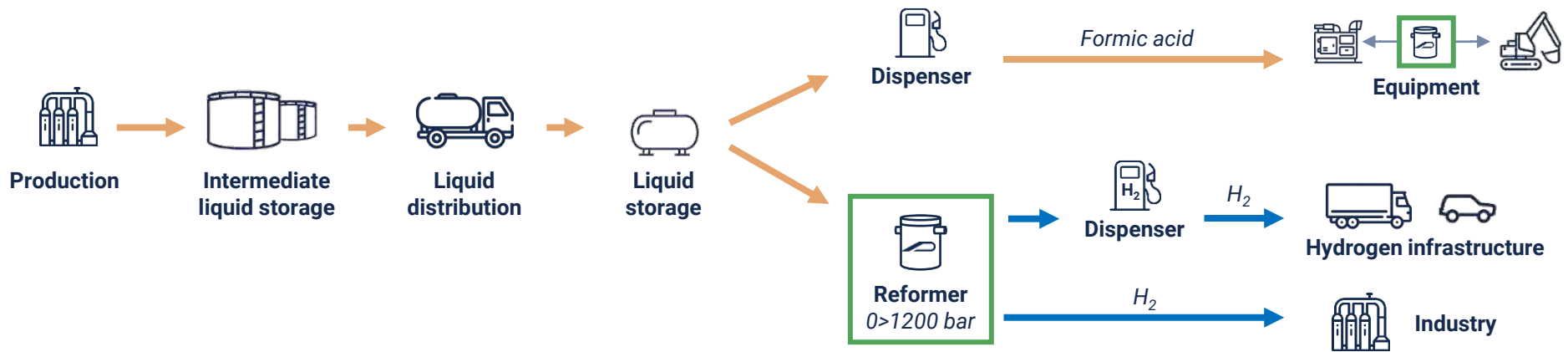
~~NO₂~~

Formic acid reconversion value proposition

By using DENS' reformer technology, hydrogen's storage and transport issues can be easily overcome.

The hydrogen economy with DENS

Storage and transport of formic acid, is significantly cheaper and safer, and therefore accelerates the hydrogen economy. DENS can convert formic acid back into hydrogen for direct use in a fuel cell or to allow for hydrogen generation on demand from liquid storage.



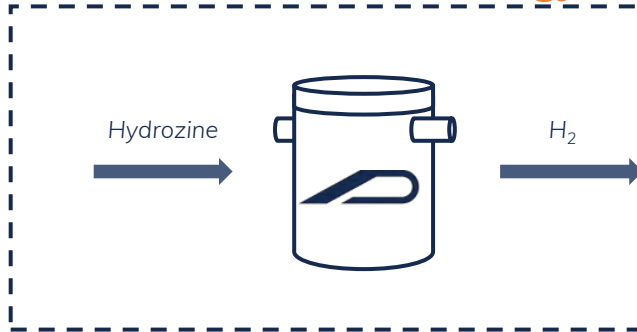
Current hydrogen economy

Storage and transport of gaseous hydrogen is highly expensive and therefore limiting the adoption of the hydrogen economy.

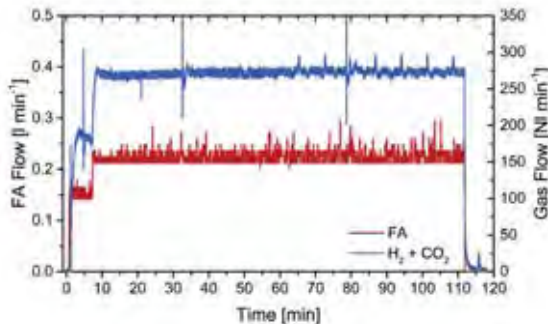


DENS generator technology

Reformer technology

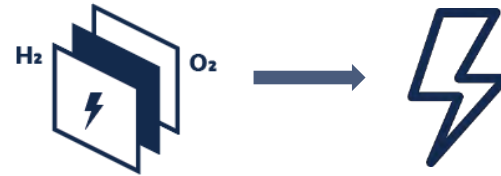


- ✓ Instantaneous reaction at low temperature



- ✓ Very little impurities
- ✓ Works up to 1200 bar

Fuel cell technology



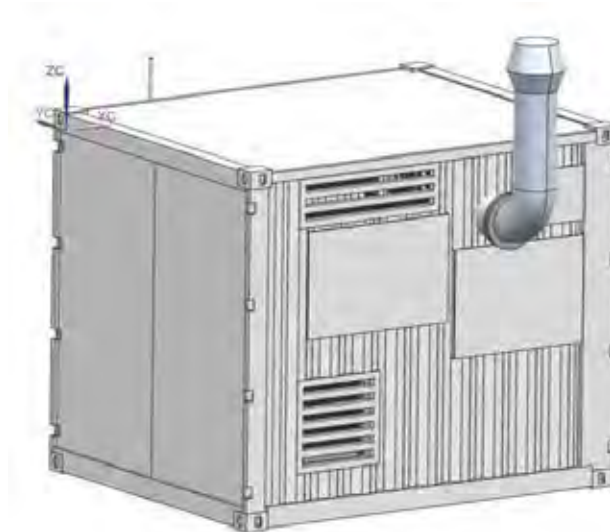
- ✓ Low temperature PEM
- ✓ Broadly certified stack
- ✓ Mass produced by BOSCH



Results

First field tests are being preformed

- Gas quality stays good to keep using the fuel cell also outdoors
 - CO production well below given target of fuel cell
 - FA levels are also well below given target value of fuel cell
- Stable reformer production for over 1000 hours
- 10 kw of nominal power achieved for at least 200 hours
- System optimalisations are being performed
- New insights in lifetime optimilisation are being tested
- Start and shutdown behaviour is being investigated



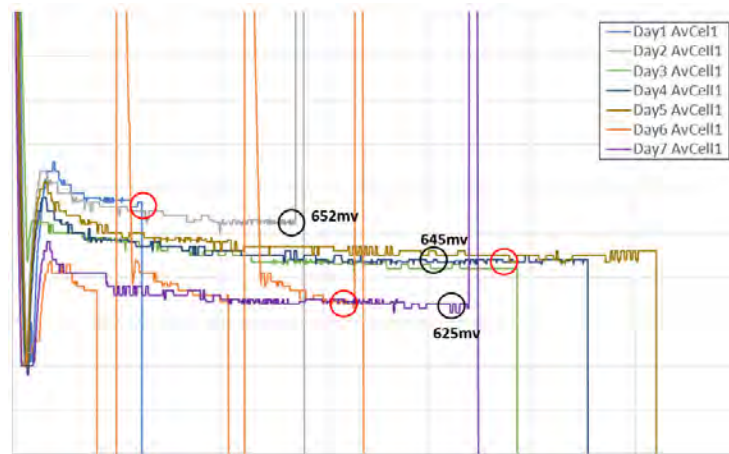
Results

Electrical components

- System has converted all the power to the local grid, enough for 20 households during tests
- Safety components have been checked by Lloyds and CE marking was checked
- Subsystem was tested and was capable of handling 30 kw's of power

Degradation

- Some degradation is witnessed not during runs but inbetween and not always
- Different Shut down and start procedures are being investigated together with partners, possible solutions are being tested (mainly due to emergency stops)



Planning

Tests are going to be performed at the end of the project at dk6 in Dunkirk

- Safety documents are being completed together with Engie
- Preliminary tests are being performed to solve start stop degradation
- Reformer components are being evaluated to make sure all wear and tear is being recorded and noted

Formic acid versus hydrogen

Hydrogens adoption barriers can be overcome via the liquid organic hydrogen carrier (LOHC) **Formic acid** in combination with **DENS'** reformer.

Adoption barriers

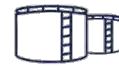
Barrier breakers

1. Pressurized gas storage

- × Compressed at 200-700 bar.
- × Liquified at -253 °C.
- × Elevated safety risks.
- × Expensive compression cost.



vs.



1. Liquid storage

- ✓ Ambient pressure.
- ✓ Limited to no safety risks.
- ✓ Affordable liquid pumping.

2. Gaseous distribution

- × Expensive tube trailers.
- × Only 360kg H₂ per trip.



vs.



2. Liquid distribution

- ✓ Affordable liquid trailers.
- ✓ 4x more per trip (1431kg H₂).

3. Compression required

- × Mechanical compression is required for refueling.
- × Expensive compression cost.



vs.



3. Hydrogen production on demand

- ✓ Chemical compression up to 1200 bar.
- ✓ No additional energy required.
- ✓ 100% renewable.

Expensive hydrogen



Affordable hydrogen



Max Aerts | CEO

+31620276608 | max.aerts@dens.one





Design and development of a membrane based post-combustion CO₂ capture system

Workshop on CCUS

16-17 / 02 / 2021

www.iwccu.org

Leonardo Roses

Contact: leonardo.roses@hygear.com

www.hygear.com

The present publication reflects only the author's views. The Commission is not responsible for any use that may be made of the information contained therein.



- Introduction to HyGear
- Introduction on CO₂ emissions
- Processes for CO₂ Capture
- MEMBER objectives
- Design requirements for demonstration at industrial site
- Design and development of post-combustion CO₂ capture system
- Conclusions and final remarks

FACTS AND FIGURES

Established in 2002

With the mission to develop
cost-effective gas supply

82

Highly motivated employees with an
entrepreneurial and innovative spirit

> €23m

Gross revenue

66

Installations operational worldwide

14

patents securing a
sustainable competitive
edge

Industries that we are active in

Flat/float glass manufacturing
Metal sintering
Food
Electronics
Semiconductor
Fuelling station for vehicles

> 85,000 kg

CO₂ reduction per customer per year
with breakthrough technologies

Active in
20 countries



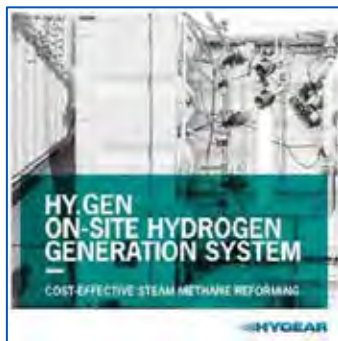
PRODUCTS & SERVICES

DELIVERING GASES THROUGH ON-SITE TECHNOLOGY



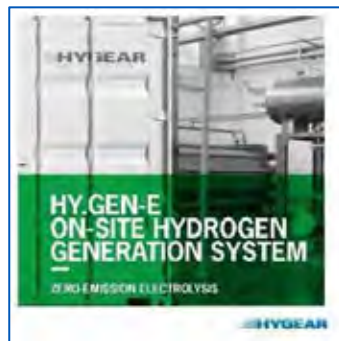
Hydrogen

Cost-effective
Steam Methane Reforming



Hydrogen

Electrolysis



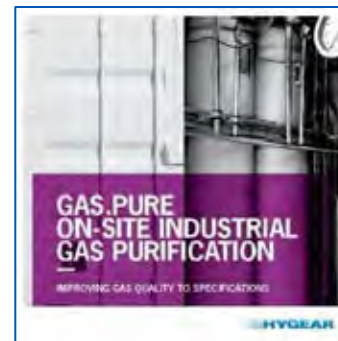
Gas Recycling

Economical recovery of gases
used as protective atmospheres

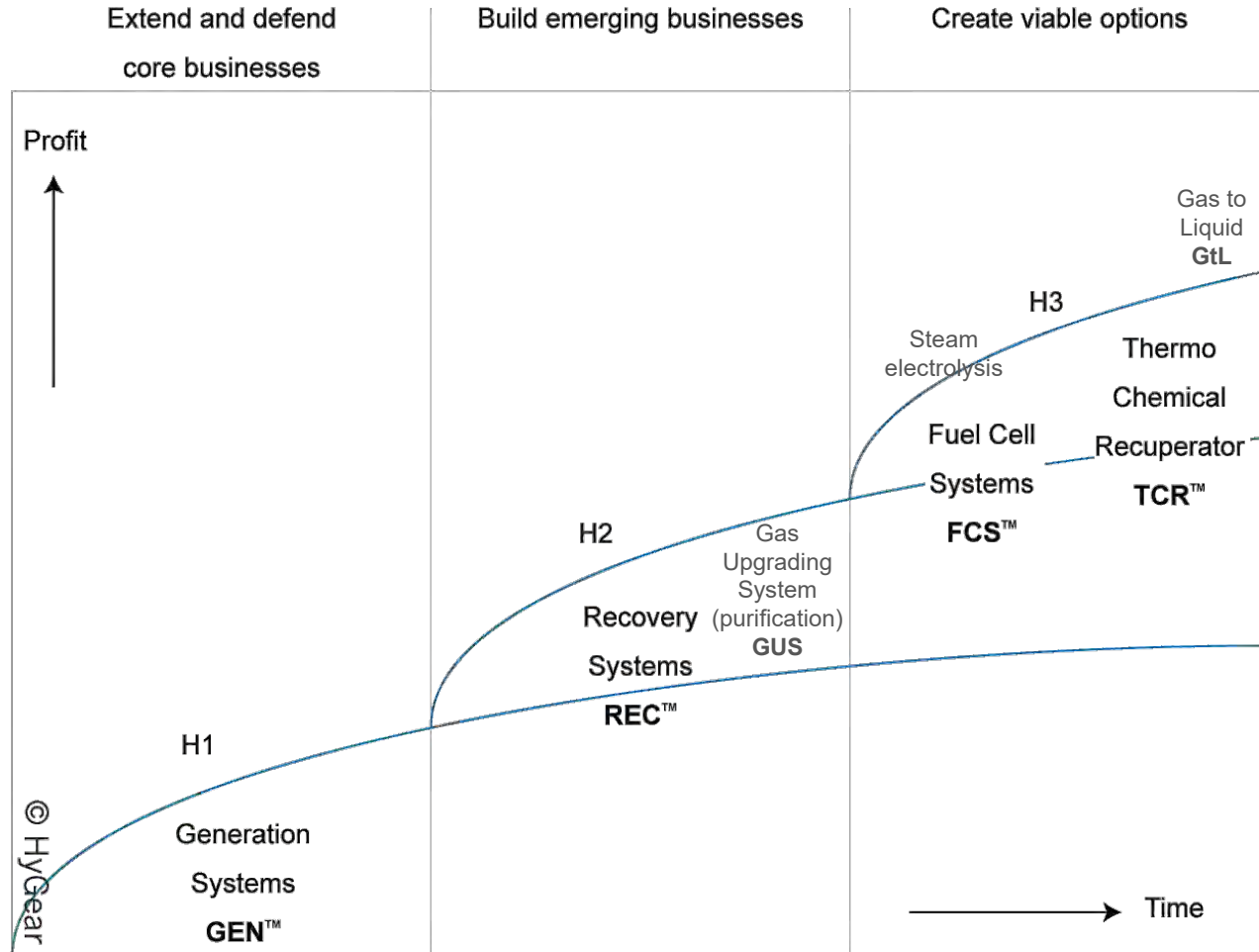


On-site Purification

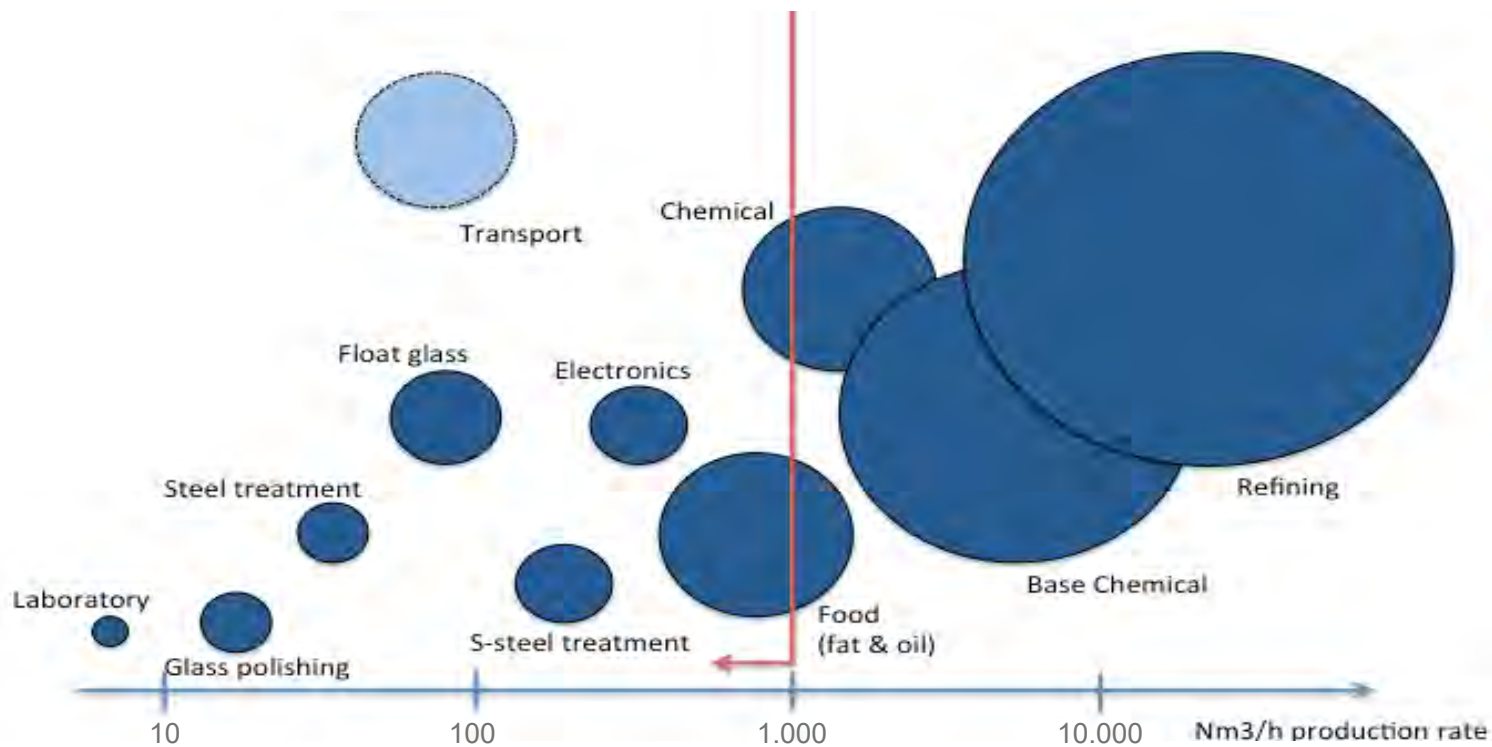
Improving gas quality to
application required specifications



DEVELOPMENT STRATEGY



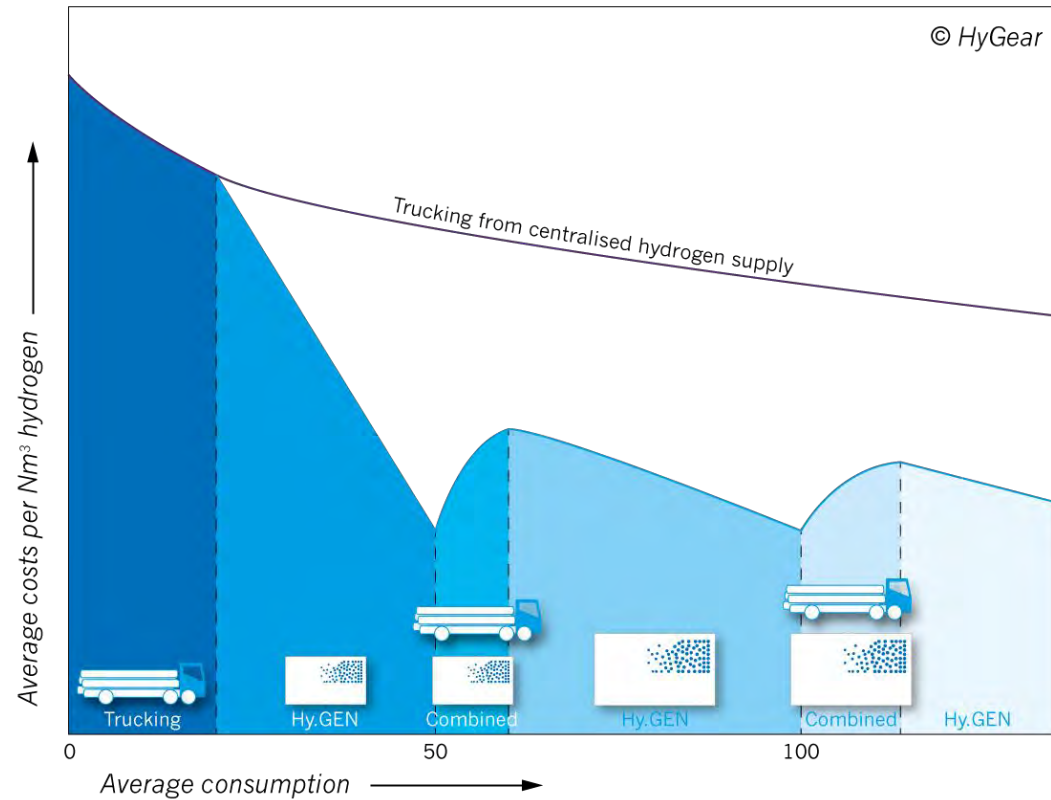
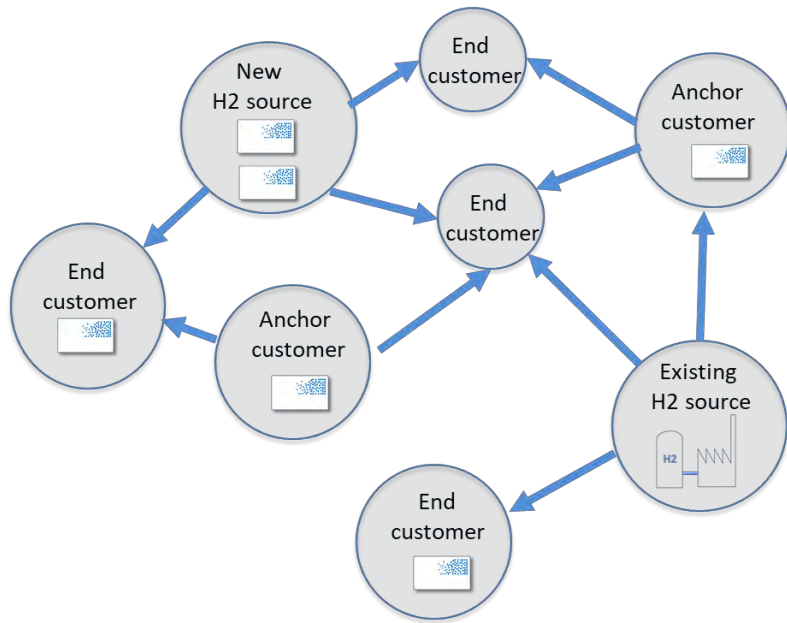
HYDROGEN MARKET



Bron: Air Liquide

THE MERITS OF ON-SITE SUPPLY

Creating a network



ON-SITE HYDROGEN GENERATION TECHNOLOGY EXPLAINED



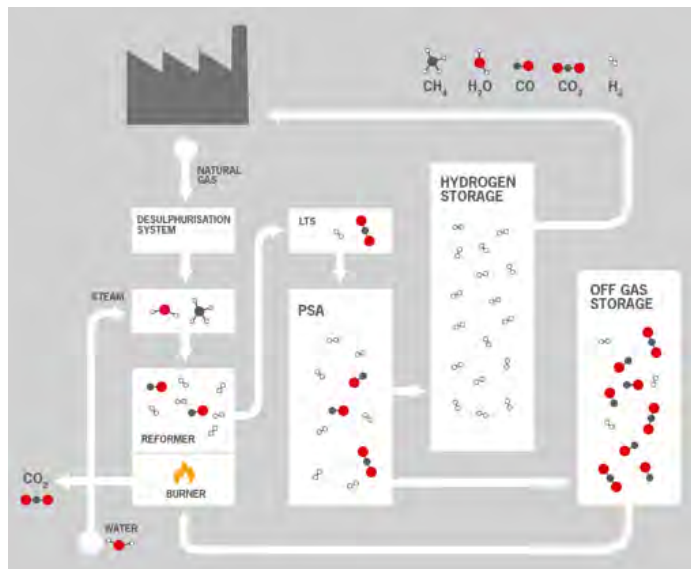
HYDROGEN TECHNOLOGY EXPLAINED

The unique strength of Hy.GEN® SMR-technology:

- Hy.GEN® Steam Reforming needs 0.5 Nm³ Natural gas per Nm³ H₂

When compared to other supply methods:

- Electrolysis; that needs 6.5 kWh Electricity per Nm³ H₂
- Trucking; that needs 40 tons of truck to move 300 kg of gas



1. Ventilation fan
2. Desulphurisation vessel
3. PSA-vessels
4. Off-gas storage

5. Hydrogen storage
6. Water separator for vacuum pump
7. Vacuum pump
8. Coolant heater

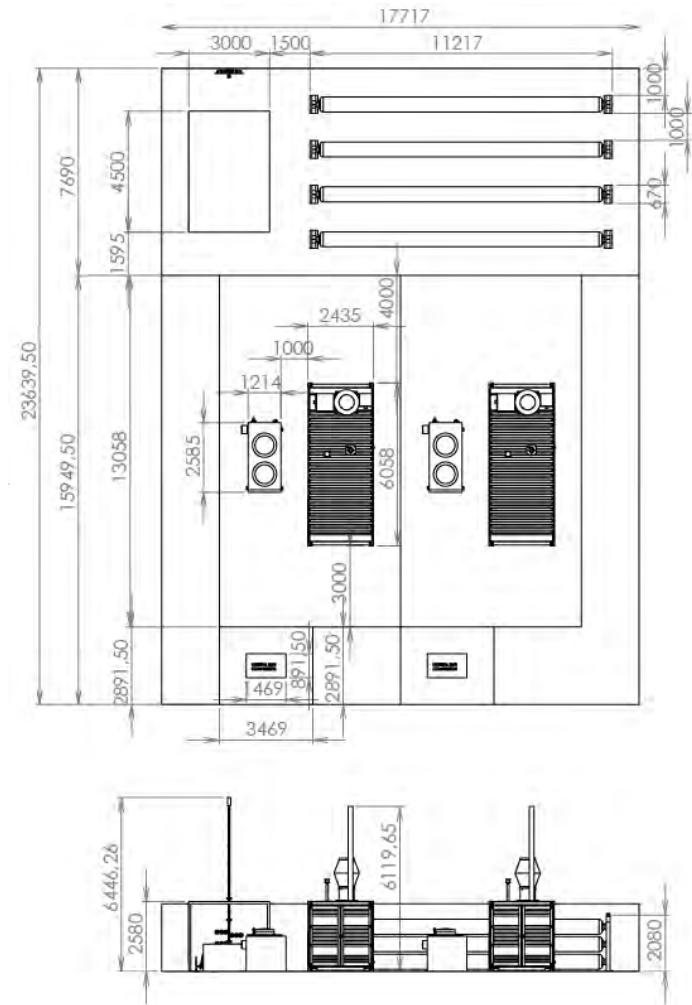
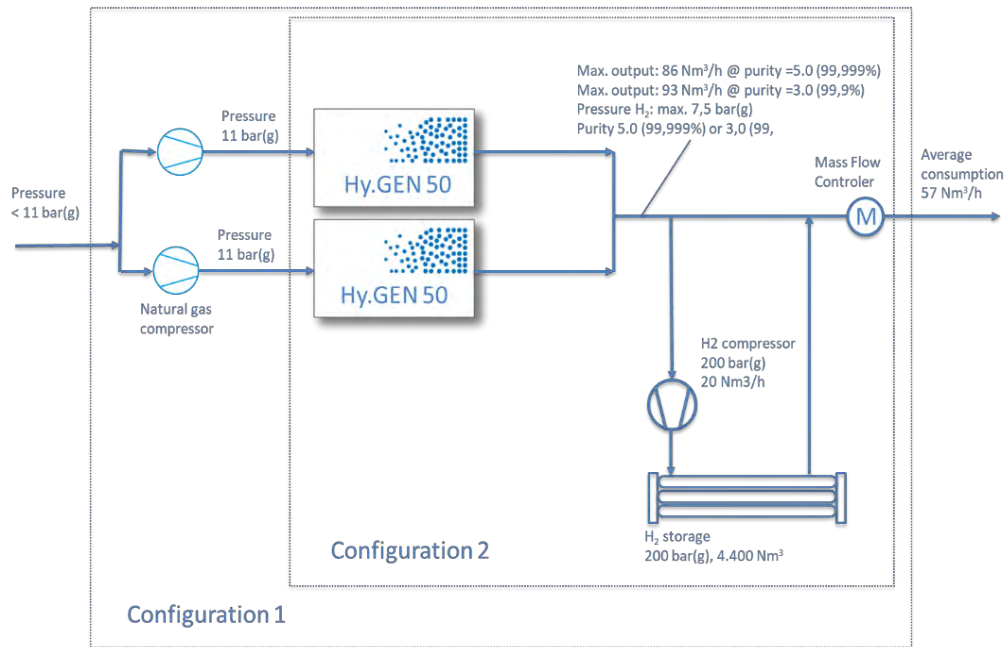
9. Reformate cooler
10. Electronics cabinet
11. Steam generator
12. Reformer unit

13. Low temperature shift
14. Coolant expansion vessel
15. Burner air blower
16. Water purification system

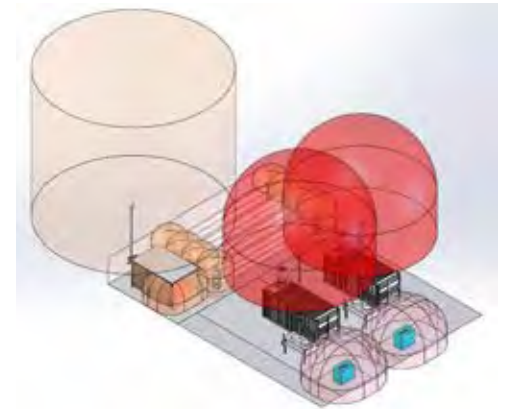
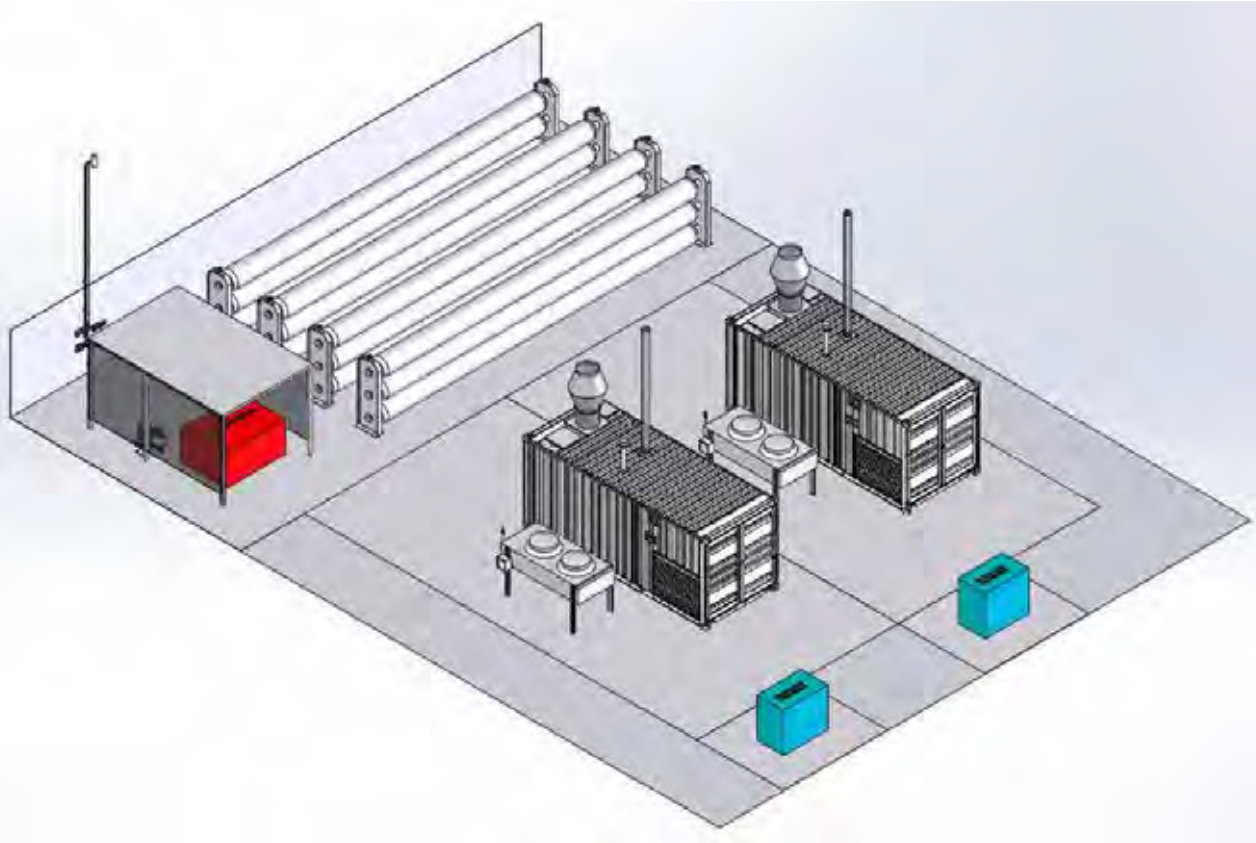
HY.GEN MODELS

| MODEL | Hy.GEN® 50 | Hy.GEN® 100 | Hy.GEN® 150 |
|--|----------------------------|----------------------------|-----------------------------|
| OUTPUT | | | |
| Nominal H ₂ flow | Max. 47 Nm ³ /h | Max. 94 Nm ³ /h | Max. 141 Nm ³ /h |
| Hydrogen Purity Range | 99.5 – 99.9999 % | 99.5 – 99.9999 % | 99.5 – 99.9999 % |
| Pressure Range | 1.5 – 7.5 bar(g) | 1.5 – 7.5 bar(g) | 1.5 – 7.5 bar(g) |
| TYPICAL CONSUMPTION DATA | | | |
| Natural Gas | Max. 23 Nm ³ /h | Max. 46 Nm ³ /h | Max. 69 Nm ³ /h |
| Electricity | 12.5 kWe | 22.5 kWe | 25 kWe |
| Water | 100 l/h | 200 l/h | 300 l/h |
| Compressed air | Max. 3 Nm ³ /h | Max. 6 Nm ³ /h | Max. 9 Nm ³ /h |
| DIMENSIONS | | | |
| Size | 20 ft. | 40 ft. | 40 ft. |
| Weight | 6,500 kg | 10,000 kg | 12,000 kg |
| OPERATING CONDITIONS | | | |
| Start up time (warm) | Max. 30 min | Max. 30 min | Max. 30 min |
| Start up time (cold) | Max. 3 hours | Max. 3 hours | Max. 3 hours |
| Modulation (H ₂ product flow) | 0 – 100 % | 0 – 100 % | 0 – 100 % |
| Modulation Reformer (output) | 10 – 100 % | 10 – 100 % | 10 – 100 % |
| Ambient Temperature Range | -20 °C to +40 °C | -20 °C to +40 °C | -20 °C to +40 °C |

TYPICAL CONFIGURATION GLASS PLANT



TYPICAL CONFIGURATION GLASS PLANT



SAINT GOBAIN L'ARBOC, SPAIN



DUZCE CAM, TURKEY



PHILIPS LUMILEDS TURNHOUT, BELGIUM



WALMART TEXAS, USA



HYGEAR HYDROGEN FILLING STATION IN THE NETHERLANDS



SUMMARY OF KEY BENEFITS

- Industrial Gas supplier in small bulk
- Ability to design, install and operate the supply
- Highest security of supply by on-site generation with trucked back up
- Against the lowest costs due to advanced technologies



FLEXIBLE CONTRACTING

| | BUY | GAS-AS-A-SERVICE (GAAS) |
|--|---------------------------|-------------------------|
| Equipment investment | Customer | HyGear |
| Infrastructural preparations | Customer | Customer |
| Installation & commissioning | HyGear | HyGear |
| Equipment operation | Customer | Customer |
| Service including system monitoring assistance | Contract option available | HyGear |
| Maintenance | Contract option available | HyGear |

FLEXIBLE CONTRACTING

YOUR BENEFITS:

**NO FINANCIAL
INVESTMENT**



**NO ADDITIONAL
RESOURCES
NEEDED**



**YOU CAN
CHOOSE...**



**NO
SURPRISES**





R&D PROJECTS

- H₂ mem+PSA hybrid system

- H₂ mem+PSA hybrid system

- O₂ mem ATR, O₂ mem OCM,
H₂ mem WGS, H₂O mem FTS

- O₂ mem ATR, O₂ mem OCM, H₂ mem WGS, H₂O mem FTS

- H2 mem for NG ATR

- H2 mem for NG ATR

- H₂ mem for flexible feedstock gas ATR

- H₂ mem for flexible feedstock gas ATR

- H_2 mem (pre-comb); CO_2 mem (post-comb)

- H_2 mem (pre-comb); CO_2 mem (post-comb)

- H₂ mem for EtOH ATR

- H₂ mem for EtOH ATR

- O₂ mem

- O_2 mem

- H₂ mem separation

- H_2 mem separation

- H_2 mem (pre-comb); CO_2 mem (post-comb)

- H_2 mem (pre-comb); CO_2 mem (post-comb)



R&D PROJECTS

EXAMPLES



PBI fuel cell system



Membrane reformer system

Gas purification of waste water treatment



PSA systems

Biogas upgrading



Fermentation and hydrogen stripping





Advanced MEMBranes and membrane assisted procEsses for pre- and post- combustion CO₂ captuRe

MEMBER

This project has received funding from the European Union's Horizon 2020 research and innovation programme under grant agreement No 760944

(Confidential. Disclosure or reproduction without prior permission of MEMBER is prohibited).



- CO₂ is the undesired by-product of hydrocarbon conversion processes and the product of combustion in power production, building heating, transportation, etc.
- CO₂ emissions from stationary system come mostly from power production (~80 %), while cement, refinery, steel and petrochemical contribute for about 20 % [1].
- The first objective of CO₂ capture is the decrease of anthropogenic CO₂ emissions. In parallel there is an effort to develop potential CO₂ applications that could, at least in part, economically support the deployment of CCS technologies

| PROCESS | CO ₂ emissions 10 ⁶ metric ton / year | % on the Total | |
|-------------------------|--|----------------|--------|
| Power production | 10,539 | 78.8 | ~80% |
| Cement production | 932 | 7.0 | } ~20% |
| Refineries | 798 | 6.0 | |
| Iron and steel industry | 646 | 4.8 | |
| Petrochemical industry | 379 | 2.8 | |
| Oil and gas processing | 50 | 0.4 | |
| Other sources | 33 | 0.2 | |

[1] IPCC reports 2018

(Confidential. Disclosure or reproduction without prior permission of MEMBER is prohibited).



CO₂ demand and potential



- The potential for CO₂ utilisation is substantial
- Existing uses and demand of CO₂:
- Purification requirements vary widely

| Existing uses | Brief description | Future potential non-captive CO ₂ demand (MTPA) | Minimum purity |
|-----------------------------|---|--|----------------|
| Enhanced oil recovery (EOR) | CO ₂ acts as a solvent that reduces the viscosity of oil fields, enabling it to flow to the production well. | 30 < demand < 300 | 90 % |
| Food | CO ₂ used in different applications, including packaging (modified or controlled atmosphere packaging), cooling while grinding powders, food spoilage prevention by acting as an inert atmosphere and dry ice as refrigerant to prolong food storage | ~15 | 99.9 % |
| Beverages | Carbonation of beverages with high-purity CO ₂ . | ~14 | 99.9 % |
| Refrigerants | Used as working fluid in refrigeration plants, especially for industrial air conditioning and refrigeration systems. | <1 | 99.9 % |
| Industrial | Used for steel manufacturing, metal working, welding and other applications. | <1 | 99.5 % |
| Storage | CO ₂ sequestration | | 95 % |

➤ In combustion processes CO₂ can be captured via three different routes:

- Post-Combustion
- Pre-Combustion
- Oxyfuel-Combustion

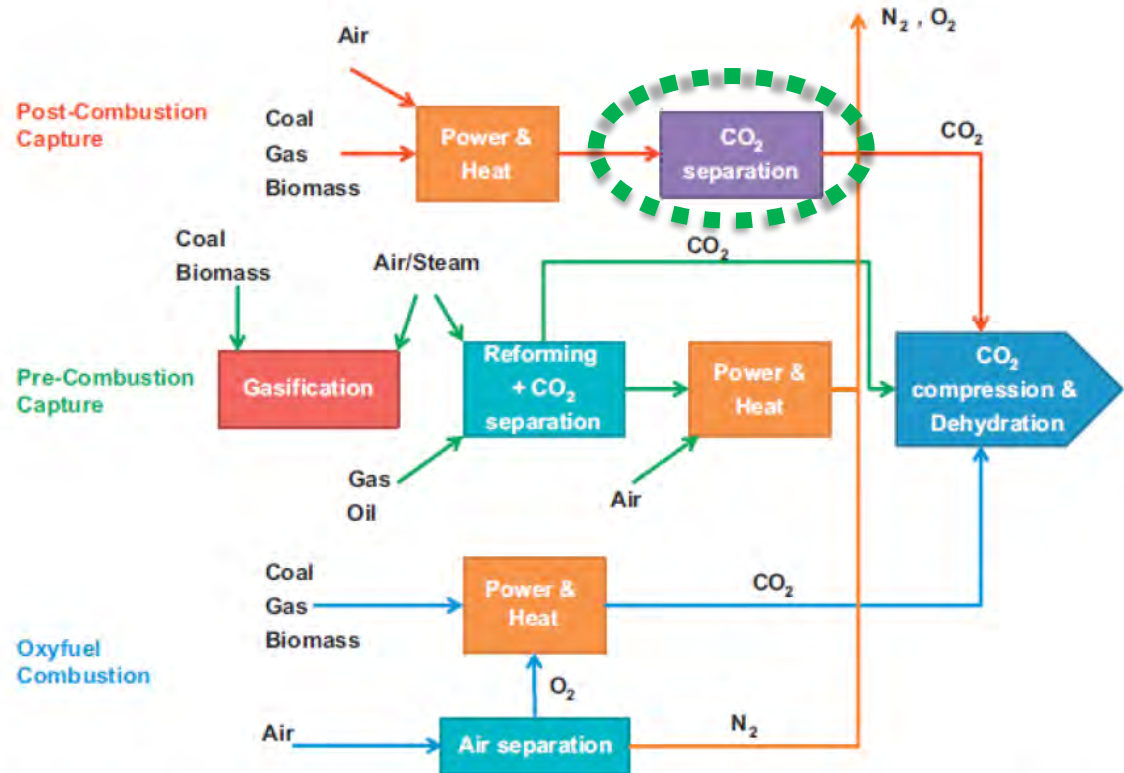


Figure 1. Schematic conceptual representation of CO₂ capture technologies [12].

Benchmark process for post-combustion CO₂ Capture

- At large scale and low CO₂ content in the feed, chemical absorption is the most widespread technology. This is the benchmark technology for the MEMBER project
- It is applied in many industrial units such as ammonia production and gas processing and in some existing CCS applications (mainly aimed at EOR)
- Physical absorption and adsorption are more suitable at smaller scales and/or when CO₂ partial pressure in the feed is sufficiently elevated. The absorption/regeneration process (both chemical and physical) is by far the most widespread technology for CO₂ separation from gaseous streams.
- For a detailed description of benchmark technologies and industrial requirements, visit public deliverable D2.2 available at the MEMBER website.

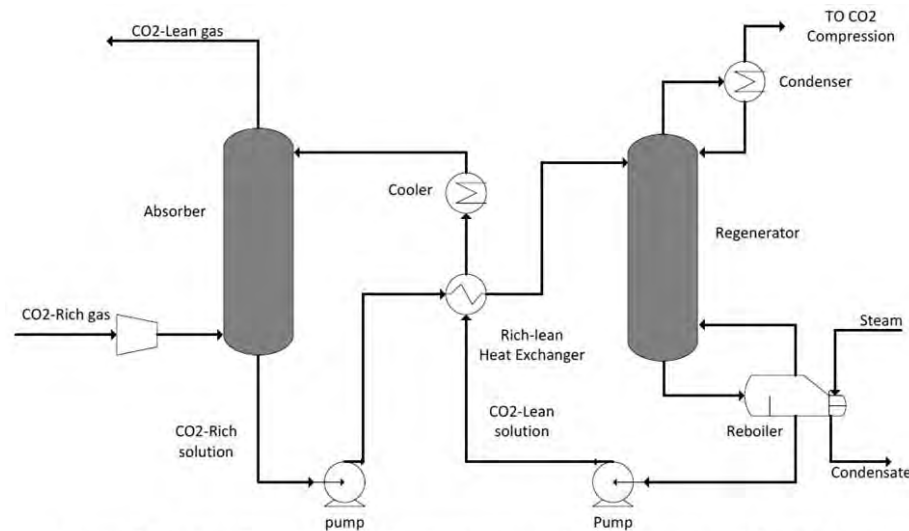


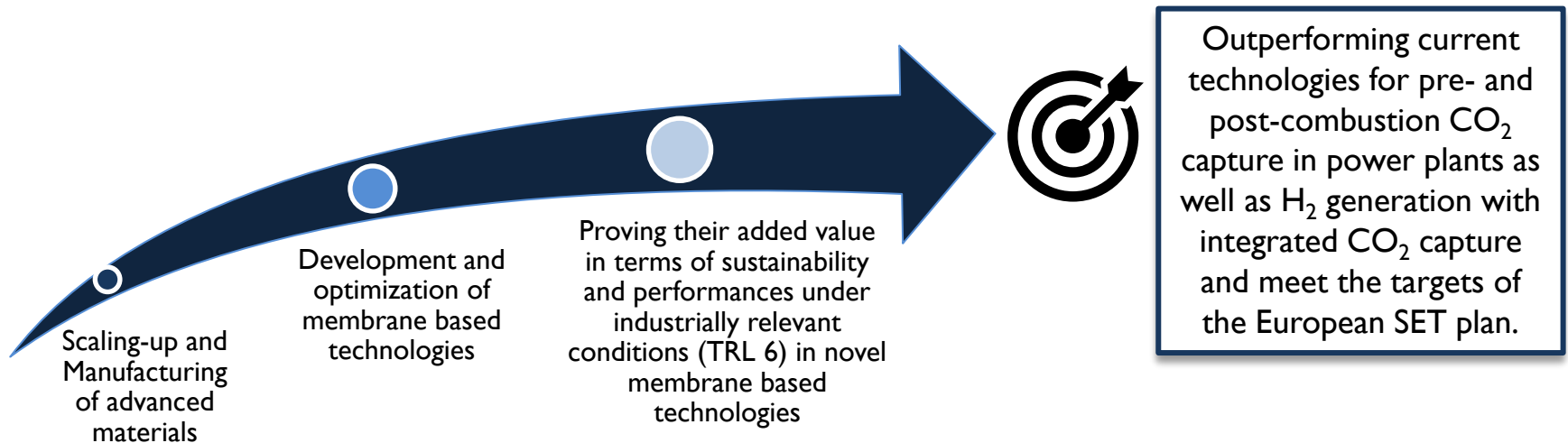
Figure 2. Typical flowsheet of a basic chemical absorption process for CO₂ capture.

Membrane based CO₂ separation for post-combustion capture

- Perm-selective membranes are thin barriers that allow selective permeation of certain gases
- Driving force for permeation is the CO₂ partial pressure, hence flue gas compression may be required, depending on the gas conditions
- In MEMBER we develop hollow fiber (HF) membrane modules permeable to CO₂, offering important advantages, such as high packing density ($>10,000 \text{ m}^2/\text{m}^3$), resistance to high pressure difference, and contained fabrication costs
- For post-combustion CO₂ capture (CO₂/N₂ separation) thin film Pebax polymer based composite hollow fibers are being prepared by dip coating of porous hollow fiber supports. Metal Organic Framework (MOF) will be in the outside coating selective layer



- The main objective of the MEMBER project is the scale-up and manufacturing of advanced materials and technologies, aimed to reduce the cost of CO₂ capture.




- Each solution is going to be demonstrated through the operation and test of a prototype
- Scale-up issues are addressed during the project and a Business Plan is prepared for the industrial application of each technology.



MEMBER Objectives



- Reference and Target Performance and Cost for the MEMBER processes
- The target CO₂ purity for MEMBER process is 95 %.



| | Reference Technology | Reference CCR [%] | Reference Cost of CO ₂ [€/ton] | MEMBER Targets for CCR [%] | MEMBER Targets for Cost of CO ₂ [€/ton] |
|---|-----------------------|-------------------|---|----------------------------|--|
| Pre-comb. Power (IGCC) | Absorption by SELEXOL | 90.9 | 33.0 | 90 | < 30 |
| Post-comb. Power (Coal) | MEA absorption | 88.1 | 54.3 | 90 | < 40 |
| Hydrogen via SMR (NG) +CO ₂ pre-comb. capture | MDEA absorption | 56 | 47.1 | 90 | < 30 |
| Hydrogen via SMR (NG) +CO ₂ post-comb. capture | MDEA absorption | 90 | 69.8 | 90 | < 30 |

Targets



Prototype A

Pre-combustion capture in power plants using MMMs at the 2 MWth biomass gasifier of CENER (Spain) aimed for BIOCCS demonstration.

CCR

> 90%

Capture Cost

< 30 €/ton



Prototype B

Post-combustion capture in power plants using MMM at the 8.8 MW CHP facilities of Agroger (GALP, Portugal).

CCR

> 90%

Capture Cost

< 40 €/ton



Prototype C

Pure hydrogen production with integrated CO₂ capture using MA-SER at the IFE-HyNor (Norway) under the supervision of ZEG POWER.

CCR

> 90%

Capture Cost

< 30 €/ton

➤ Demo Site: AGROGER CHP plant - property of Galp Energia - Portugal



- Galp Energia is a vertically integrated multi-energy operator operating in the oil and natural gas business and as a producer and seller of electricity for industrial and home consumption.
- AGROGER CHP plant consists of 2 sets of natural gas fuelled power-generators providing up to 8.8 MWe of power, plus heat to users in the area

➤ Main materials and process targets:

| Target MMM | Value | Unit |
|---|-------|------------------|
| CO ₂ permeance | 300 | GPU |
| CO ₂ /N ₂ selectivity | 70 | - |
| Membrane area | 10 | m ² |
| Design pressure | 7 | bar(g) |
| Membrane cost | <100 | €/m ² |
| Target process | Value | Unit |
| CO ₂ recovery | 90 | % |
| CO ₂ purity | 95 | % |



Other design conditions:

- Feed flow 10 Nm³/h.
- Atmospheric supply pressure

➤ Composition:

| Species | % molar |
|------------------|---------|
| CO ₂ | 5.8 % |
| H ₂ O | 3.7 % |
| O ₂ | 10.0 % |
| N ₂ | 80.5 % |
| Total | 100 % |

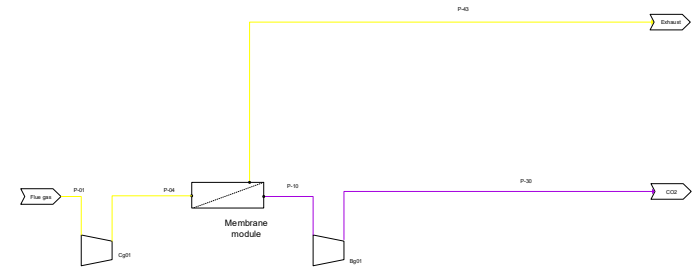
➤ Selectivities:

| | |
|-------------------------------------|-----------|
| CO ₂ /H ₂ O | 1 |
| CO ₂ /O ₂ | 28 |
| CO₂/N₂ | 70 |

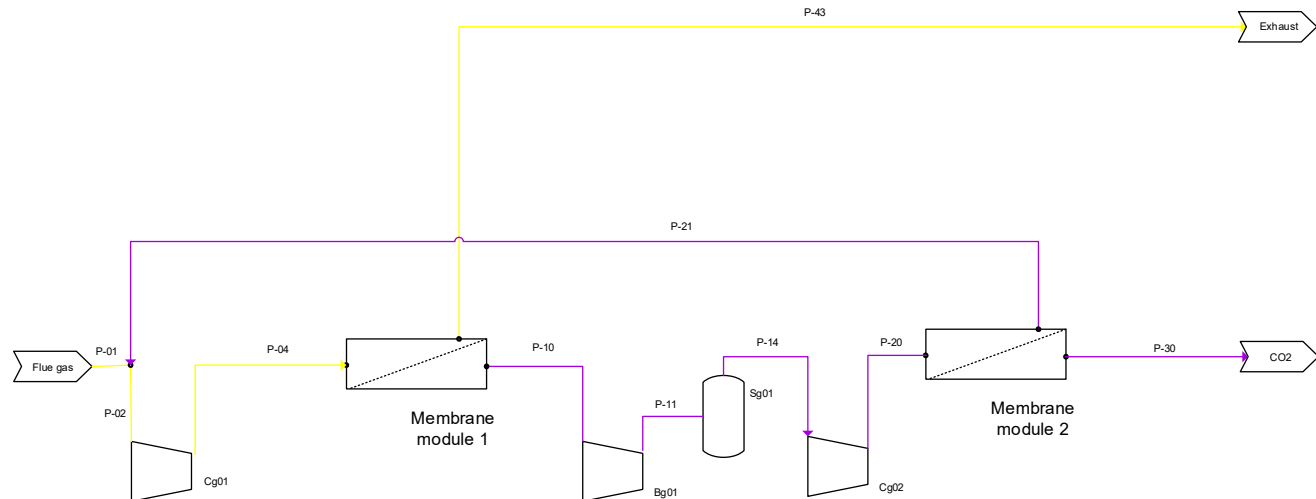
➤ 1 or 2 stage layout

Modelling different layouts

- Single stage layout;
 - CO₂ purity target not reached, neither without nor with recirculation



- Dual stage layout
 - CO₂ separation membrane #1 = 94 %
 - CO₂ separation membrane #2 = 57 %
 - Vacuum pump on permeate membrane #1



Modelling sensitivity to membrane permeance

| Permeance (GPU) | CO ₂ rec. | CO ₂ purity |
|----------------------|----------------------|------------------------|
| 300 (nominal target) | >90 % | >90 % |
| 200 | 86 % | >90 % |
| 100 | 67 % | >90 % |

* Cases with constant pressure at 4 bar

- CO₂ recovery is reduced if permeance decreases
- Purity is not compromised
- Countermeasure would be to increase operating pressure to maintain CO₂ recovery

| Permeance (GPU) | CO ₂ rec. | CO ₂ purity | Pressure membranes stages # 1/2 (bar) |
|----------------------|----------------------|------------------------|---------------------------------------|
| 300 (nominal target) | >90 % | >95 % | 7 / 6 |
| 200 | >90 % | >95 % | 9 / 9 |
| 100 | >90 % | >95 % | 14 / 14 |

Modelling sensitivity to membrane selectivity

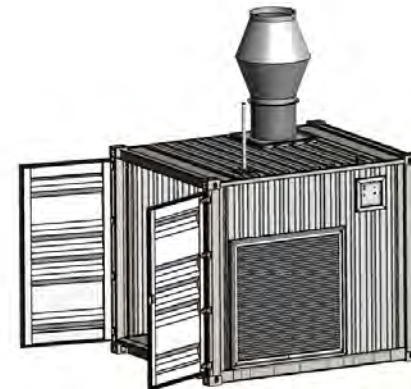
➤ Selectivity S [CO_2/N_2]

| S [CO_2/N_2] | CO_2 recov. | CO_2 purity |
|-------------------------------------|----------------------|----------------------|
| 70 | 90.6 % | 93.5 % |
| 40 | 90.6 % | 90.0 % |

* S to N_2 and H_2O left unchanged. Cases at 4 bar.

➤ Purity is affected by a decay in selectivity

- The prototype for post-combustion CO₂ capture will be demonstrated in an industrially relevant environment, allowing validation of the performance and stability of the technological solutions and materials.
- Prototype design with two stages meets targets of CO₂ purity >95 %, and recovery >90 %
- Membrane module stage #2 is smaller than membrane module stage #1
- Maximum operating pressure 7 bar(g)
- Selectivity is very important to reach the purity targets
- In case of lower permeance, we need to increase the operating pressure
- System design is finalised, and assembly is ongoing.
- System will be installed in 10 ft container





Design and development of a membrane based post-combustion CO₂ capture system

*Workshop on CCUS
16-17 / 02 / 2021*

Thank you for your attention

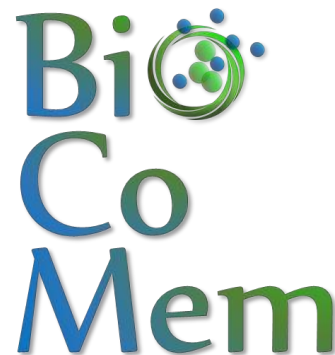
<https://member-co2.com/>

Contact:

leonardo.roses@hygear.com

www.hygear.com

Bio-based copolymers for membrane end products for gas separations



This project has received funding from the Bio Based Industries Joint Undertaking (JU) under the European Union's Horizon 2020 research and innovation programme, under grant agreement No 887075.

The JU receives support from the European Union's Horizon 2020 research and innovation program and the Bio Based Industries Consortium

WP6 : Technical, Economical, REACH and LCA assessments, circularity and plastic footprint

The present publication reflects only the author's views. The Commission is not responsible for any use that may be made of the information contained therein.

LIFE CYCLE ASSESSMENT

HOW SCIENCE-BASED ACTIONS CAN POSITIVELY
CHANGE THE INDUSTRY'S IMPACT

Stefan Frehland
Nicolas Habisreutinger

Quantis

OBJECTIVE OF THE LECTURE

- ✓ Understand key environmental issues
- ✓ Master **LCA core concepts and methodology** to be able to understand and pilot and/or conduct LCA studies
- ✓ Understand the methodological approach (assumptions, calculation methods, scope), evaluate the robustness of the results and the conclusions presented
- ✓ Be able to integrate Life Cycle Thinking into your everyday work



Good practices for this lecture

- Active listening
- No judgment
- Critical mind
- Fun !

01

What is LCA?

02

Goal & Scope definition

03

Life Cycle Inventory

04

Life Cycle Impact
Assessment



01

WHAT IS LCA?



“
Eco-design is defined as the integration of environmental perspective into products’ and services’ design and development.
”



THE LCA APPROACH

Life Cycle Assessment is recognized as the leading methodology for environmental impact evaluation. The main strengths of this tool are the following:

Metrics-based approach, allowing impact evaluations and/or comparisons to be made on a quantified and credible scientific basis.

Life-cycle oriented, allowing users to consider various product stages, to highlight potential 'burden shifting', or unintended consequences.

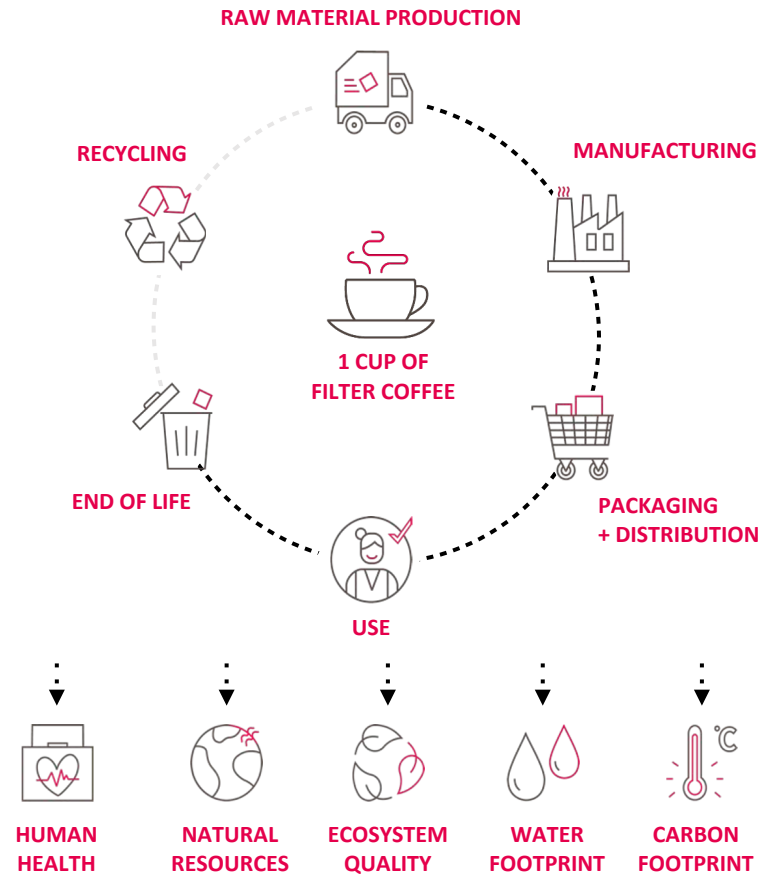
Multi-criteria: we are aligned with the PEF guidance, and cover a multiplicity of indicators in the assessment (including water use, ecotoxicity, ozone depletion, etc.)

See the whole picture

Focus on the right part

Get the facts right

Decide and act



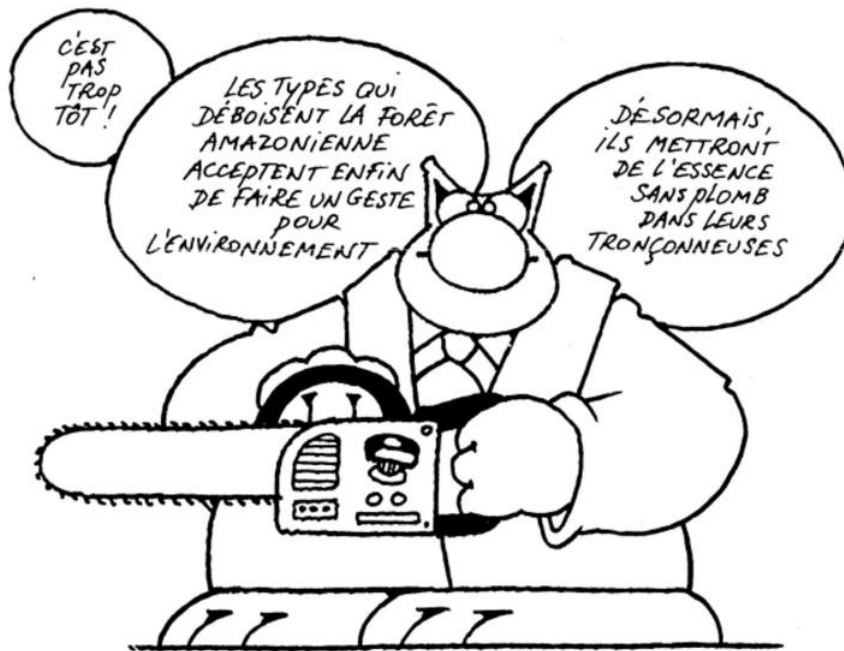
FOCUS ON THE RIGHT PART

See the whole
picture

Focus on the right
part

Get the facts right

Decide and act



It's not too early!

The guys felling trees in the Amazon have finally accepted to do something for the environment.

From now on, they will use unleaded fuel in their chainsaws!

QUESTION YOU ASK YOURSELVES

See the whole
picture

Focus on the right
part

Get the facts right

Decide and act

grocery bags?

...
from *trees, not oil*...

being **over-used**!

ripped from Brazil!

plastic comes *from China*...

paper fiber is *partly recycled*!

from **US corn**!...

bags less!

plastic?



LCA IS A GOOD DECISION MAKING TOOL



Identify environmental issues along the **value chain (hotspots)**



Identify **improvement** possibilities and production **optimization**



Compare alternatives



Set **goals** and measure **progress**



Benchmark performance



Manage **risk**



Communicate



And more

LIFE CYCLE ASSESSMENT (LCA) HAS MANY CLEAR BENEFITS

See the whole
picture

Focus on the right
part

Get the facts right

Decide and act



Get the facts
right

- Offer **appropriate solutions**
- Avoid **shifting the burden** between life cycle stages, regions, compartments or type of impact



See the whole
picture

- Iterative, **step-by-step** process looks at the complete life cycle
- **Quantitative** and robust tool
- **Compare** product alternatives



Focus on the
right part

- Find **environmental hotspots** along the value chain
- Define **priority actions**
- Encourage **supplier engagement**



Decide, act
and share

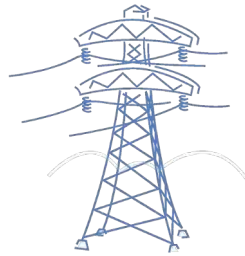
- Set smart **strategy**
- **Communicate** to customers and consumers
- **Facilitate conversations** with stakeholders

WHAT ARE THE BENEFITS OF LCA ?

The holistic perspective of LCA helps prevent shifting the burden



Electric vehicle = No emissions?



Or are emissions simply shifted?

Shifts can happen:

- From one life cycle stage to another
- From one region to another
- From one compartment (water, air, ground) to another
- From one impact to another (social or economical for instance)

WHICH OPTION IS THE MOST ECOFRIENDLY?



Plastic bag



Paper bag

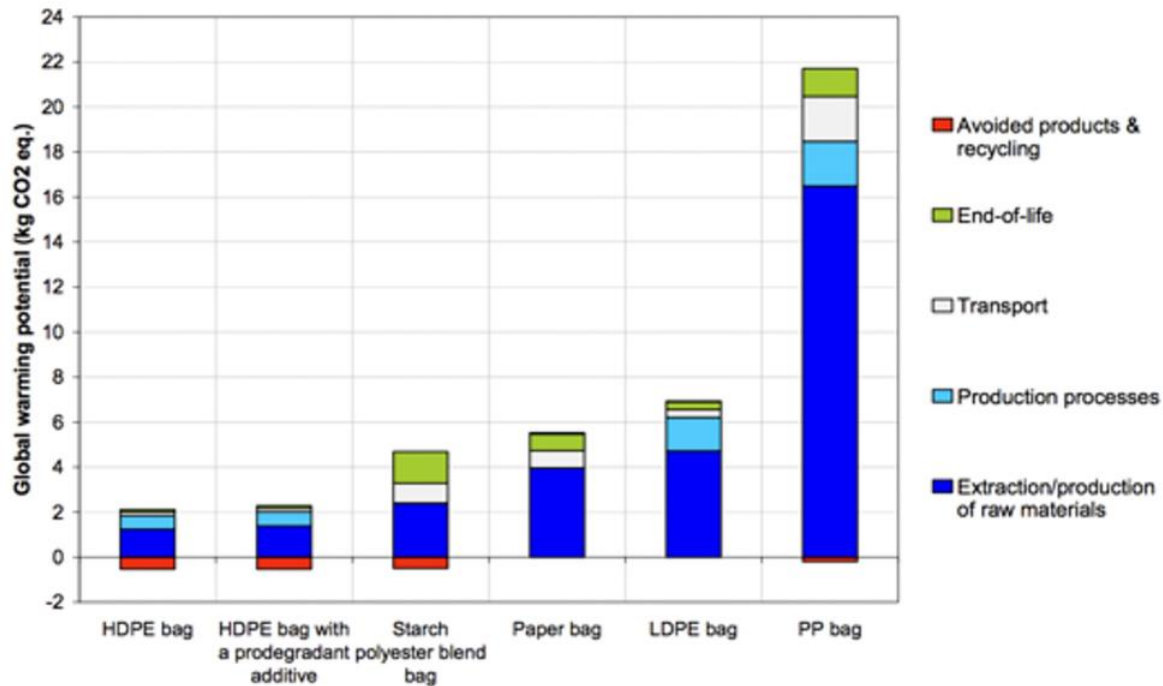
WHICH OPTION IS THE MOST ECOFRIENDLY?



Plastic bag



Paper bag



WHICH OPTION IS THE MOST ECOFRIENDLY?



Paper hand dryer

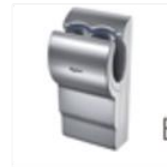


Electric hand dryer

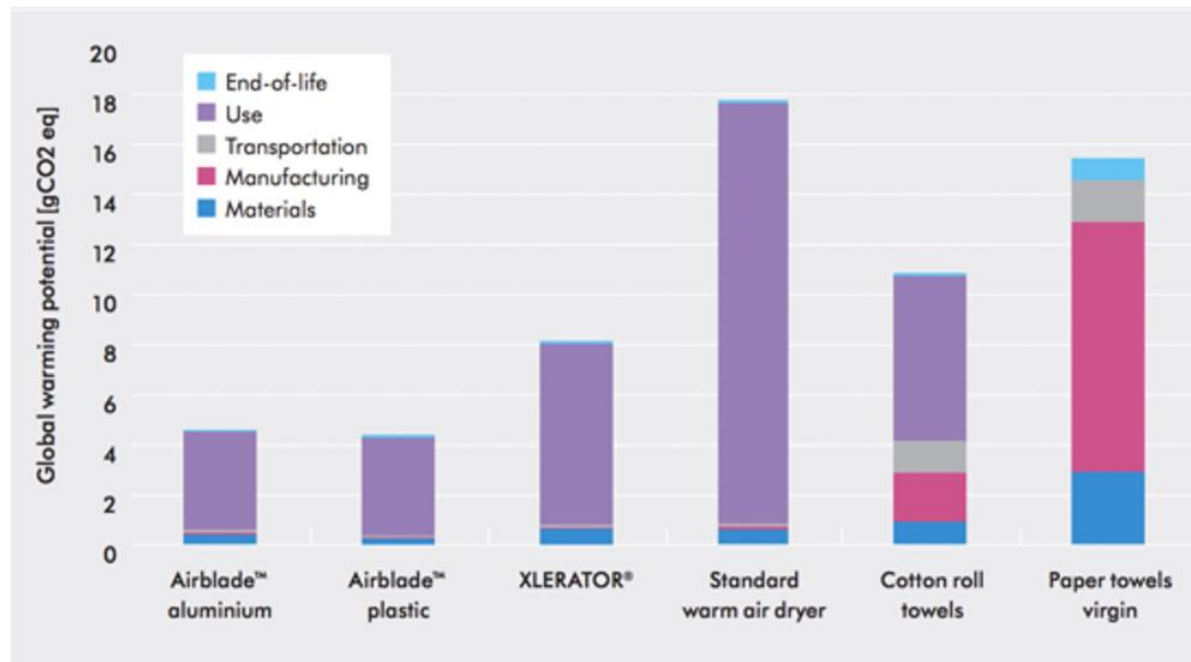
WHICH OPTION IS THE MOST ECOFRIENDLY?



Paper hand dryer



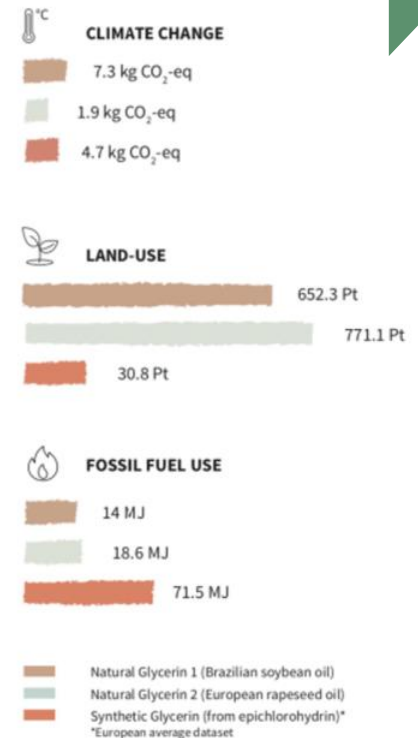
Electric hand dryer



NATURAL VS. SYNTHETIC INGREDIENTS

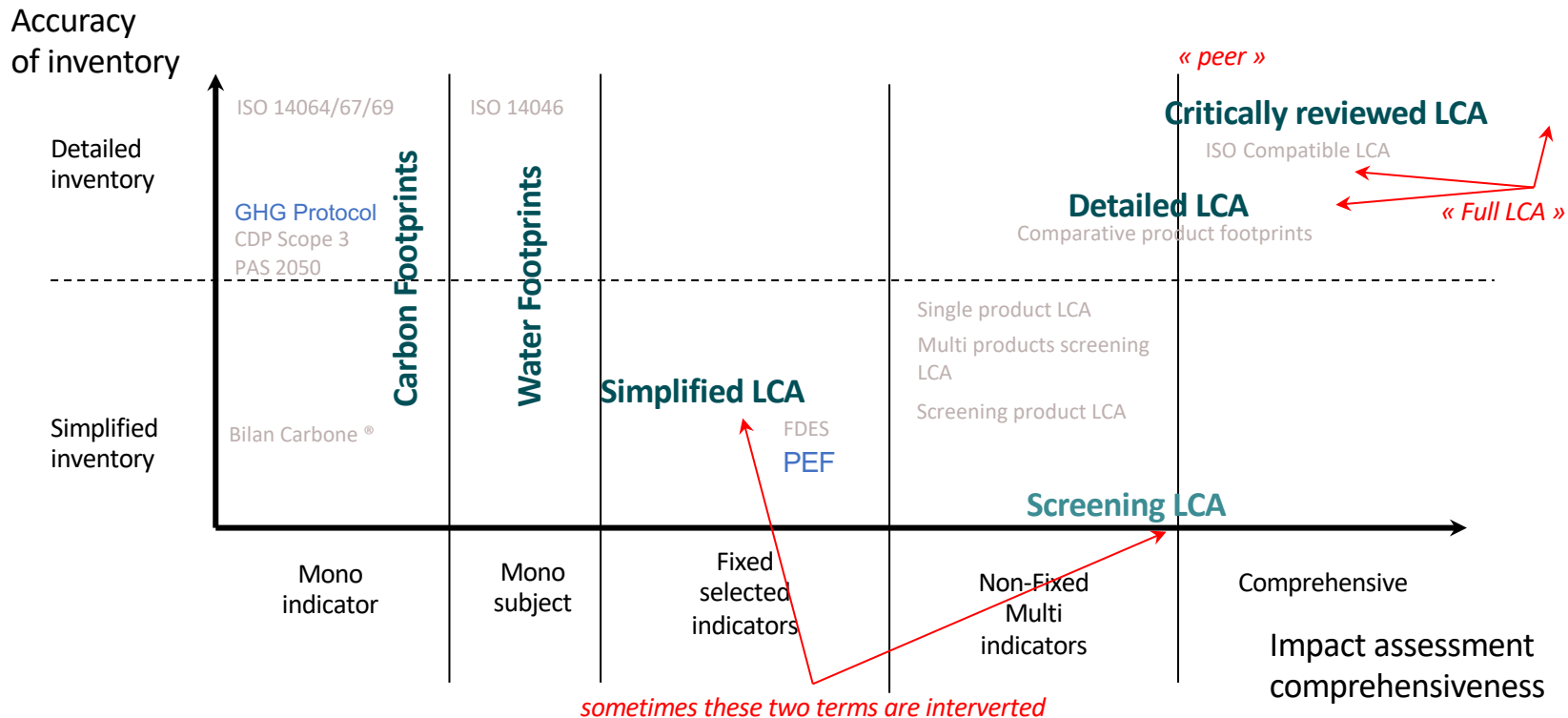
- + Consumer demand for natural beauty products is on the rise
- + Natural = Sustainability: it's not that simple
- + Need to consider the whole life cycle of a formula + its ingredients across multiple environmental criteria

IMPACT OF 1KG NATURAL VS. 1KG SYNTHETIC INGREDIENTS

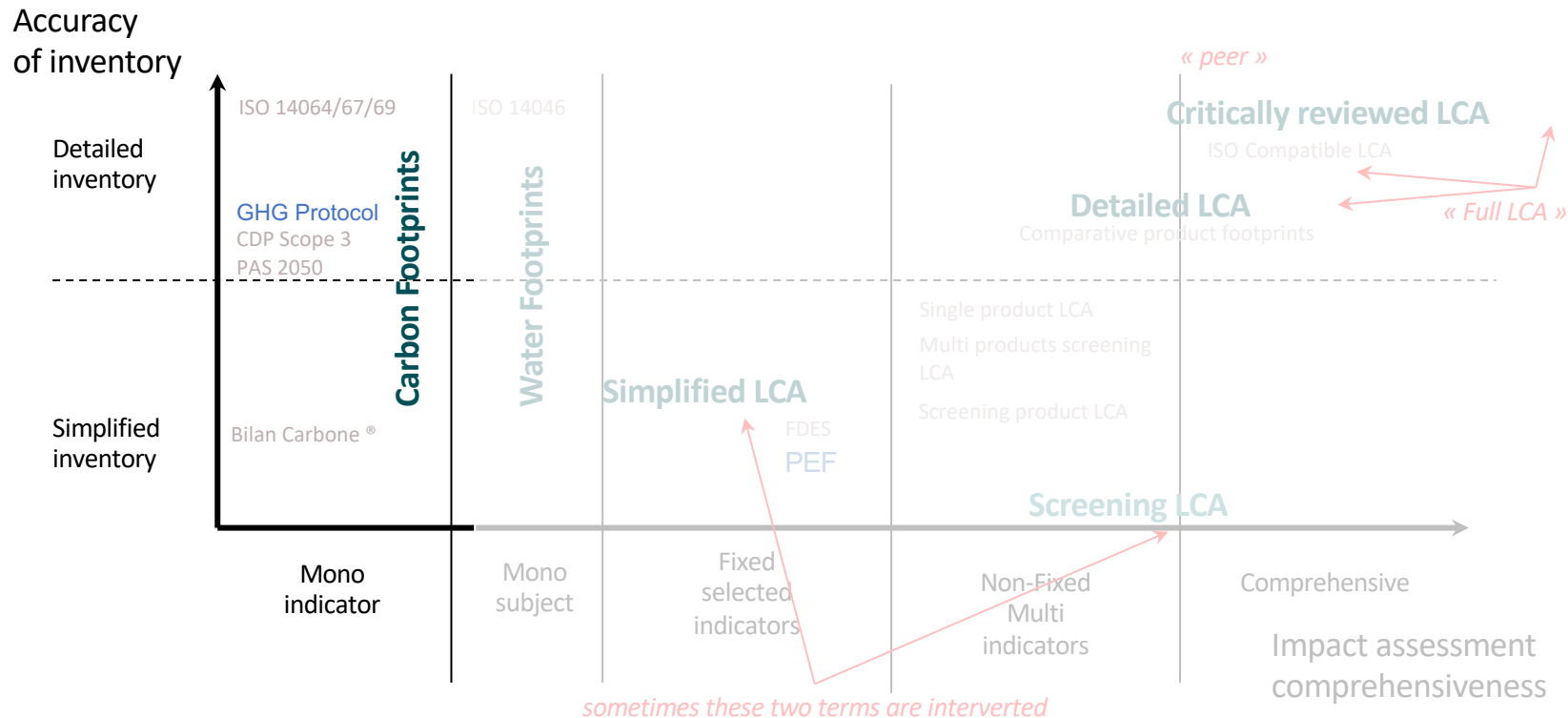


*Calculations done by Quantis in 2020.

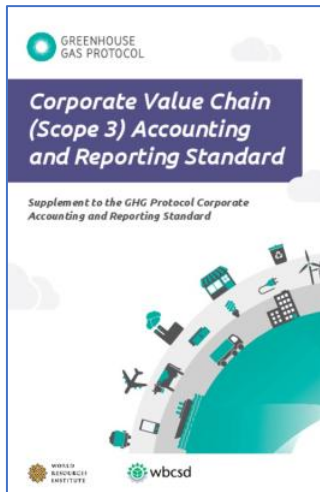
TYPES OF LCA / STUDIES



TYPES OF LCA / STUDIES



GHG PROTOCOL STANDARD

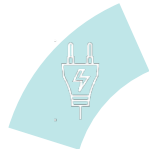


Scope 1



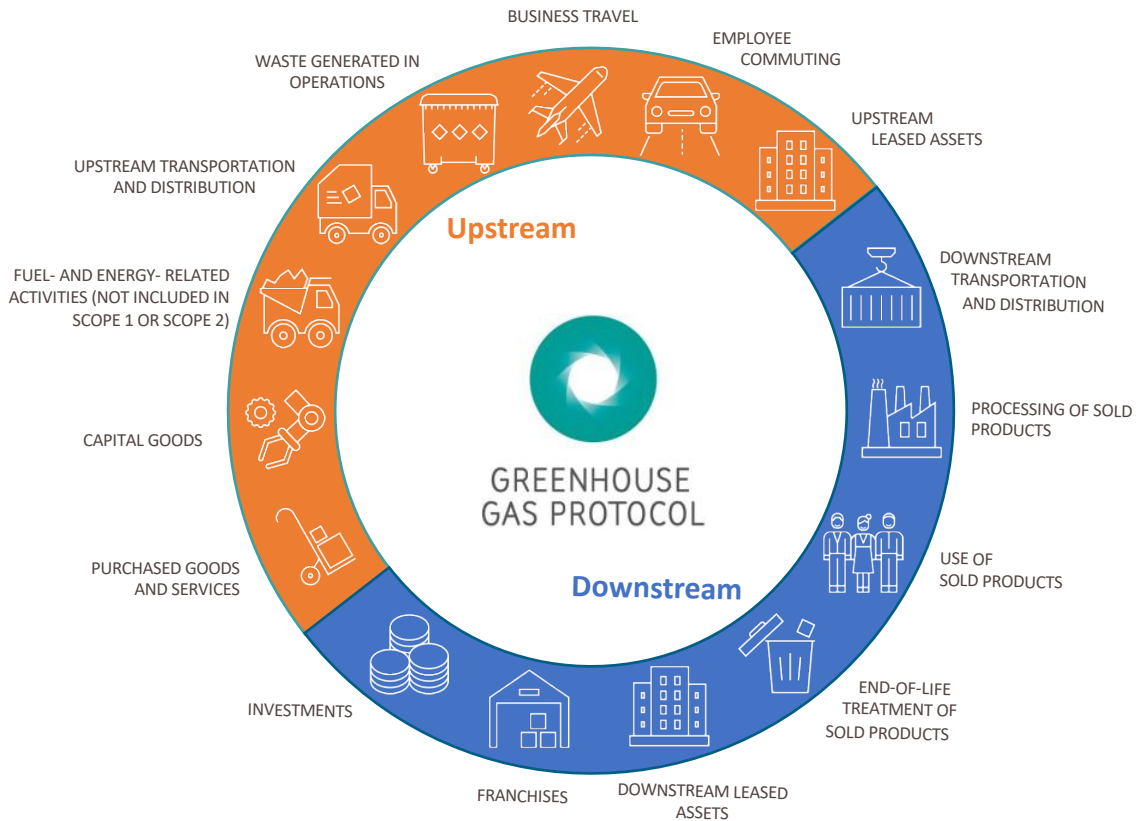
DIRECT GHG EMISSIONS

Scope 2



ELECTRICITY
INDIRECT GHG
EMISSIONS

Scope 3



GHG PROTOCOL: SCOPES DEFINITION

- **Scope 1: Direct emissions**

These occur from sources that are owned or controlled by the company, for example emissions from combustion in owned or controlled boilers, furnaces, vehicles, etc. or emissions from chemical production in owned or controlled process equipment.

- **Scope 2: Electricity and heat indirect GHG emissions**

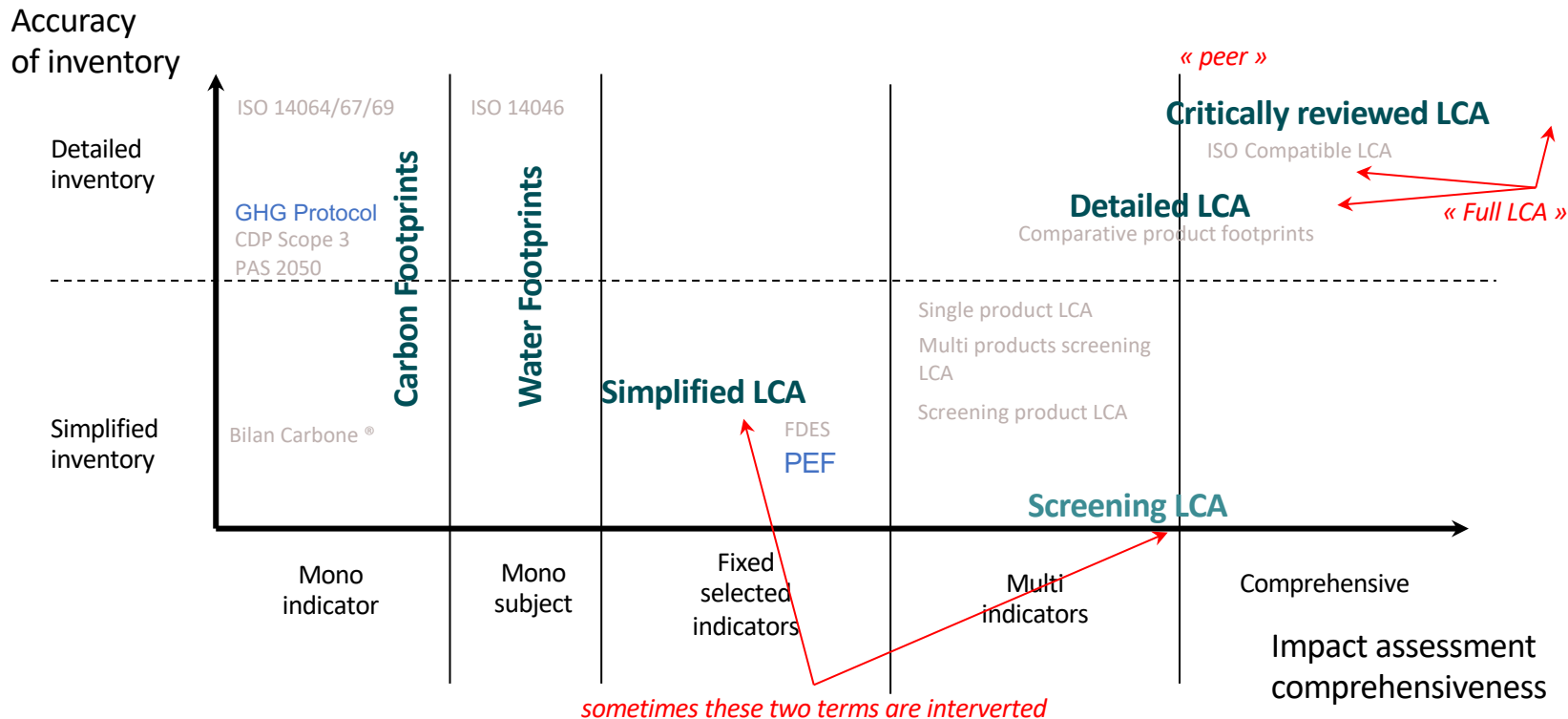
This accounts for GHG emissions from the generation of purchased electricity and heat consumed by the company (emissions from GHG sources that we consume but which production we cannot control).

Purchased electricity is defined as electricity that is purchased or otherwise brought into the organizational boundary of the company. Scope 2 emissions physically occur at the facility where the electricity is generated.

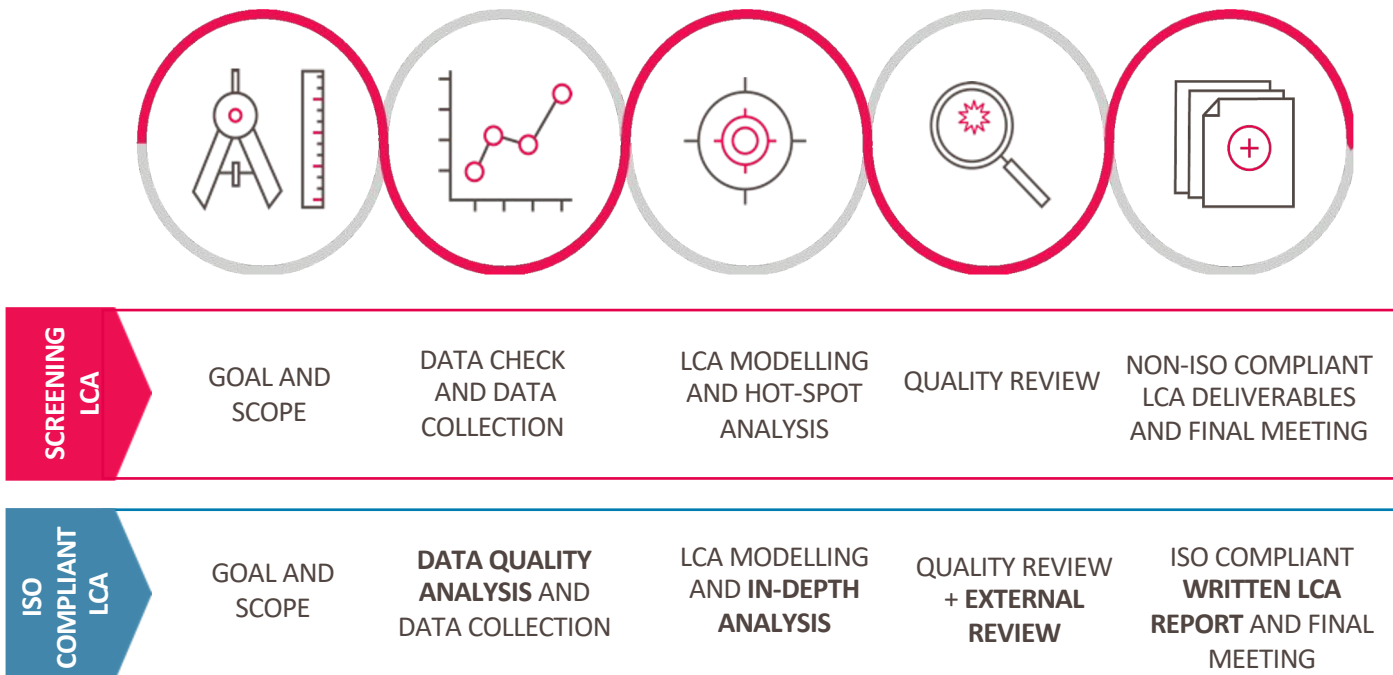
- **Scope 3 : Other indirect GHG emissions**

This is a reporting category that allows for the treatment of all other indirect emissions. Scope 3 emissions are a consequence of the activities of the company but occur from sources not owned or controlled by the company. Some examples of Scope 3 activities are the extraction and production of purchased materials, the transportation of purchased fuels and the use of sold goods and services.

TYPES OF LCA / STUDIES



WHAT ARE THE DIFFERENT STEPS TO CONDUCT AN LCA ?



*in bold approach details that are different from non-ISO compliant LCA

LCA OPTIONS AND COMMUNICATIONS

| | Give internal teams insights into comparative claims | Identify parts of the life cycle where your product performs better or needs improvement | Show impacts of different life cycle stages | Communicate externally about your own product footprint across different indicators | Communicate externally about your own product footprint versus other products of your own portfolio across different indicators | Communicate externally about your own product footprint versus other products |
|--|--|--|---|---|---|---|
| Screening Product LCA | | ✓ | ✓ | ✓ | | |
| Screening comparative LCA | ✓ | ✓ | ✓ | | ✓ | |
| Full comparative ISO-compliant LCA (peer reviewed) | ✓ | ✓ | ✓ | ✓ | ✓ | ✓ |

THE LCA FRAMEWORK YOU NEED TO KNOW

ISO NORMS 14 040 + 14 044 (2006) FOR LCA



Goal and scope

The functional unit
The system boundaries

Inventory analysis

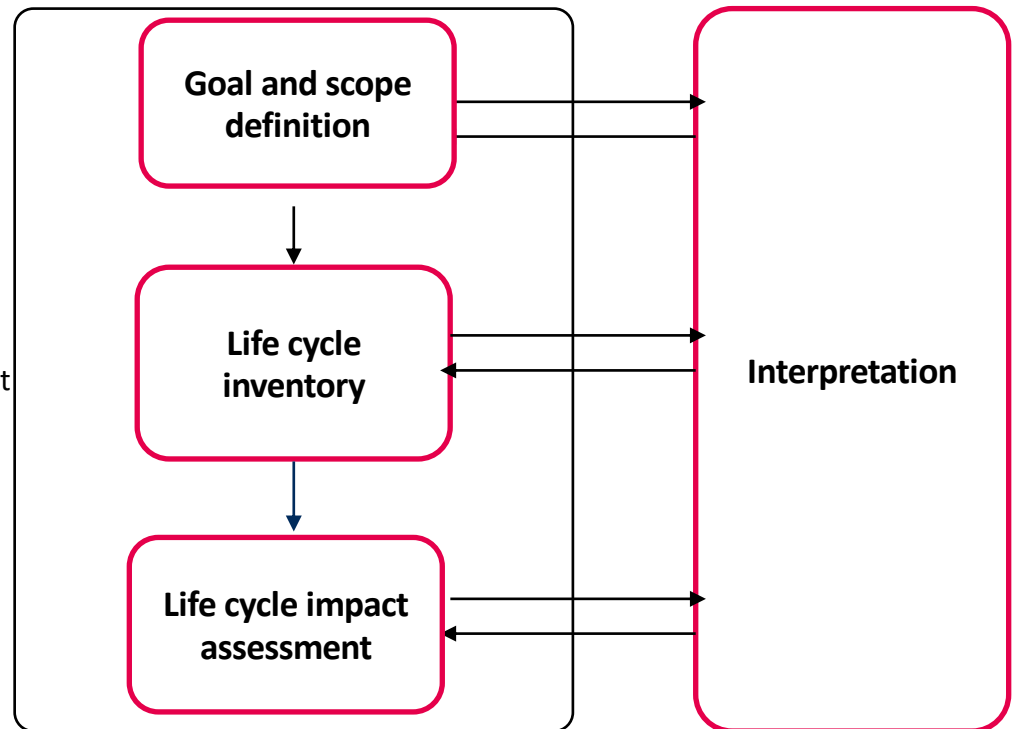
Tools and software
Inventory data and databases

Impact assessment

The synthetic nature of impact assessment
Avoiding tradeoffs (e.g., single indicator)

Interpretation

Numbers are not enough



02

GOAL & SCOPE DEFINITION





*“All the really important mistakes
are made on the first day.”*

GOAL AND SCOPE

The scope includes the following items:

- **Product system** to be studied
- **Functions** of the product system or, in the case of comparative studies, the systems
- **Functional Unit (FU)** and **reference flow**
- System **boundaries**
- **Allocation** procedures
- **Impact categories** selected and methodology of impact assessment
- Data requirements; **assumptions; limitations**
- Initial data quality requirements
- **Type of critical review, if any**
- Type and format of the report required for the study

CASE STUDY :What is the function of a light bulb?



CASE STUDY : Is this comparison fair?



VS



CASE STUDY : What is the function of a light bulb?



VS



Provide light at a certain intensity and for a certain time

CASE STUDY : Which unit would allow to make a fair comparison?



VS



Provide 500 to 900 lumens for 10 000 hours

CASE STUDY : What should be compared



x10

Incandescent light bulb
60 W - 1 000h

VS



x1

Fluorescent light bulb
13 W - 10 000h

CASE STUDY : Could you provide a functional unit for this comparison?



Source: Alessandro Fontana – SUPSI

Little exercise (yay!)

| Product or system | Main function | Functional unit | Reference flow (what you buy) | Key parameters linking UF with reference flow |
|-------------------|---------------|----------------------|---|---|
| Hand dryer | Dry hands | 1 pair of hand dried | 1.5 serviettes et 1/50000 support pour serviette papier Ou 1800 W pendant 30s et 1/50000 sèche-mains électrique | Number of towels Drying power |

CASE STUDY : Is this comparison fair?



iPhone 12
1000h of phone calls

VS



Nokia 3310
1000h of phone calls

CASE STUDY : What about this comparison?



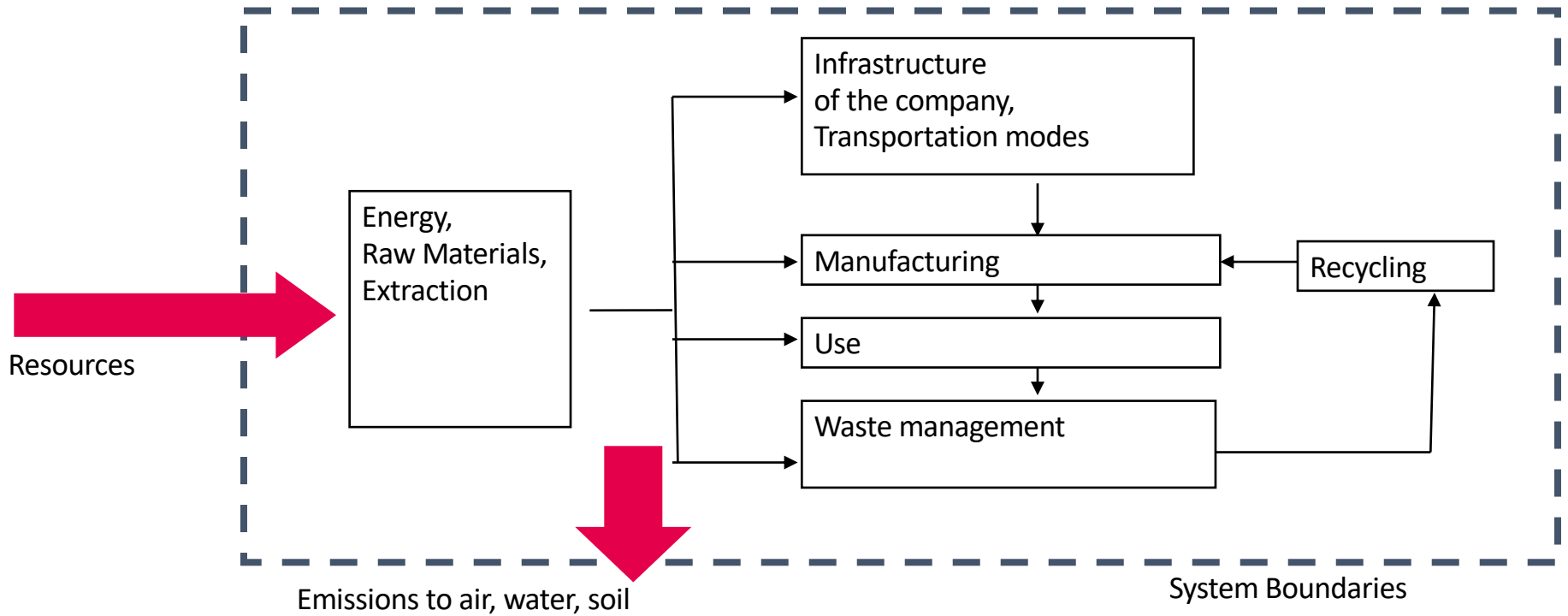
Polyethylerne
1 kg

VS

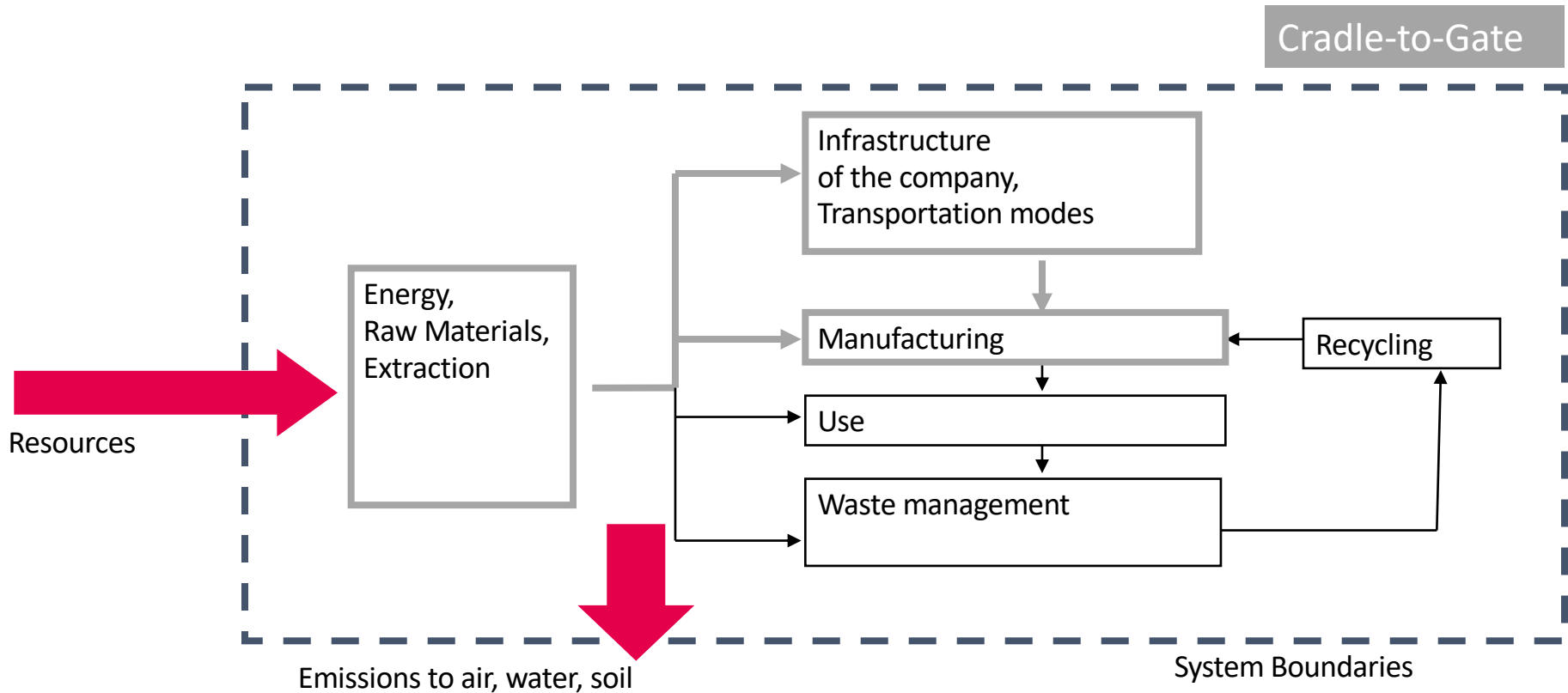


Glass
1 kg

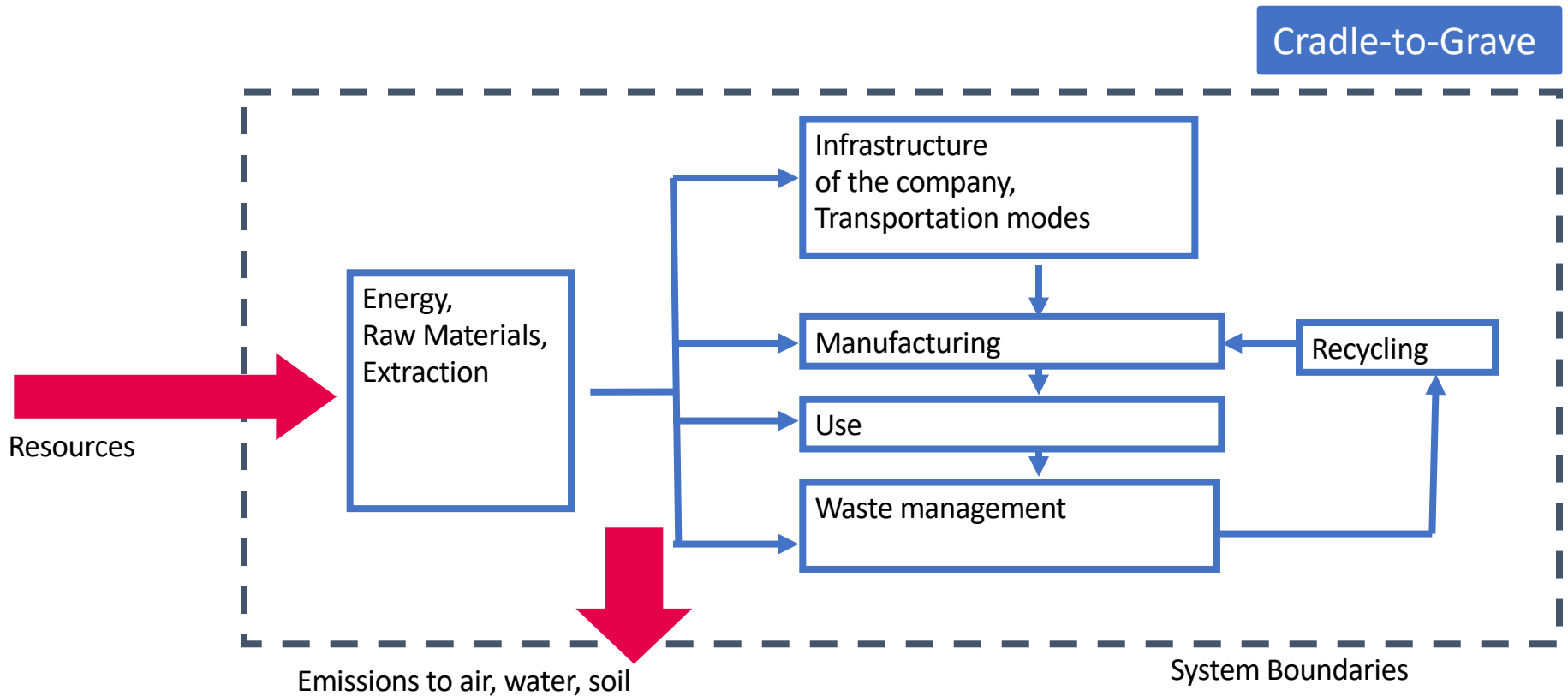
SYSTEM BOUNDARIES



SYSTEM BOUNDARIES



SYSTEM BOUNDARIES



SYSTEM BOUNDARIES

- ❓ **Cradle-to-Cradle:** Regenerative design, turning waste into product (=no more waste)
- ❓ **Gate-to-Gate:** Gate-to-gate is a partial LCA looking at only one value-added process in the entire production chain

03

LIFE CYCLE INVENTORY



THE LCA FRAMEWORK YOU NEED TO KNOW

ISO NORMS 14 040 + 14 044 (2006) FOR LCA



Goal and scope

The functional unit
The system boundaries

Inventory analysis

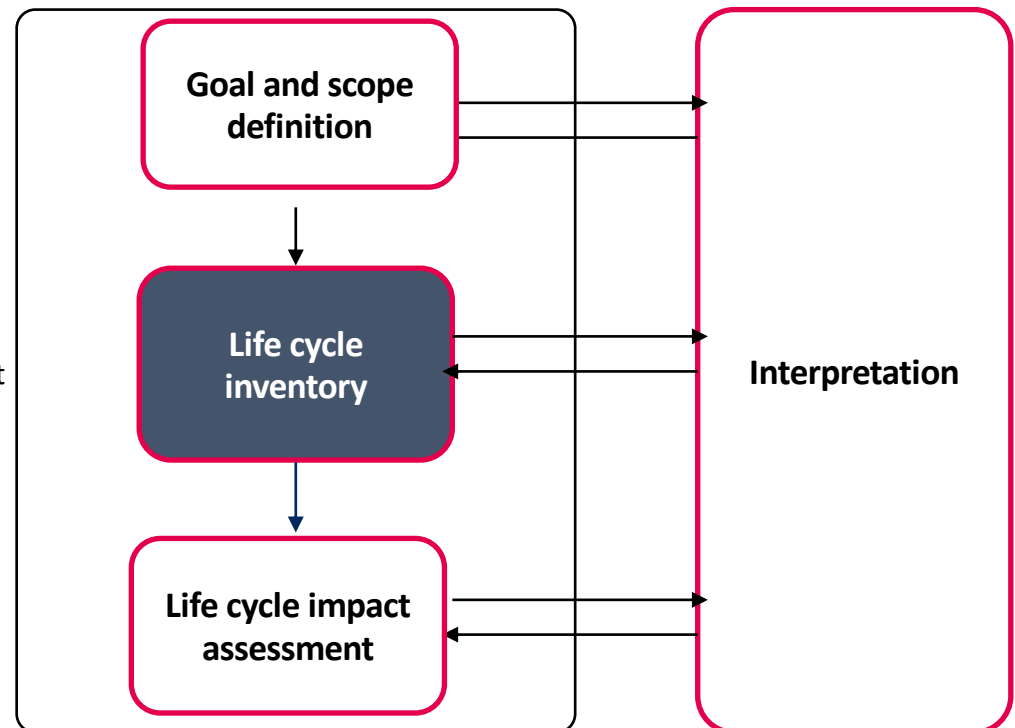
Tools and software
Inventory data and databases

Impact assessment

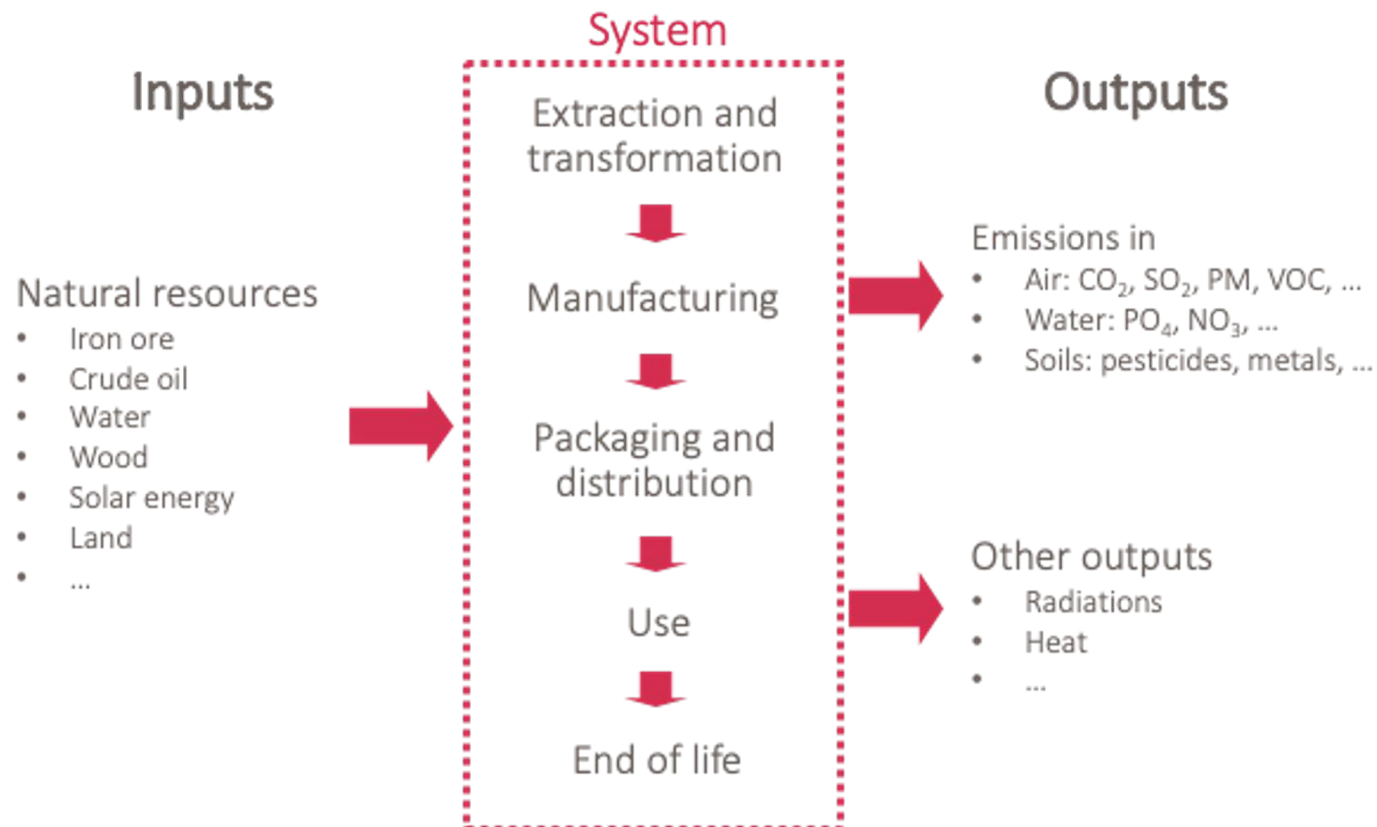
The synthetic nature of impact assessment
Avoiding tradeoffs (e.g., single indicator)

Interpretation

Numbers are not enough



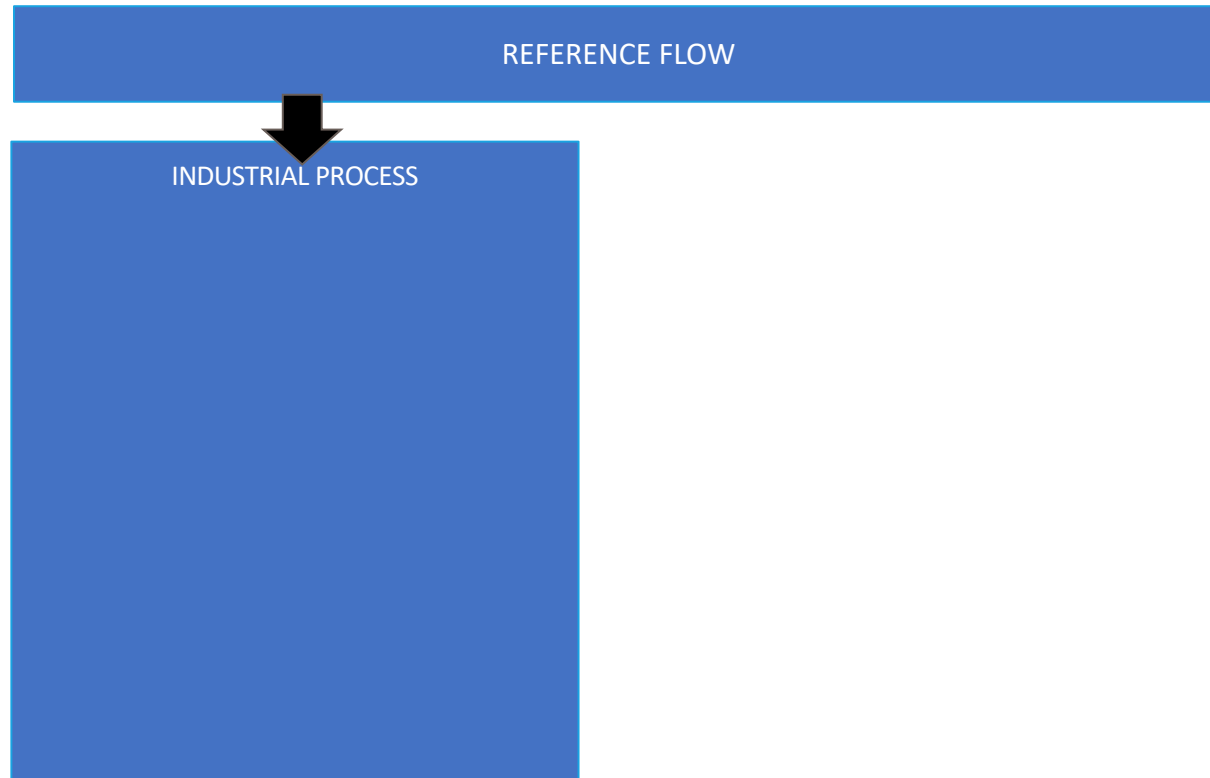
LIFE CYCLE INVENTORY



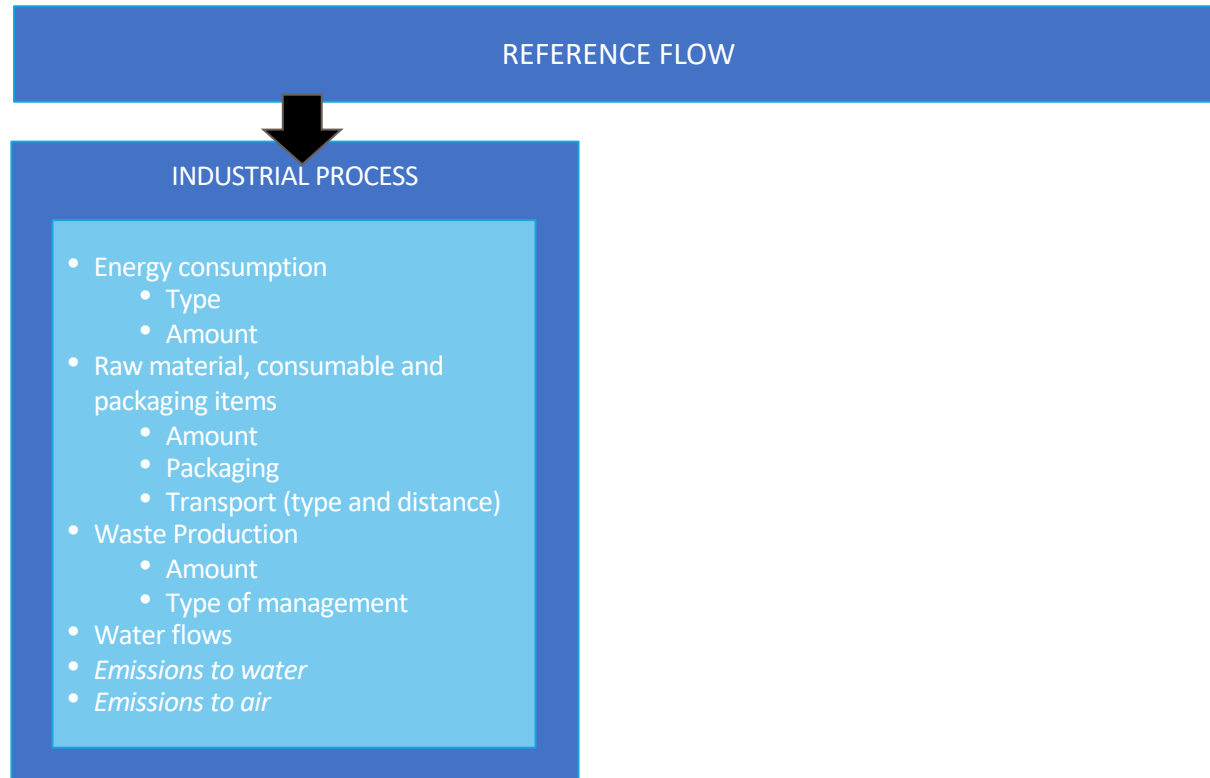
COLLECTING THE DATA

REFERENCE FLOW

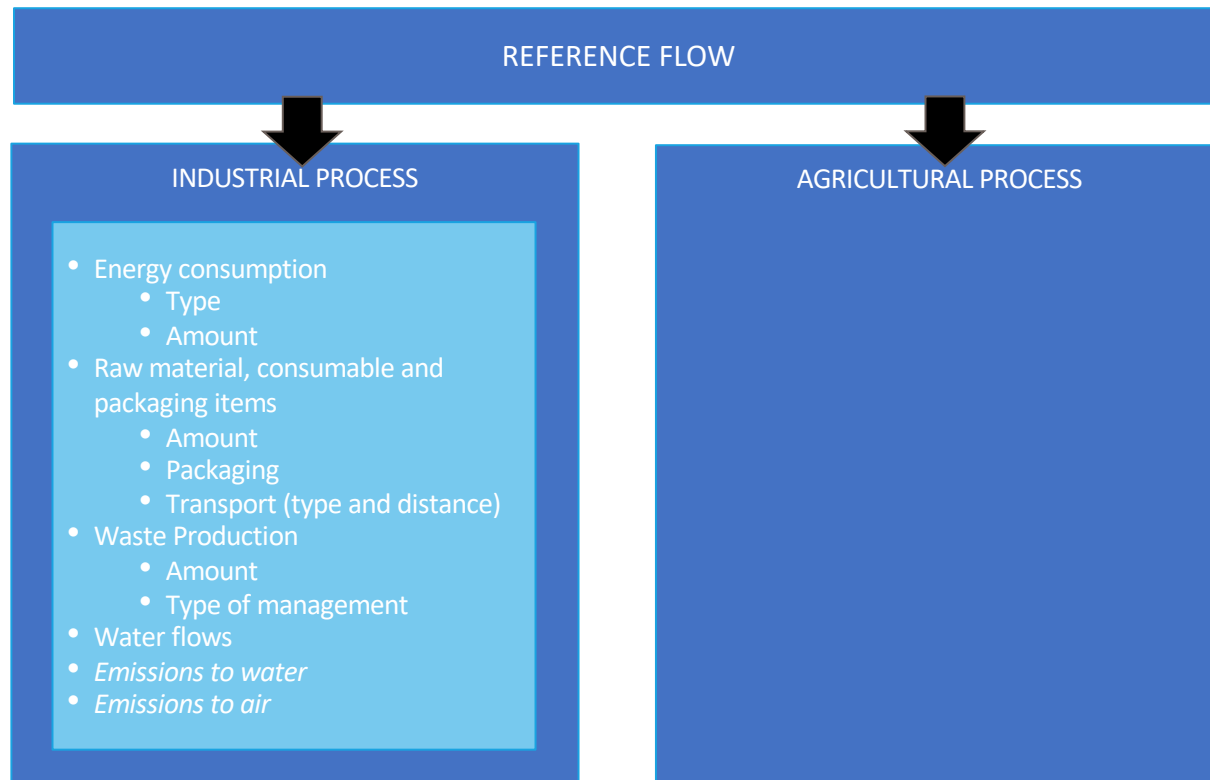
COLLECTING THE DATA



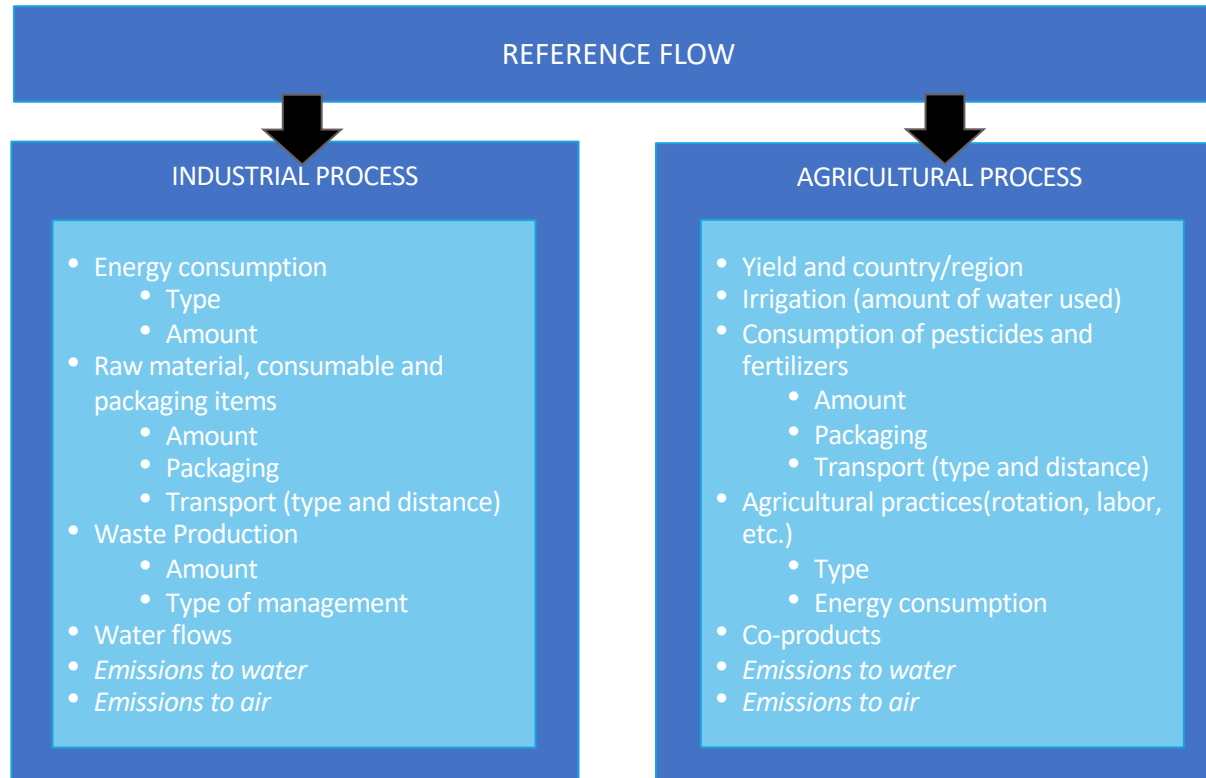
COLLECTING THE DATA



COLLECTING THE DATA



COLLECTING THE DATA



EVALUATE DIFFERENT FLOWS

PRIMARY DATA

Comes from specific measurements. Primary data Data from measurements and operational technical specifications. The main primary data are:

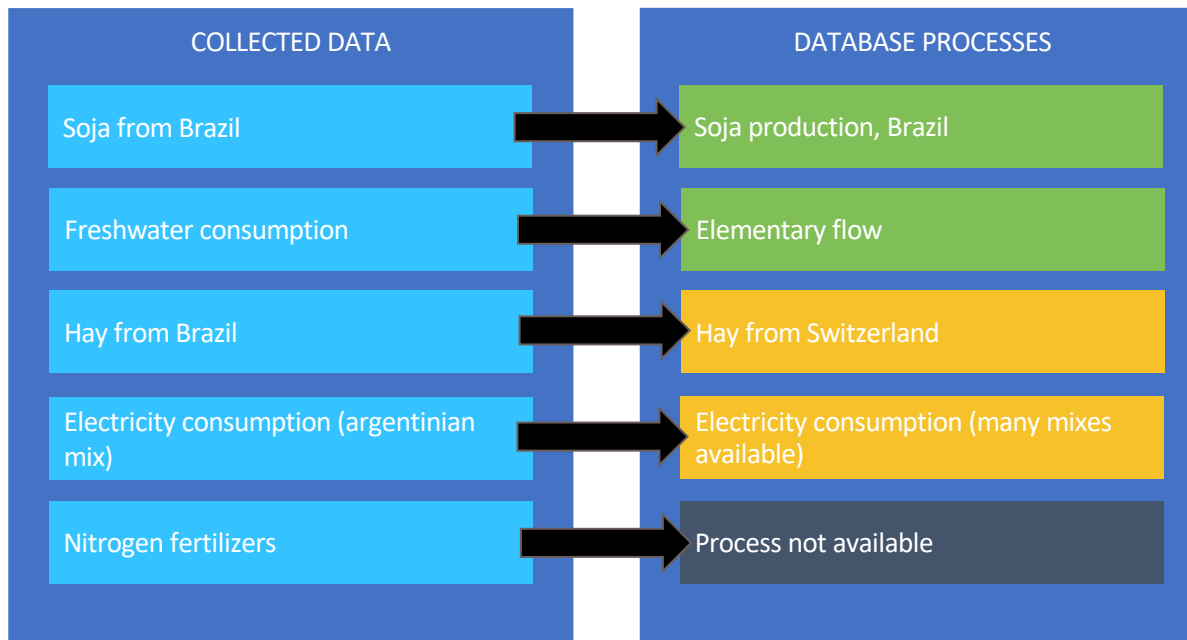
- Energy and water consumption
- Purchases (raw materials, packaging items)
- Origin of materials purchased and associated transport

SECONDARY DATA

Data from recognized and public sources (e.g. waste management data, generic data)

Data from evaluation models (e.g. emissions to air from combustion, emissions to water from the use of fertilizers)

IDENTIFY AVAILABLE PROCESSES IN OUR DATABASES

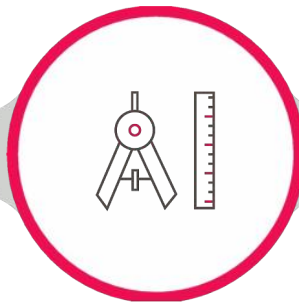


COMMON PROBLEMS



PROCESS

No process in the database describes the measured flow



FLOWS

Identified flows cannot be measured



UNITS

Units available do not match the ones available in our DB



MEASUREMENTS

I've done my model but there's no impacts in my results

COMMON PROBLEMS



A recurring problem in LCA, the databases used are in continuous development and are enriched each year with new processes. A significant part of LCA practitioner job is to create new datasets

PROCESS

No process in the database describes the measured flow

Use of proxies

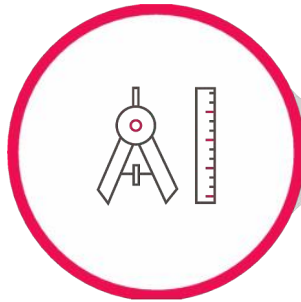
Adapt existing processes

Use data from scientific literature

SOLUTION TO THE PROBLEM

ORIGIN OF THE PROBLEM

COMMON PROBLEMS



FLOWS

Identified flows cannot be measured

In many cases, it is difficult to obtain specific data for a process. This is typical when the relevant steps take place outside the operational control of the company.

Use of data from literature
□ secondary data

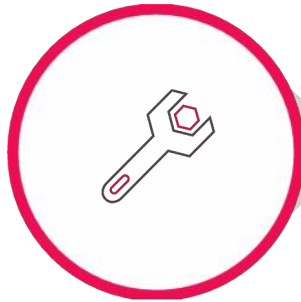
Expert hypothesis and sensitivity analysis

Flow exclusion
□ cut-off

SOLUTION TO THE PROBLEM

ORIGIN OF THE PROBLEM

COMMON PROBLEMS



UNITS

Units available do not match the ones available in our DB

Operationally measured data may not be aligned with data presented in the database.



Identification of parameters enabling the conversion from a flow to another. They can be linked by:

- Energy LHV (PCI in French)
- Density
- Weight
- Surface / Volume

SOLUTION TO
THE PROBLEM

ORIGIN OF THE
PROBLEM

COMMON PROBLEMS



When analyzing results of an LCA, one may be surprised by the absence of certain flows perceived as important in the results. This may be due to several reasons related to the approach used.

MEASUREMENTS

I've done my model but there's no impacts in my results

Datasets' nomenclature problem

Flow is not characterised in the method

No existing method evaluate the flow

SOLUTION TO THE PROBLEM

ORIGIN OF THE PROBLEM

04

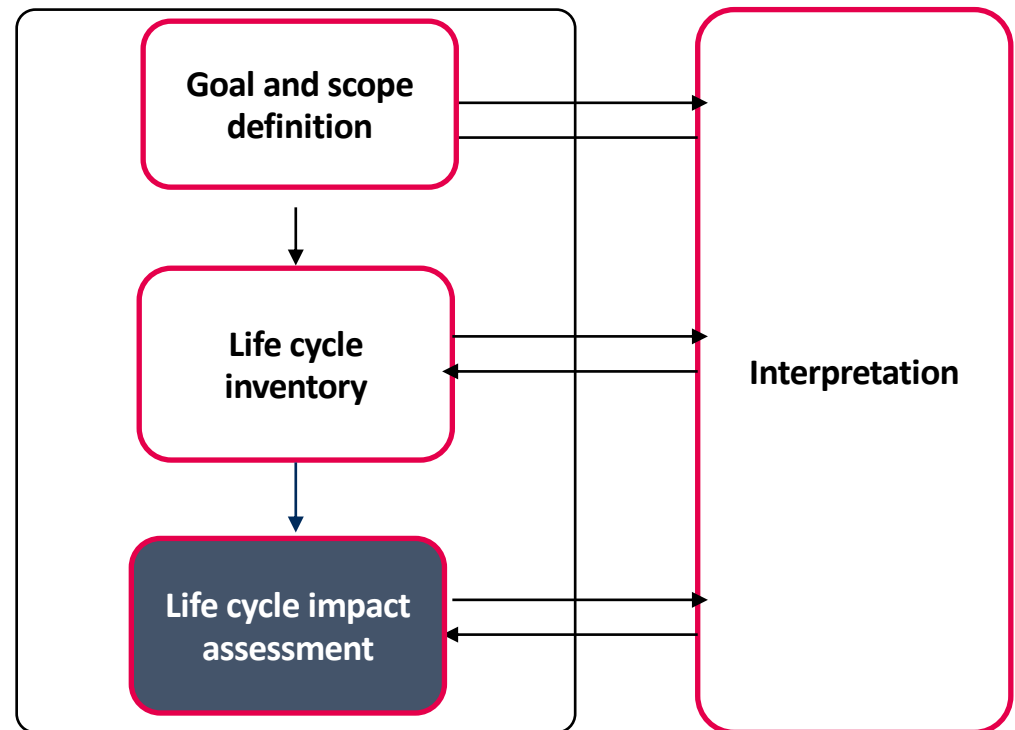
LIFE CYCLE IMPACT ASSESSMENT

+ KEY
METHODOLOGICAL
CHALLENGES IN LCA

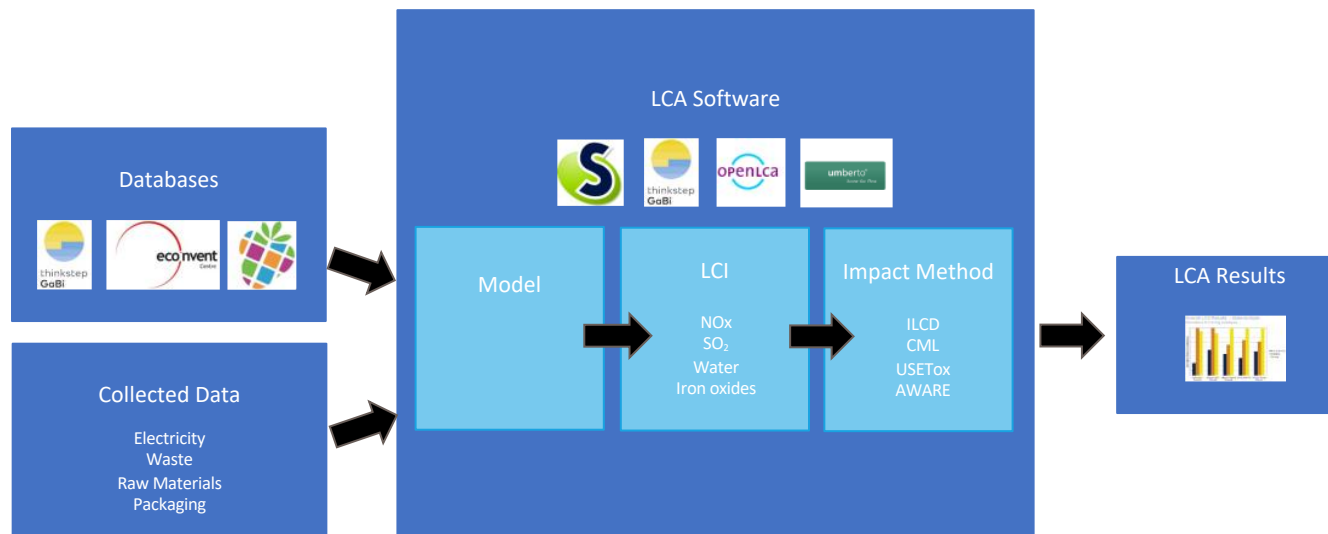


THE LCA FRAMEWORK YOU NEED TO KNOW

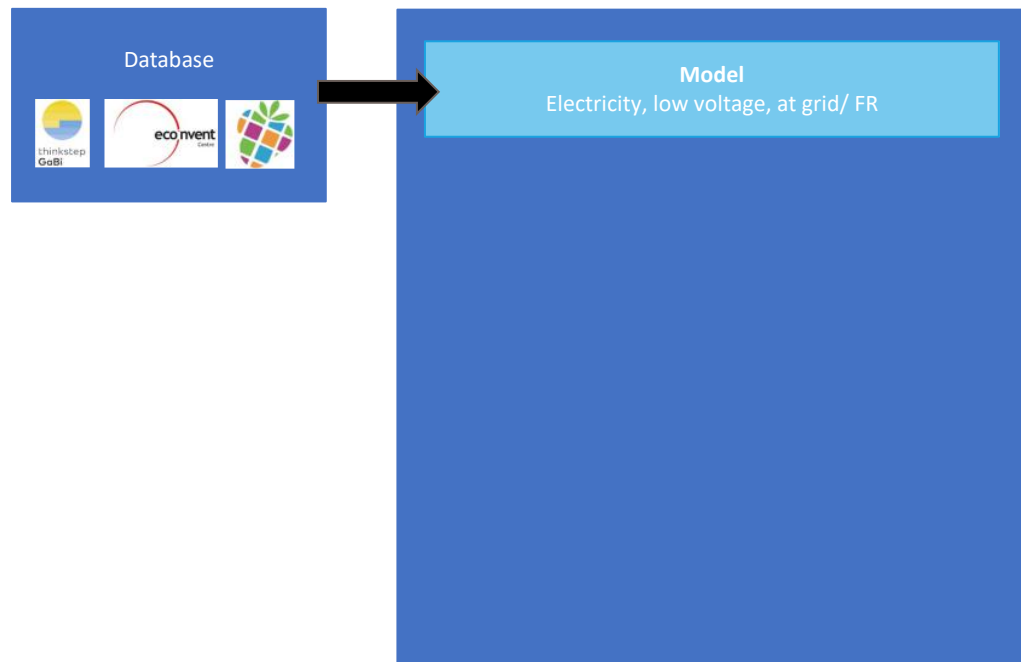
ISO NORMS 14 040 + 14 044 (2006) FOR LCA



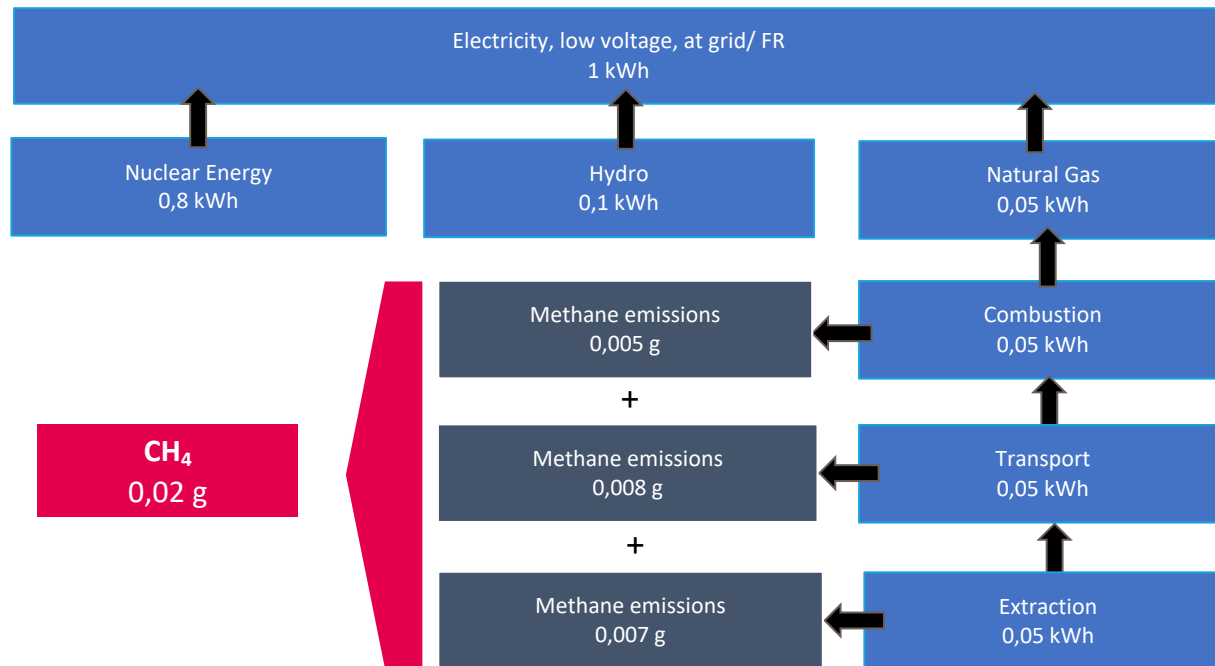
LCA MODELLING TOOLS AND DATABASES



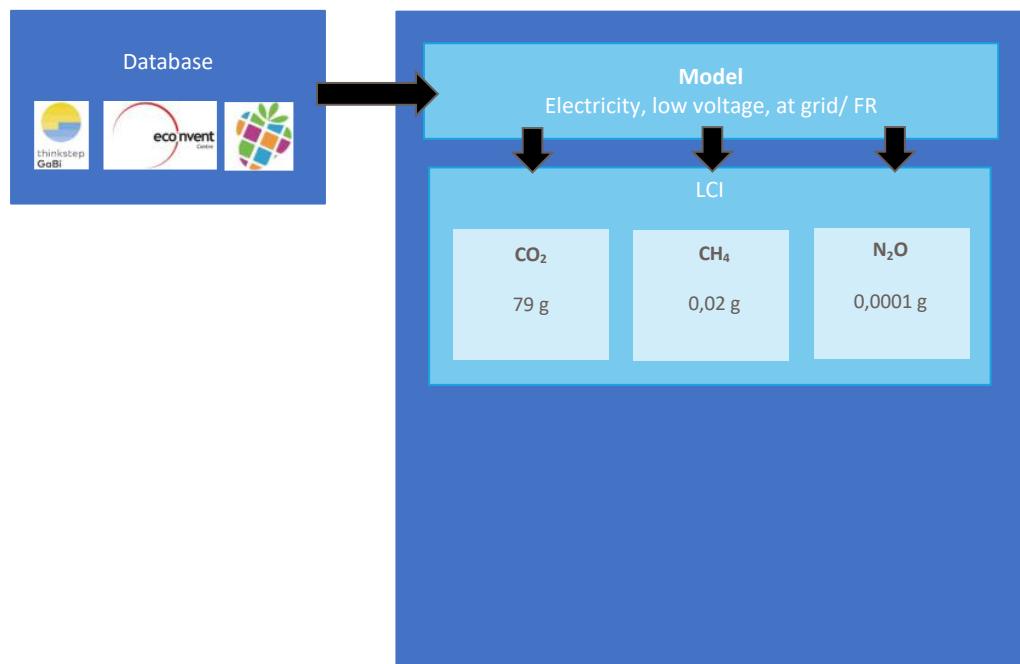
CHOOSING EMISSION FACTORS



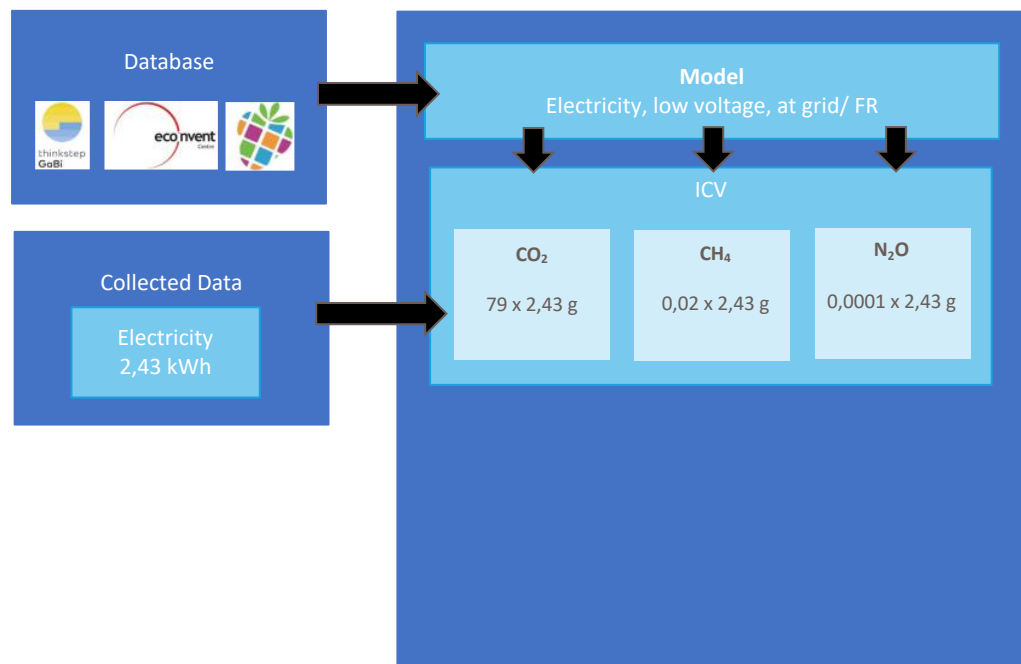
COMPUTING THE LCI



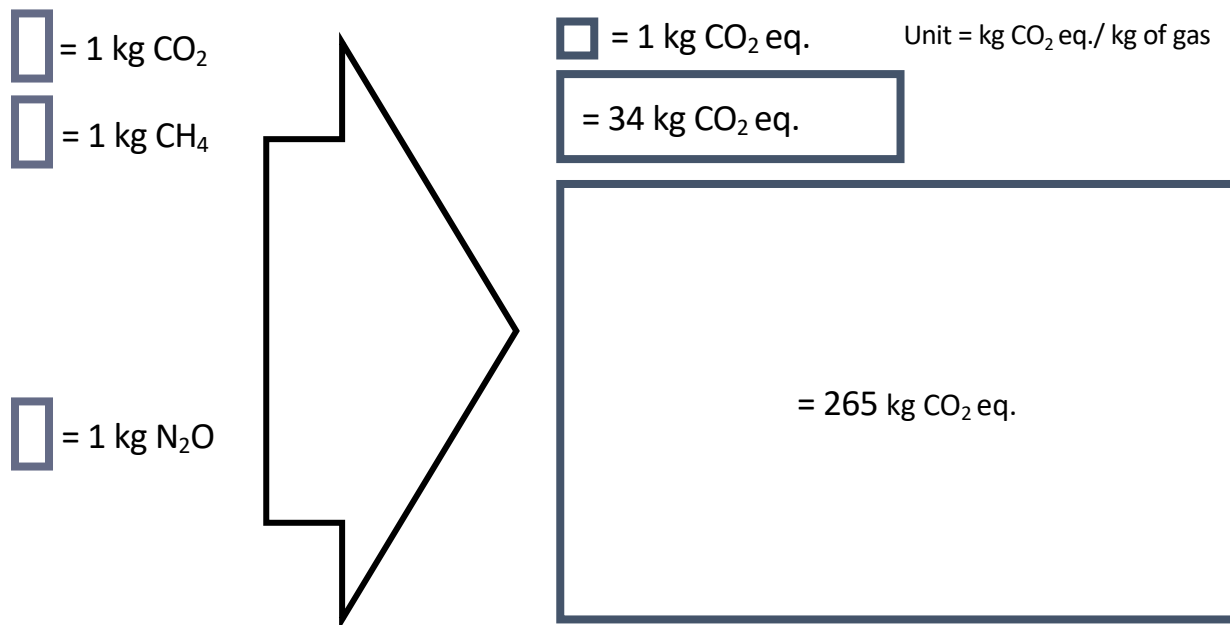
COMPUTING THE LCI



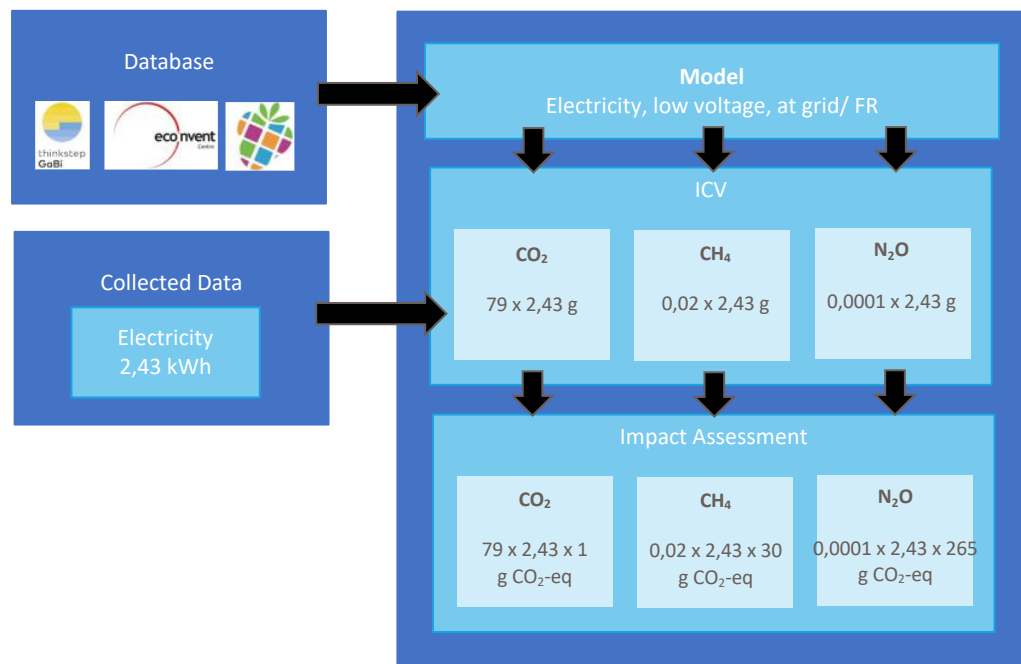
USING THE INPUT DATA



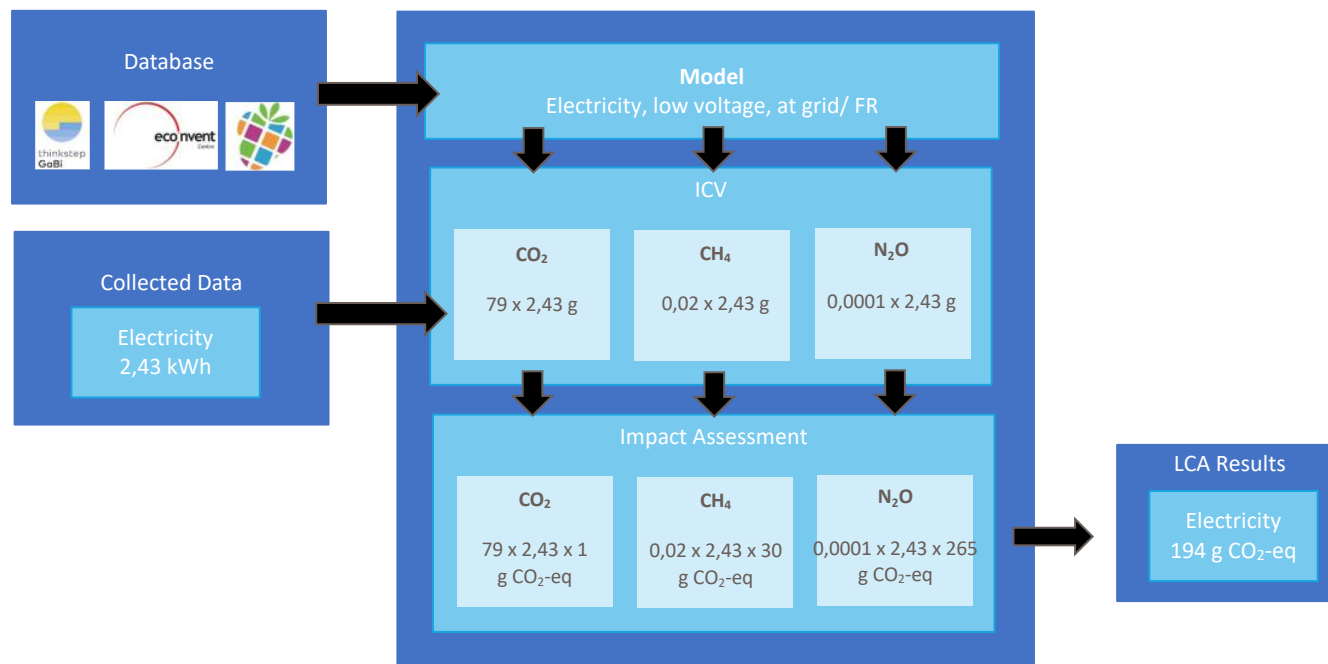
CALCULATING THE LCIA



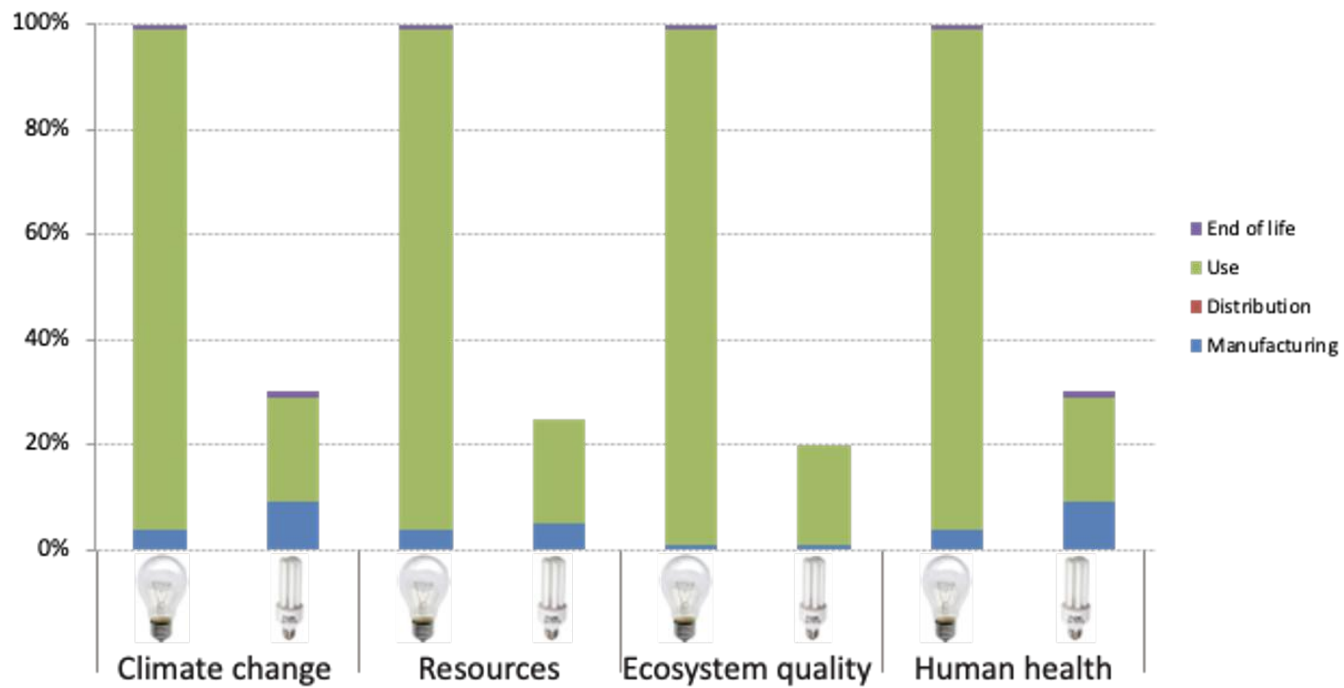
CALCULATING THE LCIA



CALCULATING THE LCIA



IMPACT ASSESSMENT

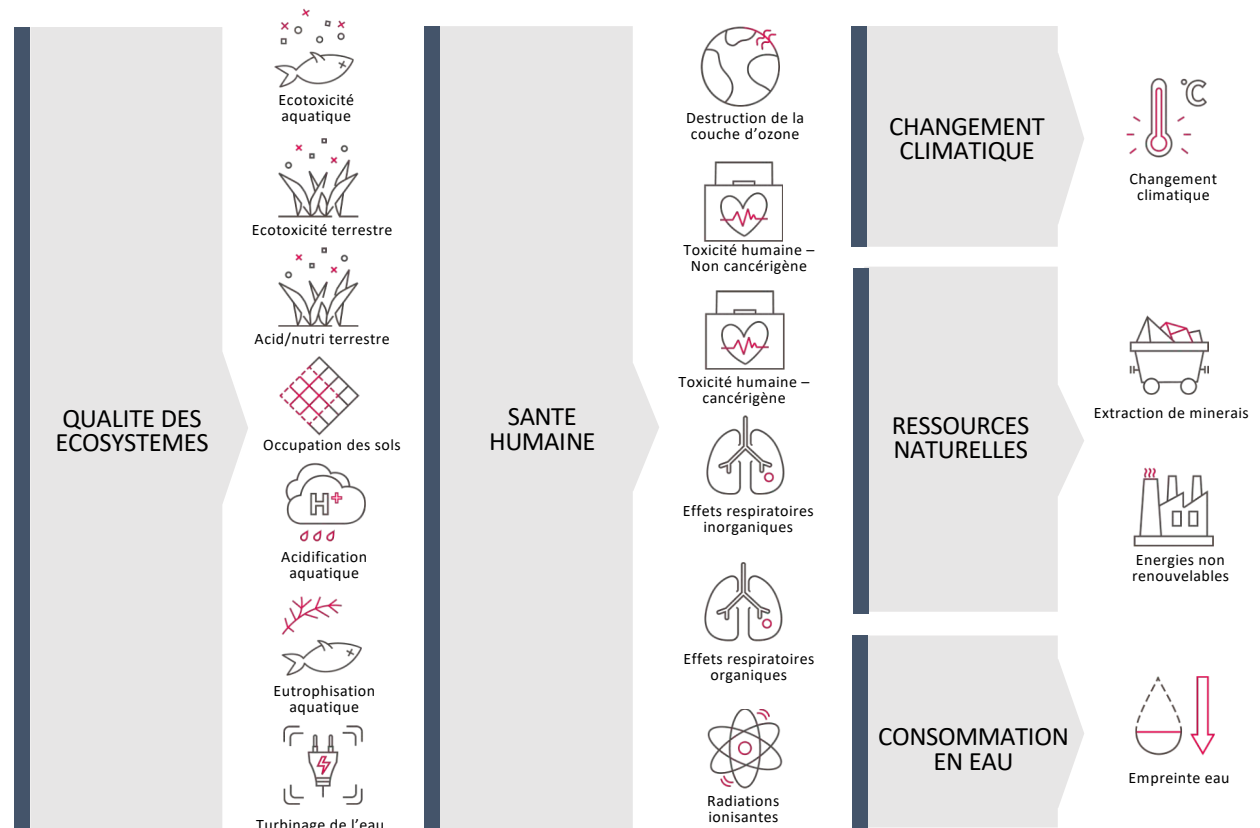


2. UNCERTAINTY OF IMPACT METHODS

| Impact category or LCI indicator | Unit | Class* | Minimal significance level |
|---|-------------------------------------|---|----------------------------|
| | | I: recommended and satisfactory | |
| | | II: recommended, but in need of some improvements | |
| | | III: recommended, but to be applied with caution | |
| Climate change | kg CO ₂ eq | I | Factor 2 |
| Ozone depletion | kg CFC-11 eq | I | Factor 2 |
| Human toxicity – non-cancer effects | CTUh | III (interim) | Factor 10 |
| Human toxicity – cancer effects | CTUh | III (interim) | Factor 5 |
| Particulate matter | Deaths/kg PM _{2.5} emitted | I | +/-20% |
| Ionising radiation | kg U235 eq | II | Factor 2 |
| Photochemical ozone formation | kg NMVOC eq | II | Factor 2 |
| Acidification | mol H ⁺ eq | II | Factor 2 |
| Terrestrial eutrophication | mol N eq | II | +/-33% |
| Freshwater eutrophication | kg P eq | II | Factor 2 |
| Marine eutrophication | kg N eq | II | +/-33% |
| Freshwater ecotoxicity | CTUe | III (interim) | Factor 5 |
| Mineral & metal resource depletion | kg Sb eq | III | Factor 5 |
| Non-renewable energy resource depletion | MJ | III | Factor 2 |
| Land use | points | III | +/-33% |
| Water scarcity footprint | m ³ water deprived eq | III | Factor 2 |

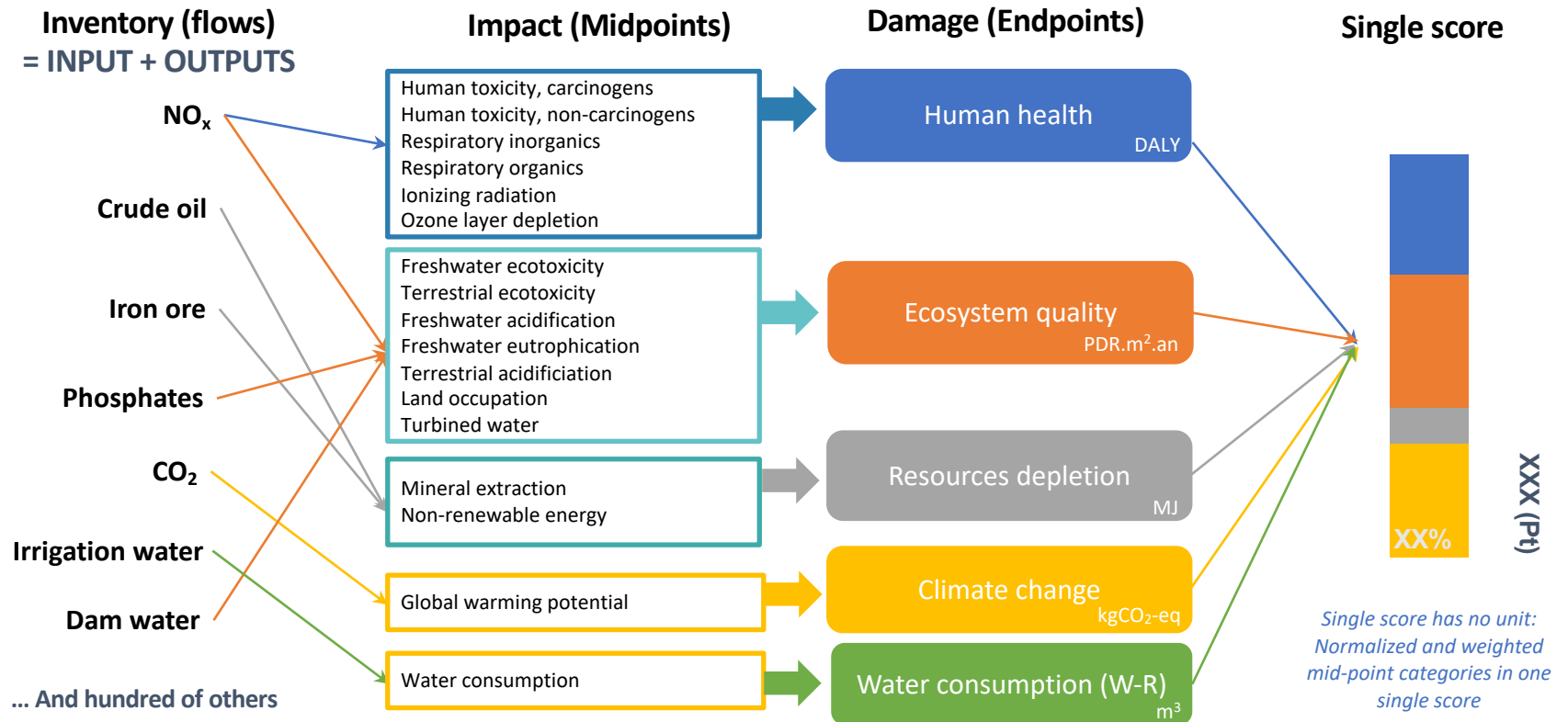
IMPACT 2002 + (IN FRENCH)

Méthodologie Quantis mondialement reconnue



IMPACT ASSESSMENT

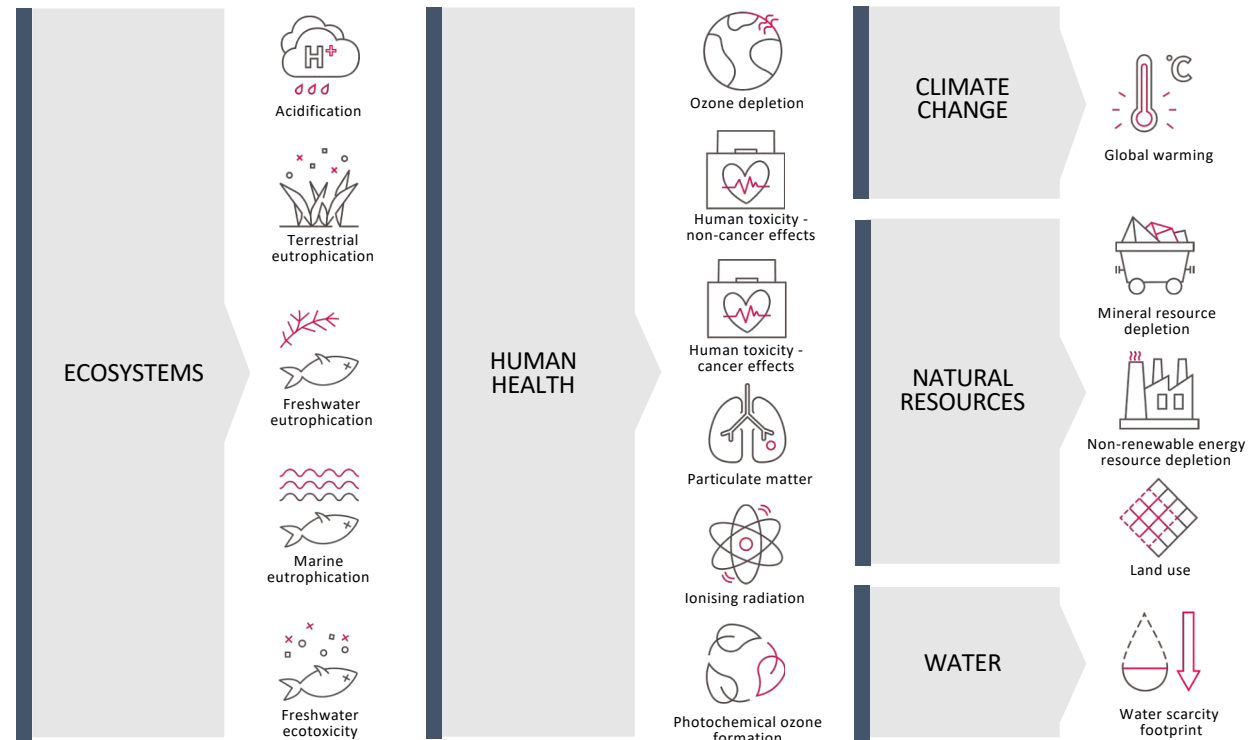
A LARGE PANEL OF INDICATORS (IMPACT 2002+)



IMPACT ASSESSMENT, ENVIRONMENTAL FOOTPRINT (EF) METHOD

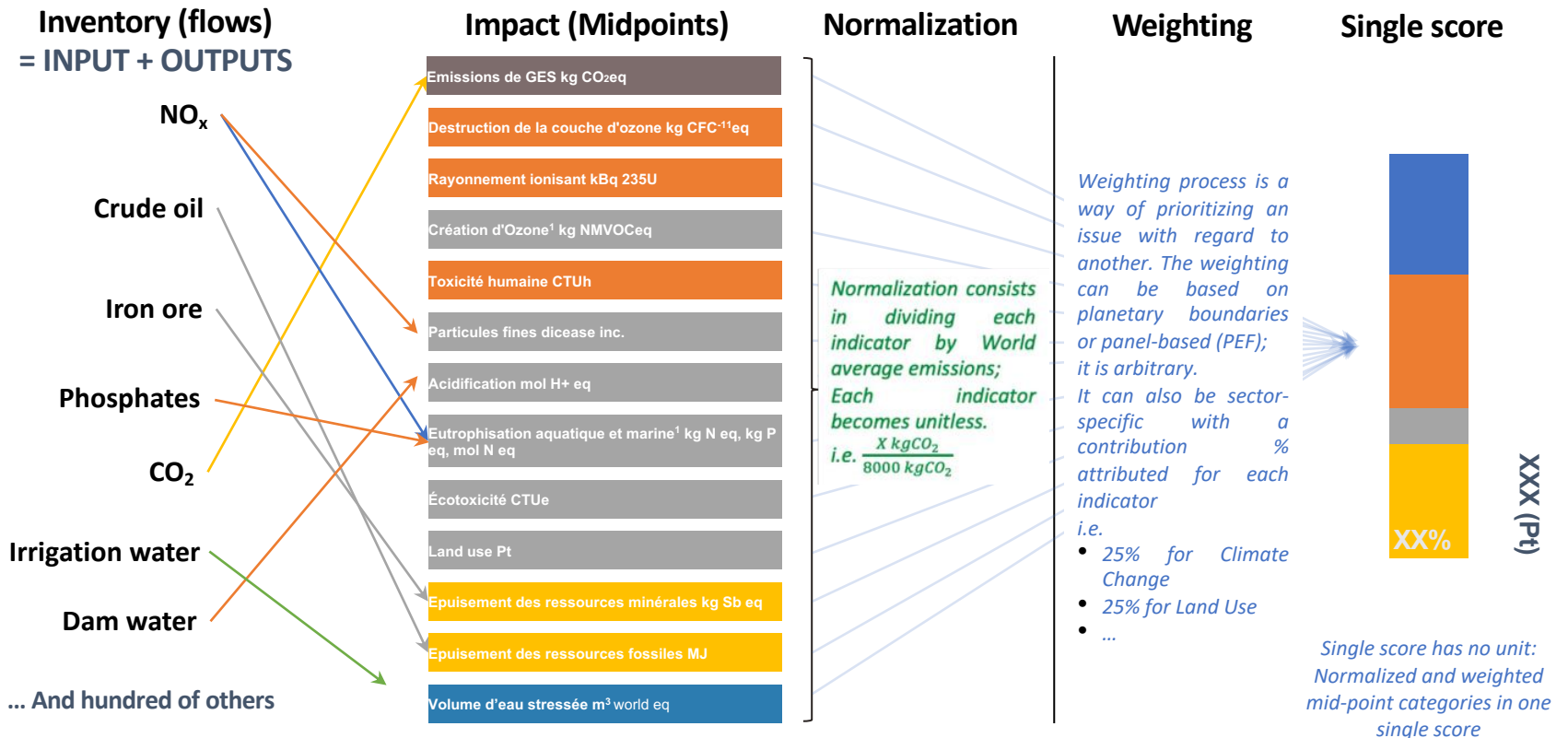
Choice of LCIA method depends on

- Type of indicator desired; mid-point, end-point, single score...
- Single score helps to see if a big contributor is missing
- Maturity of the client
- Subject of the project; characterization factors of an indicator.
- EF3.0 LCIA method is recommended if the sector of interest is covered by the methodology



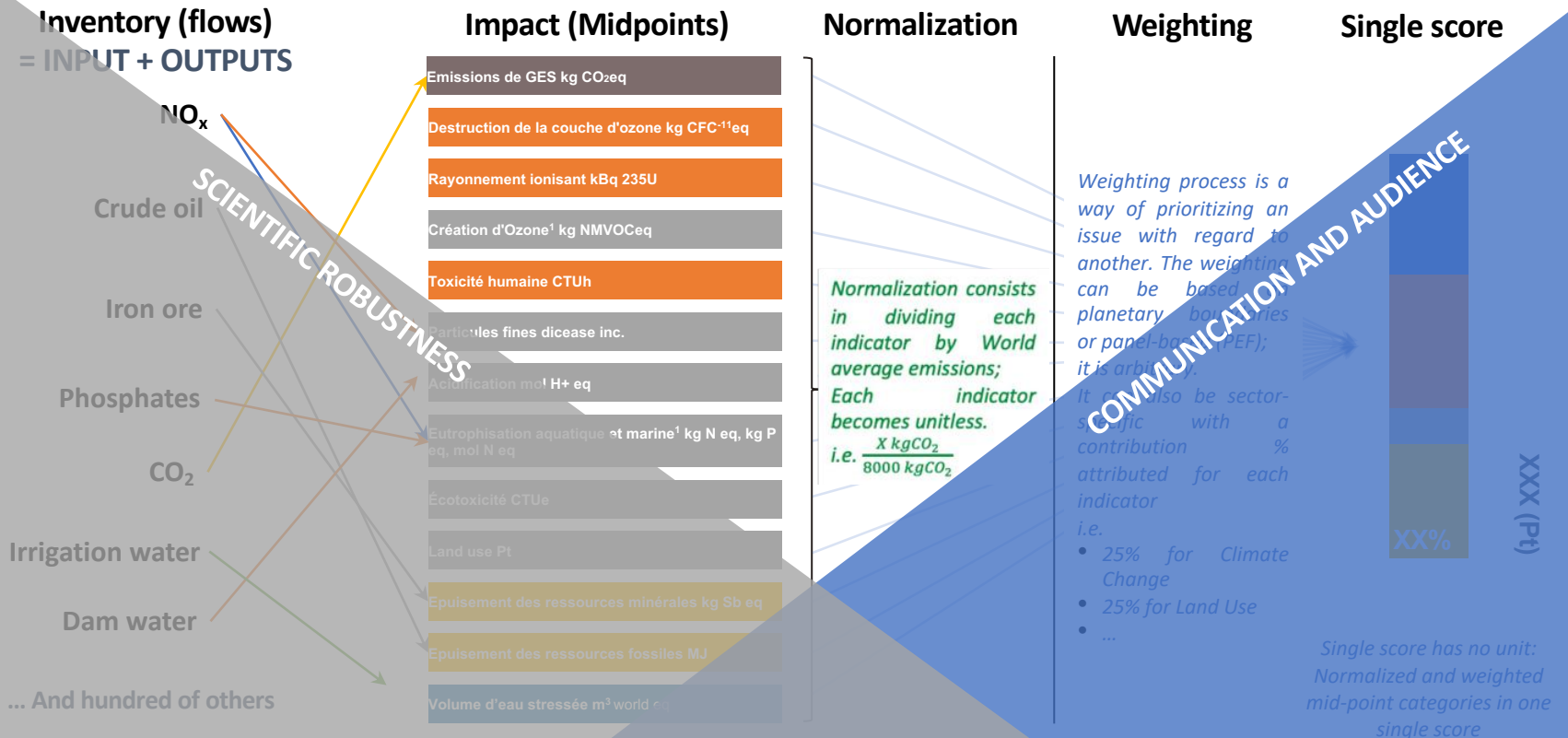
IMPACT ASSESSMENT

A LARGE PANEL OF INDICATORS (EF 3.0)



IMPACT ASSESSMENT

A LARGE PANEL OF INDICATORS (EF 3.0)



**Bio-based copolymers for membrane
end products for gas separations**

Thank you for your attention

Bio-based copolymers for membrane end products for gas separations



This project has received funding from the Bio Based Industries Joint Undertaking (JU) under the European Union's Horizon 2020 research and innovation programme, under grant agreement No 887075.

The JU receives support from the European Union's Horizon 2020 research and innovation program and the Bio Based Industries Consortium

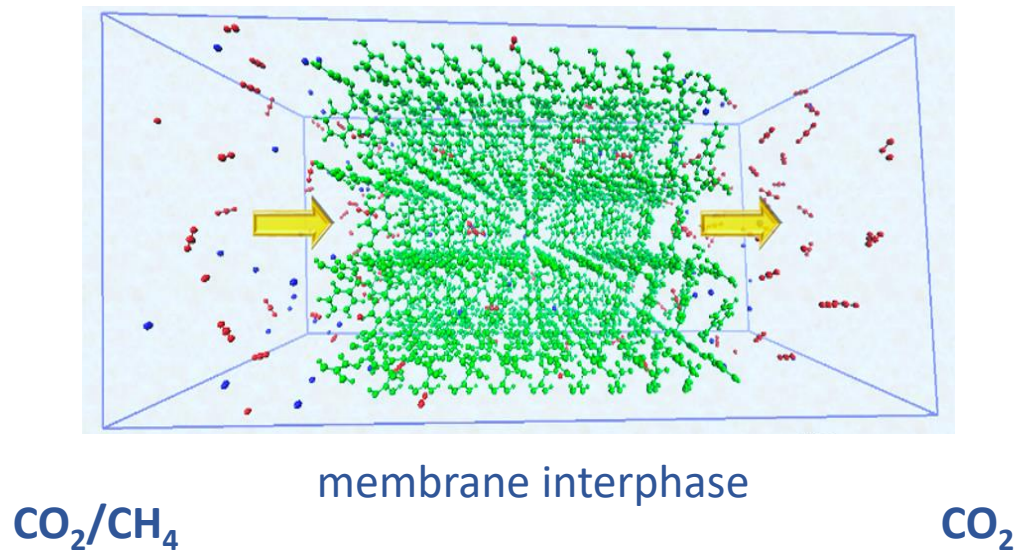
Membrane Process Design

Contacts: Fausto Gallucci

f.gallucci@tue.nl

Membrane Gas Separation

Representation of a selective separation process



- A membrane allows selective permeation of one or more of the components present in a mixture.
- Feed enters on one side of the membrane, some of it permeates through the membrane and so the stream leaving from the other side of the membrane is called permeate and the remaining unseparated mixture on the feed side is called retentate.
- The goal of a model for a membrane unit for gas separation is to predict the flow rate and composition of retentate and permeate streams, for a given feed stream.

Gas Separation in dense polymeric membranes

Solution-Diffusion mechanism

Permeability

Selectivity

$$P = D \cdot S$$

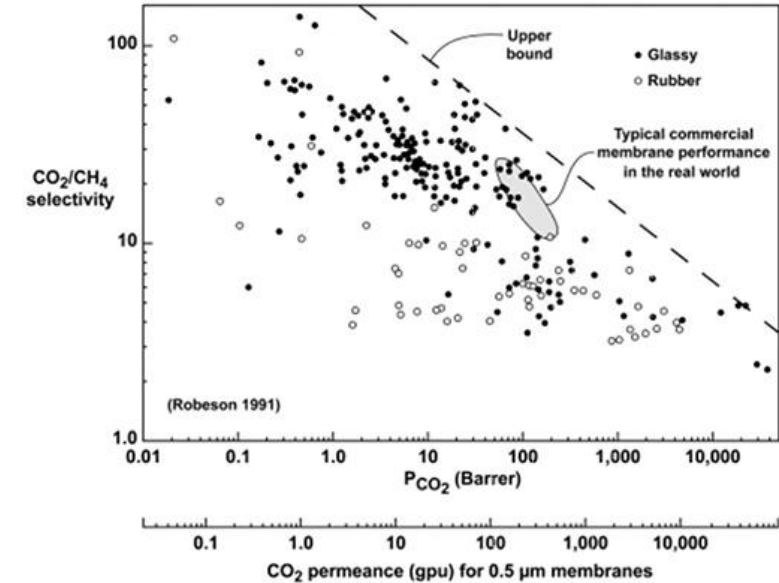
$$\alpha_{ij} = \frac{P_i}{P_j} = \alpha_{ij}^D \cdot \alpha_{ij}^S$$

diffusion selectivity

sorption selectivity

- Permeability can be deconvoluted into the product of a **kinetic factor** and a **thermodynamic factor**, namely diffusion and sorption coefficients

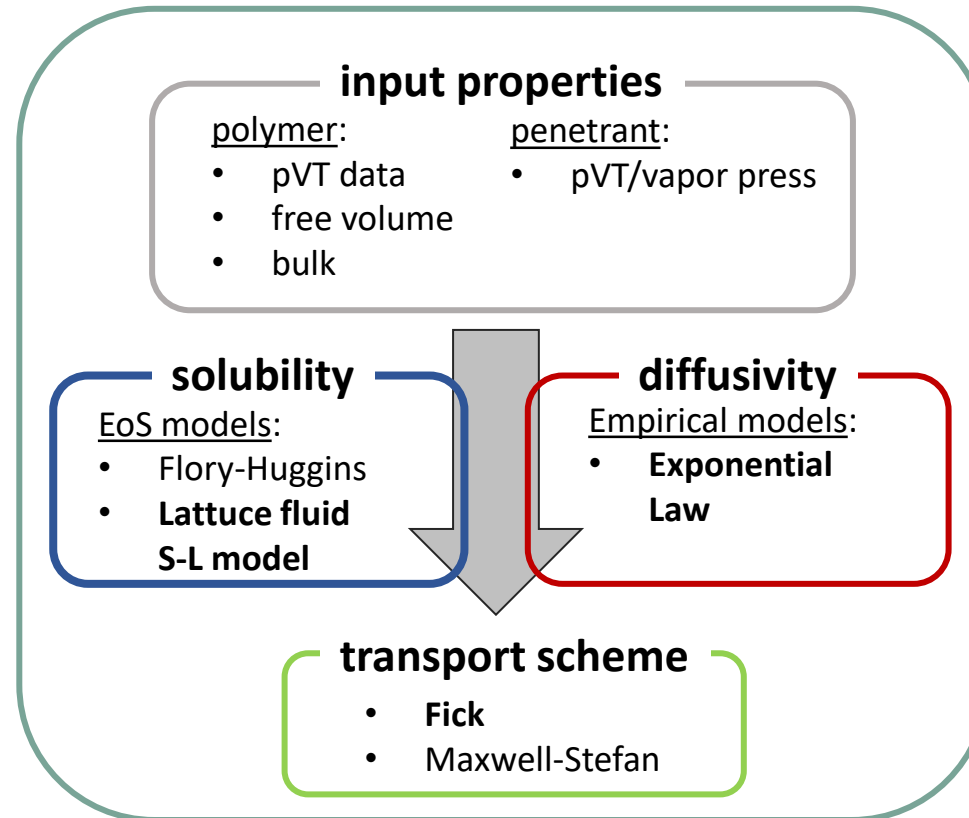
CO₂/CH₄ Robeson Plot



- Robeson Plot reports the performance of different polymeric membranes for a certain gas separation
- This graph actually tells you that you cannot exceed a certain value of selectivity at a fixed permeability and viceversa, **which represents a tradeoff for the separation performance.**

Gas Separation in dense polymeric membranes

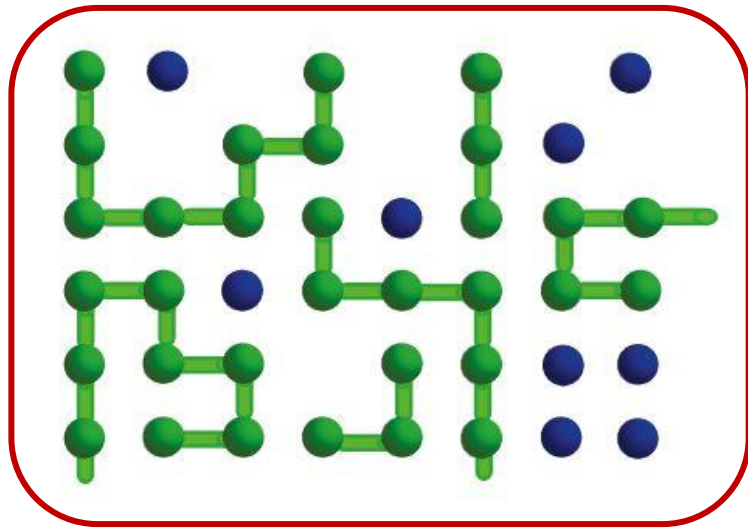
Working Flow Chart






Model for multicomponent Solubility

Lattice Fluid (Sanchez-Lacombe) Equation of State

2-D Lattice representation



 polymer monomer
  gas molecule
  free volume



In the *Sanchez Lacombe* framework:

- polymer macromolecules are considered as a set of beads on a lattice
- polymer chains are mixed randomly with penetrant molecules
- The SL EoS considers also configurations with empty sites in the lattice, so that **free volume exists** in the polymer–penetrant mixture



thus **volume changes** upon mixing penetrant and polymer molecules are allowed.

Model for multicomponent Solubility

Lattice Fluid (Sanchez-Lacombe) Equation of State

Phase equilibrium condition between the gas phase and the polymer membrane phase:

$$\mu^{(S)}(T, p, \Omega) = \mu^{(G)}(T, p, y)$$

- $\mu^{(G)}$ and $\mu^{(S)}$ are the chemical potential values of the fluid species i in the gaseous and in the solid phase, respectively.
- The **gas phase** is characterized by **T , p** , and **composition y**
- The **polymer/penetrants phase** is characterized by **T , p** , and **composition Ω**
- The model contains energetic **binary interaction parameter k_{ij}**
- The chemical potential of the gas phase ($\mu^G(T, p, y)$) can be calculated either with the same EoS or with more convenient ones depending on the operational conditions (**T , p**) taken into account

Binary mixture case

$$D_{ip} = D_{ip}^{\infty} \exp(\gamma_i \phi)$$

Ternary mixture case

$$D_{ip} = D_{ip}^{\infty} \exp[\gamma_i (\phi_i + \xi_{ij} \phi_j)]$$

- D_{ip}^{∞} penetrant diffusivity in the limit of infinite dilution (i.e. at moderate pressures, in which the polymer structure is unaltered)
- γ_i empirical plasticization constant
- ϕ_i the volume fraction of component i
- ξ_{ij} is a measure of the influence of j on the diffusion coefficient of component i in the polymer

Observations:

- ξ can vary between 0 and 1, where:
 - i. $\xi_{ij} = 0$ means the diffusion coefficient of component i in the polymer is not affected by component j
 - ii. $\xi_{ij} = 1$ the diffusion coefficient of penetrants in the polymer is affected in the same way.

To correctly predict the permeability, the fit of binary permeation data (gas₁-gas₂-polymer) is needed to evaluate the empirical value of parameters such as the plasticization constant.

Model for multicomponent Diffusivity

The simplest description of gas diffusion through a dense membrane is based on the Fick's Law, assuming the diffusion coefficient D as constant.

$$J_i = -D \frac{\partial C}{\partial x}$$

$$J_i = D_i \frac{C_{i,0} - C_{i,z}}{z}$$

where:

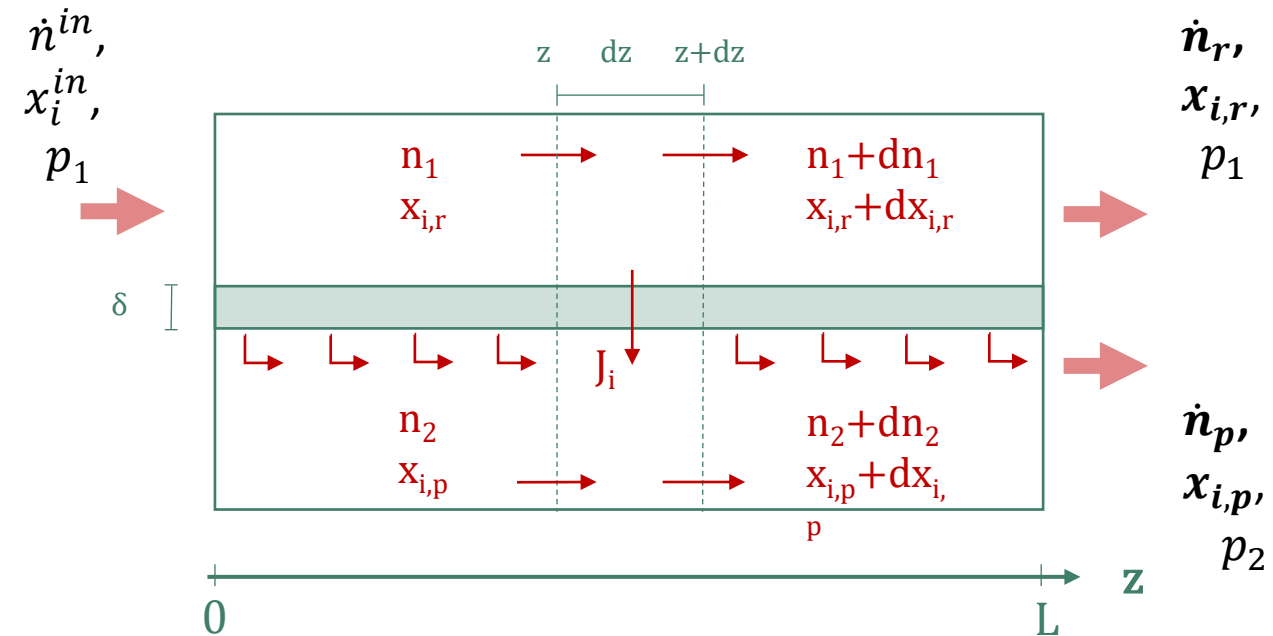
- D_i is the diffusion coefficient of the component i ,
- $C_{i,0}$ concentration of component i at the retentate side
- $C_{i,z}$ concentration of component i at the permeate side

Then, considering that the permeability is the product of solubility and diffusivity we obtain:

$$J_i = \frac{P_i}{z} (p'x_i - p''y_i)$$

This way, permeability P_i can be integrated into a mass transfer scheme for multicomponent permeation which is here below outlined.

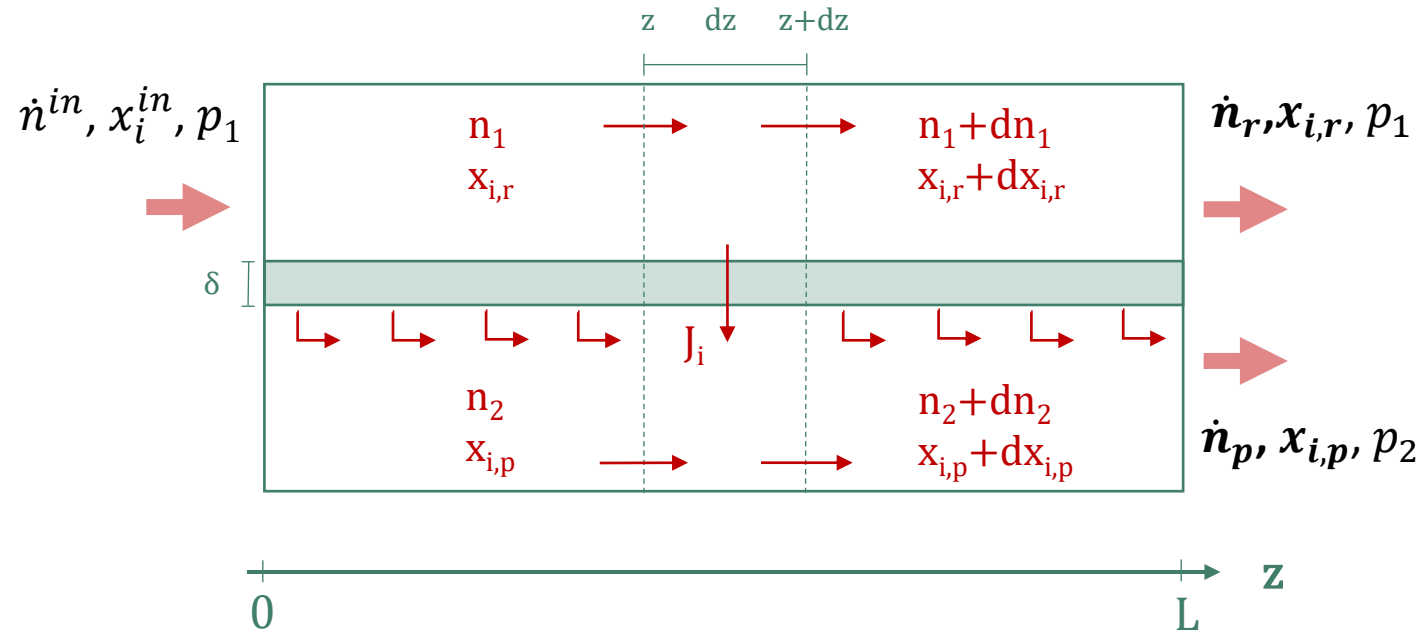
- A membrane allows selective permeation of one or more of the components present in a mixture.
- Feed enters on one side of the membrane, some of it permeates through the membrane and so the stream leaving from the other side of the membrane is called permeate and the remaining unseparated mixture on the feed side is called retentate.
- The goal of the model for membrane unit for gas separation is to predict the flow rate and composition of retentate and permeate streams, for a given feed stream.



$$\begin{cases} \frac{dn_1}{dz} = - \sum_{i=1}^n J_i(p_1, p_2, x_{i,r}, x_{i,p}) \cdot SN_f \\ \frac{dx_{i,r}}{dz} = \frac{x_i \sum_{i=1}^n J_i(p_1, p_2, x_{i,r}, x_{i,p}) - J_i(p_1, p_2, x_{i,r}, x_{i,p})}{n_1} \cdot SN_f \\ \frac{dn_2}{dz} = + \sum_{i=1}^n J_i(p_1, p_2, x_{i,r}, x_{i,p}) \cdot SN_f \\ \frac{dx_{i,p}}{dz} = \frac{J_i(p_1, p_2, x_{i,r}, x_{i,p}) - y_i \sum_{i=1}^n J_i(p_1, p_2, x_{i,r}, x_{i,p})}{n_2} \cdot SN_f \end{cases}$$

where:

- \dot{n}^{in} feed entering the unit
- $\dot{n}_{r/p}$ retentate/permeate leaving the unit
- $x_{i,r/p}$ upstream/downstream molar fraction of component i
- J_i local transmembrane molar flux for species i
- p_1 upstream pressure
- p_2 downstream pressure
- S geometrical factor (e.g. πD – hollow fibers)
- N_f number of fibers



Initial conditions ($z=0$):

- $n_1 = \dot{n}^{in}$
- $x_i = x_i^{in}$
- $n_2 = 0$

Model description

The system includes $2 \cdot n + 2$ coupled differential equations (where n represents the number of species in the feed gas mixture).

The feed conditions are assumed to be given: $n_f, x_{i,f}, p_f$, as well as the geometrical features of the membrane providing for the boundary conditions for the differential equations and the interval of integration.

- **Finite material balance** between $z = 0$ and $z = L$

$$n_f = n_r + n_p$$

$$n_f \cdot x_{i,f} = n_r \cdot x_{i,r} + n_p \cdot x_{i,p}, \quad \forall i = 1, \dots, N_c$$

- **Differential material balance**, retentate side

$$dq = -J S dz$$

$$d(qx_{i,r}) = -J_i S dz$$

- **Constitutive Flux Equations**

$$J_i = -\frac{P_i}{\delta} \cdot (p_1 \cdot x_{i,r} - p_2 \cdot x_{i,p}), \quad \forall i = 1, \dots, N_c$$

- **Composition Equations**

$$\sum_{i=1}^{N_c} x_{i,f} = \sum_{i=1}^{N_c} x_{i,r} = \sum_{i=1}^{N_c} x_{i,p} = 1$$

Dimensionless parameters

Dimensionless parameters are mainly used to lighten the computational effort as the model will be used for process design and optimization purposes.

Introducing:

- $\mathbf{r_p} = \frac{p_2}{p_1}$
- $\gamma_i = \frac{P_i}{P_1} = \frac{\Pi_i}{\Pi_1}$
- $\bar{n}_1 = \frac{n_1}{n_f}$
- $\bar{A} = \frac{AP_1 p_1}{\delta n_f}$
- $\zeta = \frac{Sdz}{SL}$



$$\frac{1}{\frac{P_1}{\delta}} \cdot \frac{n_f}{n_f} \cdot \frac{1}{p_1} \cdot \frac{d(n_1)}{dA} = - \sum_i^{N_c} \frac{P_i}{\delta} \cdot (p_1 \cdot x_{i,r} - p_2 \cdot x_{i,p}) \cdot \frac{1}{p_1} \cdot \frac{\delta}{P_1}$$

$$1. \quad \frac{d\left(\frac{n_1}{n_f}\right)}{d\left(\frac{AP_1 p_1}{n_f}\right)} = \frac{d\bar{n}_1}{d\bar{A}} = \frac{d\bar{n}_1}{d\zeta \cdot \bar{A}}$$

$$2. \quad - \sum_i^{N_c} \frac{P_i}{\delta} \cdot \frac{\delta}{P_1} \cdot \left(\frac{p_1}{p_1} \cdot x_{i,r} - \frac{p_2}{p_1} \cdot x_{i,p} \right) = - \sum_i^{N_c} \gamma_i \cdot (x_{i,r} - \mathbf{r_p} \cdot x_{i,p})$$

where:

$$\Pi_1 = \frac{P_1}{\delta}$$

$$A = SN_f L$$

$$\frac{d\bar{n}_1}{d\zeta} = - \sum_i^{N_c} \gamma_i \cdot (x_{i,r} - \mathbf{r_p} \cdot x_{i,p}) \cdot \bar{A}$$

Permeate Pressure Loss – Viscosity calculations

$$dp = \frac{-256RT\mu q_2}{\pi D_i^4 Np}$$



Perry's Chemical

$$\mu_i = \frac{C_1 \cdot T^{C_2}}{1 + \frac{C_3}{T} + \frac{C_4}{T^2}}$$

Wilke (1950)

$$\mu_{mix} = \sum_{i=1}^n \frac{\mu_i}{1 + \frac{1}{x_i} \sum_{j=1, j \neq i}^n x_j \phi_{ij}}$$

$$\phi_{ij} = \sum_{i=1}^n \frac{\mu_i}{1 + \frac{1}{x_i} \sum_{j=1, j \neq i}^n x_j \phi_{ij}}$$

| Components | CO ₂ | O ₂ | CO | H ₂ | CH ₄ | N ₂ | C ₂ H ₆ | $\mu \times 10^6$ | |
|------------|-----------------|----------------|------|----------------|-----------------|----------------|-------------------------------|--|-------------|
| | | | | | | | | $\frac{g}{(cm \cdot s)}$ μ_{calc} | μ_{exp} |
| | 6,2 | 10,7 | | | | 83,1 | | 175 | 179,3 |
| x_i (%) | 10,6 | | 29,8 | 3,9 | 0,3 | 55,4 | | 171,3 | 174,3 |
| | 2,5 | 0,8 | 14,9 | 53,0 | 18,1 | 9,1 | 1,6 | 126,05 | 135,5 |

Wilke, A Viscosity Equation for Gas Mixtures J. Chem. Phys. **18**, 517 (1950); <https://doi.org/10.1063/1.1747673>

Steps of design of a membrane system

Process design is essential to provide an energy-efficient membrane technology for natural gas sweetening.

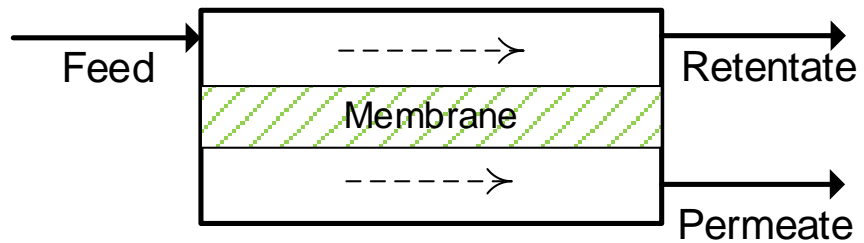
1. Consider feed source and feed quality
2. Consider product flow and required product quality
3. Select the flow configuration
4. Select membrane element type
5. Select the design flux according to the feed source
6. Select number of stages
7. Select the staging ratio
8. Analyze and optimize the membrane system

Flow arrangements in membrane modules

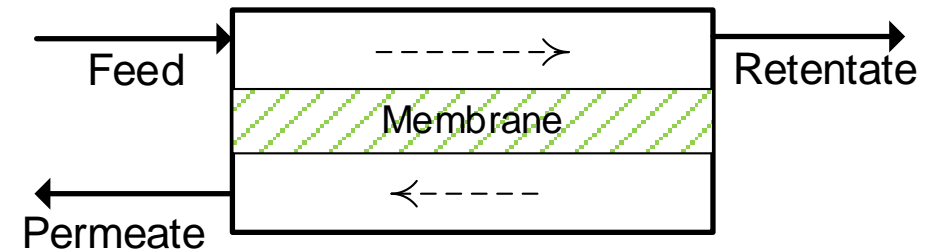
- The performance of a membrane is influenced by the way in which the permeate and retentate flow in the membrane.
- Several flow arrangements, such as perfect mixing, co-current, counter-current, and cross flow are possible in the design of a membrane module.
- Parametric studies of these flow patterns have shown that given equal operating conditions, the counter-current flow pattern is most efficient (meaning less membrane area is needed), followed by the cross flow pattern.

Flow arrangements in membrane modules

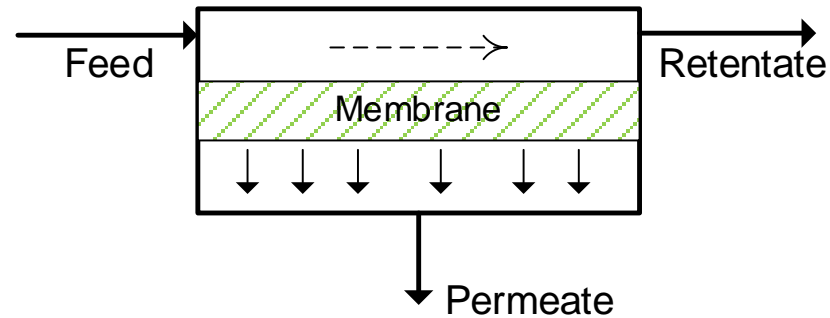
Co-current Flow



Counter-current Flow

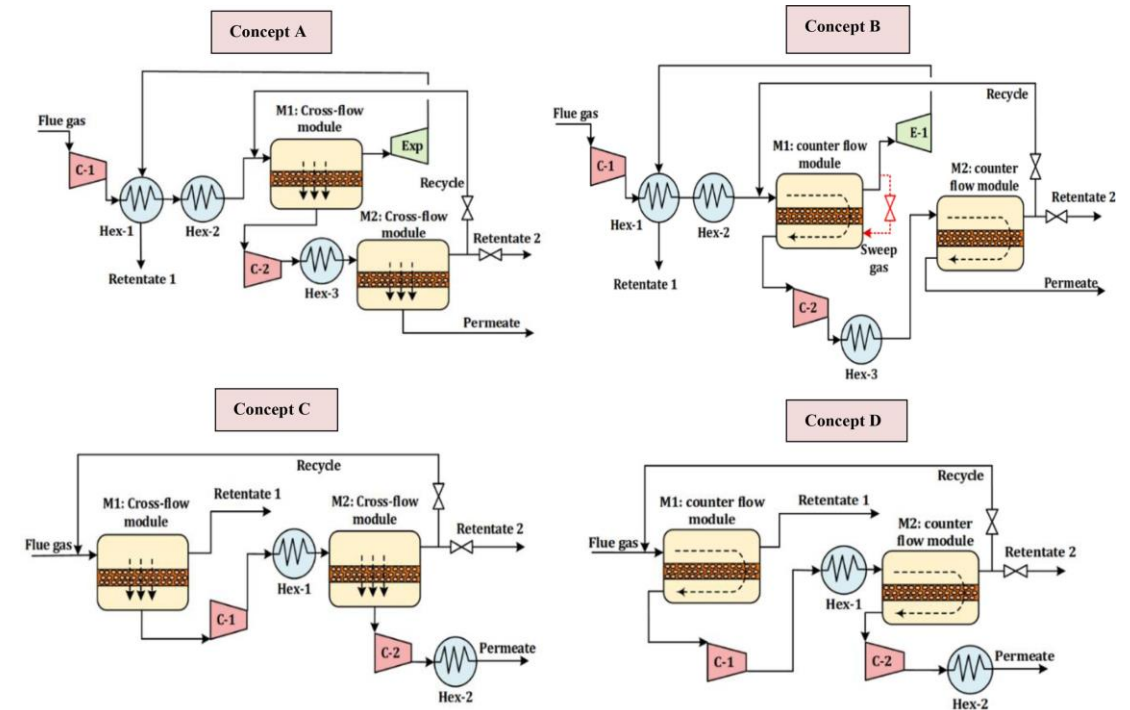
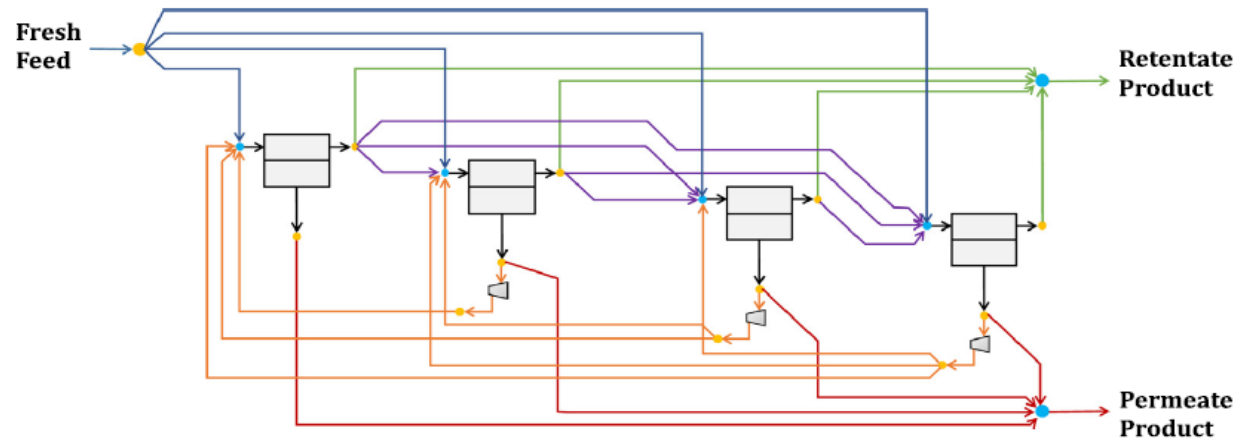


Cross Flow



Multi-stage membrane module

- ❖ Single stage processes cannot provide both, high product gas purity and high recovery at the same time.
- ❖ To improve purity and recovery, membrane stages are cascaded with recycle.
- ❖ The selection of the best configuration is highly related to feed quality, separation objectives and market values.



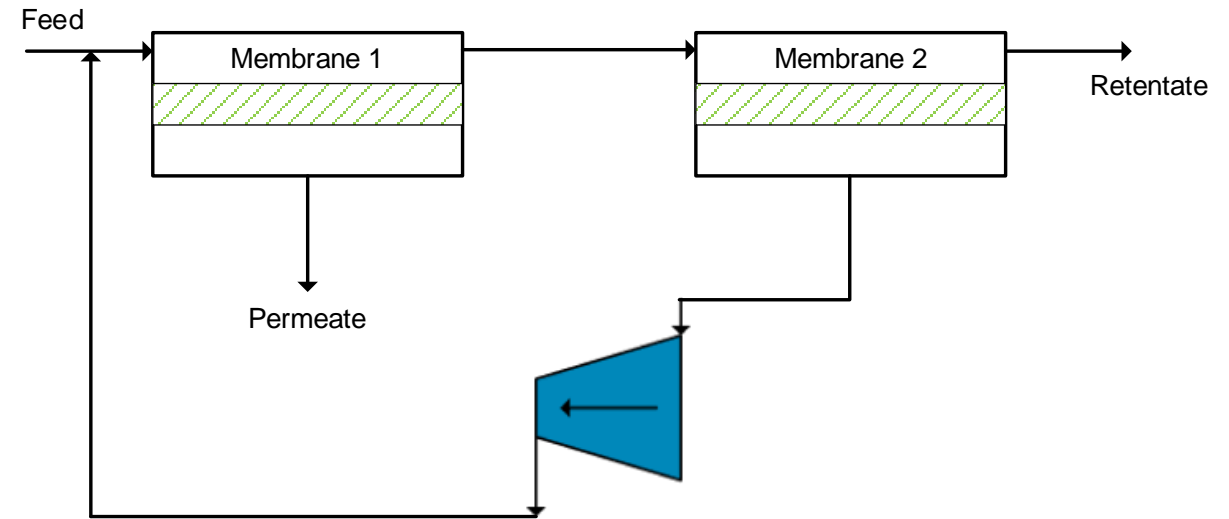
Two-stage cascade for purer retentate

The raw gas is compressed and fed to the first membrane stage.

The first stage performs a bulk separation of for example CO_2 and CH_4

The retentate of the first stage is fed to a second stage in which the final product purity is obtained.

The permeate of the second stage is recycled and mixed with the raw gas stream to enhance the CH_4 recovery.



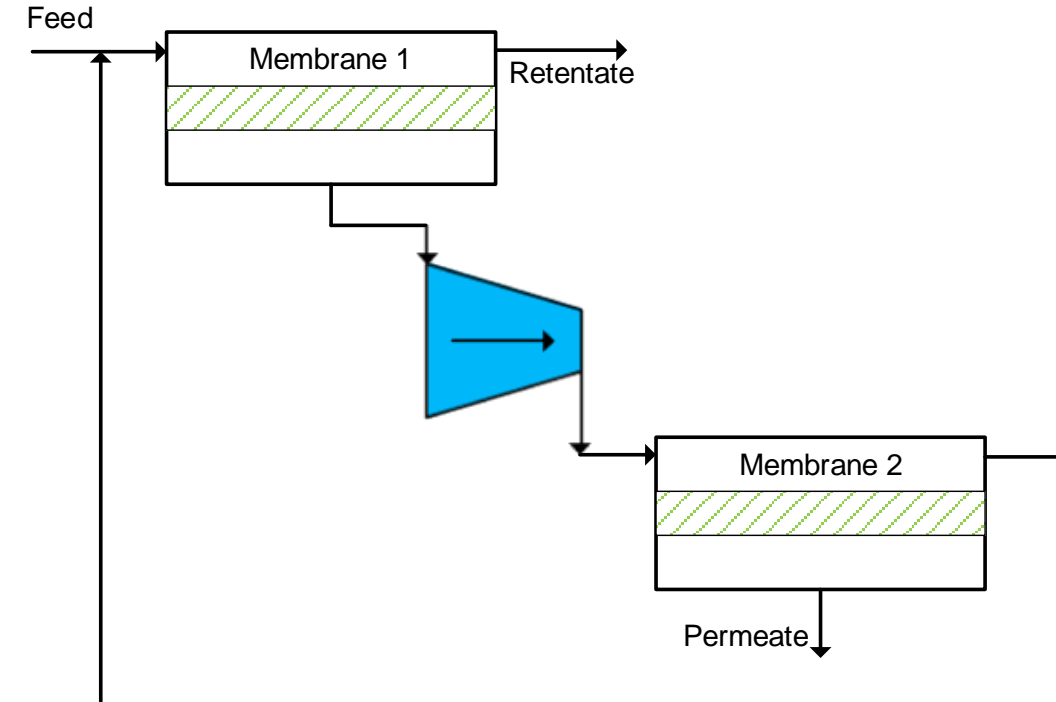
Two-stage cascade for purer permeate

In this configuration, the permeate stream of the first membrane unit, after passing through a compressor and a cooler, enters the second stage

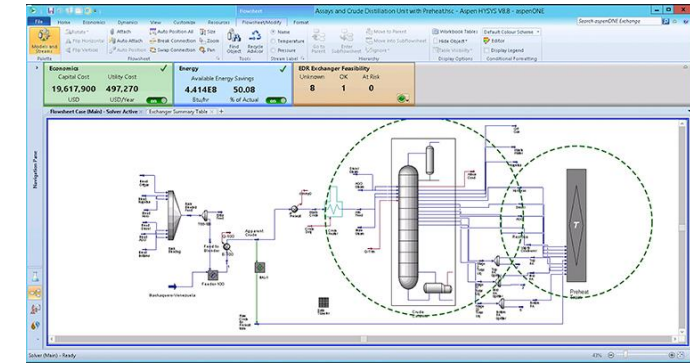
In this design, the permeate stream of the second membrane unit is considered as the final product.

The product purity and recovery of this configuration are higher than those of the previous configuration.

The combination of similar membranes or/and different membranes in the two-stage process results in good separation performance as product purity reaches the desired values.



Process simulators have been proven to be successful in modeling, simulate, and optimize various industrial processes.



| | |
|-----------------------------------|--|
| Aspen Plus Aspen Hysys | Can be used for batch and continuous processes for design, troubleshooting in regular operations, monitoring the plant performance through online, and real-time optimization. |
| gPROMS | An advanced equation oriented process modeling software, which can be used to model, analyze, and optimize in an easy-to-use process flow-sheeting environment. |
| PRO/II | A steady-state simulator which has an in-built membrane unit operation to simulate crossflow symmetric membranes for gas separations. |
| ProMax | A multifaceted process simulation software which it is designed to optimize gas processing, refining, and chemical facilities. |
| SuperPro Designer | A flowsheet driven simulator for batch, continuous as well as combination processes, that perform material and energy balances, equipment sizing, and costing. |
| Aspen Custom Modeler | Provides the capability to create unique process and equipment simulation models by describing the equations which can be exported into Aspen Plus/Hysys. |

Process simulators contain:

1. mathematical models for many common process units (for example, reactor, distillation column, heat exchanger, pump and compressor)
2. different numerical methods for solving process models
3. property database for numerous chemicals
4. thermodynamic models for predicting properties of chemical mixtures.

To design chemical processes, relevant components and thermodynamic models from the database are chosen, and process units in the simulator are put together according to the process flow diagram.

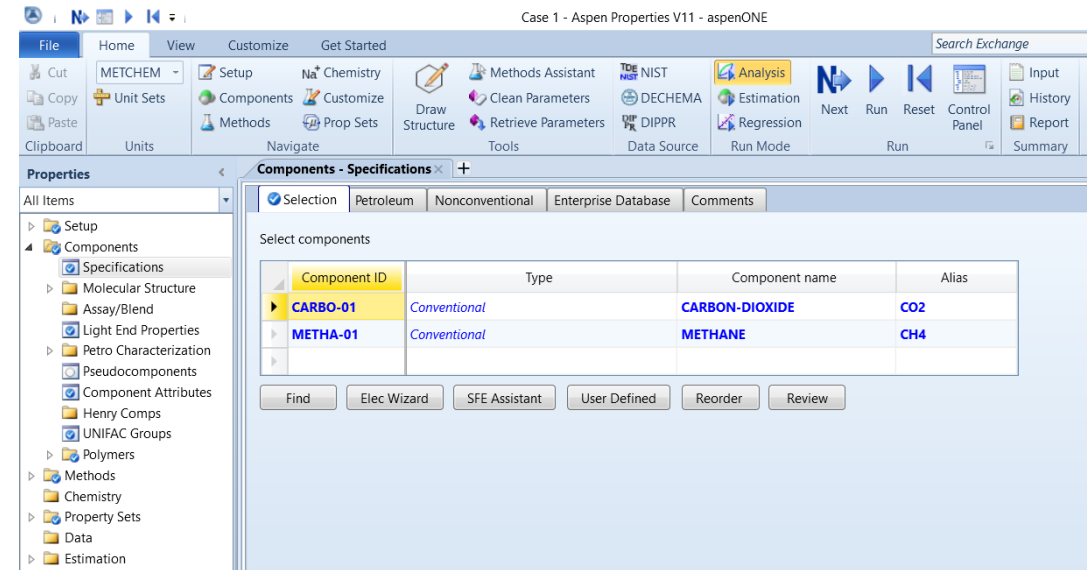
The user needs to provide some design/operating conditions of each process unit as per its degrees of freedom.

Some process models like membrane separation are not available in Aspen Plus.

- The model for membrane gas separation can be implemented and solved in ACM, which can be added to Aspen Plus.
- To implement the membrane model in ACM, all chemicals are defined from the component list in the Aspen Properties User Interface program.
- Fixed variables or inputs (feed temperature, pressure, composition and membrane area) are defined, and the process parameters (for example, permeance) and variables are declared.
- In ACM, all the model equations are solved simultaneously, and so degrees of freedom are important.
- The membrane model in ACM can now be used with other process models in ACM itself.

Implementation of Membrane model in ACM

- Open Aspen Properties User Interface program
- Include the required chemical components (New – Chemical Processes – Chemicals with Metric Units – Components – Specifications – Selection).
- Run the simulation (using F5 key)
- Save it as Aspen Properties Backup file.



Implementation of Membrane model in ACM

Open ACM file and click Configure Properties to open Physical Properties Configuration window, and import the Aspen Properties Backup file.

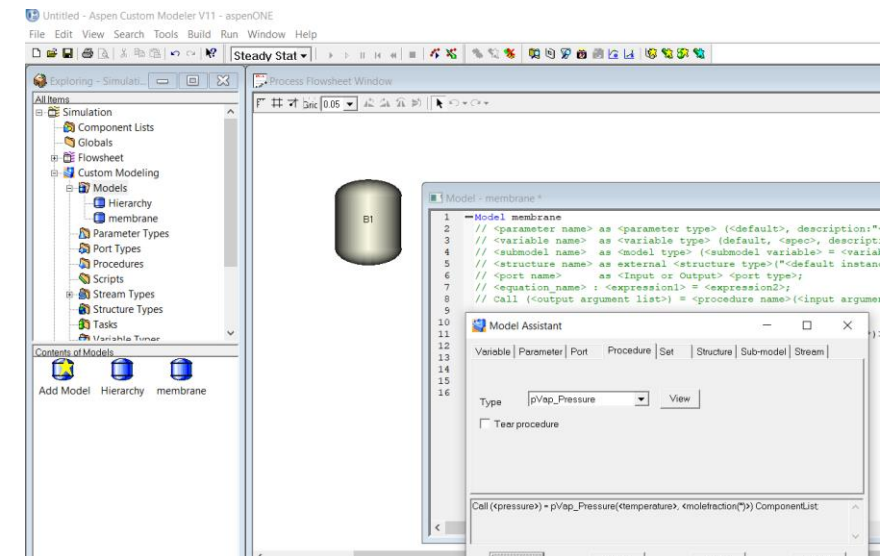
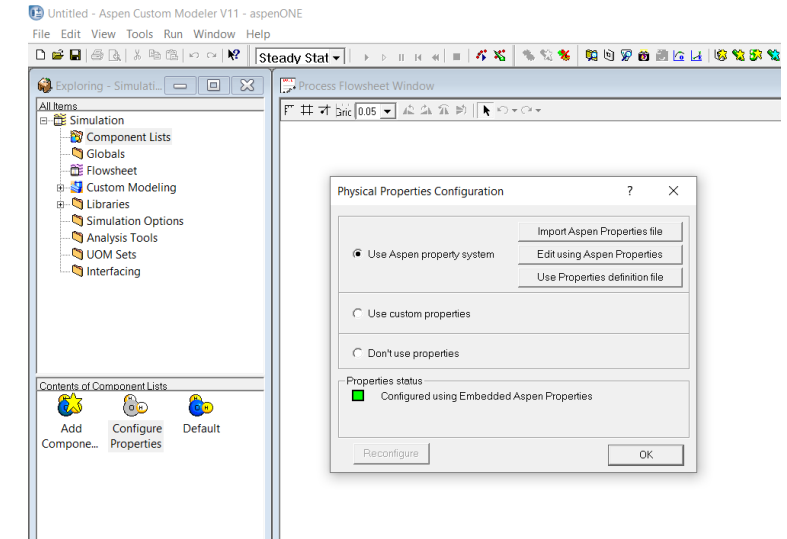
Click Default to select the components from the available components.
Add the new model with a suitable name.

Use Model Assistant to get the syntax of different variables for ACM code.

The model form provides all variables in the membrane model, which can be seen using Ctrl+D.

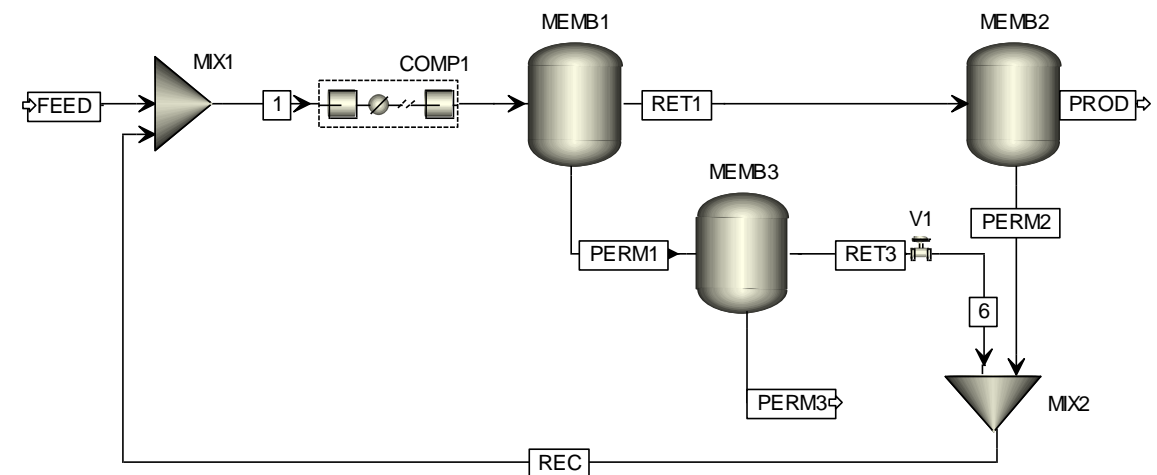
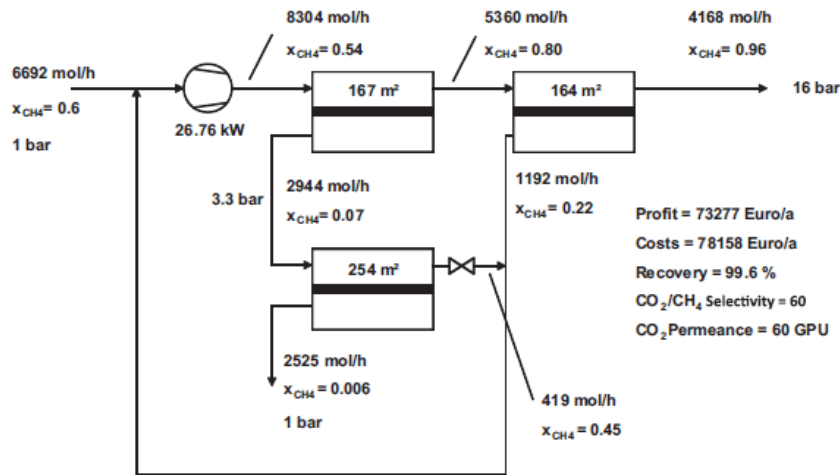
This membrane model in ACM can now be used with other process models in ACM itself

To use the model in Aspen Plus, the membrane model in ACM has to be saved as a *.msi file using the export wizard.



Membrane design of biogas upgrading process

- ✓ The developed mass transfer model for the gas separation membrane process is coded by MATLAB.
- ✓ The second step is to integrate the model with Aspen Plus using ACM.
- ✓ The mass and energy balances are written in the model created in the ACM.
- ✓ The model has one port for feed stream and two ports as permeate and retentate streams.
- ✓ By entering the pressure, temperature, concentration, and flow rate of feed, the flux and concentration of components are calculated.
- ✓ Various configurations can be proposed for the membrane process.
- ✓ CO₂ will permeate faster through the membrane so that the permeate is enriched in CO₂, and CH₄ is enriched on the retentate side.



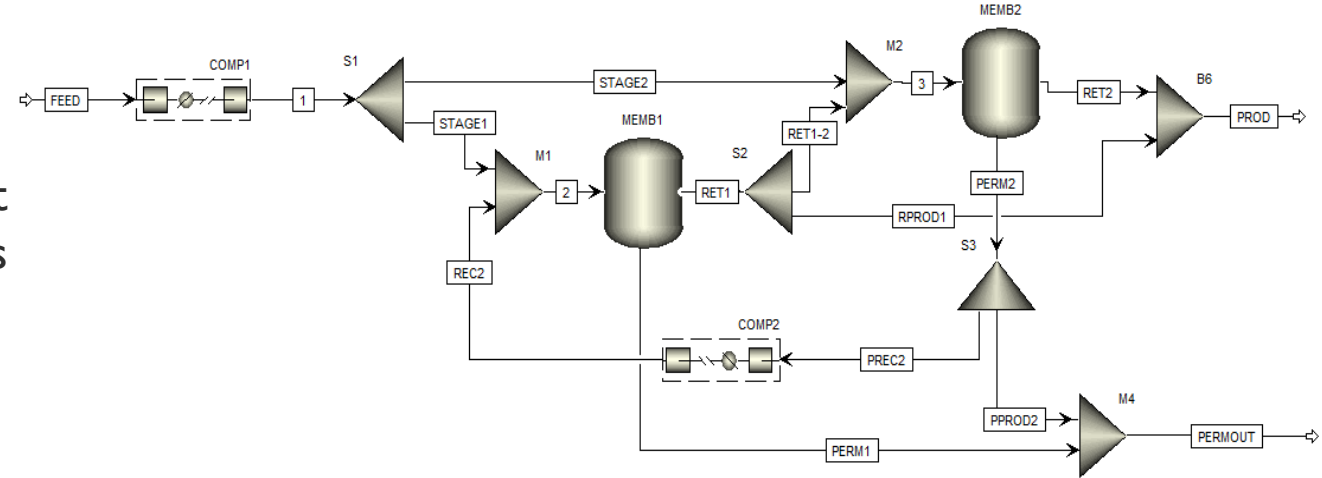
Membrane design of biogas upgrading process

Commonly gas permeation processes include multiple membrane stages to achieve high gas purities and recoveries simultaneously.

By applying a structural optimization approach, the most profitable process configuration including stage numbers can be determined.

In general, feed gas conditions, product gas requirements and economic parameters such product gas pressure and energy costs considerably determine the optimal process configuration.

To find the best configuration of the multi-stage gas separation membrane process and to compare with the single-stage process, the cost analysis is performed, and various simulated cases are evaluated.



- ❑ The optimization function for any chemical process consists mainly of capital (CAPEX) and plant operating (OPEX) expenses.
- ❑ The operational cost is a sum of utilities, labor, maintenance, depreciation of equipment and eventual replacement costs.
- ❑ In the case of membrane gas separation plant the maintenance and labor costs are very low comparable to the power bill. Therefore, these costs can either be ignored or simply added as a fraction of the capital cost.
- ❑ Capital cost is mainly the installation cost of vacuum pumps, compressors, piping system and membrane modules.
- ❑ The application of a compressor and vacuum pump leads to electrical energy consumption, which increases the energy penalty of the existing power plants.
- ❑ The feasibility study of polymer membranes shows that the energy requirement for the compressors is the **dominant cost factor** in the recovery process.

To optimize the process, it is more appropriate to determine the **economic optimum** rather than the energetic optimum, since the membrane-based biogas upgrading process has to compete economically with well established gas separation techniques.

The **GPC** must be a minimum subject to the operating conditions, material and energy balances, and individual permeator mathematical model.

Economics parameters for gas processing cost

| | |
|---|---|
| Total plant investment (TPI): | $TPI = TFI + SC$ |
| Membrane module cost (MC) | $\$/ft^3$ |
| Installed compressor cost (CC) | $\$8650 * (W_{cp}/\eta_{cp})^{0.82}$ |
| Fixed cost (FC) | $MC + CC$ |
| Base plant cost (BPC) | $1.12 * FC$ |
| Project contingency (PC) | $0.20 * BPC$ |
| Total facilities investment (TFI) | $BPC + PC$ |
| Start up cost (SC) | $0.10 * VOM$ |
| Annual variable operating and maintenance cost (VOM): | $VOM = CMC + LTI + DL + LOC + MRC + UC$ |
| Contract & material maintenance cost (CMC) | $0.05 * TFI$ |
| Local taxes and insurance (LTI) | $0.015 * TFI$ |
| Direct labor cost (DL) | $\$15/h$ |
| Labor overhead cost (LOC) | $1.15 * DL$ |
| Membrane replacement costs (MRC) | $\$3/ft^2$ of membrane |
| Utility cost (UC) | $\$0.07/kwh$ |
| Annual cost of CH ₄ lost in permeate (CH ₄ LS): | $CH_4LS = NGLS * NHV * NWP$ |
| Annual natural gas lost (NGLS) | $NGLS = 365 * OSF * L_f * y_{P(CH_4)} * X_{f(CH_4)}$ |
| Gas processing cost (GPC) | $GPC = (CRC + CH_4LS + VOM) / [365 * OSF * L_f * (1 - SCE) * 1000]$ |
| Annual capital related cost (CRC) | $0.2 * TPI$ |
| Membrane life (t) | 4 years |
| Wellhead price of crude natural gas | $\$2/MMBTU$ |
| Heating value of natural gas | 1066.8 MMBTU/MMSCF |
| On stream factor (OSF) | 96% |
| Compressor efficiency (η_{cp}) | 0.8 |

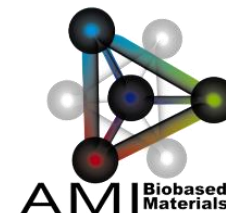
F. Ahmad, Journal of Industrial and Engineering Chemistry 21 (2015)

1. S. Sharma et al. (2016) Mathematical modeling, simulation and optimization for process design. In Chemical Process Retrofitting and Revamping.
2. F. Ahmad et al. (2015) Hollow fiber membrane model for gas separation: Process simulation, experimental validation and module characteristics study, Journal of Industrial and Engineering Chemistry.
3. M. Samei et al. (2022) Separation of nitrogen from methane by multi-stage membrane processes: Modeling, simulation, and cost estimation, Journal of Natural Gas Science and Engineering.
4. M. Scholz et al. (2015) Structural optimization of membrane-based biogas upgrading process, Journal of Membrane Science.
5. R. Kancherla et al. (2021) Modeling and simulation for design and analysis of membrane-based separation processes, Computers & Chemical Engineering.

Bio-based copolymers for membrane end products for gas separations



Maastricht University



This project has received funding from the Bio Based Industries Joint Undertaking (JU) under the European Union's Horizon 2020 research and innovation programme, under grant agreement No 887075.

The JU receives support from the European Union's Horizon 2020 research and innovation program and the Bio Based Industries Consortium

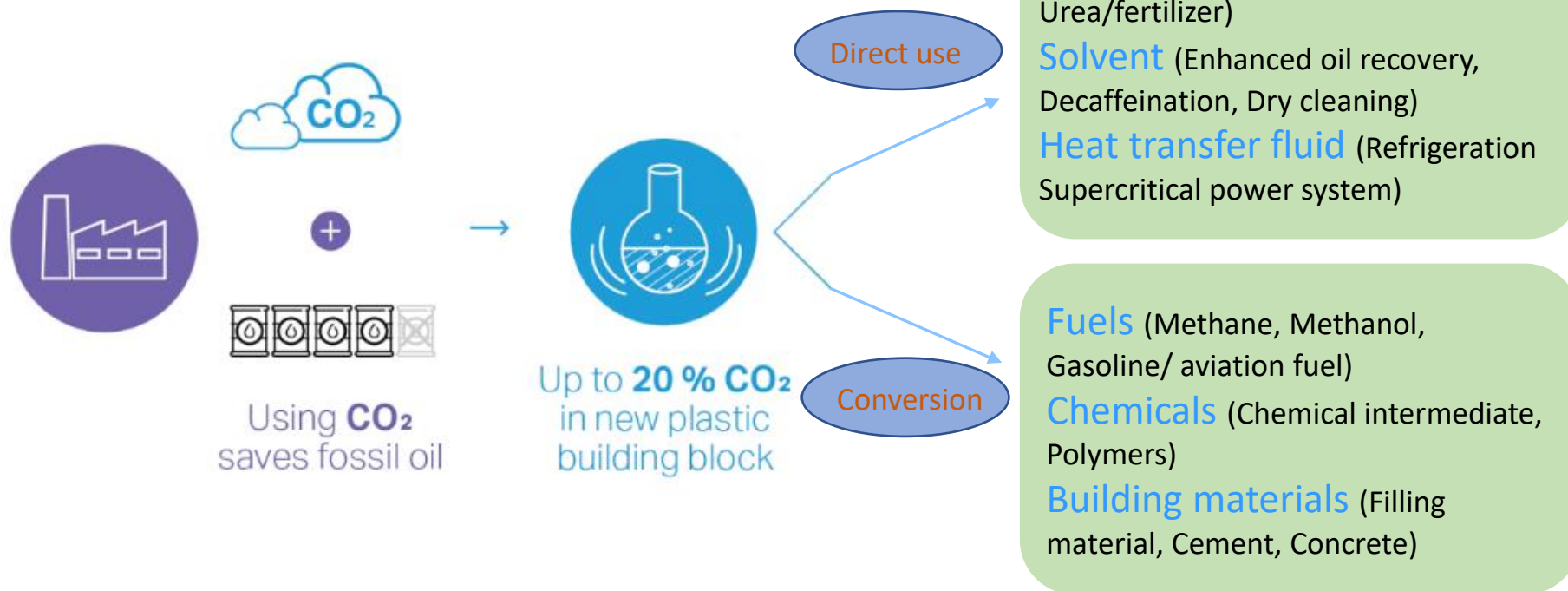
Polymeric membrane preparation and scaleup

Amol Ichake and Katrien Bernaerts

The present publication reflects only the author's views. The Commission is not responsible for any use that may be made of the information contained therein.

Introduction and Literature Overview

CO₂ as a raw material



Carbon dioxide can partially replace fossil fuel in plastics production

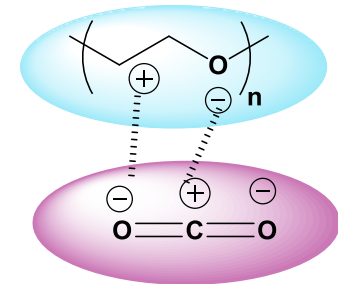
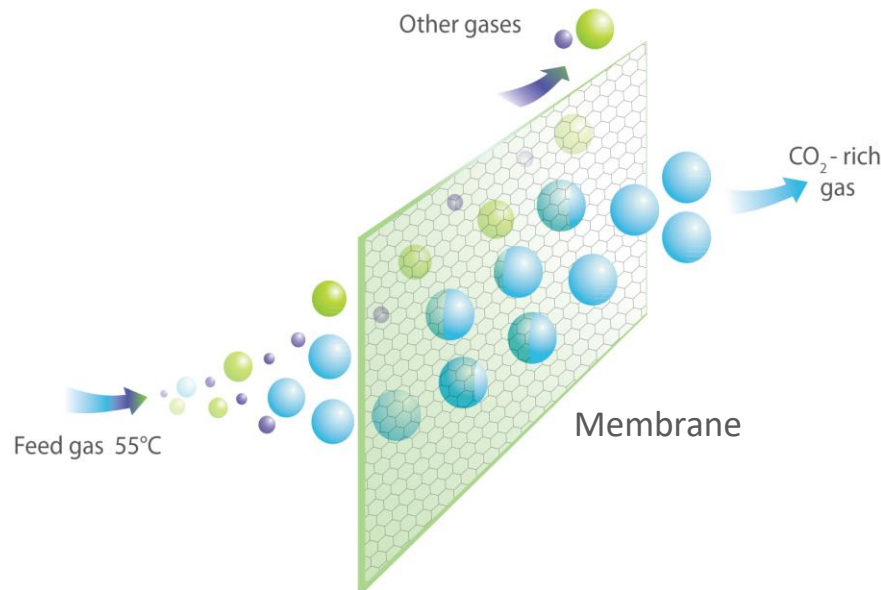
<https://www.covestro.com/en/sustainability/flagship-solutions/co2-as-a-raw-material>

Gas separation membranes

- **Permeability** is the rate at which gaseous molecules permeate through membrane
- **Selectivity** is the ability of membrane to separate the gas molecule from their mixture

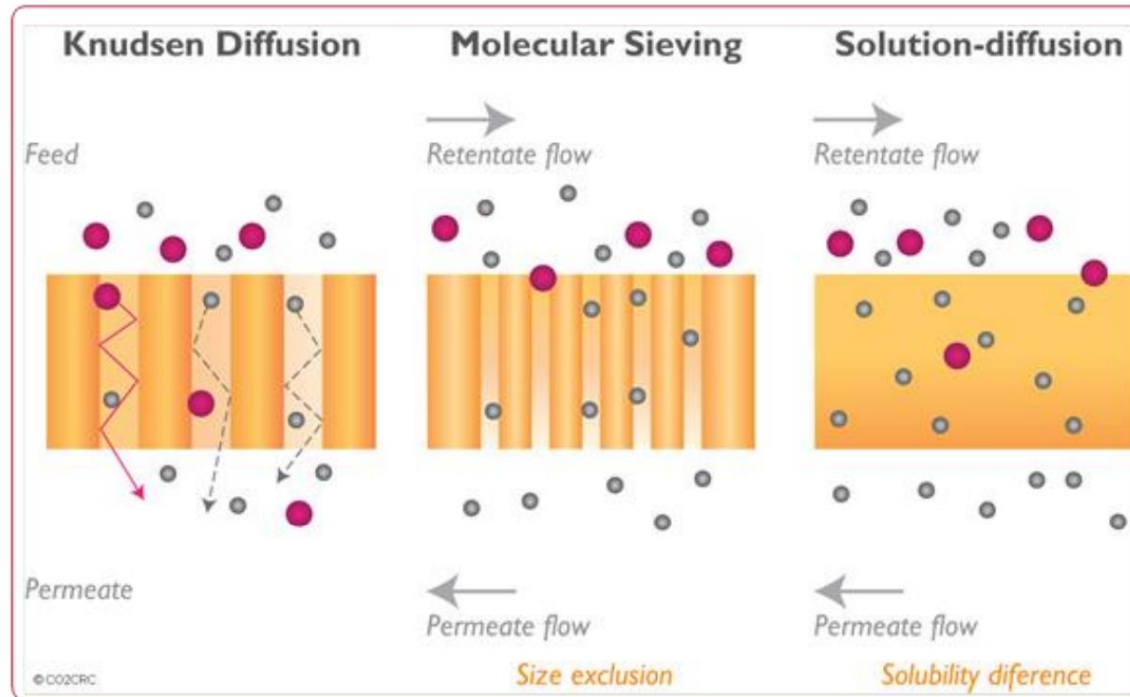
Inorganic, metallic and polymeric membranes have been reported for gas separations

Polymeric membranes



quadrupole-quadrupole interaction

Gas transport mechanism through membrane



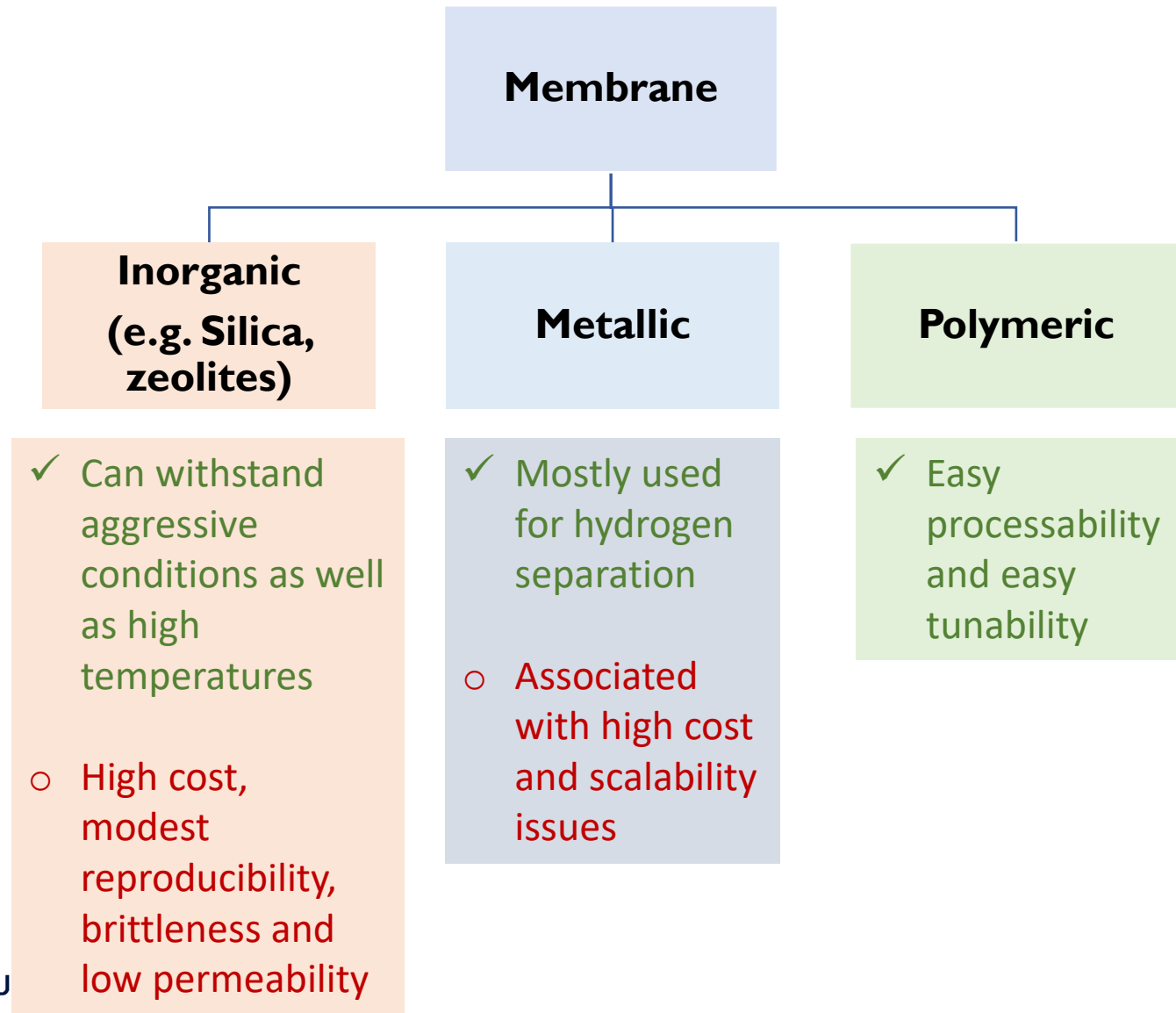
Knudsen diffusion is based on the molecular mass of gas and inversely proportional to the square root of the molecular mass of diffusing species. This separation is followed by macroporous and mesoporous membranes.

Molecular sieving mechanism depends on the size of the penetrant molecules. Generally, small size molecules readily permeate through the membrane while larger molecules do not permeate.

Solution-diffusion mechanism consists of three main steps: (i) sorption of the gases at upstream side, (ii) diffusion of gas across the membrane and (iii) desorption at the downstream side.

The transport of gas molecules through dense, nanoporous membranes is based on solution-diffusion mechanism.

Membrane materials for gas separation applications

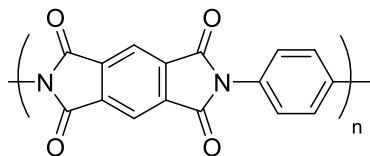


Membrane materials for gas separation applications

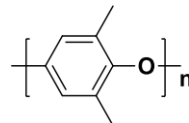
- The design of a membrane material for a gas separation application is based on specific physical and chemical properties.
- Robust, thermally and mechanically stable materials are required to be applied in a membrane gas separation process.
- The properties of membranes depend upon the material, membrane structure, thickness and membrane configuration (e.g., flat, hollow fiber).

Commercially available polymers for gas separation applications

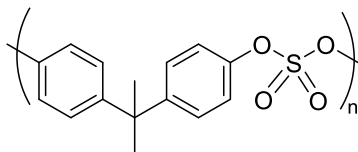
Various polymeric materials - Cellulose acetate, polyethersulfone, polyamide, polyimide, cross-linked poly(2,6 dimethylphenylene oxide)



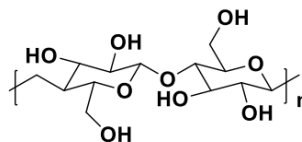
Polyimides



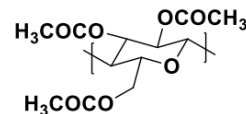
Poly(2,6-dimethyl-1,4-phenylene oxide) (PPO)



Polysulfones



Cellulose



Cellulose triacetate (TCA)

Membrane properties for industrial applications-

- High permeability and selectivity over other gases
- Thermal and chemical robustness
- Resistance to plasticization and aging
- Cost-effectiveness and
- Manufactured into different membrane forms such as flat sheet or hollow fibers with low cost.

Factors affecting gas separation performance

Physical Properties of Polymer

- I. Chain packing density
- II. Chain and subgroup mobility
- III. Polarity
- IV. Crosslinking

Properties of Gas

- I. Condensability of gas molecules
- II. Size and shape of gas molecules

Effects of Operating Parameters

- I. Temperature
- II. Pressure

Effects of Membrane Preparation Parameters

- I. Membrane fabrication method
- II. Solvent used for casting
- III. Casting temperature

Challenges in polymeric membrane materials for gas separation applications

Plasticization

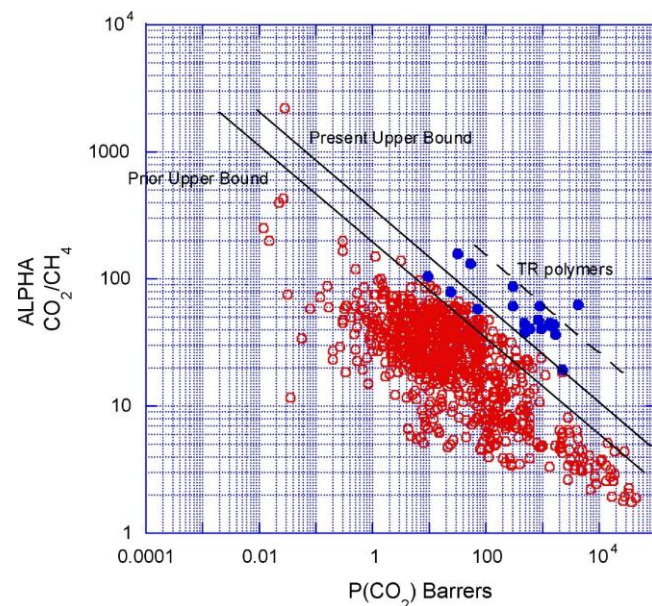
When the membrane is exposed to highly soluble gases that produce significant swelling in the polymer matrix. Due to this, polymer chain mobility and free volume increases which results into increased permeability and decreased selectivity.

Physical aging

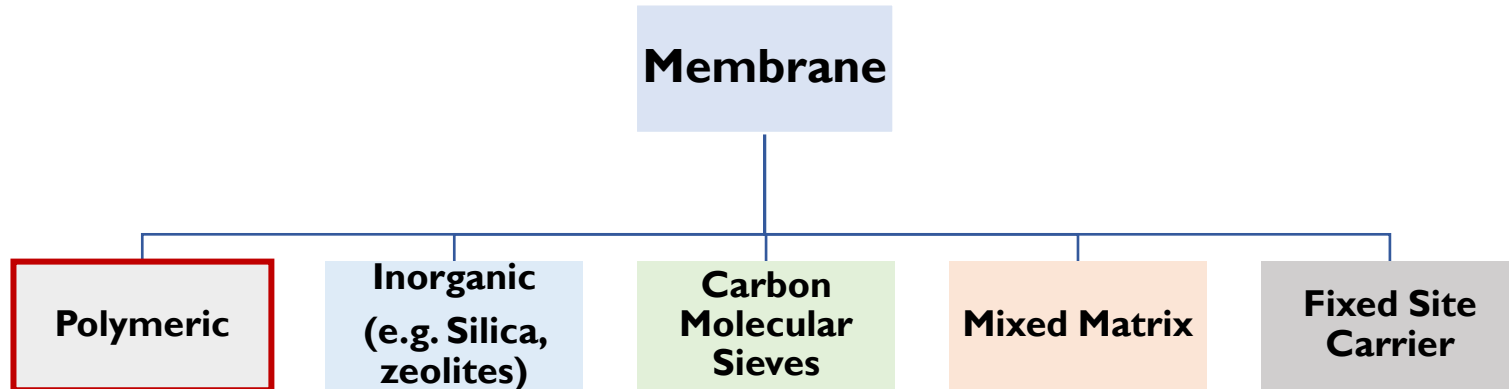
Generally, glassy polymer chains pack loosely, creating excess free volume in the polymer matrix. The polymer chains gradually get closer with time to fill this excess free volume which ultimately results in the reduction in the free volume. Due to this, a decrease in permeability is generally accompanied by an increase in selectivity. This decay in membrane permeability is due to the relaxation of the non-equilibrium free volume and subsequently re-ordering of polymer chains

Permeability/selectivity trade-off (Robeson upper bound)

Polymeric materials exhibit high permeability and low selectivity or vice versa as recognized by Robeson.



Membrane materials for gas separation applications



- ✓ Easy processability and easy tunability
- ✓ Low production cost
- Poor thermal and mechanical properties

Polymeric Poly-ethylene oxide (PEO) based membranes

Advantages

- Especially for CO₂ capture
- PEO-based polymers show a considerable CO₂ solubility, and the CO₂ selectivity mainly stems from the solubility selectivity.

Disadvantages

- Polar ether groups tend to form strong hydrogen bonding, which induces compact chain packing.
- A high degree of crystallinity in pure PEO or PEO-based materials

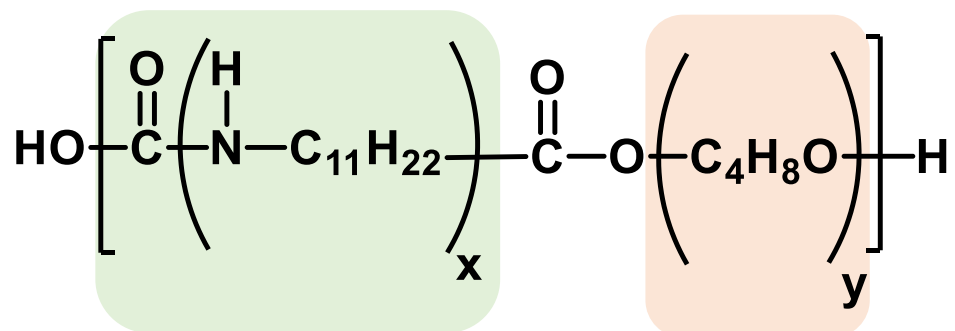
Various approaches to overcome these limitations

- ☐ Block copolymerization with other hard segments
- ☐ Blending with low molecular weight PEG and PEG-derivatives
- ☐ Crosslinking to form highly branched PEO polymer network.

Chemical Structure and properties of PEBA

The general method for the two-step preparation –

- A first step of synthesis of the polyamide blocks then
- A second step of condensation of the polyamide and polyether blocks



- Polyamide (PA)
- Semi-crystalline segments
- Hard PA segments provide mechanical stability

- Polyether (PE)
- Amorphous rubbery blocks
- Soft PE blocks,
- Owing to their high chain mobility, are gas permeable

PEBA offers a balanced combination of mechanical strength, breathability, flexibility, chemical resistance, and ease of processing

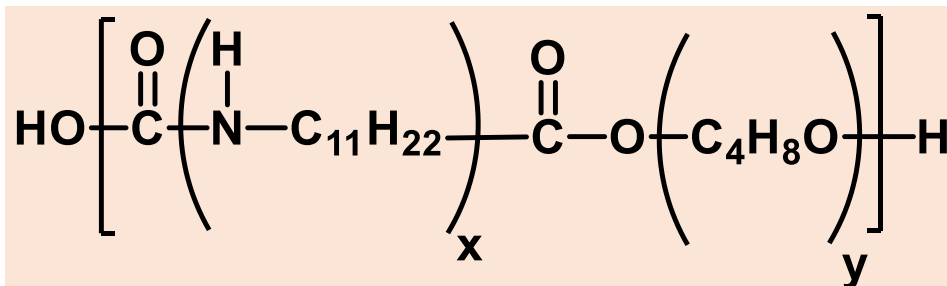
Transport properties of selected PEO-based polymers

| Strategy | Material | $p(\text{CO}_2)/\text{atm}$ | $T/^\circ\text{C}$ | $P(\text{CO}_2)/\text{Barrer}$ | $a(\text{CO}_2/\text{N}_2)$ | $a(\text{CO}_2/\text{CH}_4)$ | $a(\text{CO}_2/\text{H}_2)$ |
|---------------------|-------------------------|-----------------------------|--------------------|--------------------------------|-----------------------------|------------------------------|-----------------------------|
| Copolymer | PEO-b-PA6 | 10 | 35 | 120 | 51.4 | --- | 9.8 |
| | PEO-b-PBT | 0.3 | 30 | 150 | 51.5 | 16.8 | 10.3 |
| | PEO-g-POEM | 1 | 35 | 147 | 47 | | |
| | PEO-ran-PPO-T6T6T | 4 | 35 | 470 | 43 | 13 | 10 |
| | GPA1000-g-PEG-azide | 2 | 45 | 1840 | 36 | --- | 8.3 |
| | PEO-b-PBT on PDMS | 5 | 30 | 1815* | 50 | --- | --- |
| | PEO-b-PS | 1 | 70 | 20400* | 27.7 | --- | --- |
| | | | | | | | |
| Blending | PEBAX®1074/PEG1500 | 5 | 60 | 528 | 34.6 | 7.4 | 10.6 |
| | PEBAX® MH1657/PEGDME500 | 0.3 | 30 | 650 | --- | --- | 14.9 |
| | PEBAX® MH1657/PEG-AE | 0.3 | 30 | 335 | --- | --- | 12.9 |
| | PEBAX® MH1657/PEG-DVE | 0.3 | 30 | 570 | --- | --- | 12.9 |
| | PEBAX® MH1657/PEG-AME | 0.3 | 30 | 620 | --- | --- | 14.5 |
| | PEO-PPO-T6T6T/PDMS-PEG | 4 | 35 | 896 | 36 | 10.9 | 10.6 |
| | PEBAX® 1657/PEGDME500 | 0.17 | 57 | 940* | 30 | --- | --- |
| | PEBAX® 2533/PEG-b-PPFPA | 3.5 | 35 | 940* | 17 | --- | --- |
| Crosslinking | PEGDA/PEGMEA | 11 | 10 | 300 | --- | 23 | --- |
| | PEGDA/PEGMEA | 4 | 35 | 570 | 41 | --- | --- |
| | PEGDA/TRIS-A | 15 | 35 | 716 | 19.9 | --- | 7.7 |
| | PEA/TMC | 0.2 | 25 | 360* | 67.2 | --- | --- |
| | DGBAmE/TMC | 0.71 | 22 | 1310* | 33 | --- | --- |

$p(\text{CO}_2)$ = CO_2 partial pressure; $P(\text{CO}_2)$ = CO_2 permeability; a =ideal CO_2 /gas selectivity;

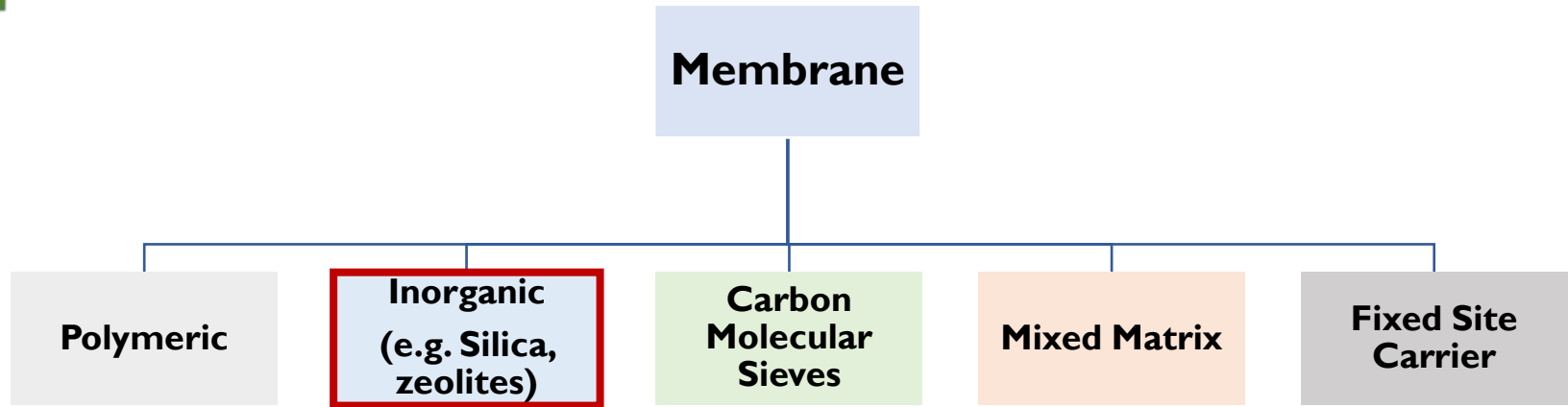
*Permeance measured in thin film-composite membrane, GPU

Polyether block amide (PEBA) based membranes for CO₂ separation



| Membrane | Gas mixture | Membrane Feature | Process performance | Main remarks |
|---|--|---|---|---|
| Commercially available Pebax® MH1657 and its blends with low molecular weight PEG | Pure gases (H ₂ , N ₂ , CH ₄ , CO ₂) | Membrane Thickness = 60-100 mm | Permeability (Barrer): CO ₂ = 73-151 Permeance (GPU): CO ₂ < 2.5. Selectivity: CO ₂ /N ₂ = 43-47 CO ₂ /CH ₄ = 15.1-15.9 CO ₂ /H ₂ = 9.1-10.8 | The permeability of CO ₂ in Pebax®/PEG membrane (50 wt.% of PEG) is twofold regarding to the pristine Pebax® and an enhancement of CO ₂ /H ₂ selectivity of ~11 is produced due to the presence of EO units that increases CO ₂ permeability. |
| Hollow fiber PEBA/PSf composite membranes and dense PEBA membranes | Pure gases: CO ₂ ; N ₂ | Membrane thickness = 55 mm Layer (PEBA) Thickness < 5 mm | <i>Dense PEBA membranes:</i> Permeability (Barrer): CO ₂ = 200-550 N ₂ = 8-36 Selectivity: CO ₂ /N ₂ = 16-40 <i>Composite membranes:</i> Permeance (GPU): CO ₂ = 61 Selectivity: CO ₂ /N ₂ = 30 | CO ₂ permeability tends to increase with an increase in gas pressure due to plasticization of the membrane caused by the relatively high solubility of CO ₂ in the membrane. But the plasticization and swelling of the membrane are less significant at higher temperatures. The selectivity of the composite membrane is very close to the intrinsic selectivity of PEBA dense membrane. |

Membrane materials for gas separation applications



- ✓ Can withstand aggressive conditions as well as high temperatures
- High cost, modest reproducibility, brittleness and low permeability

Membranes

Inorganic membranes

Advantages

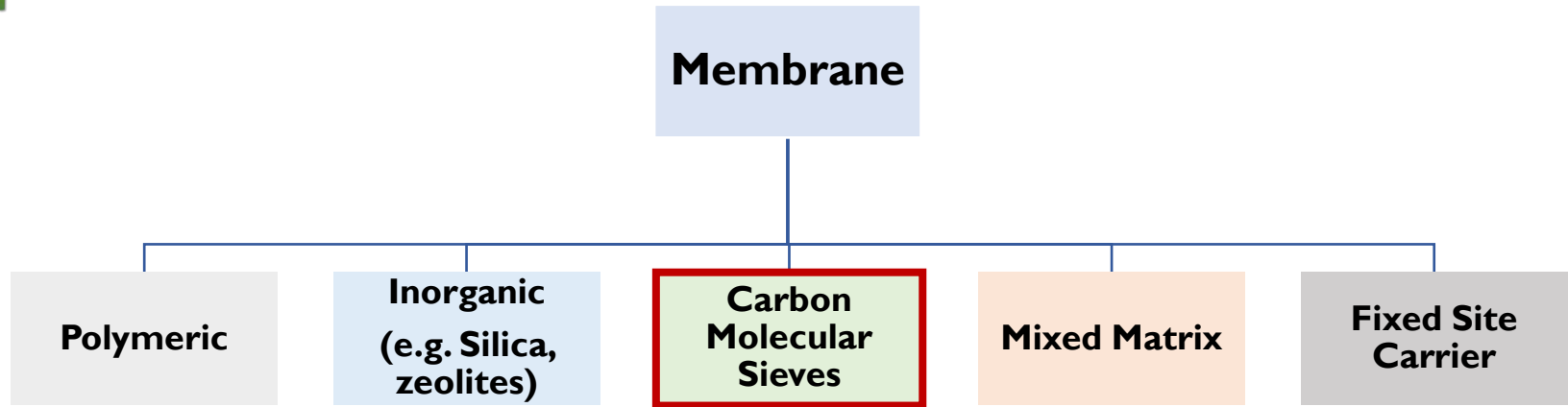
- Based on different materials like metal (alumina, cobalt, copper, iron, nickel, niobium, palladium, platinum, tantalum and vanadium), zeolites, carbon, and ceramic
- Generally, these membranes show higher gas separation performances combined with substantial chemical and thermal stability.

Disadvantages

- Materials have poor mechanical properties and are difficult to process.
- Brittle and expensive -their conversion into high surface area modules is rather difficult

| Organic polymers | Inorganic materials |
|-------------------------------|-----------------------------------|
| Polysulfone, polyethersulfone | Carbon molecular sieves |
| Cellulose acetate | Nanoporous carbon |
| Polyimide, polyetherimide | Zeolites |
| Polycarbonate (brominated) | Ultramicroporous amorphous silica |
| Polyphenylene oxide | Palladium alloys |
| Polymethylpentene | Mixed conducting perovskites |
| Polydimethylsiloxane | Metal organic frameworks |
| Polyvinyltrimethylsilane | - |

Membrane materials for gas separation applications



- ✓ Excellent chemical and thermal stability
- ✓ Can be used as aggressive conditions
- ✓ Surpass the trade of curve
- High cost
- brittle

Membranes

Carbon Molecular Sieve

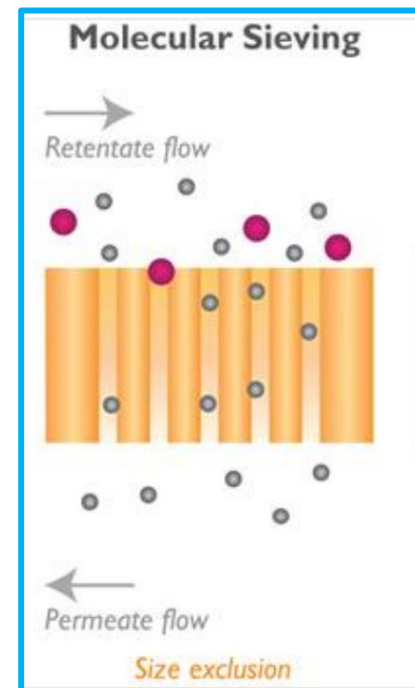
- High-performance gas separation membrane
- Separation mechanism- The gas molecules are separated by the size sieving effect

Advantages

- Excellent chemical stability
- Surpass the trade-off curves
- Can be used under aggressive condition
- Porous solid membrane with extreme rigidity and microporosity

Disadvantages

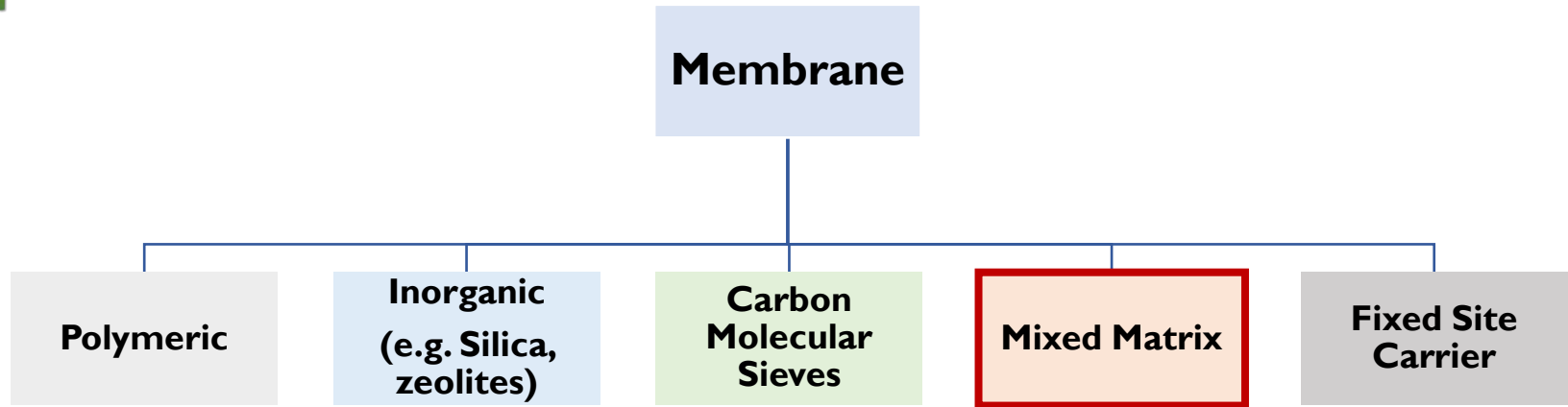
- Brittle
- High cost



Performance of asymmetric membranes for natural gas purification

| Membrane | Feed gas CO ₂ /CH ₄ | Feed pressure (bar) | CO ₂ permeance (GPU) | CO ₂ /CH ₄ selectivity |
|-----------------------------------|---|---------------------|---------------------------------|--|
| 6FDA/BPDA-DAM CMS HF | 10/90 (vol%) | 3.40 | 30 | 73 |
| Matrimid 5218 CMS HF | 10/90 (vol%) | 3.40 | 12 | 69 |
| 6FDA/BPDA (1:1)-DAM CMS HF | 50/50 (vol%) and 500ppm C ₇ HC | 124.13 | 50 | ~60 |
| ULT CMS-6F0.5 HF | 50/50 (mol%) | 6.90 | 2546 | 24.10 |
| 6FDA:BPDA-DAM CMS HF | Pure gas | 0.34 | 273 | 32 |

Membrane materials for gas separation applications



- ✓ Acceptable mechanical properties and cost-effective processability
- ✓ high selectivity, high permeability
- complex interaction
- Critical membrane morphology

Membranes

Mixed Matrix Membranes

- Consist of an organic polymer combined with inorganic (or sometimes organic) particles
- The dispersed phase may be zeolites, carbon molecular sieves (CMS), carbon nanotubes (CNT) or other nano-size particles.
- Metal organic frameworks (MOFs) are a newer class of crystalline and porous materials and are now used to overcome the limitations of inorganic membranes.

Advantages

- Combining the advantages of inorganic fillers with the acceptable mechanical properties and cost-effective processability of polymers were performed for CO₂/CH₄ gas separation.
- Potential for high selectivity, high permeability or both, compared to actual polymer and inorganic membranes.

Disadvantages

- The performance of MMM is not the sum of the intrinsic properties of each individual component
- The performance can be seriously affected by the complex interaction between all parameters.
- Transport properties of MMM are highly function of membrane morphology at the nanoscale, which is critical for the overall membrane properties

Mixed matrix membranes composed of polymers and zeolites

Physical molecular properties of zeolites

Size and shape:

Gas molecules smaller than the pore size can adsorb on zeolites, whereas larger gas molecules cannot.

- Small pore size (0.30-0.45 nm). These zeolites have 8 membered-rings pore apertures with free diameters like zeolite NaA.
- Medium pore size (0.45-0.60 nm). These zeolites have 10 membered ring apertures, within free diameter like zeolite ZSM-5.
- Large pore size (0.6-0.8 nm). These zeolites have 12 membered-ring apertures or more within free diameter like zeolite faujasite (X, Y).

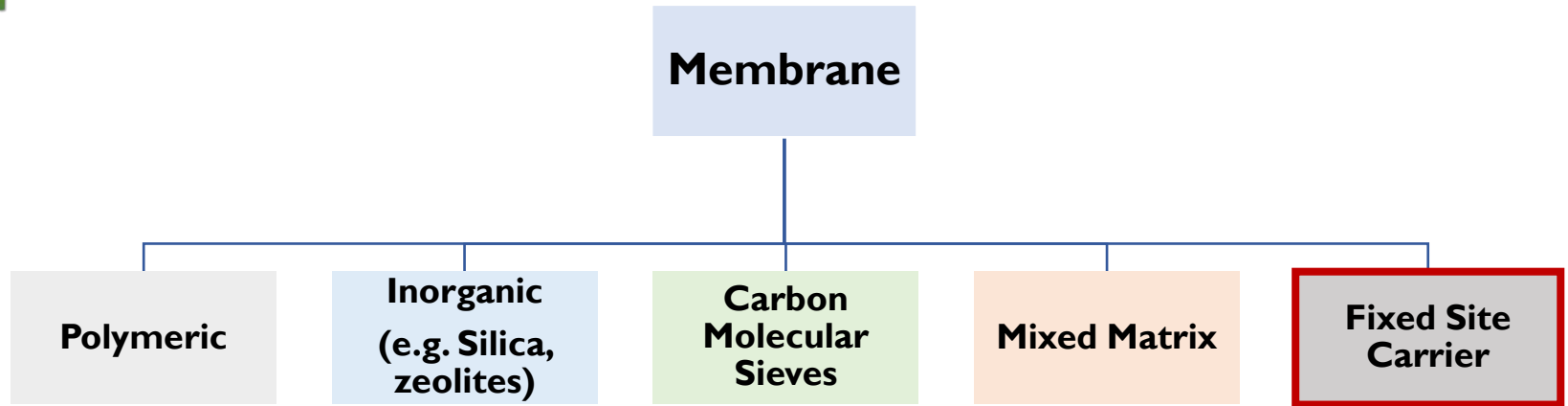
Molecular polarity:

- Gas molecules with higher polarity can be better adsorbed than non-polar gas for the majority of zeolites under identical conditions.

Counter-ion:

- The type of cation controls the electric field inside the pores, basicity, and the available pore volume, which offers a convenient means for tuning adsorption properties.

Membrane materials for gas separation applications

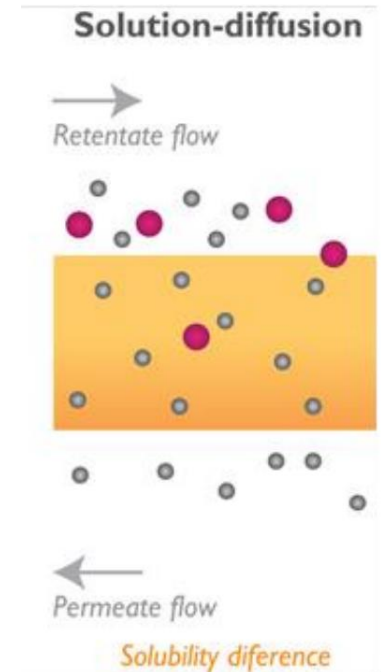


- ✓ Solution-diffusion
- ✓ Active transport mechanism

Membrane

Fixed-site carrier membranes

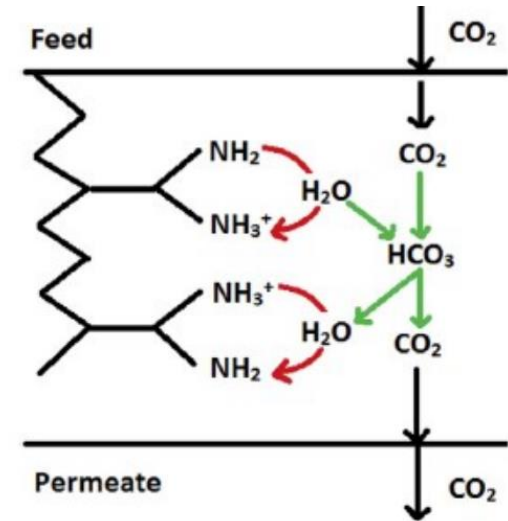
- Exhibit “solution-diffusion” characteristics and also contain an active transport mechanism that increases the permeability and selectivity of the membrane material.
- The target species reversibly reacts with either a fixed or mobile carrier present in the membrane that then diffuses across the membrane driven by a concentration gradient in the complex rather than a gradient in the permeate.
- The main characteristic of these membranes is represented by the decrease of both CO₂ permeance and selectivity with increasing CO₂ feed partial pressure.



Membrane

Fixed-site carrier membranes

- The CO_2 is absorbed and reacts to form bicarbonate, the form in which it permeates the membrane. Upon reaching the other side it back reacts to form CO_2 and is then released on the permeate side.
- eg. PVAm



Mechanism for a fixed carrier amine based facilitated transport membrane

Biocomem Results

Develop new bio-based CO₂ gas separation membranes using polyether block polyamide copolymer (PEBA)

- High processability into monolithic hollow fiber membrane (i.e. solubility)
- Higher bio-based content
- High gas separation performance
- High chemical resistance

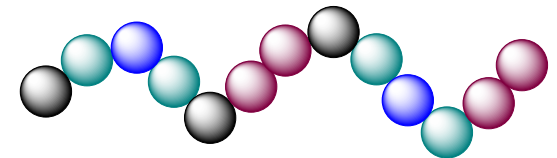
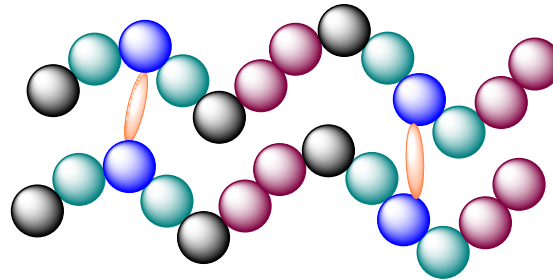
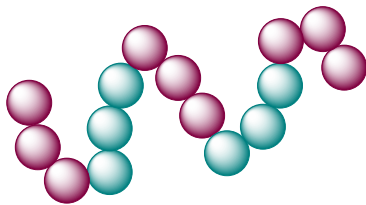
Block copolymers

**Original
prototypes**

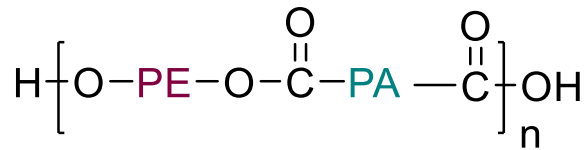
Prototype A
Commercial

Prototype B
Photocrosslinkable
Partially bio-based

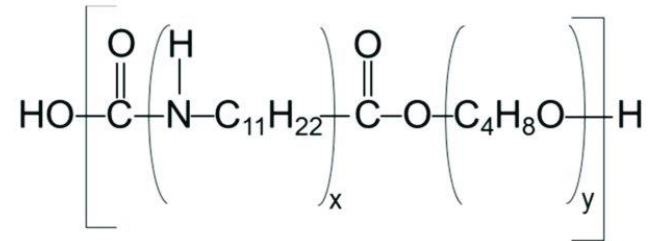
Prototype C
Fully bio-based



PEBA Prototype A



General structure of Poly(ether-*b*-amide)



Chemical Structure of PEBAX

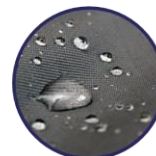
VARIETY OF TECHNOLOGIES



COMPONENTS

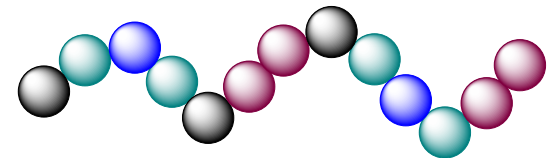
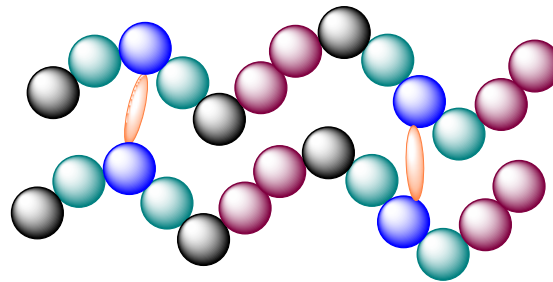
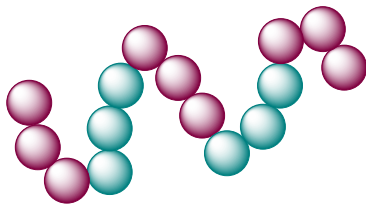
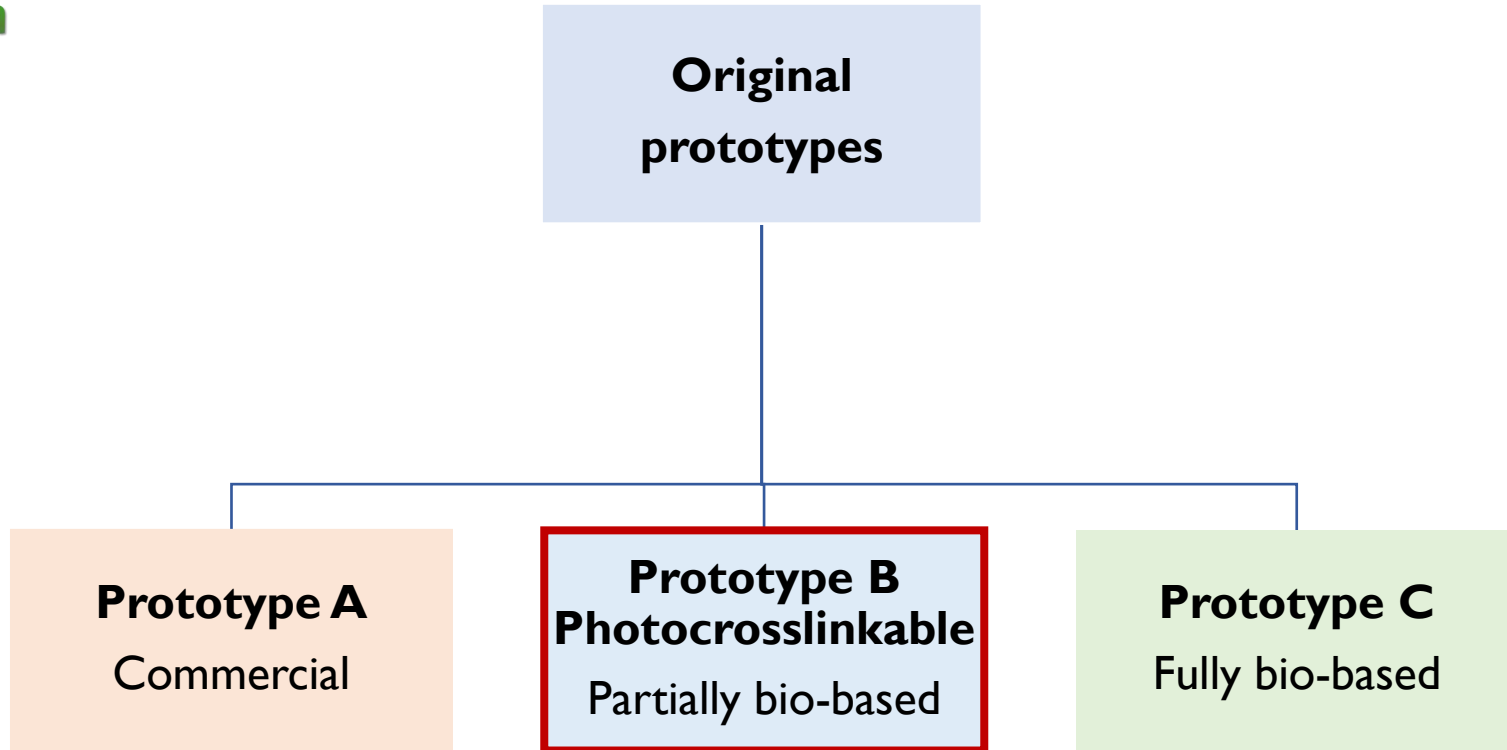


FOAMS



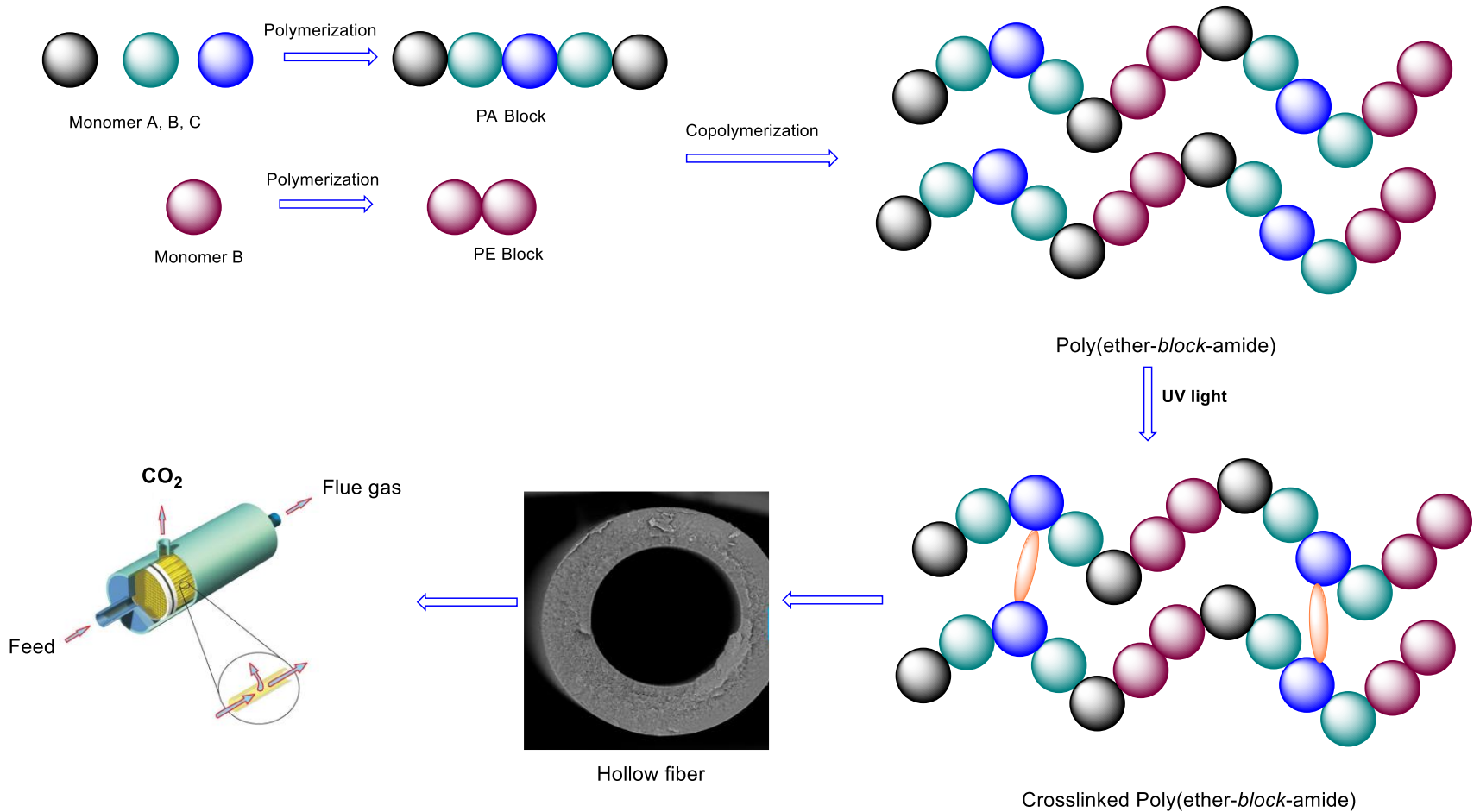
MEMBRANES

Bio-based block copolymers



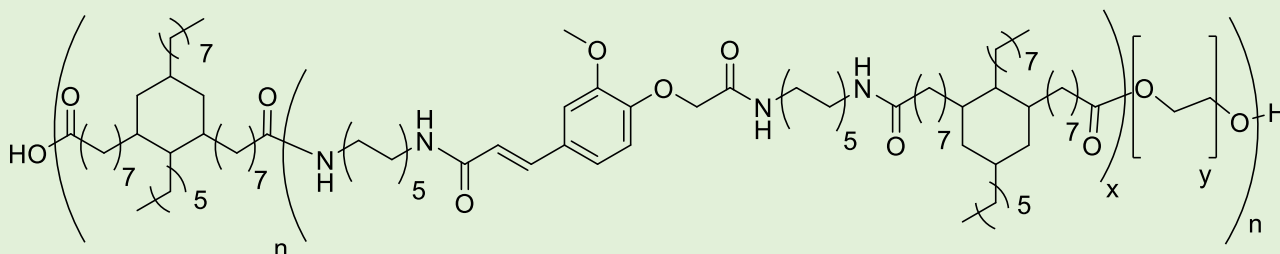
New bio-based block copolymers

Prototype B

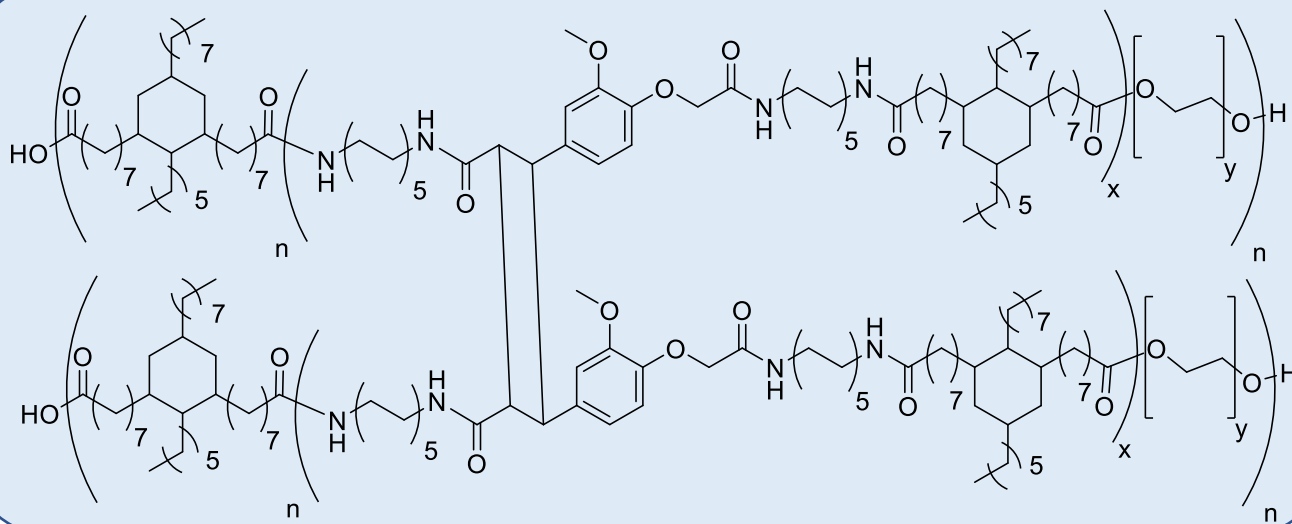


Photocrosslinkable PEBA, Prototype B

PEBA

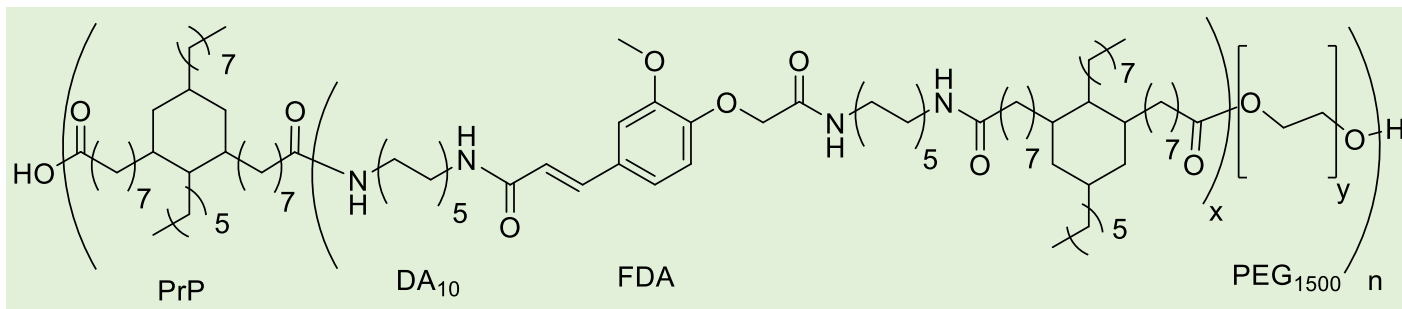


UV crosslinking



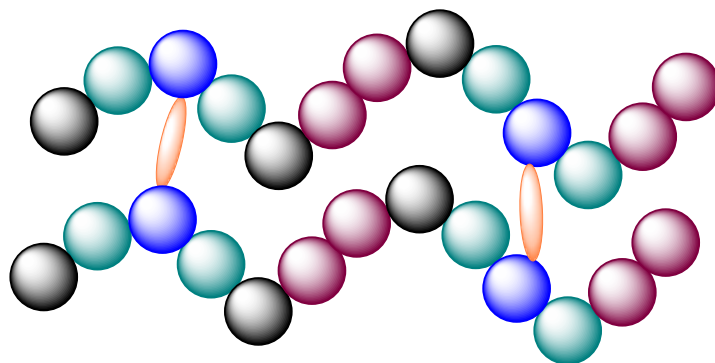
Photocrosslinking

PEBA (prototype B, photocrosslinkable) with FDA monomer



| Sample | PA prepolymer (M_n titration) | $M_{n, GPC}$ [g / mol] | \bar{D} | wt% PA/PEG ₁₅₀₀ (feed) | wt % PA/PEG ₁₅₀₀ (NMR) | T_g [°C] | T_m [°C] | $\Delta H_{m(PEG)}$ [J / g _{PEG}] | $\Delta H_{m(PA)}$ [J / g _{PA}] |
|---------------|--|------------------------|-----------|-----------------------------------|-----------------------------------|------------|------------|---|---|
| PEBA ref | | 83 000 | 2.0 | 40/60 | | -20 | 13, 149 | 40 | 29 |
| MS-2021-035B5 | PA (PrP/DA10) ₂₃₀₀ | 42 000 | 1.72 | 60/40 | 57/43 | -62 | 15, 79 | 55 | 16 |
| AI-20 (PEBA) | PA(PrP ₄₀ /DA10 ₅₀ /FDA ₁₀) ₂₁₀₀ one step | 32 500 | 1.74 | 59/41 | 61/39 | <-40 | 28, 74 | 34 | 11 |

Photocrosslinkable PEBA, Prototype B



Crosslinked Poly(ether-*block*-amide)



Before crosslinking

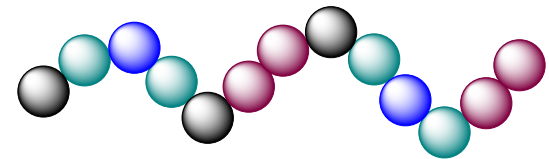
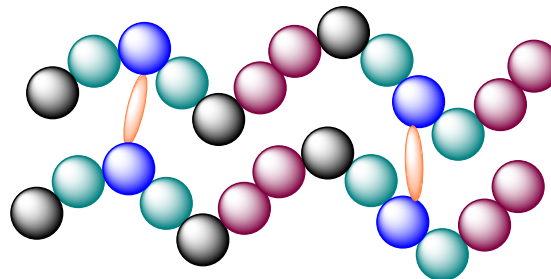
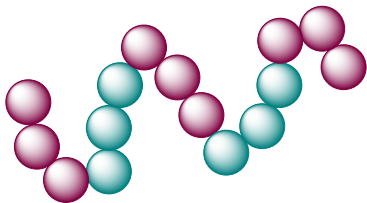
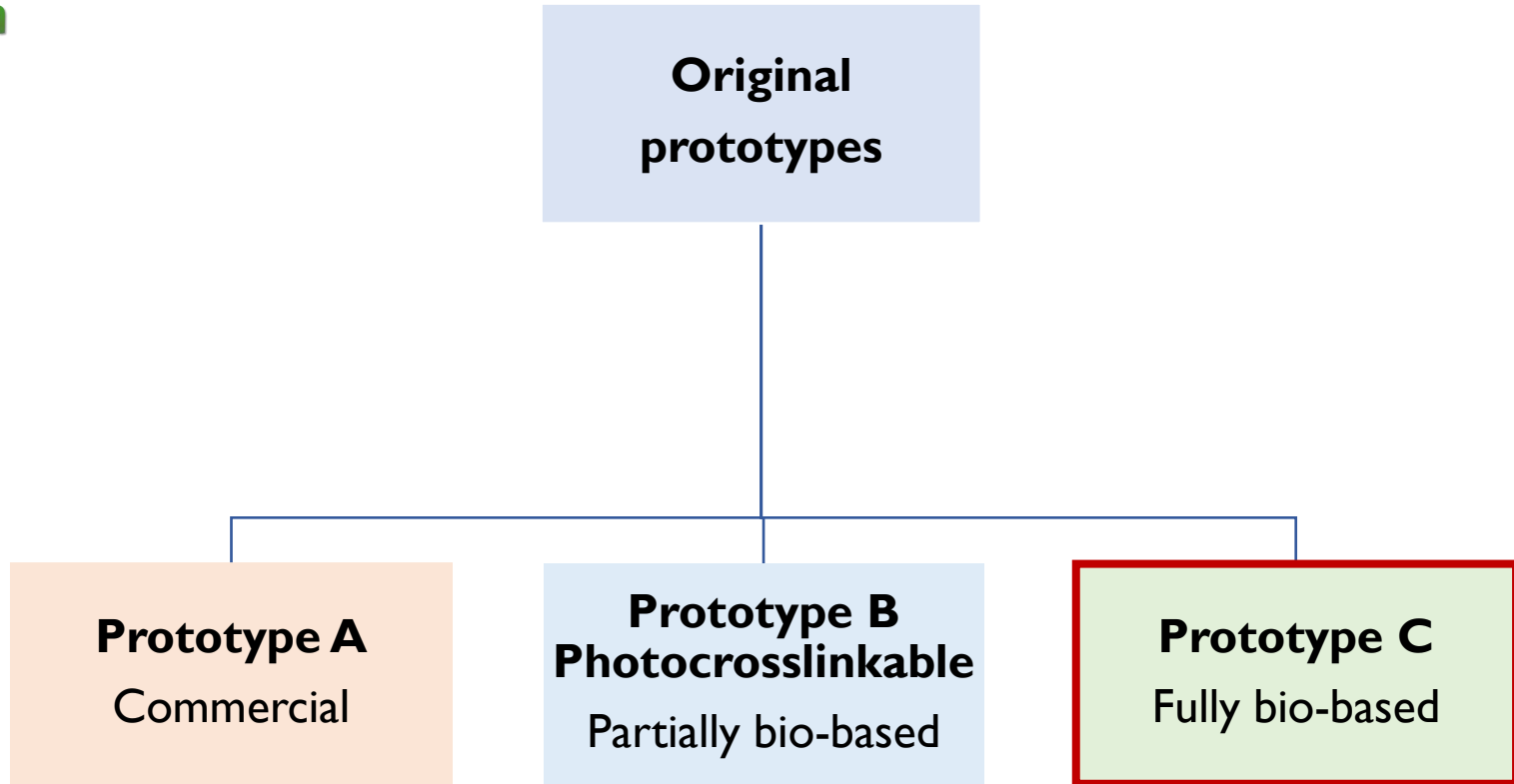
1 h UV
Autoheating
~70 °C



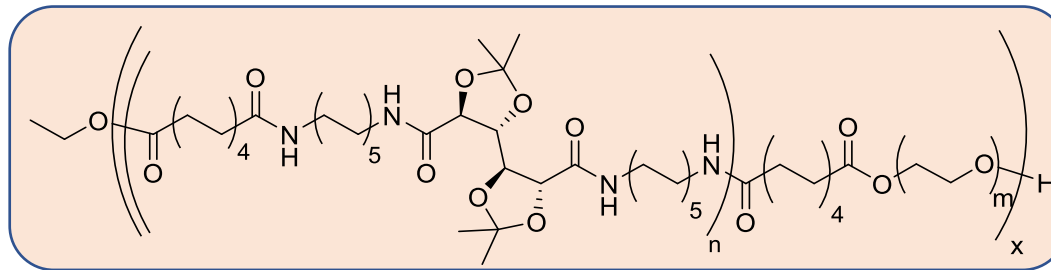
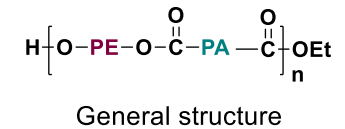
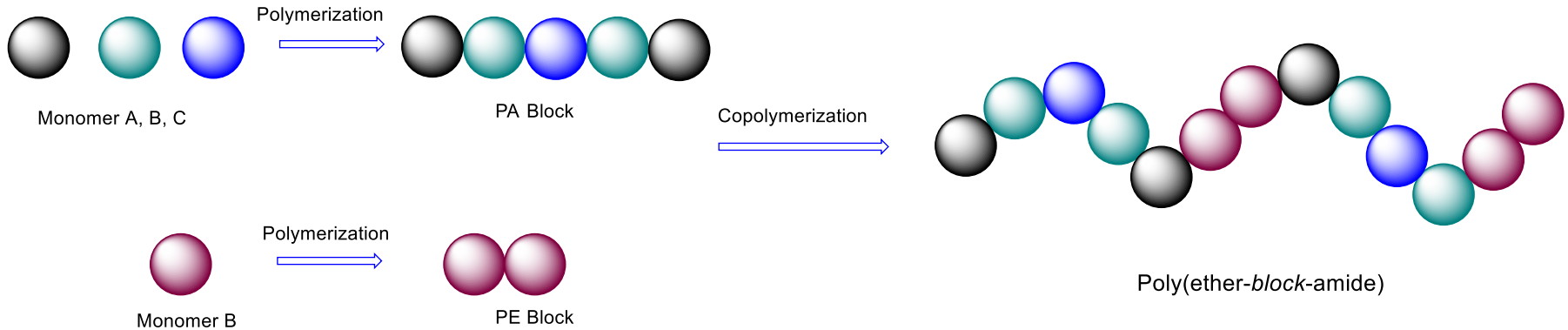
After crosslinking
Hot press

| PEBA | Sample Casted Film ^a | Curing time (min) | Sensitizer type | Gel content (%) | Gel content (%) After hot press |
|-------|------------------------------------|-------------------------|------------------|--------------------|------------------------------------|
| Al-20 | Transparent ~0.05 mm | 60 | Michler's ketone | 67 % | 67 % |

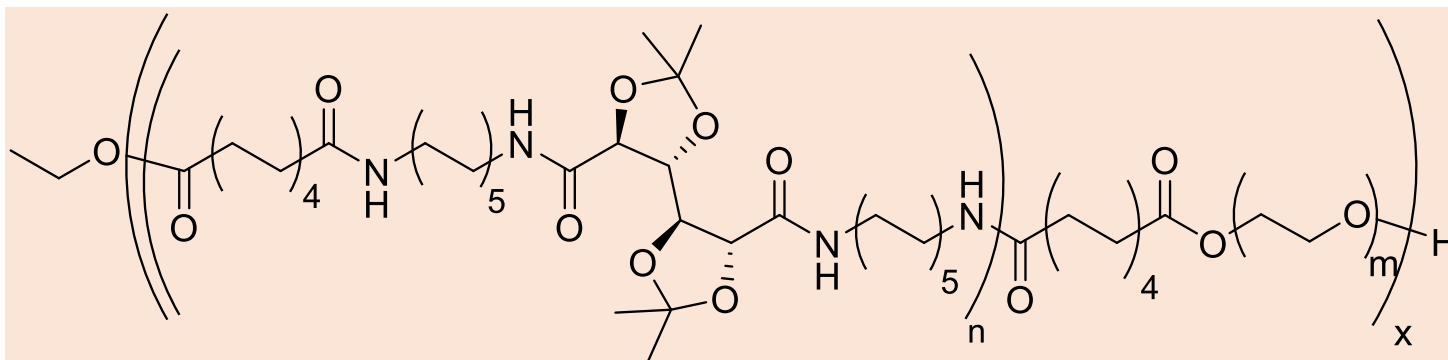
Bio-based block copolymers



Prototype C, Semicrystalline



PEBA prototype C (Semicrystalline PEBA)



| Sample | $M_{n, \text{ end groups for PA [g/mol]}}$ | $M_{n, \text{ GPC (g/mol)}^a}$ | \bar{D}^a | T_m [°C] | $\Delta H_{m(\text{PEG})}$ [J/g _{PEG}] | $\Delta H_{m(\text{PA})}$ [J/g _{PA}] | Weight Ratio PA/PEG (feed) | Weight ratio PA/PEG (NMR) | η (Pa.s) at 220 °C |
|--------------------|--|--------------------------------|-------------|------------|--|--|----------------------------|---------------------------|-------------------------|
| Bio-PEBA | 1050 PA11 | 83000 | 2.0 | 13; 149 | 40 | 29 | 40/60 | - | 20± 2.23 |
| AI-38 (1 mol% cat) | 1100 PA SAM100226 | 37300 | 2.16 | 27, 160 | 51 | 15 | 47/53 | 42/58 | 3± 0.17 |
| AI-39 (2 mol% cat) | 1100 PA SAM100226 | 39000 | 2.15 | 27, 160 | 48 | 12 | 47/53 | 41/59 | 6.77±0.35 |
| AI-40 (3 mol% cat) | 1100 PA SAM100226 | 41500 | 2.25 | 27, 160 | 47 | 15 | 47/53 | 42/58 | 15.3±0.23 |



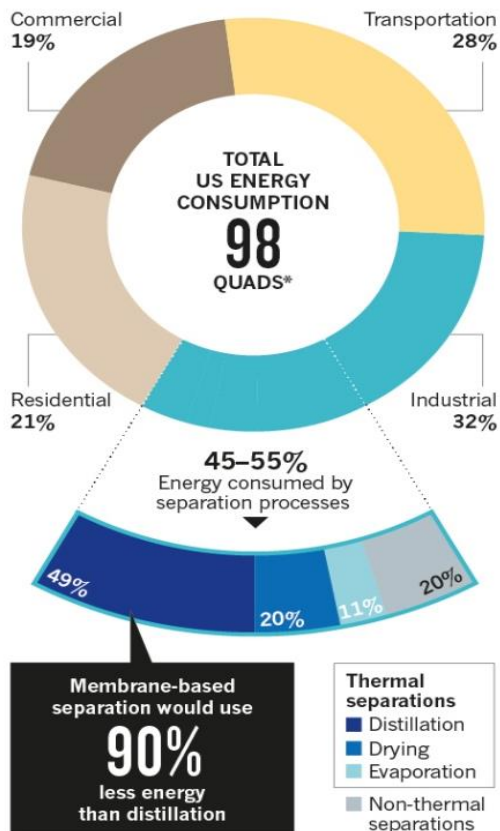
Thank you for your attention!

Polymeric membrane preparation and scaleup: Hollow Fiber membranes

Dr. Miren Etxeberria Benavides and Dr. Oana David

Membrane Technology and Process Intensification





MEMBRANE SEPARATION

- No require a gas-liquid phase change
- Smaller separation units → small footprint
- Lack of mechanical complexity
- Operate under continuous, steady-state conditions





APPLICATIONS

CO₂
capture

CH₄
purification

H₂
purification

Olefin / paraffin
separation

Water
separation

MEMBRANE CLASSIFICATION

MATERIAL

Inorganic

Metallic

Ceramic

Carbon

Zeolite

Organic

Polymeric

STRUCTURE

Symmetric

Asymmetric

Integral asymmetric

Composite

GEOMETRY

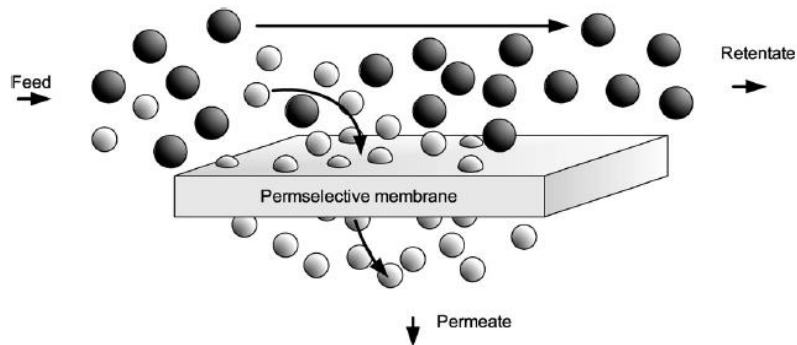
Flat sheet

Tubular

Hollow fiber

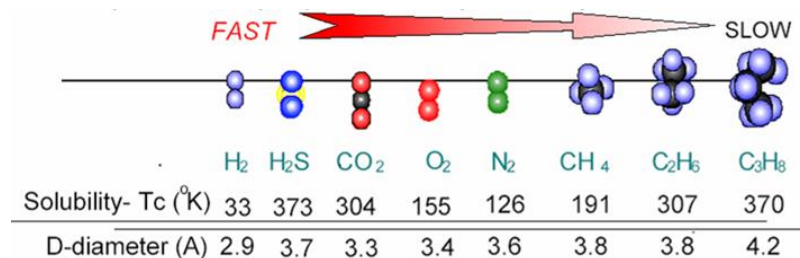


POLYMERIC MEMBRANES: SOLUTION-DIFFUSION MODEL



$$P_i = S_i \cdot D_i$$

$$\alpha_{ij} = \frac{P_i}{P_j} = \frac{S_i}{S_j} \cdot \frac{D_i}{D_j}$$



Permeability
(intrinsic property)

$$P_i = \frac{F_i \cdot l}{\Delta p_i \cdot A}$$

$$\text{Barrer} = 10^{-10} \frac{\text{cm}^3 \text{STP cm}}{\text{s} \cdot \text{cm}^2 \cdot \text{cmHg}}$$

Permeance
(membrane property)

$$\frac{P_i}{l} = \frac{F_i}{\Delta p_i \cdot A}$$

$$\text{GPU} = 10^{-6} \frac{\text{cm}^3 \text{STP}}{\text{s} \cdot \text{cm}^2 \cdot \text{cmHg}}$$

Table 1. Current Big Four Commercial Gas Separation Membrane Applications

| application | separation performed | selective layer polymer | approximate market size |
|---------------------------|--|--|-------------------------|
| hydrogen recovery | H ₂ /N ₂ , H ₂ /CH ₄ , H ₂ /CO | polysulfone, polyimides | \$200 million/year |
| N ₂ production | O ₂ /N ₂ | polyimides, polysulfone, polyphenylene oxide, substituted polycarbonates | \$800 million/year |
| natural gas treatment | CO ₂ /CH ₄ , H ₂ S/CH ₄ , He/CH ₄ | cellulose acetates, polyimides | \$300 million/year |
| vapor recovery | C ₃ H ₆ /N ₂ , C ₂ H ₄ /N ₂ , C ₂ H ₄ /Ar, C ₃ +/CH ₄ , CH ₄ /N ₂ , gasoline/air | silicone rubber | \$100 million/year |

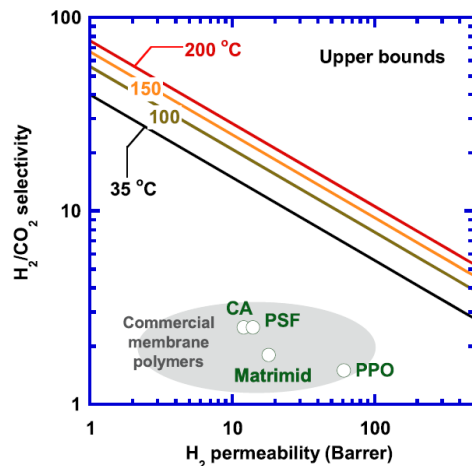
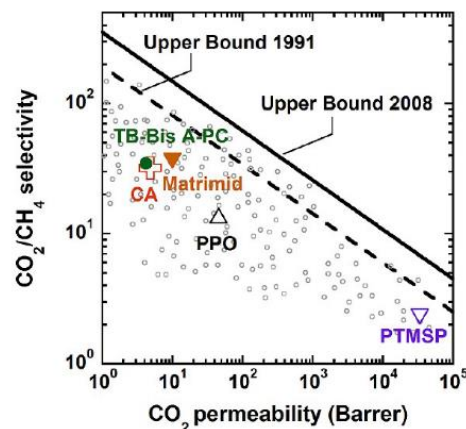
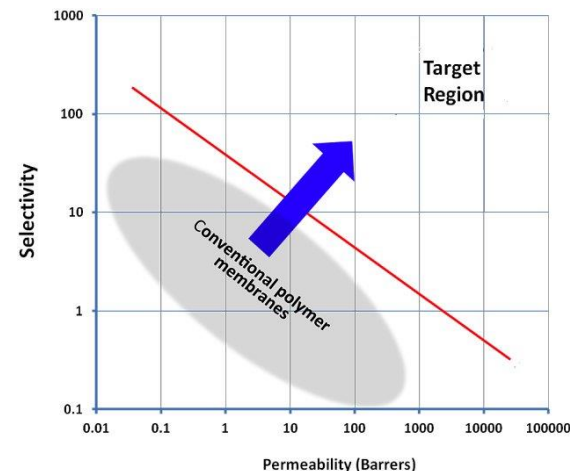
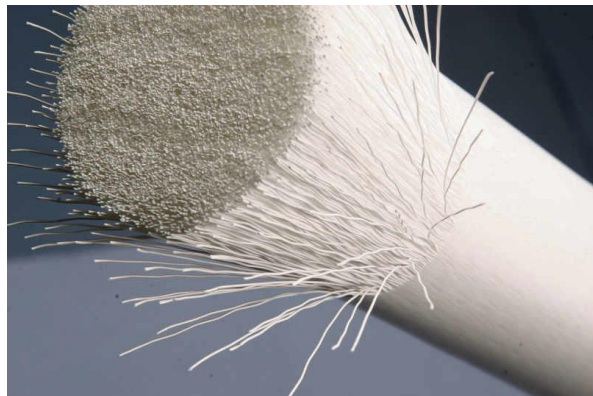


FIGURE 1 Upper bounds of H₂/CO₂ separation at 35, 100, 150, and 200 °C calculated using the parameters shown in Table 1.^[11–13] The separation properties of commercial membrane polymers were determined at 35 °C. 1 Barrer = 10⁻¹⁰ cm³ (STP) cm/(cm² s cmHg)



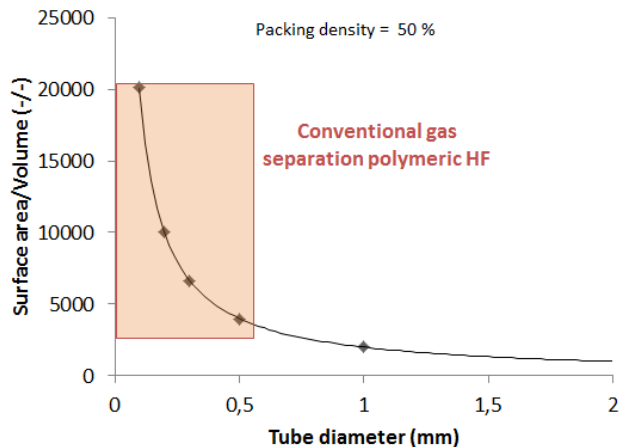
CO₂/CH₄ Robeson diagram for conventional glassy polymers.



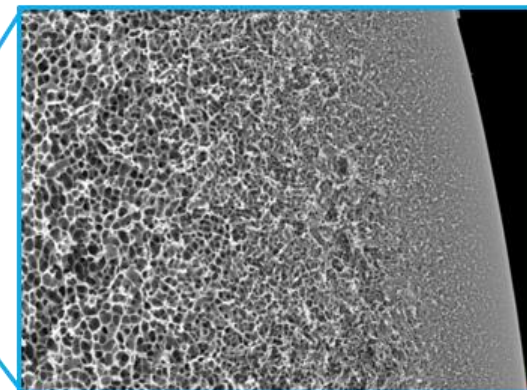
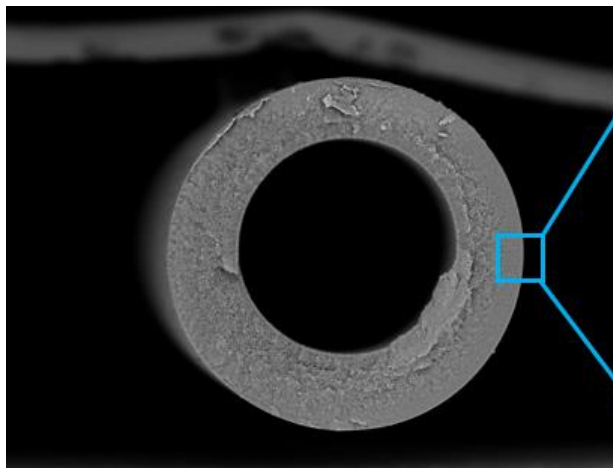


Advantages of HF

- High packing density (over 10000 m²/m³), 10 times higher than plate and frame modules
- Can handle very high transmembrane pressure differences (up to 70 bar)
- 5 to 20 times lower fabrication costs



Asymmetric hollow fiber



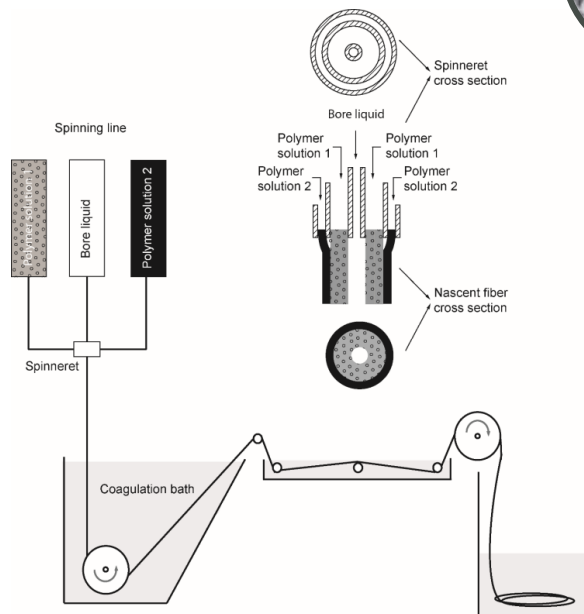
Thin and dense separating skin layer (<1μm)

Highly porous support

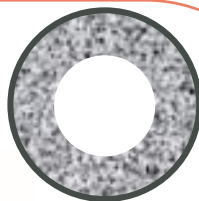
HOLLOW FIBER PREPARATION METHODS

SPINNING

Monolithic hollow fiber

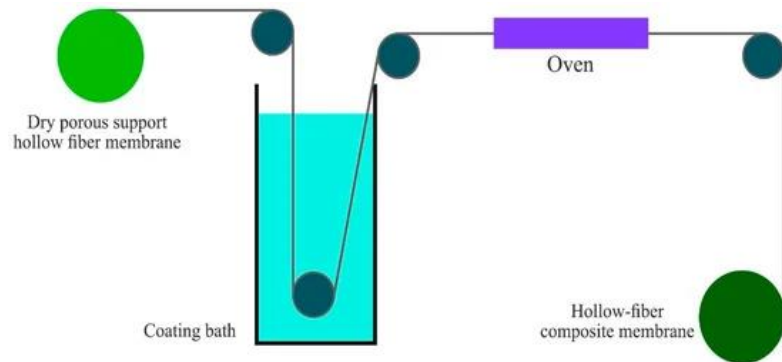


Single step process: simultaneous formation of the porous support + dense selective layer

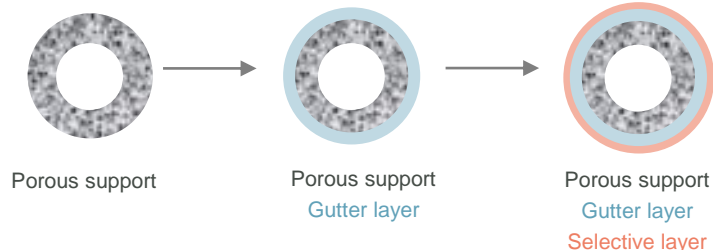


DIP COATING

Composite hollow fiber



Multiple step process



MEMBRANE DEVELOPMENT STRATEGY



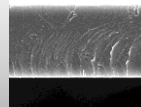
Defining target performance



Material development
and/or selection



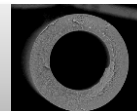
Dense film preparation and
characterization



Intrinsic separation properties
Permeability and selectivity



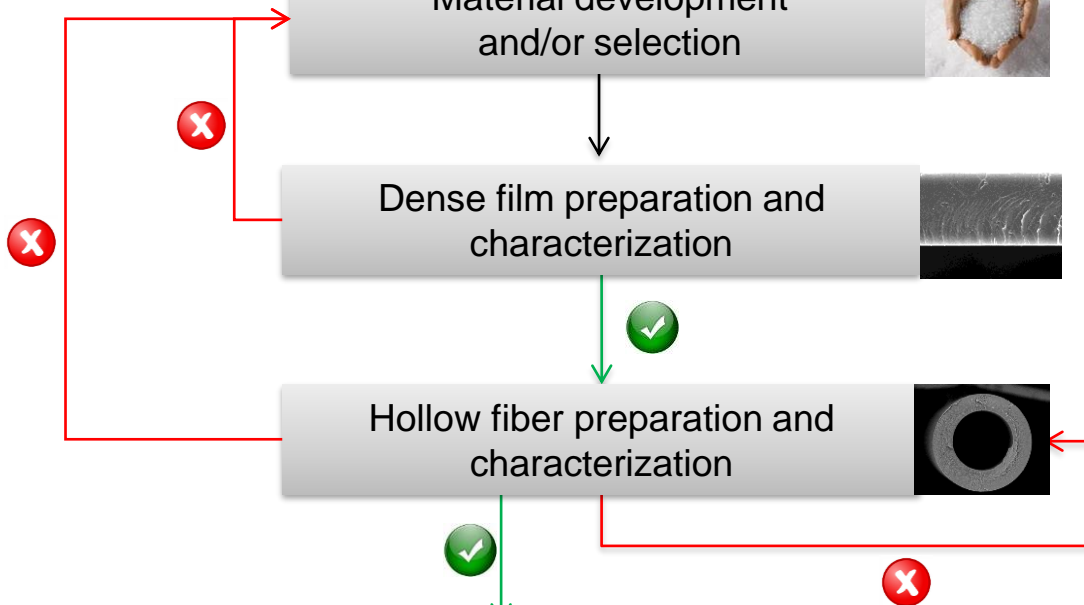
Hollow fiber preparation and
characterization



Separation properties
Permeance and selectivity



Possible to Scale-up, Prototype??





Contents lists available at ScienceDirect

Journal of Membrane Science

journal homepage: <http://www.elsevier.com/locate/memsci>



Thinking the future of membranes: Perspectives for advanced and new membrane materials and manufacturing processes

Suzana P. Nunes^{a,*}, P. Zeynep Culfaz-Emecen^b, Guy Z. Ramon^c, Tymen Visser^d,
Geert Henk Koops^e, Wanqin Jin^f, Mathias Ulbricht^{g,*}

Table 3

Need for improved or novel membranes and membrane manufacturing technologies.

| Membrane type | Challenges |
|--------------------------|--|
| Gas and vapor separation | <p>Membranes with higher selectivity and sufficient permeance</p> <p>Zero defects</p> <p>Higher thermal stability</p> <p>Stability in hydrocarbons and harsh vapors</p> <p>Improved ageing stability</p> |

Example 1: “zero defects”

P84 polyimide

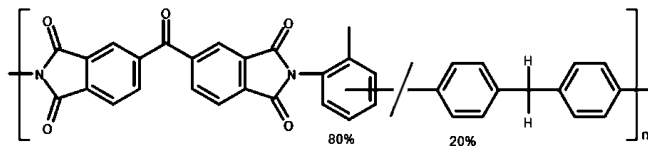


Table 2

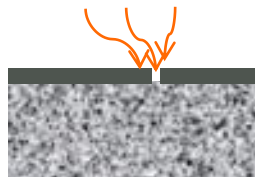
Permeability and selectivity for P84 and Matrimid 5218 (25 °C)

| | P_{He} (barrer) | P_{He}/P_{N_2} | P_{CO_2} (barrer) | P_{CO_2}/P_{N_2} | P_{O_2} (barrer) | P_{O_2}/P_{N_2} |
|---------------|----------------------|------------------|------------------------|--------------------|-----------------------|-------------------|
| P84 | 7.2 | 292 | 0.99 | 40.2 | 0.24 | 10.0 |
| Matrimid 5218 | 22.5 | 122 | 8.7 | 37.8 | 1.32 | 7.2 |

J. N. Barsema, G. C. Kapantaidakis, N. F. A. van der Vegt, G. H. Koops, M. Wessling, *J. Memb. Sci.* **2003**, 216, 195.

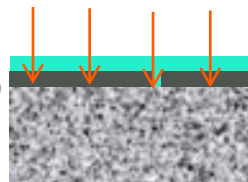
Selective layer (defective)

Porous support



Protective layer
Selective layer (defective)

Porous support



membranes

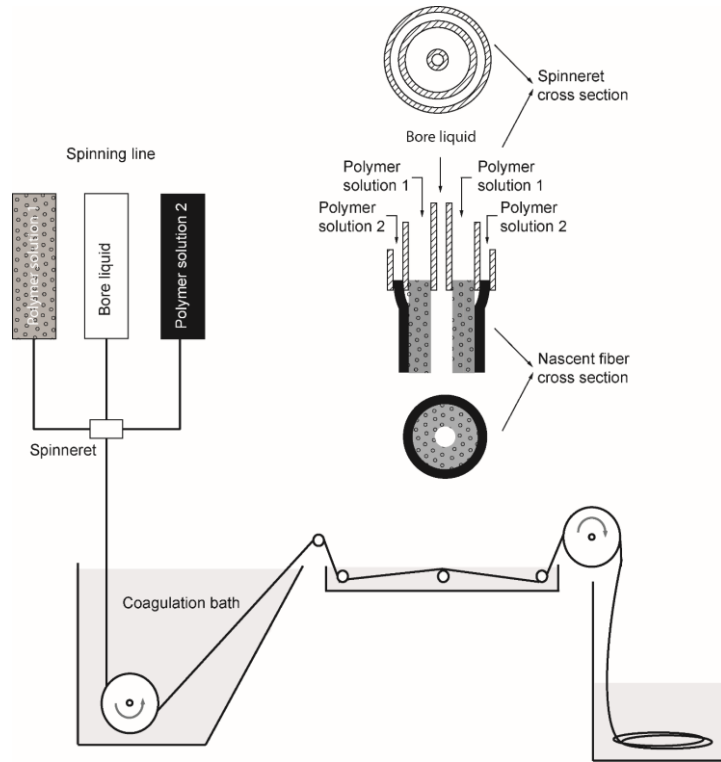


Article

Fabrication of Defect-Free P84[®] Polyimide Hollow Fiber for Gas Separation: Pathway to Formation of Optimized Structure

Miren Etcheberria-Benavides ^{1,2,*}, Oguz Karvan ^{1,3}, Freek Kapteijn ², Jorge Gascon ^{2,4} and Oana David ^{1,*}

Development of **defect-free as-spun ultrathin P84[®]** asymmetric hollow fiber membranes that **do not require a silicone rubber coating post-treatment step**



Process parameters

Dope Composition

Dope Flow rate

Bore Composition

Bore Flow Rate

Spinning Temp

Coagulation Bath Temp

Air Gap height

Take-up rate

Room T

Humidity

Dope composition: key parameter

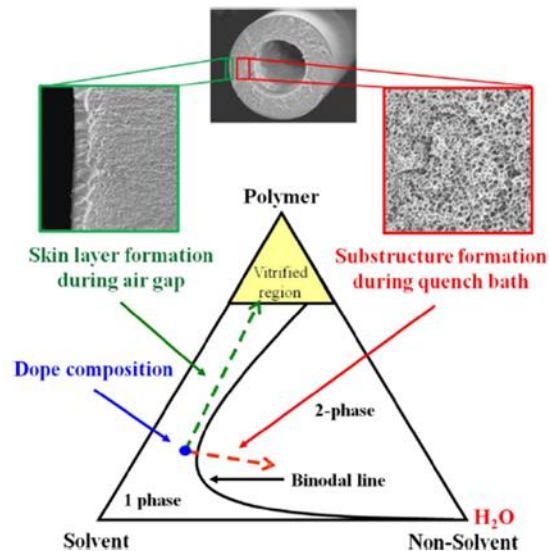


Figure. Gas separation asymmetric hollow fiber formation process represented in a ternary phase diagram

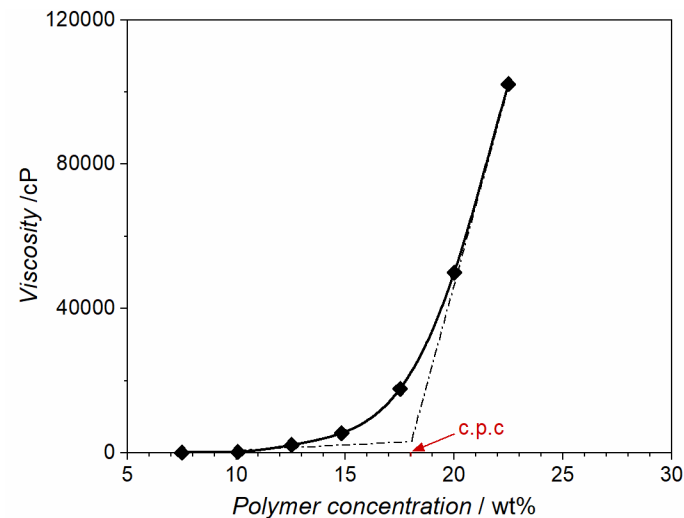
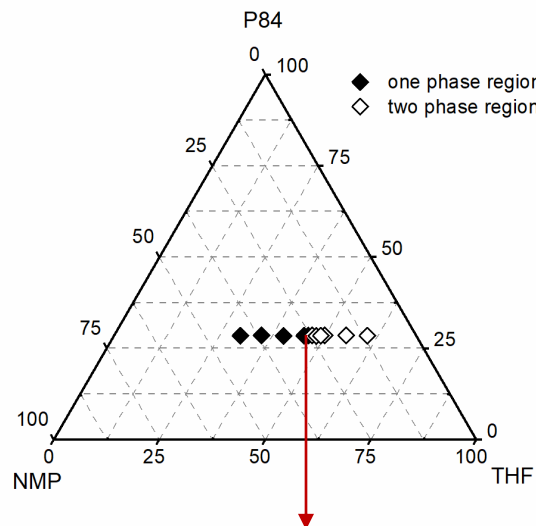


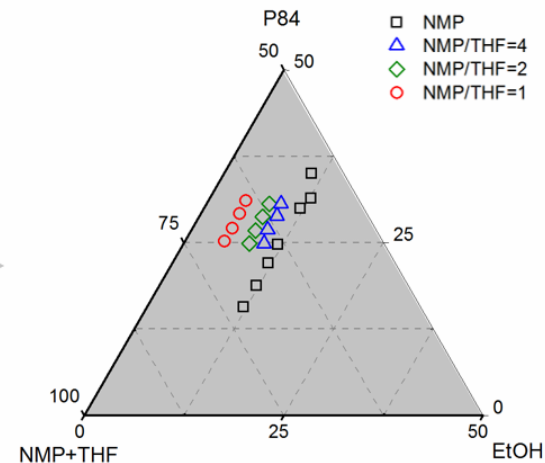
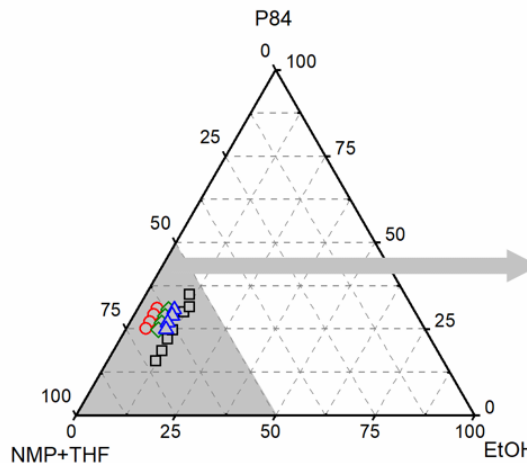
Figure 1.6. Typical viscosity versus polymer concentration curve and the determination of the critical polymer concentration, c.p.c.

Dope composition

- N-methyl-2-pyrrolidone (NMP) Solvent
- Tetrahydrofuran (THF) Solvent
- Ethanol (EtOH) Non-solvent



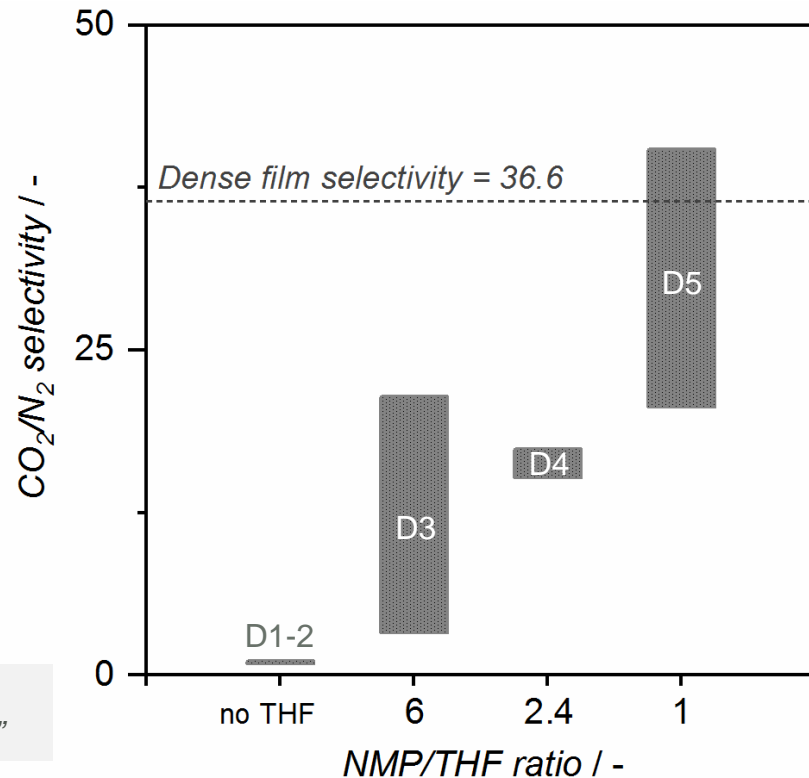
NMP/THF ratio = 0.52



Dope composition

| Spinning session | D1 | D2 | D3 | D4 | D5 |
|------------------|------|------|------|------|------|
| wt% P84® | 28.5 | 28.5 | 28.5 | 28 | 28.5 |
| wt% NMP | 64.5 | 62.5 | 58.7 | 46.9 | 35.2 |
| wt% THF | - | - | 9.8 | 19.1 | 35.3 |
| wt% EtOH | 7 | 9 | 3 | 6 | 1* |
| NMP/THF ratio | - | - | 6 | 2.4 | 1 |

“Asymmetric membranes are defined to be “defect-free” if the ideal selectivity is greater than 80% of the intrinsic selectivity of dense films”

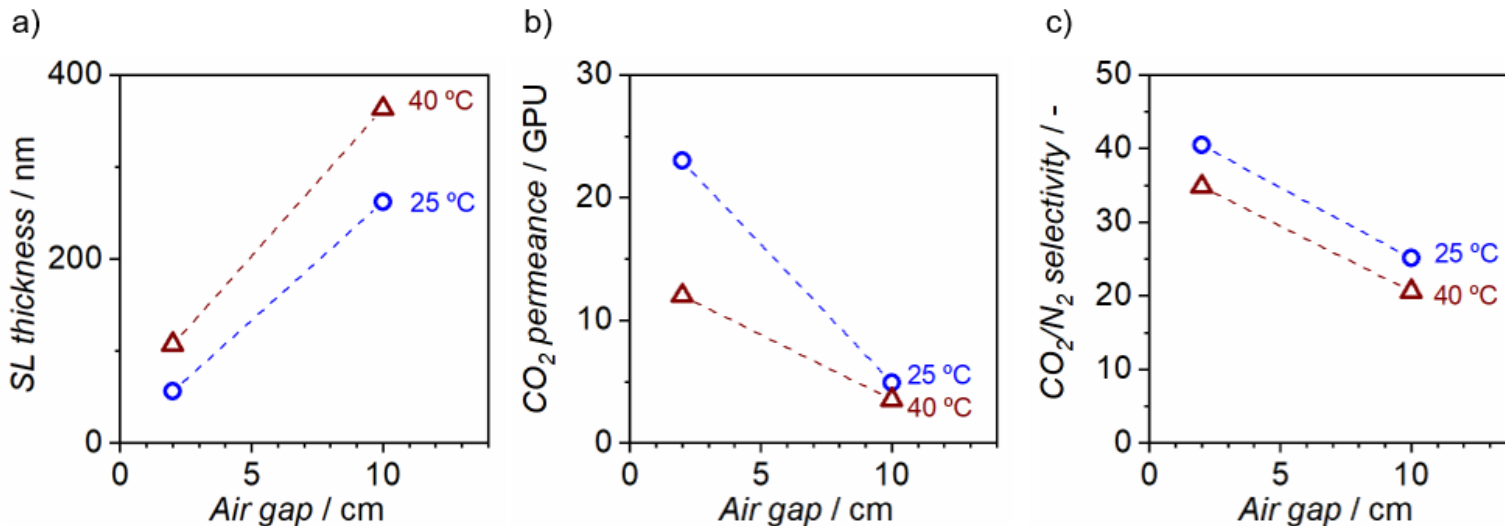


Spinning sesión D05

Spinning parameters influence:

- Spinneret temperature (25-40°C)
- Air gap height (2-10 cm)

Separation performance for single gas permeation at 35°C and 7 bar transmembrane pressure

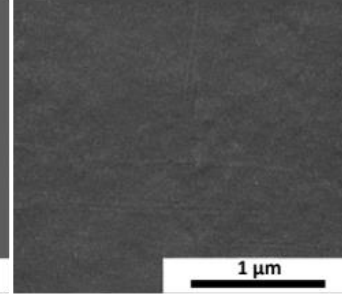
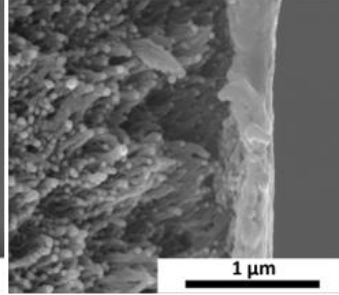
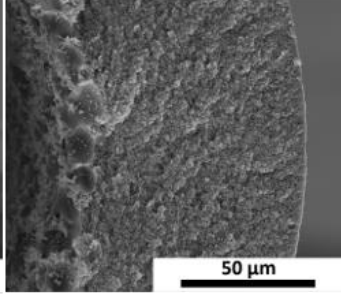
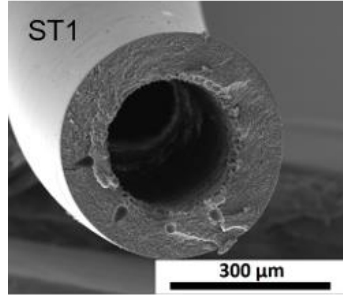


Cross section

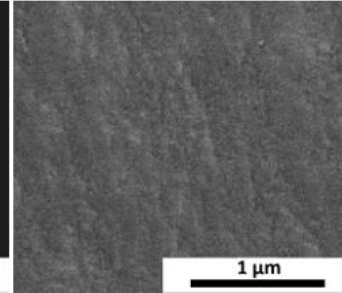
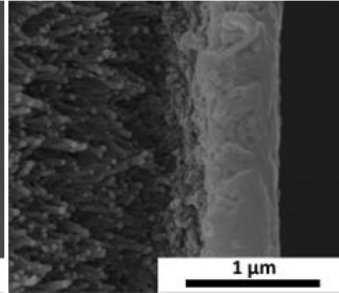
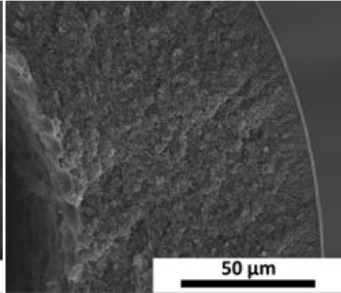
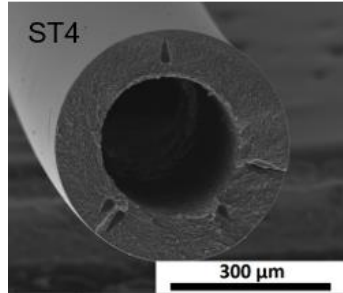
Fiber wall

Selective layer

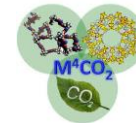
Outer surface



- Spinneret temperatura: 25°C
- Air gap height: 2 cm



- Spinneret temperatura: 40°C
- Air gap height: 10 cm



Barsema et al. (at 25°C)

2.2 GPU CO₂

46.8 CO₂/N₂

500 nm (selective layer thickness)

PDMS coated

TECNALIA (at 35°C)

23 GPU CO₂

40.4 CO₂/N₂

56 nm (selective layer thickness)

With out PDMS coating

Example 2: “Bio-Based HF membranes”



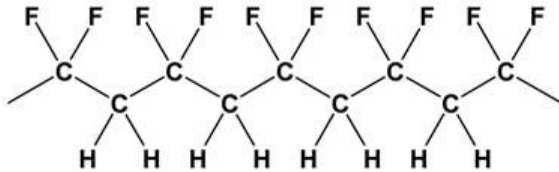
| Co-polymer | Polyamide block | Polyether block | Main expected result |
|---|--|--|---|
| A Reference bio-PEBAs | Bio-based polyamide II derived from castor oil (PA_{ref}^{bio}) | Fossil based polyether block (PE_{ref}^{fossil}) | Composite HF Membrane |
| B New bio-PEBAs Pathway I aromatic/cycloaliphatic polyamide-b-polyether | Bio-based polyamides derived from new building blocks (PA_{new}^{bio}) | Fossil based polyether block (PE_{ref}^{fossil}) | Better processability: (Monolithic HF membrane) <i>and</i> Higher gas separation performance |
| C New bio-PEBAs Pathway 2 lignin-g-(polyether-b-polyamide II) | Bio-based polyamide II derived from castor oil (PA_{ref}^{bio}) | Bio-based polyether block derived from lignin-g-polyether (PE_{new}^{bio}) | Better processability: (Monolithic HF membrane) <i>and</i> Development of PEBA type co-polymer with bio-based components in both blocks |

Prototype B – Polymer Properties

| Co-Polymer | T_g [°C] | T_m [°C] PEO/PA | CO ₂ permeability (Barrer) | CO ₂ /N ₂ Selectivity | CO ₂ /CH ₄ Selectivity |
|------------|------------|----------------------|---|--|---|
| 1 | -45 | n.d. / 30 | 20,87 | 22,5 | n.d. |
| 2 | -45 | n.d. / 37 | 150 | 12,6 | n.d. |
| 3 | <-40 | 31 / 102 | 139,4 | 24,3 | 8,0 |
| 4 | <-40 | 40 / 98 | 47,5 | 23,76 | 8,4 |
| 5 | <-40 | 16 / 80 | 237,0 | 30,1 | 9,9 |
| 6 | n.d. | 53 / n.d. | 40,1 | 25,5 | 8,8 |

Prototype B – Polymer spinning

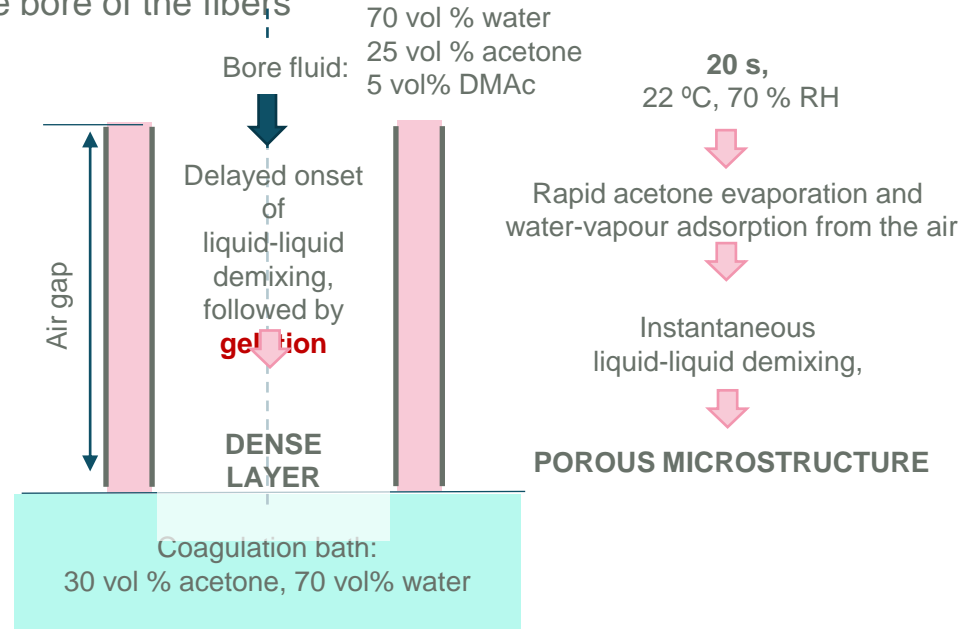
Literature background: Procedure for casting integral asymmetric PVDF pervaporation hollow fiber membranes with a dense layer on the inside bore of the fibers



| Xc | Tm (°C) | Tc (°C) |
|------|---------|---------|
| 50,7 | 168,3 | 142,1 |

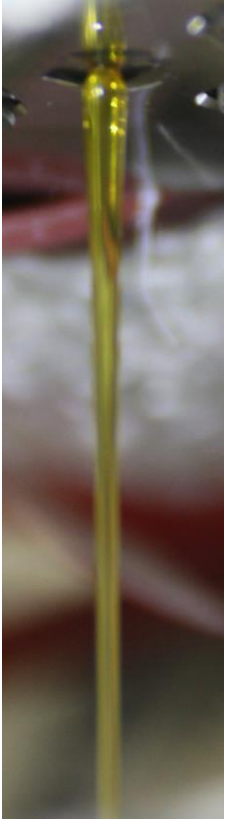
Polymer dope composition:

25 wt% PVDF
 30 wt% DMAc
 45 wt% Acetone

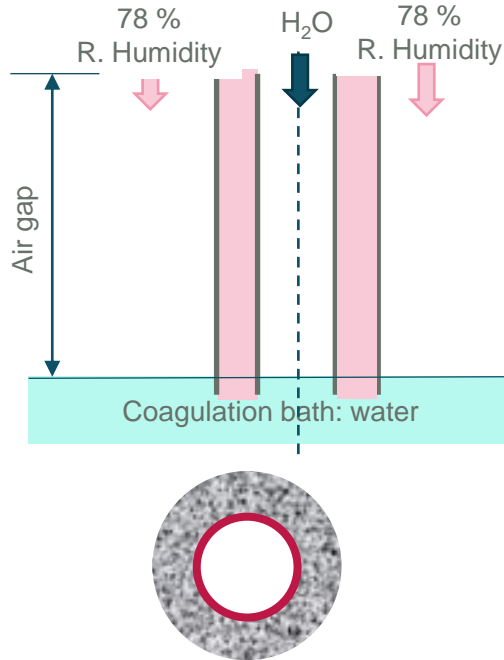


K. Jian, P.N. Pintauro, Asymmetric PVDF hollow-fiber membranes for organic/water pervaporation separations, Journal of Membrane Science, Volume 135, Issue 1, 1997, Pages 41-53

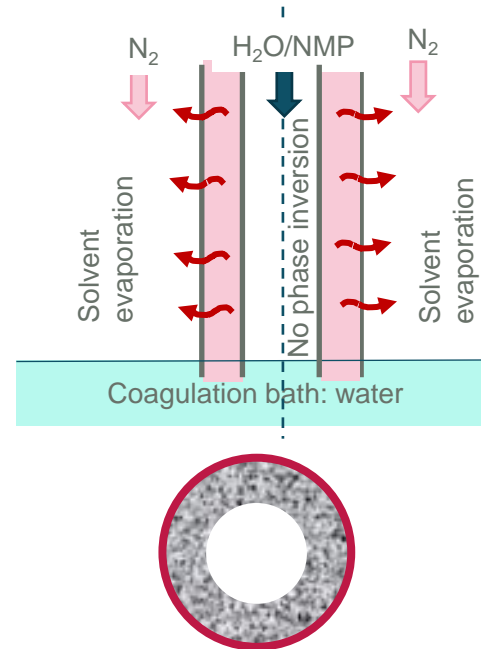
Prototype B – Polymer spinning



Forming the selective layer at the **inside** part of the fiber:



Forming the selective layer at the **outer** part of the fiber:









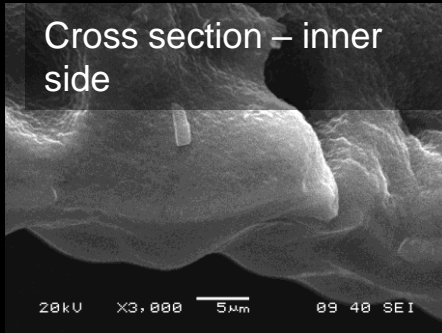
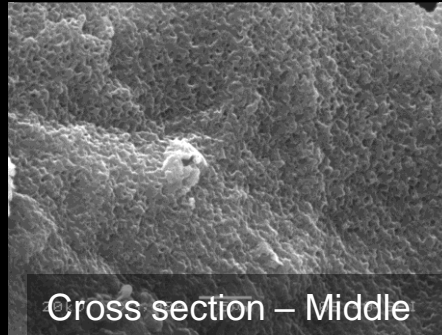
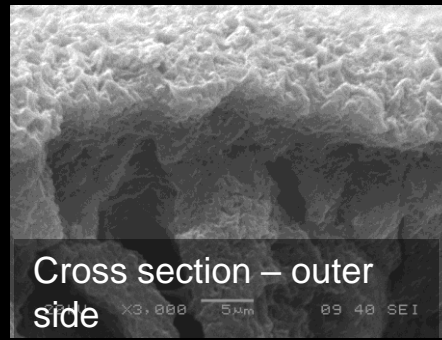
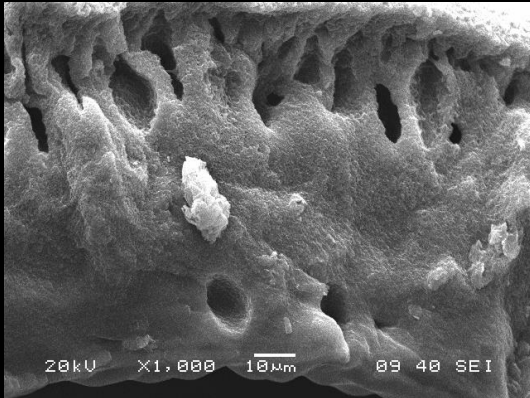
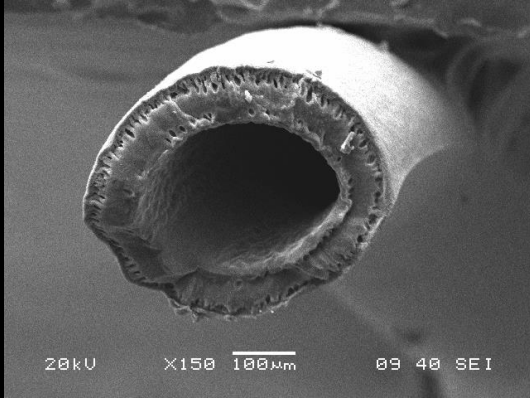
Prototype B – Polymer spinning

Polymer dope composition:

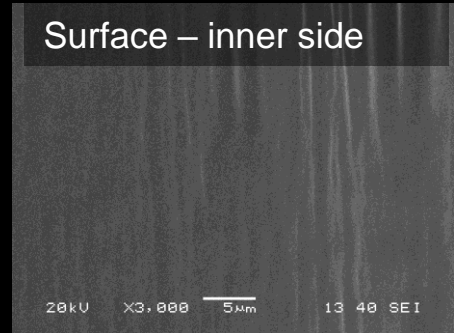
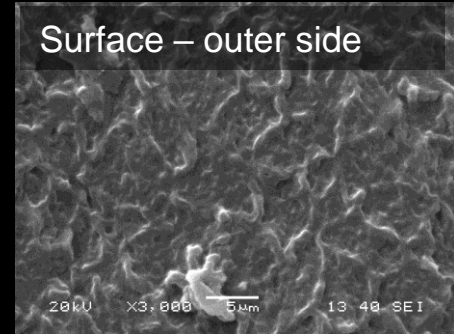
| | |
|--------------------|---------------|
| MS-2021-035 | 20 and 23 wt% |
| LiCl | 3.67 wt% |
| NMP | 73.33 wt% |

Gel at RT liquid at 40 °C

| | Pump temperature (°C) | Spinneret temperature (°C) | Bore liquid composition H ₂ O/NMP wt% | Air gap (cm) | Air gap environment | Hollow fiber? |
|---|-----------------------------|----------------------------------|---|-----------------|------------------------|---|
|  | 50 | 50 | 100/0 | 26 | 78% RH |  |
|  | 50 | 50 | 30/70 | 5 - 20 | N ₂ |  |
|  | 50 | 21 | 50/50 | 5, 11 | N ₂ |  |



BiCoMem



Eskerrik asko zuen arretagatik!

Thank you for your attention!